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UCB-NE-101 User's Manual

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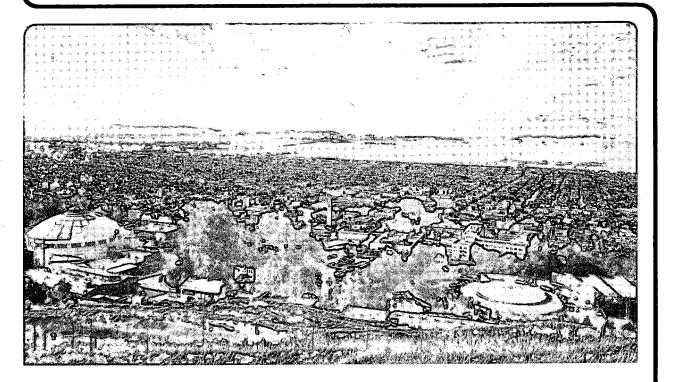
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February 1989

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UCB-NE-101

User's Manual

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February 1989

Work supported by the Director, Office of Civilian Radioactive Waste Management, Office of System Integration and Regulation, Licensing and Compliance Division, of the U.S. Department of Energy under contract DE-AC03-76SF00098.

INTRODUCTION

The purpose of this manual is to provide users of UCB-NE-101 with the information necessary to use UCB-NE-101 effectively.

DESCRIPTION OF THE CODE

UCB-NE-101 calculates the concentration of solubility-limited species as a function of space and time and its mass flux rates from a waste sphere buried in a nuclear waste repository in water-saturated rock. The waste is surrounded by one type of rock, and some distance away, there is another type of rock. The inner layer of rock can be a backfill around a nuclear waste package and the outer layer the natural rock. The mass flux calculated is at the interface of the two layers. The species concentration calculated is in the inner layer. A constant concentration of the species, usually the solubility, is specified at the waste sphere/inner layer interface. Dissolution and transport is governed by the solubility of the species, and diffusion in the porous media.

THEORY

Nuclear waste placed in geologic repositories in water-saturated rock will gradually dissolve. For many species such as actinides and rare earths, the process of dissolution is governed by the exterior flow field, and the chemical reaction rate or leaching rate [Chambré *et al.* 1987]. The need is to study the rate of dissolution, and the resultant concentration field of the dissolved species. Figure 1 shows the situation studied and some of the terms used. The waste sphere radius is R_o and is surrounded by a layer of rock/sediment/backfill of thickness $b = R_1 - R_o$. At the waste surface, a constant species concentration of c_o is specified. The subscript 1 refers to the inner layer and the subscript 2 refers to the outer layer. The species retardation coefficient is K. The species diffusion coefficient is D_f and σ_1 and σ_1 are geometric factors for the two layers. The porosities of the layers are denoted by ϵ and the species concentration in ground water in the layers are c_1 and c_2 respectively.

By defining $\nabla^2 = \frac{\partial^2}{\partial r^2} + \frac{2}{r} \frac{\partial}{\partial r}$ we can write the governing equations for this mass transfer

$$\frac{\partial c_1}{\partial t} = D_1 \nabla^2 c_1 - \lambda c_1, \qquad R_o < r < R_1, t > 0, D_1 = \frac{\sigma_1 D_f}{K_1}$$
(1)

$$\frac{\partial c_2}{\partial t} = D_2 \nabla^2 c_2 - \lambda c_2, \qquad R_1 < r < \infty, t > 0, D_2 = \frac{\sigma_2 D_f}{K_2}$$
(2)

$$c_1(r,0) = 0, \qquad R_o < r \le R_1,$$
 (3)

$$c_2(r,0)=0, \qquad R_1 \leq r < \infty \qquad (4)$$

$$c_1(R_o,t)=c_s, \qquad t\geq 0 \tag{5}$$

$$c_1(R_1,t) = c_2(R_1,t), \qquad t \ge 0$$
 (6)

$$-\epsilon_1 \sigma_1 D_f \frac{\partial c_1}{\partial r} = -\epsilon_2 \sigma_2 D_f \frac{\partial c_2}{\partial r} \quad \text{at} \quad r = R_1, \qquad t \ge 0$$
(7)

$$c_2(\infty,t)=0, \qquad t\geq 0 \tag{8}$$

The solution to (1) through (8) is given in Chambré et al. [1985]

$$\frac{c_1(r,t)}{c_s} = f(r) + e^{-\lambda t} \int_0^\infty \frac{e^{-D_1 t \eta^2}}{1 + \left(\frac{\lambda}{D_1 \eta^2}\right)} I(r,\eta) d\eta, \qquad R_o \le r \le R_1, t \ge 0$$
(9)

where

$$H(\eta) = [\epsilon'_1 \eta \cos(\eta b) + \alpha \sin(\eta b)]^2 + [\beta \epsilon'_2 \eta \sin(\eta b)]^2$$

$$f(\mathbf{r}) = \frac{R_o}{r} \frac{1 + \delta(\frac{\mathbf{r}}{R_1})}{1 + \delta(\frac{R_o}{R_1})}, \qquad I(\mathbf{r}, \eta) = -\left(\frac{2R_o\epsilon'_1\epsilon'_2\beta}{\pi r}\right) \frac{\eta \sin(\eta[\mathbf{r} - R_o])}{H(\eta)}$$
$$\alpha = \frac{\epsilon'_2 - \epsilon'_1}{R_1}, \qquad \beta = \sqrt{K'_2/K'_1}, \qquad \delta = \frac{\epsilon'_2 - \epsilon'_1}{\epsilon'_2}$$
$$b = R_1 - R_o, \qquad K'_\ell = K_\ell/\sigma_\ell, \qquad \epsilon'_\ell = \epsilon_\ell/\sigma_\ell, \qquad \ell = 1, 2$$

If $\lambda = 0$ in (9), we obtain the solution for a stable species.

ALGORITHM

This program computes the concentration of the species at the interface of the two layers and mass transfer rates at inner surface of the first layer and at the interface of the two layers. The transient solution is calculated using the D01AJF routine from the NAG library with the help of the exact steady-state solution.

INPUT

There are ten (10) input lines, all in free format. The first 9 lines are the physical properties of the system, described below. Each line gives 3 pieces of data: the initial value of this parameter, the increment multiplier of this parameter, and the number of times the calculations will be repeated using the different values of this parameter. For example, if the input line for the diffusion coefficient is "1e-5 10.0 3", which means the initial value used for D_f is 1×10^{-5} cm²/s, the increment multiplier is 10, and the number of evaluations is 3. Hence the entire set of calculations will be repeated three times, for values of $D_f 1 \times 10^{-5}$ cm²/s, 1×10^{-4} cm²/s, and 1×10^{-3} cm²/s, respectively.

The ten lines of input are for

Df - diffusion coefficient (cm^2/sec)

K1 - retardation coefficient of inside layer

K2 - retardation coefficient of outside layer

E1 - porosity of inside layer

E2 - porosity of outside layer

R0 - radius of waste sphere (cm)

XL - insider layer thickness (cm)

T12 - species half life (years)

T - time (years).

To do calculations for 10⁶ years, the ninth line should read

1., 10., 7.,

The last line has three (3) input data, EPS - relative error bound, IBUG - debug option, and CUT - upper limit of integral. Numerical experiments showed that for an upper limit of the integral in (9) of 20, the relative error bound for the integral is 10^{-6} . We have used values of CUT from 20 to 100. In practice, we often use

$$1.e - 4, 0., 20.,$$

as input for the last line.

The program currently reads from the keyboard as a default. In the DEC/VMS system the command

ASSIGN inputfile FOR005

will cause inputfile to be the input.

OUTPUT

The program currently sends output to the screen.

The output is in three parts. First, input data is repeated. Second, a set of numbers for \bullet mass flux from the waste sphere/solubility of the species (cm³/s),

•mass flux at the interface of the layers/solubility of the species (cm³/s),

•concentration at the interface of the layers,

all as a function of time, but WITHOUT radioactive decay.

The next set of lines are for the species. First, the half life read in is written out. Then comes a series of lines. In order, they are

-time (years),

-mass flux from the waste sphere/solubility of the species (cm^3/s) ,

-maximum error in the line just above,

-work space,

-number of subintervals used in numerical integration for the result above,

-mass flux at the interface of the layers/solubility of the species (cm^3/s) ,

-maximum error in the line just above,

-work space,

-number of subintervals used in numerical integration for the result above,

-concentration at the interface of the layers/solubility of the species,

-maximum error in the line just above,

-work space,

-number of subintervals used in numerical integration for the result above,

-The mass transfer coefficient (m/yr).

In Appendix C, the example output has been annotated. If more than one iteration has been requested for any one of the parameters, then the entire output shown in Appendix C is repeated as many times as requested.

RESOURCE REQUIREMENTS

UCB-NE-101 is written in FORTRAN and calls both the IMSL and NAG libraries. It operates on DEC/VAX and DEC/UNIX machines.

VERIFICATION & BENCHMARKING

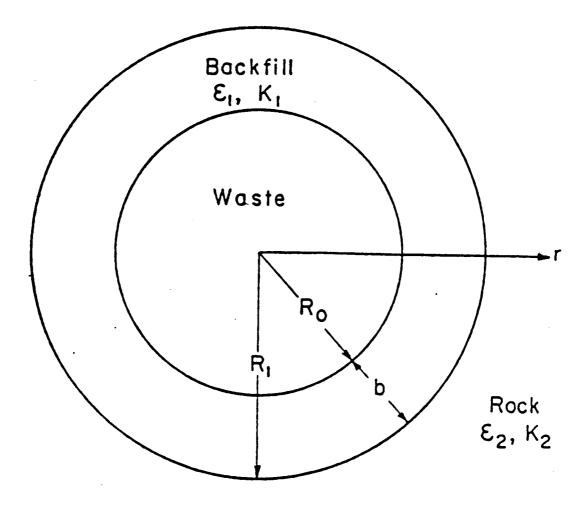
UCB-NE-101 is an implementation of (9). It was verified through hand calculations. The correctness of UCB-NE-101 was also checked this way. Eq. (9) was given to several workers and they were asked to write computer programs independently. The outputs of the various programs are then compared or benchmarked. They gave identical results.

ACKNOWLEDGEMENTS

UCB-NE-101, was originally known as MASLAM. The author is Dr. H. C. Lung who kindly reviewed this User's Manual in draft form. Work was supported in part by the U. S. Department of Energy under contract DE-AC03-76SF00098.

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P. L. Chambré, T. H. Pigford, W. W.-L. Lee, J. Ahn, S. Kajiwara, C. L. Kim, H. Kimura, H. Lung, W. J. Williams and S. J. Zavoshy, *Mass Transfer and Transport in a Geologic Environment*, Report LBL-19430, 1985.



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Fig. 1. Geometry of spherical waste form with backfill layer.

APPENDIX A: CODE LISTING

```
program ucbne101
C----
         c UCBNE101 - mass transfer from canister surface
С
c This program computes the concentration at the backfill-rock
c interface and mass transfer rates at canister surface and at
c backfill-rock interface from a spherical canister surrounded
c by a backfill layer with radioactive decay
С
c Transient solution using NAG DOIAJF routine with the help
c of exact steady state solution
с
c For early time, the semi-infinite medium assumption will be
c used and the single-region solution will be applied
C
c This program also computes the results without decay
C
с
  If the half life of the radionuclide is longer than or equal
С
   to 1E15 years it will be treated as non-decay nuclide
c Input parameters:
C
С
    There are ten (10) input lines, all in free format. The first 9
    lines are the physical properties of the system, described below.
c
    Each line has 3 input data: the initial value of this parameter,
C
    the increment multiplier of this parameter, and the number of
c
     evaluations used for this parameter. For example, the input line
     for diffusion coefficient is "le-5 10.0 3", which means the initial
C
     value used for Df is le-5 cm**2/sec, the increment multiplier is
С
     10, and the number of evaluations for Df is 3. Hence the values
     used for Df will be 1e-5, 1e-4, and 1e-3, respectively.
C
c
        Df - diffusion coefficient (cm**2/sec)
С
С
       K1 - retardation coefficient of backfill
С
        K2 - retardation coefficient of rock
С
        E1 - porosity of backfill
с
        E2 - porosity of rock
с
        R0 - radius of waste (cm)
с
        XL - backfill thickness (cm)
        T12 - half life (years)
с
с
        T - time (years)
с
С
    The last line has three (3) input data, described below.
c
         EPS - relative error bound
c
с
        IBUG - debug option
С
        CUT - upper limit of integral
С
c Output data:
c
c
        The output data will be mass transfer rates at both sides of
        backfill, the concentration at backfill-rock interface, and
С
с
        the mass transfer coefficient.
с
¢
c
c
C
             H.C.Lung
                            11/06/85
С
c
     double precision f,g,h,fl,gl,hl
     external f,g,h,fl,gl,hl
     integer ibug,ndf,idf,nk1,ik1,nk2,ik2,ne1,ie1,wspc(20)
```

integer nt12, it12, wsp0 (20), wsp1 (20), n, icode, isb0 (20), isb1 (20) integer ne2, ie2, nr0, ir0, nx1, ix1, nt, it, i, wsp (20), isbc (20)

```
5
```

```
real*8 sum, low, up, abe, df0, deldf, k10, delk1, k20, delk2, k11, k22
      real*8 d,c1,c2,c3,t,eps,b,year,flux0(20),e10,dele1,e20,dele2
      real*8 df, k1, k2, e1, e2, r0, x1, sk21, gamma, r1, pie, r00, delr0, cut
      real*8 time(20), x10, delx1, t0, delt, mxe0(20), con(20), mxec(20)
      real*8 t12,delt12,t120,t1,e,x0,x1,tr(20,6),hm(20),coeff,arg
      real*8 flux01(20), flux1(20), flux11(20), con1(20), mxe1(20)
      real*8 d1, d2, r01, al1, al2, co1, co2, den, sm0, sm1, smc, sh, ch, alg2
      common /para/ d,cl,c2,c3,b,e,r1
      data year/3,1536d7/, abe/0.0/
      pie-3.14159265358979
      alg2-dlog(2d0)/year
c
   read df,k1,k2,e1,e2,r0,x1,t1/2, and time
c
с
      low-0.0
      read (5,*) df0,deldf,ndf
      read (5,*) k10,delk1,nk1
      read (5,*) k20,delk2,nk2
      read (5,*) e10, dele1, nel
      read (5,*) e20,dele2,ne2
      read (5,*) r00,delr0,nr0
      read (5,*) x10,delx1,nx1
      read (5,*) t120, delt12, nt12
      read (5,*) t0, delt, nt
с
с
   read eps, ibug, and upper cut
с
      read (5,*) eps, ibug, cut
     write (6,90) eps, ibug, cut
c
      df-df0/deldf
      do 8 idf=1,ndf
      df-df*deldf
      kl-k10/delk1
      do 7 ik1-1, nk1
      k1=k1*delk1
      k2=k20/delk2
      do 6 ik2=1,nk2
      k2=k2*de1k2
      xl=x10/delx1
      do 5 ixl=1,nxl
      xl-xl*delxl
      d-xl
      r0-r00/delr0
      do 4 ir0=1, nr0
      r0-r0*delr0
      r1=r0+x1
      coeff=3.1536e5/(4.0*pie*rl*rl)
      r01-r0/r1
      e1-e10/dele1
      do 3 iel-1, nel
      el-el*delel
      k11-k1
      if (dabs(e1-1.0).lt.le-4) k11=1.0
      dl-df/kll
      ts-d**2/d1/120.0
     ts=le12*year
С
      c1-01
      x0=4.0*pie*e1*df*r0**2
      x1=x0/r01
      e2=e20/de1e2
      do 2 ie2-1, ne2
      e2-e2*dele2
      k22=k2
      if (dabs(e2-1.0).lt.le-4) k22=1.0
      d2 - df/k22
```

```
6
```

.

1.0

```
sk21-dsgrt (k22/k11)
      c2=(e2-e1)/(r1)
      c3-sk21*e2
      gamma= (e1-e2) /e2
      if (ibug.gt.0) write (6,100) d,c1,c2,c3
      write (6,80) df,k11,k22,e1,e2,r0,x1
c
    steday state parts of flux and concentration without decay
C.
c
      ssm=1.0/r0/(1.0+gamma*r0/r1)*x0
      ssc=r0/r1*(1.0+gamma)/(1.0+gamma*r0/r1)
С
с
    beginning calculations
c
      t=t0/delt
      do 1 it=1, nt
      t=t*delt
      time (it) -t
      ty=t*year
      b=d1*ty
      if (ty.lt.ts) then
с
с
   early time, use single region approx.
c
с
    set concentration and flux at b-r interface to zero
c
        flux0(it)=x0*(1.0/dsqrt(pie*b)+1.0/r0)
        flux1(it)=0.0
        con(it)=0.0
      el se
c
   later time, use exact solution
с
с
        up=dsqrt (cut/b)
С
   calculate flux at waste surface without decay
c
с
        error-eps
        1code=1
        call intgrl(f,0.0,low,up,error,sum,icode,n)
        if (n.gt.le6) go to 1000
        mxe0(it)-0.0
        if (sum.gt.0.0) mxe0(it) -error/sum
        tr(it,1)=2.0*e1*e2*sk21/pie*sum*x0
        flux0(it)=ssm+tr(it,1)
        wsp0 (it) =n
с
   calculate flux at backfill-rock interface without decay
c
С
        error-eps
        1code=1
        call intgrl(h,0.0,low,up,error,sum,icode,n)
        if (n.gt.1e6) go to 1000
        mmel(it)=0.0
       if (sum.gt.0.0) mxel(it) -error/sum
       tr(it,3)=2.0*e1*e2*sk21/pie*sum*x1
        flux1(it) =ssm+tr(it,3)
        wapl (it) -n
c
с
   calculate concentration at b-r interface without decay
c
       error-eps
       icode=1
       call intgrl(g,0.0,low,up,error,sum,icode,n)
       if (n.gt.1e6) go to 1000
       mxec(it) =0.0
```

```
7
```

```
if (sum.gt.0.0) mxec(it) -error/sum
         tr(it,5) =-2.0*e1*e2*sk21/pie*sum*r0/r1
         con(it)=ssc+tr(it,5)
        wspc(it) -n
      end if
   1 continue
      write (6,25)
      write (6,20) (time(i), i=1, nt)
      write (6,50) (flux0(1),1-1,nt)
      write (6,10) (flux1(i),i=1,nt)
      write (6,10) (con(i),i=1,nt)
с
С
   start decay part
с
      t12=t120/delt12
      do 11 it12=1,nt12
      t12-t12*delt12
      write (6,15) t12
c
    if half life .ge. 1E15 years, treated as non-decay
c
c
      if (t12.ge.1e15) go to 11
с
c
    otherwise begin calculation with decay
с
      tl-alg2/t12
с
    first calculate the steady state solutions
с
с
      all-dsqrt (t1/d1)
      al2-dsqrt(t1/d2)
      col=al1*el
      co2=a12*e2+c2
      arg-al1*d
      sh=dsinh(arg)
      ch=dcosh (arg)
      den=col*ch+co2*sh
      smc=r01*col/den
      sm0=x0/r0*(1.0+all*r0*(col*sh+co2*ch)/den)
      sml=x1/r0*(smc+all*r0*co2/den)
с
С
    begin transient calculations
С
      t=t0/delt
      do 12 it=1,nt
      t=t*delt
      ty=t*year
      e=tl*ty
      b=d1*ty
      if (ty.lt.ts) then
С
c
    early time, use single region approx.
c
С
    set the concentration and flux at backfill-rock interface
С
    to zero
c
        mxe0(it)=0.0
        wsp0(it)-0
        mxel(it)=0.0
        wspl(it)=0
        mxec(it)-0.0
        wspc(it)=0
        isb0(it)=0
        isb1 (it) =0
        isbc(it) =0
        flux01(it) =x0* (all*erf(dsqrt(e)) +expo(-e)/dsqrt(pie*b)+1.0/r0)
```

```
flux11(it)=0.0
        con1 (1t) =0.0
      else
с
с
    later time, use exact solution
с
        up=dsqrt (cut/b)
С
    calculate flux at waste surface with decay
с
с
        icode=1
        error-eps
        call intgrl(f1,0.0,low,up,error,sum,icode,n)
        if (n.gt.le6) go to 1000
        mxe0(it)-0.0
        if (sum.gt.0.0) mxe0(it) -error/sum
        tr(it,2) =-2.0*e1*e2*sk21/pie*sum*x0
        flux01(it) =sm0+(tr(it,2)+tr(it,1)) *expo(-e)
        wsp0(it) =n
        isb0(it)=icode
С
    calculate flux at backfill-rock interface with decay
С
c
        icode=1
        error-eps
        call intgrl(hl,0.0,low,up,error,sum,icode,n)
        if (n.gt.le6) go to 1000
        mxel(1t)=0.0
        if (sum.gt.0.0) mxel(it) -error/sum
        tr(it,4)-2.0*el*e2*sk21/pie*sum*x1
        flux11(it) =sml+(tr(it,4)+tr(it,3)) *expo(-e)
        wspl(it) -n
        isbl(it)-icode
С
c
    calculate concentration at b-r interface with decay
С
        icode=1
        error-eps
        call intgr1(g1,0.0,low,up,error,sum,icode,n)
        if (n.gt.1e6) go to 1000
        mxec(1t)=0.0
        if (sum.gt.0.0) mxec(it) -error/sum
        tr(it,6)=2.0*e1*e2*sk21/pie*sum*r0/r1
        conl(it) ====c+(tr(it,6)+tr(it,5)) *===po(-e)
        wspc(it)=n
        isbc(it)-icode
С
C
    calculate mass transfer coefficient
С
        hm (it) =1e38
        if (conl(it).gt.0.0) hm(it)-flux11(it)/conl(it)*coeff
      end if
  12 continue
      write (6,30)
      write (6,20) (time(1), i=1, nt)
      write (6,50) (flux01(1), i=1, nt)
      write (6,10) (mxe0(1),1=1,nt)
      write (6,40) (wep0(i), i=1, nt)
      write (6,40) (isb0(i),i=1,nt)
      write (6,50) (flux11(i), i-1, nt)
      write (6,10) (mxel(i),1-1,nt)
      write (6,40) (wspl(i),i=1,nt)
     write (6,40) (isb1(i),i=1,nt)
     write (6,50) (conl(i),i=1,nt)
      write (6,10) (mxec(i), i=1, nt)
      write (6,40) (wspc(i),i=1,nt)
```

```
write (6,40) (isbc(i),i=1,nt)
      write (6,50) (hm(i),i=1,nt)
  11 continue
  2 continue
   3 continue
      continue
   4
   5
      continue
   6
      continue
  7 continue
   8 continue
  10 format (11(1pe11.4))
  15 format (//' half life=',1pel3.5,' years'/)
  20 format (11(1pe11.4)/)
  25 format (/' time, flux0, flux1, and concentration without decay
     +
              1/)
  30 format (*
                       time (years) // flux (cm**3/sec) // max. error ',
              '// work space // cl/cs // max. error // work space // hm'
     +
              ' (m/yr)'//)
     +
  40 format (11(16,5x))
  50 format (/11(1pel1.4))
  80 format (//12('-----')//1x,'df,k1,k2,e1,e2,r0,x1=',
     +7(lpe10.3)///)
 90 format (1h1, 'eps, ibug, cut=', 1pe10.3, i3, 1pe10.3)
100 format (/'d, c1, c2, c3=', 4(1pe13.6)/)
     go to 1100
1000 continue
     write (6, '(a) ') 'Too many subintervals, fortran stop'
1100 continue
      stop
     end
с
      subroutine intgrl(f,omega,a,b,err,ans,ierr,n)
C-
c intgrl - calculate an integral
с
с
С
   where
С
c
        f-function of integrand
        omega-frequency (0 if not sinusoidal function)
С
С
        a,b-lower and upper limits
С
        err-relative error bound
С
        ans-result of integration
        ierr-error flag (also served as output - no. of subintervals)
c
с
        n-number of subdivisions used
c
С
C-
с
      implicit double precision (a-h,o-z)
     double precision f
     external f
     integer nw, niw
     parameter (nw-4000)
     parameter (niw-nw/8+2)
     double precision a, b, err, ans, omega, eps, om
     double precision as, bb, abe, errd, sum, error, work (nw), tmp, tmp1
     integer ierr, n, nn, iw (niw)
С
     eos-err
     abe=0.0
     tmp=0.0
     aa-a
     if (omega.ne.0) then
       om=10.0*3.1415926535/omega
```

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11

```
10
```

```
bb-a+om
        if (bb.gt.b) bb-b
      else
        bb=b
      end if
      nn=0
      11-0
  10 continue
      errd-eps
      icode=ierr
      call d01ajf(f, aa, bb, abe, errd, sum, error, work, nw, iw, niw, icode)
      if (icode.ne.0) then
С
    not enough accuracy, reduce integral limits
с
C
        bb=(bb+aa)/2.0
        go to 10
      else
С
c got it!
с
        nn=nn+1
        11=11+1w(1)
        if (tmp.eq.0) go to 20
        if (dabs(sum/tmp).le.eps) go to 30
  20
        continue
        tmp1-sum
        tmp=tmp+sum
        if (bb.eq.b) go to 30
        if (nn.gt.1e6) go to 30
        aa-bb
        if (omega.ne.0.0) then
          bb-aa+om
          if (bb.gt.b) bb=b
        ....
          bb=b
        end if
        go to 10
      end if
  30 continue
      ans-tmp
      n=nn
      ierr-ii
      err-error
      if (n.gt.1e6) err--1e38
      return
      end
с
C-
      function f(x)
C---
      common /para/ d, cl, c2, c3, b, e, r1
      double precision x,d,c1,c2,c3,b,a,c,e,r1,expo
      double precision f
      a-x++2
      c-x+d
      f=a/((cl*x*dcos(c)+c2*dsin(c))**2+(c3*x*dsin(c))**2)*expo(-b*x**2)
      return
      end
С
c
      function fl(x)
C----
     common /para/ d, c1, c2, c3, b, e, r1
      double precision x,d,c1,c2,c3,b,a,c,e,r1,expo
     double precision fl
```

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with a

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- -

```
a=x**2
      c=x*d
      fl=a/((cl*x*dcos(c)+c2*dsin(c))**2+(c3*x*dsin(c))**2)
     + /(1.0+b/e*x**2)*expo(-b*x**2)
      return
      end
с
      function g(x)
C-
      common /para/ d,cl,c2,c3,b,e,r1
      double precision x,d,c1,c2,c3,b,a,c,e,r1,expo
      double precision g
      c=x*d
      a=x*dsin(c)
      g=a/((cl*x*dcos(c)+c2*dsin(c))**2+(c3*x*dsin(c))**2)*expo(-b*x**2)
      return
      end
c
      function gl(x)
C---
      common /para/ d, c1, c2, c3, b, e, r1
      double precision x,d,c1,c2,c3,b,a,c,e,r1,expo
      double precision gl
      c=x*d
      a=x*dsin(c)
      gl=a/((cl*x*dcos(c)+c2*dsin(c))**2+(c3*x*dsin(c))**2)
     + /(1.0+b/e*x**2)*expo(-b*x**2)
      return
      end
c
      function h(x)
      common /para/ d,cl,c2,c3,b,e,r1
      double precision x,d,c1,c2,c3,b,a,c,e,r1,expo
      double precision h
      c=x+d
      a=x* (x*dcos(c)-dsin(c)/rl)
      h=a/ ((cl*x*dcos(c)+c2*dsin(c))**2+(c3*x*dsin(c))**2)*expo(-b*x**2)
      return
      end
С
      function hl(x)
      common /para/ d, cl, c2, c3, b, e, r1
      double precision x,d,c1,c2,c3,b,a,c,e,r1,expo
     double precision hl
     c=x*d
      a=x* (x*dcos(c)-dsin(c)/r1)
     hl=a/((cl*x*dcos(c)+c2*dsin(c))**2+(c3*x*dsin(c))**2)
     + /(1.0+b/e*x**2)*expo(-b*x**2)
     return
      end
c
     function expo(x)
C----
     double precision expo, x
     if (dabs(x).lt.87.0) expo-dexp(x)
     if (x.gt.87.0) expo-le38
     if (x.lt.-87.0) expo=0.0
     return
```

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```
end
```

APPENDIX B: SAMPLE INPUT

•

1, dd.	65.9 36.9 5730 1.40

 $\boldsymbol{\wp}$

e2, r0, x] flux1, flux1, .0000E+f .6333E-f .0000E+f .0000E+f .0000E+f .0000E+f .0000E+f .0000E+f .0000E+f .0000E+f .0000E+f	10.200-1.0000000000000000000000000000000	and concentration without decay	.0000E+02 1.0000E+03 1.0000E+04 1.0000E+05 1.0000E+06	2622E-02 4.6905E-03 2.7698E-04 1.5360E-04 1.2895E-04 2593E-06 3.1330E-04 2.4212E-04 1.5325E-04 1.2894E-04 7513E-04 3.4263E-01 9.4944E-01 9.7101E-01 9.7564E-01	years	:lux (cm**3/sec) // max. error // work space // cl/cs // max. error // work space // hm	0000E+02 1.0000E+03 1.0000E+04 1.0000E+05 1.0000E+06 <i>Tバイモ</i>	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	7345E-04 3.1899E-01 7.6581E-01 7.6852E-01 7.6852E-01 $C1/CS$ 3083E-05 3.6337E-05 1.7500E-10 5.4578E-07 4.3643E-07 1 1 1 1 1 68 28 20 4 4 4	2430E-02 2.5353E-03 9.8269E-04 9.4649E-04 9.4649E-04 NASS TRANSFER WEFFICIENT
<pre>df,kl,k2,el,e2,r0,xl- df,kl,k2,el,e2,r0,xl- l.0000E+00 1.0000E+01 l.1131E-01 3.6333E-02 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 l.1133E-01 3.6374E-02 0.0000E+00 0.00000E+00 0.0000E+00 0.0000E+000 0.0000E+00 0.00</pre>		nd concentratio	Ξ.	1.2622E-02 4. 1.2593E-06 3. 2.7513E-04 3.)3 years	<pre>/ flux (cm**3/80</pre>	г.	1.2754E-02 5 8.5721E-05 6 1 80	6E-06 2. 1E-05 3.	5E-04 3. 3E-05 3.	2.

eps, ibug, cut= 1.000E-04 0 2.000E+01

APPENDIX C: SAMPLE OUTPUT

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