

UCLA

UCLA Previously Published Works

Title

Reset of Secondary Compression Clock for Peat by Cyclic Straining

Permalink

<https://escholarship.org/uc/item/9p07h93p>

Journal

Journal of Geotechnical and Geoenvironmental Engineering, 141(3)

ISSN

1090-0241

Authors

Shafiee, Ali
Stewart, Jonathan P
Brandenberg, Scott J

Publication Date

2015-03-01

DOI

10.1061/(asce)gt.1943-5606.0001286

Peer reviewed

1 This is the final authors' version. We are not permitted to
2 upload the typeset version due to copyright law. The
3 publisher's version of the manuscript may be found at the
4 following URL:

5 <http://ascelibrary.org/doi/abs/10.1061/%28ASCE>
6 [/%29GT.1943-5606.0001286](http://ascelibrary.org/doi/abs/10.1061/%28ASCE)

7

8 **Reset of Secondary Compression Clock for Peat by** 9 **Cyclic Straining**

10

11 Ali Shafiee, S.M.ASCE¹; Jonathan P. Stewart, F.ASCE²; and Scott J. Brandenburg, M.ASCE³

12

13 Peat soils are widely recognized as being highly compressible. The virgin compression index, C_c ,
14 is often 5 to 20 times larger than for soft clay, and the secondary compression index, C_{α} , is in the
15 range of $(0.05 \text{ to } 0.07)C_c$, which is also higher than for typical clays (Mesri and Ajlouni, 2007).
16 Secondary compression is often the dominant source of volume change in peat over time. The
17 compressibility of peat has typically been investigated due to total stress increase imposed by
18 static loads. This manuscript discusses time-dependent volumetric strains due to cyclic shear
19 straining.

20 A multi-stage cyclic simple shear laboratory testing program using the UCLA digitally
21 controlled direct simple shear device (Duku et al. 2007), modified for constant height testing,

11 PhD Candidate, Department of Civil and Environmental Engineering, University of California, Los Angeles, CA 90095.

2

32 Professor and Chair, Department of Civil and Environmental Engineering, University of California, Los Angeles, CA 90095.

4

53 Associate Professor and Vice Chair, Department of Civil and Environmental Engineering, University of California, Los Angeles, CA 90095.

22 was used to investigate post-cyclic volume change of relatively undisturbed specimens of fibrous
23 peat from Sherman Island in the Sacramento / San Joaquin Delta. During each stage, 15 strain-
24 controlled cycles (1 Hz) were imposed on peat specimens while maintaining constant height by
25 varying the vertical stress, after which specimens were reconsolidated to the initial vertical stress
26 (σ_{vc}'). Post-cyclic reconsolidation was monitored for approximately 20 min. following each
27 loading stage. Oedometer tests indicate primary consolidation was complete after 1 min, leaving
28 the remaining time to record the rate of secondary compression.

29 Test results for a peat specimen with 55% organic content, $\sigma_{vc}' = 12$ kPa, OCR = 4.9, $C_c = 2.21$,
30 and $C_r = 0.14$ are shown in Fig. 1. Part (a) shows that excess pore pressure ratios (r_u) are non-zero
31 when $\epsilon_{cyc} > 3\%$, with a residual $r_u = 0.2$ for $\epsilon_{cyc} = 10\%$. As shown in part (b), although these r_u
32 values are modest, post-cyclic volumetric strains are significant when $\epsilon_{cyc} > 1\%$ because of the
33 peat's high compressibility. Part (c) shows that the secondary compression rate, which is related
34 to the difference between ϵ_v at 1 and 20 min, increases with ϵ_{cyc} . This suggests that cyclic
35 straining can increase the secondary compression rate, which has not been previously
36 recognized. Similar increases in secondary compression rate are routinely observed when total
37 stress is increased in laboratory oedometer tests, which can be viewed as re-setting the "clock" to
38 zero at the time the load is applied. The data in Fig. 1 indicates that cyclic straining can at least
39 partially reset the secondary compression clock, without total stress increase.

40 Implications

41 Seismic risk is a significant issue for the Sacramento / San Joaquin Delta because levees are
42 composed of saturated, often liquefiable soils that rest atop soft compressible peats and organic
43 soils. If seismic ground failure were to occur in or beneath a levee, the interior islands could
44 flood. If repeated over a sufficient number of islands, this process would likely draw saline water

45into the Delta from the San Francisco Bay, compromising fresh water delivery via several of
46California's major aqueduct systems.

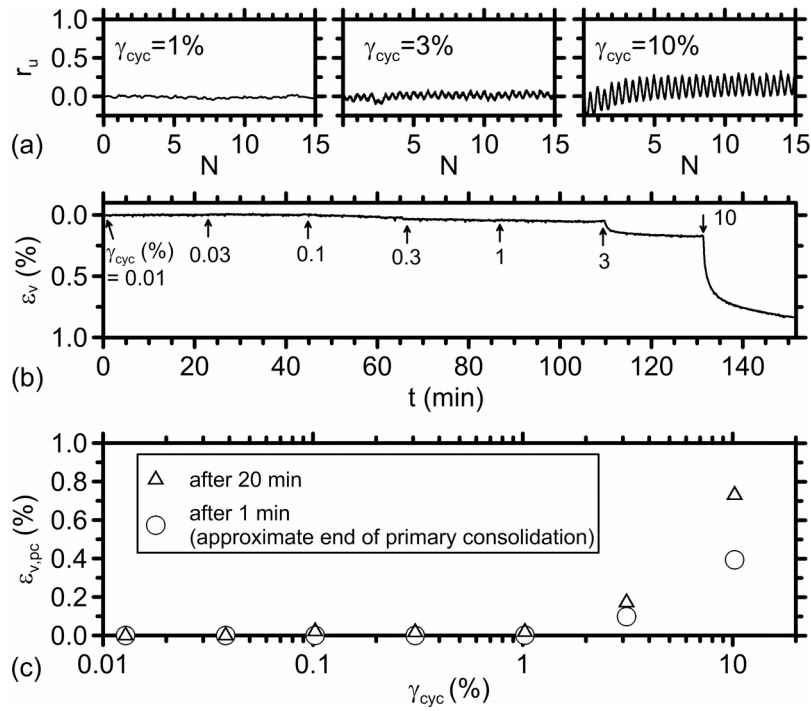
47 Liquefaction of saturated loose cohesionless levee fill and foundation soil is recognized as a
48significant driver of ground failure risk in the Delta. This work identifies a new mechanism by
49which levees that do not fail during shaking may experience increased settlement rates due to
50secondary compression following an earthquake, possibly causing overtopping. Further study is
51required to better characterize this potential hazard. Although γ_{cyc} as high as 10% is considered
52very large for typical inorganic soils, the Delta peats are unusually soft and such large shear
53strains are feasible during design-level shaking.

54**Acknowledgments**

55Support for this research has been provided by the Department of Water Resources (DWR) under
56contract number 4600010406, and the US Geological Survey under contract number
57G11AP20169.

58**References**

- 59Duku, P.M., Stewart, J.P., Whang, D.H., and Venugopal, R. (2007). "Digitally controlled simple
60 shear apparatus for dynamic soil testing." *Geotech. Test. J.*, 30(5) 368-377.
- 61Mesri, G., and Ajlouni, M. (2007). "Engineering properties of fibrous peats." *J. Geotech.*
62 *Geoenviron. Eng.*, 133(7), 850–866.



64 **Fig. 1.** Cyclic direct simple shear test results of Sherman Island peat (a) pore pressure ratio (r_u) versus number of cycles (N), (b)

volumetric strain (ϵ_v) versus time (t), and (c) ϵ_v versus cyclic shear strain amplitude (γ_{cyc}).