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Use of the Hydro-Salinity, Crop Production Optimization Model APSIDE to Validate Results from an Updated Regional Flow Model of the San Joaquin River Basin

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### Authors

Quinn, Nigel WT  
Cronin, John

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# 2 Simple Models and Analytical Procedures for Total 3 Maximum Daily Load Assessment

4 Harry X. Zhang, Ph.D., P.E.

5 Program Director, Water Research Foundation, 1199 N Fairfax St., Suite  
6 900, Alexandria, VA 22314 (corresponding author). Email: hzhang@  
7 waterrf.org




8 Nigel W. T. Quinn, Ph.D., P.E., D.WRE.

9  Berkeley National Laboratory, Berkeley, CA. Email: nwtquinn@gmail  
10  .com

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## 19 Introduction

 20  The degree of analysis required for each component of TMDL de-  
21  22 velopment can range from simple screening-level approaches based  
23 on limited data to detailed investigations that might need several  
24 months or even years to complete (USEPA 1999).

25 Many simple models and analytical procedures were developed  
26 prior to the advent of fast digital computers to manage environmen-  
27 tal impacts. Simple methods are often used when data limitations  
28 and budget and time constraints preclude using more detailed  
29 approaches. These tools are used to diagnose non-point-source  
30 pollution problems when information is relatively limited.

31 For watershed loading estimates, simple models and analytical  
32 procedures can be used to support an assessment of the relative  
33 significance of different pollutant sources, guide decisions for man-  
34 agement plans, and focus continuing monitoring. Simple models  
35 estimate pollutant loads based on land use or other watershed char-  
36 acteristics. Typically, simple methods rely on a large-scale aggreg-  
37 ation of these watershed characteristics and neglect detailed  
38 features of land uses and natural processes. These tools rely on gen-  
39 eralized sources of information and therefore have low to medium  
40 requirements for site-specific data. Default values provided for  
41 these methods are derived from empirical relationships that are  
42 based on regional or site-specific data. The estimates are usually  
43 expressed as mean annual values. Simple methods provide only  
44 preliminary estimates of sediment and pollutant loadings and may  
45 only have limited predictive capability (Zhang 2005).

46 The major advantage of simple methods is that these tools can  
47 provide a rapid means of identifying critical pollutant loads with  
48 minimal effort and data requirements. Simple methods are typically  
49 derived from empirical relationships between physiographic char-  
50 acteristics of the watershed and pollutant export. In addition, sim-  
51 pler approaches can save time and expense and can be applied by a  
52 wider range of personnel. Simple approaches also generally are  
53 easier to understand than more detailed analyses (USEPA 1999).

54 Progress in science and computing, along with changing envi-  
ronmental problems, have allowed modelers to develop increasingly

55 complex and comprehensive modeling frameworks. Unfortunately,  
56 this often leads to the common misconception that complex models  
57 are necessarily superior to simpler approaches. In fact, the choice  
58 of a water quality model involves trade-offs among model complex-  
59 ity, required reliability, cost, and time (Chapra 2003). Therefore,  
60 this paper presents a review of simple models and analytical proce-  
61 dures in TMDL applications and illustrates the strengths and weak-  
62 nesses of utilizing simple methods in TMDL development and  
63 implementation.

## 64 Review of Simple Models and Analytical 65 Procedures

66 The simple models and analytical procedures introduced in this  
67 paper may be used initially in phased TMDLs to estimate TMDLs  
68 but usually are employed to check and analyze TMDLs (Mysiak  
69 et al. 2005; Voinov 2008). Some models like the Revised Universal  
70 Soil Loss Equation 2 (RUSLE2) are auxiliary tools to identify loads  
71 like sediment yields from different catchments to prioritize imple-  
72 mentation. Spreadsheets are typically used to list and track imple-  
73 mentation actions as well as perform simple mass balances for  
74 checking assessments as well as for other tasks. Occasionally, in  
75 the hands of an expert, methods like a simple mass balance spread-  
76 sheet can rule out some allocations and implementation options.

77 Some simple models for receiving water analysis use a mass  
78 balance approach that assumes steady-state conditions. Accuracy  
79 is limited when default parameters are substituted for site-specific  
80 data. The procedure neglects seasonal variation in predicting annual  
81 loadings and considers only steady-state conditions for receiving  
82 water analysis (USEPA 1999). However, in some circumstances,  
83 getting a reasonable estimate for an average watershed water bal-  
84 ance and contributions to constituent load may be sufficient for a  
85 TMDL to proceed.

86 Other models may deploy similar concepts of mass balance but  
87 employ annual or monthly time steps, avoiding the limitations of  
88 steady-state conceptual models while keeping data requirements to  
89 a minimum and avoiding the complexity of more refined numerical  
90 models. Model integration and linkage of models is often desirable  
91 for many TMDLs, where analysts can achieve greater acceptance of  
92 model-based analysis by employing existing models in widespread  
93 use. Where these modeling tools and analytical techniques do not  
94 fully characterize the system, they can be complemented with other  
95 functions or models linked to the main modeling tool to provide the  
96 needed level of analysis.

97 Table 1 summarizes several simple methods and analytical  
98 procedures for TMDL assessment.

## 99 Simple Mass Balance Equation

100 The basic principle of water quality models is that of mass balance.  
101 A water system can be divided into different segments or volume  
102 elements, also called computational cells. For each segment or cell,  
103 there must be a mass balance for each water quality constituent over  
104 time (Loucks and van Beek 2005).

105 Simplified mass balances are typically applied in spreadsheets  
106 to discrete water volumes containing a uniform concentration of a

**6 Table 1.** Comparison of simple methods and analytical procedures for TMDL assessment

	Number	Method	Advantages/benefits	Disadvantages/shortcomings	Key references/example applications
T1:1	1	Simple mass balance equation	(1) Most easily understood by the users; and (2) clearly show the inputs and outputs of the calculation	The assumptions may be oversimplified and inaccurate for complex systems	McCutcheon (1989) and Chapra (1997)
T1:3	2	Simple method to estimate urban stormwater loads	(1) Use of runoff coefficient and mean concentration based on EPA's NURP data; and (2) time scale is for annual and monthly events	(1) Only provides a general planning estimate of likely storm pollutant export; and (2) does not consider pollutants associated with base flow volume	USEPA (1983), Schueler (1987), and Capiella and Brown (2001)
T1:4	3	USGS regression method	(1) Based on regression equations from USGS studies; and (2) can incorporate regional variations in the estimate	Only valid for areas where regression coefficients are obtainable (i.e., regional transferability is limited)	Tasker and Driver (1988) and Driver and Troutman (1989)
T1:5	4	Revised Universal Soil Loss Equation	(1) Applied and validated by broad users for decades; and (2) with consistent enhancement by USDA	Only estimates average annual erosion and sediment delivery from runoff	Wischmeier and Smith (1978), Renard et al. (1997), and USDA (2003)
T1:6	5	BATHTUB	(1) Easy to use tool for eutrophication analysis for lakes and reservoirs; and (2) used routinely in the lake TMDLs when steady-state condition is sufficient for water quality analysis	(1) Only for steady-state application; and (2) the model is based on accuracy of empirical equations built in the model	Walker (1985, 1986)
T1:8	6	Stream Segment Temperature Model (SSTEMP)	(1) Easy to use model that can simulate heat balance; and (2) used to analyze the effects of changing riparian shade for temperature TMDL application	Lacks many of the detailed features of dynamic models needed for complex temperature TMDLs	Theurer et al. (1984), Bartholow (2010), and Chen et al. (1993, 1998a, b)
T1:9	7	Load-duration curve	(1) Has been applied in various type of TMDLs; and (2) TMDL load is expressed as a function of flow conditions	(1) Does not mechanistically relate sources and receiving water quality response; and (2) does not allow simulation of scenarios evaluating the impact of various implementation options	USEPA (2007), Risley et al. (2008), and SCDHEC (2010)
T1:10	8	Simple transient mass balance models	(1) Conceptually clear, addition/subtraction of mass; and (2) model assumptions explicit and readily changed	(1) Spreadsheet format can be cumbersome for simulations greater than one year; and (2) version control challenging because spreadsheet can be easily modified	(1) WETMANSIM is a spreadsheet based monthly water and salt balance for managed wetlands; and (2) SJRIO model performs daily flow and salt mass balance of inflow to the River and diversions from the River from surface and groundwater sources
T1:11 T1:12		WETMANSIM; San Joaquin River Input-Output Model (SJRIO)			
T1:13	9	GIS workflow models	(1) Object-oriented approach, easy to implement; and (2) visually appealing—takes advantage of power of GIS technology	(1) Requires acquisition and knowledge of GIS; and (2) data often lacking to fully exploit GIS application	Universal soil loss equation is a simple product of spatial coverages to obtain soil loss estimates

T1:7

107 nonreactive material or pollutant so that concentration  $C$  and load  
 108  $W$  are easily related via flow  $Q$  as follows (McCutcheon 1989;  
 109 Chapra 1997):

$$C = \frac{1}{Q} W; \quad W = QC \quad (1)$$

110 The waste assimilative capacity or TMDL for any discrete vol-  
 111 ume of water containing a conservative substance or pollutant is the  
 112 water quality standard in concentration of the substance multiplied  
 113 by the flow rate.

### Simple Method to Estimate Urban Stormwater Loads

The Simple Method (Schueler 1987) is an easy-to-use empirical equation for estimating pollutant loadings of an urban watershed by the Metropolitan Washington Council of Governments (MWCOG). The Simple Method is essentially an approach to rapidly estimate loads based on available information such as (1) catchment drainage area and impervious cover, and (2) stormwater runoff concentrations.

The Simple Method estimates pollutant loads for chemical constituents as a product of annual runoff volume and pollutant concentration

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$$L = 0.226 \times R \times C \times A \quad (2)$$

where  $L$  = annual load (lbs);  $R$  = annual runoff (in.);  $C$  = pollutant concentration (mg/L);  $A$  = area (acres); and 0.226 = unit conversion factor.

The method is best adapted for use in small watersheds of less than 1 sq mi (USEPA 1999). The Simple Method uses different impervious cover values for separate land uses within a subwatershed, including agricultural land use category. These numbers are derived from a study conducted by the Center for Watershed Protection under a grant from the USEPA to update impervious cover estimates for a variety of land uses (Cappiella and Brown 2001). The Simple Method provides estimates of storm pollutant export that are probably close to the true but unknown value for a development site, catchment, or subwatershed. It can be used for analyzing a smaller watershed or site planning. The method was developed using the database generated during a Nationwide Urban Runoff Program (NURP) study (USEPA 1983) in the Washington, DC, area and the national NURP data analysis. The equations, however, may be applied anywhere in the country. Some precision is lost as a result of the effort to make the equation general and simple.

The Simple Method is adequate for decision making at the site planning level. For example, it may be used to estimate runoff pollutant concentration from urban drainage areas. Runoff volume is estimated using runoff coefficients for the fraction of rainfall converted to runoff. A correction factor is used to account for those storms that do not produce runoff. Potential applications of the Simple Method are to estimate pollutant loading from an uncontrolled development site or to estimate expected extreme concentrations that will occur over a specified time period (USEPA 1999).

### 154 USGS Regression Method

The USGS Regression Method (Tasker and Driver 1988) is an example of a statistical-based method. This method estimates source loading as a function of several variables such as land use, percentage of imperviousness, drainage area, and mean annual rainfall. The USGS has developed equations for determining pollutant loading rates based on regression analyses of data from sites throughout the country (76 gauging stations across 20 states).

The regression approach is based on a statistical description of historic records of storm runoff responses on a watershed level (Tasker and Driver 1988). This method may be used for rough preliminary calculations of annual pollutant loads when data and time are limited (Tasker and Driver 1988; Driver and Troutman 1989). Inputs required for this level of modeling include drainage data, percent imperviousness, mean annual rainfall, general land use pattern, and mean minimum monthly temperature. Application of this method provides mean planning loads and corresponding confidence intervals for storms. The most significant explanatory variables in all of the linear regression models were total storm rainfall and total contributing drainage area. Impervious area, land use, and mean annual climatic characteristics were also significant explanatory variables in some linear regression models (Driver and Troutman 1989).

The USGS Regression Method gives mean storm-event pollutant loads and corresponding confidence intervals. The method is used to estimate the pollutant concentration from urbanized watersheds and relies upon a statistical approach to estimate annual, seasonal, or storm-event mean pollutant loads. The method is valid only for areas where regression coefficients are obtainable (i.e., regional transferability is limited). The method typically applies to smaller watersheds, although a specific size range of the watersheds was not provided by USGS.

### Revised Universal Soil Loss Equation

The Revised Universal Soil Loss Equation 2 (RUSLE2) (USDA 2003) is an updated advanced erosion prediction technology that uses the familiar empirical structure of the Universal Soil Loss Equation (USLE) and RUSLE1. This conservation planning tool has an extensive history of development beginning with the Universal Soil Loss Equation (Wischmeier and Smith 1978), then RUSLE (Renard et al. 1997) and been used on farms and ranches as well as for planning roadside protection and soil erosion in strip mining. A computer interface makes RUSLE2 easily used and adaptable to special conditions.

Robust and computationally efficient, RUSLE2 estimates the effects of soil, climate, and land management on sheet and rill erosion and sediment delivery from hillslopes; it also estimates the size distribution and clay enrichment of sediment delivered to the channel network in a watershed. This software is linked to extensive databases maintained by the USDA's Natural Resources Conservation Service (NRCS) and to other computer programs. For TMDL assessment, RUSLE2 allows a water quality analyst to specify a representative runoff event sequence at a site using soil characteristics, land management techniques, and a user-specified return period that can be coupled with a channel erosion and routing model. This software is flexible, easy to use, and has extensive, reliable databases for almost any climate, soil, and land management alternative in the United States.

RUSLE2 estimates average annual erosion and sediment delivery from runoff. Like the USLE, erosion is calculated as the product of several factors: rainfall and runoff factor  $R$ ; soil erodibility factor  $K$ ; slope length factor  $L$ ; steepness topographic factor  $S$ ; cover and land management factor  $C$ ; and support practice factor  $P$ . However, in RUSLE2, these factors are no longer independent, and computations are done on a daily or event basis so that the product of the annual averages of these factors may not be equal to the sum of the daily values. Another difference from USLE is that RUSLE2 represents sediment transport and deposition on concave areas so that the RUSLE2 concept defines hillslopes from the top of a hill and through depositional areas, ending in a concentrated flow channel.

A strength of RUSLE2 as a tool for TMDL development is the extensive database that includes climate and soils descriptions for every county in the United States. Land management scenarios are organized into 78 crop management zones. Each scenario represented using RUSLE2 is created by combining field operations (e.g., grading, tillage, planting, applying materials, or harvest), vegetation growth over time, and residue decomposition, biomass, and cover. As of January 2011, the NRCS database contained over 29,000 management scenarios composed of combinations of approximately 600 tillage and field operation records, 1,400 vegetation records, and 140 residue records. At that time, the database also contained about 600 choices of support practices consisting of contour systems, hydraulic element systems (diversions, terraces, and impoundments), and strip-barrier systems.

Although an individual one-dimensional hillslope profile is the fundamental unit over which RUSLE2 computes erosion and sediment delivery, RUSLE2 can also be accessed through the application programming interface to estimate distributed hillslope runoff and sediment yields. Distributed hillslope runoff and sediment yield calculations can be used with ephemeral gully and channel models to estimate sources and sinks of sediment from gullies and streams and to route sediment to a watershed outlet.

Accurate development of sediment TMDLs must deal with the complexity of sediment generation and transport through watersheds, which include erosion and deposition on the hillslopes, delivery to channels, and sediment scour or deposition within the

249 channels. Implementation of a sediment TMDL assessment re- 308  
250 quires evaluation of management alternatives that reduce sediment 309  
251 delivery to the channels in a watershed. The RUSLE2 framework 310  
252 covers most of the field management alternatives that farmers use 311  
253 on hillslopes to prevent soil loss. 312

254 As an example based on the USLE, the EPA's screening proce- 313  
255 dures can be used to assess point and nonpoint source loadings 314  
256 and atmospheric deposition loads. Agricultural nonpoint loads 315  
257 are based on the USLE, Soil Conservation Service [SCS, now the 316  
258 Natural Resource Conservation Service (NRCS)] runoff curve 317  
259 number procedure, and loading functions using enrichment ratios. 318  
260 Urban nonpoint loads are estimated using the buildup-washoff con- 319  
261 cept (i.e., the buildup-washoff concept accounts for incremental 320  
262 buildup of nutrients between storms). 321

## 263 **BATHTUB**

264 **BATHTUB** is an empirical lake eutrophication model developed 322  
265 for the USACE in the 1980s based on data from USACE reservoirs 323  
266 (Walker 1985, 1986). It is a steady-state eutrophication model 324  
267 applicable to lakes and reservoirs based on empirical assessments 325  
268 of reservoir data.

269 **BATHTUB** is designed to facilitate application of empirical 326  
270 eutrophication models to reservoirs or lakes. The program formu- 327  
271 lates steady-state water and nutrient mass balances in a spatially 328  
272 segmented hydraulic network that accounts for advective transport, 329  
273 diffusive transport, and nutrient sedimentation. Eutrophication- 330  
274 related water quality conditions (expressed in terms of total phos- 331  
275 phorus, total nitrogen, chlorophyll a, transparency, organic nitrogen, 332  
276 nonorthophosphorus, and hypolimnetic oxygen depletion rate) are 333  
277 predicted using empirical relationships previously developed and 334  
278 tested for reservoir applications. To provide regional perspectives on 335  
279 reservoir water quality, controlling factors, and model performance, 336  
280 **BATHTUB** can also be configured for simultaneous application to 337  
281 collections or networks of reservoirs. 338

282 The basic elements defining each application include (1) seg- 339  
283 ments, which are reservoir zones specified in a one-dimensional, 340  
284 branched network (e.g., upper pool, midpool, near dam, and differ- 341  
285 ent tributary arms); and (2) tributaries, which are inflow or outflow 342  
286 streams, each associated with a particular segment. The **BATHTUB** 343  
287 model can assess the impacts of changes in water and/or nutrient 344  
288 loadings and impacts of changes in mean pool elevation during the 345  
289 growing season and estimate nutrient loadings consistent with 346  
290 given water quality management objectives. 347

291 **BATHTUB** is a tool for modeling reservoirs, chains of lakes, 348  
292 lakes with multiple inlets, or situations where more detailed nutri- 349  
293 ent and water budgets are required. **BATHTUB** is used routinely 350  
294 in developing nutrient-based TMDL studies. 351

## 295 **Stream Segment Temperature Model**

296 Stream Segment Temperature Model (SSTEMP) is a scaled-down 352  
297 version of the Stream Network Temperature Model (SNTEMP) de- 353  
298 veloped by Theurer et al. (1984). This USGS-supported model is 354  
299 based on a simplified heat balance. The model simulates steady- 355  
300 state stream temperatures for a specified time period and location 356  
301 in a stream or river (Bartholow 2010). 357

302 The SSTEMP program requires inputs describing the average 358  
303 stream geometry, as well as (steady-state) hydrology and meteor- 359  
304 ology plus stream shading. SSTEMP optionally estimates the com- 360  
305 bined topographic and vegetative shade as well as solar radiation 361  
306 penetrating the water. It then predicts the mean daily water temper- 362  
307 atures at specified distances downstream. It also estimates the daily 363

308 maximum and minimum temperatures. Unlike the large network 309  
310 model SNTEMP (Bartholow 2010), this program simulates single- 311  
312 stream segments for a single time period (e.g., a month, week, or 312  
313 day) for any given set of model specifications. Initially designed as 313  
314 a training tool, the SSTEMP program may be used satisfactorily for 314  
315 a variety of simple cases. The SSTEMP model is especially useful to 315  
316 perform sensitivity and uncertainty analysis. With good-quality 316  
317 specifications, SSTEMP should adequately reproduce mean daily 317  
318 water temperatures throughout a stream reach. Users should not 318  
319 expect too much from SSTEMP if the input values are of poor qual- 319  
320 ity or if the model's assumptions were not met. 320

321 The SSTEMP model is not specifically designed for TMDL 321  
322 analysis and lacks many of the detailed features of complex model 322  
323 adapted for the first temperature TMDL in Oregon (Chen et al. 323  
324 1993, 1998a, b). However, SSTEMP can be used to analyze the 324  
325 effects of changing riparian shade or the physical features of a 325  
326 stream and examine the effects of different stream withdrawals and 326  
327 returns on instream temperature for TMDL-related applications. 327

## Load-Duration Curve 326

327 The load-duration curve (LDC) approach allows for characterizing 327  
328 water quality concentrations at different flow regimes. The pollu- 328  
329 tant load is expressed as a function of all flow conditions, including 329  
330 critical flow condition (USEPA 2007). This statistical-based ap- 330  
331 proach quickly estimates existing and allowable loads with limited 331  
332 information. Some practitioners value the insight that load-duration 332  
333 curves provide into the relationship between water quality impair- 333  
334 ment and hydrologic regime (ASCE 2017). 334

335 The first step in a TMDL analysis using a load-duration curve is 335  
336 to generate a flow-duration curve, which is a cumulative frequency 336  
337 curve of daily mean flows without regard to chronology of occur- 337  
338 rence (Leopold 1994). The flow-duration curve includes all flows 338  
339 observed at a stream gauge for the applicable period of record. Flow 339  
340 rates are typically sorted from the largest value to the smallest. For 340  
341 each flow, the flow-duration curve provides the corresponding per- 341  
342 cent of time that a magnitude of flow is equaled or exceeded. The 342  
343 percentage of time is the flow-duration interval or flow-duration 343  
344 percentile (Risley et al. 2008). Once a flow-duration curve has been 344  
345 created, a load-duration curve is created by multiplying flow by the 345  
346 applicable water quality criterion or target. The independent  $x$ -axis 346  
347 remains as the flow-duration interval, and the dependent  $y$ -axis 347  
348 depicts the load at specific point in the watershed where flow mon- 348  
349 itoring data are available. A specific curve derived from flow and 349  
350 the water quality criterion therefore represents the allowable load at 350  
351 each flow condition. Points above that curve represent exceedances 351  
352 of the water quality criterion and are therefore excess loads. Those 352  
353 points below that curve represent compliance with the water quality 353  
354 criterion and allowable pollutant loads. 354

355 A fecal coliform TMDL development in South Carolina pre- 355  
356 pared by the South Carolina Department of Health and Environ- 356  
357 mental Control (SCDHEC 2010) is one example that illustrates the 357  
358 use of the load-duration curve approach. An appendix in the EPA 358  
359 guide *An Approach for Using Load Duration Curves in the Devel-* 359  
360 *opment of TMDLs* (USEPA 2007) describes a case study in which 360  
361 load-duration curves were used to support TMDL development. 361  
362 Important information can be derived from a load-duration curve 362  
363 to support TMDL assessment. The extent of the impairment can 363  
364 be visually assessed based on the number of loads that are greater 364  
365 or less than the allowable loading curve. The nature of the impair- 365  
366 ment can also be inferred based on when the loads occur (USEPA 366  
367 2007). Loads that are greater than the curve for allowable pollutant 367  
368 loads during low-flow conditions are likely indicative of constant 368

369 discharge, such as wastewater-treatment plants. Those loads are  
370 greater than the curve for allowable pollutant loads during wet  
371 weather conditions likely reflect contributions associated with sheet  
372 and rill erosion, washoff processes, and, potentially, streambank  
373 erosion. Those loads plotting above the curve at the high and small  
374 ends of the curve reflect extreme hydrologic conditions of flood or  
375 drought. If sufficient data are available, the load-duration curve  
376 method accurately identifies the allowable and existing loads at the  
377 point in the stream where the data were collected and can be used to  
378 meet the basic regulatory requirement for TMDL development.  
379 Load-duration curves are relatively easy to develop and offer in-  
380 sight into critical conditions.

381 On the other hand, although the relative importance of low-flow  
382 point sources versus wet weather nonpoint sources can often be  
383 identified from the load-duration curve, no specific information is  
384 provided regarding what types of point or nonpoint sources exist in  
385 the watershed. Load-duration curves also do not allow simulation of  
386 scenarios evaluating the impact of various implementation options.  
387 The load-duration curves do not mechanistically relate sources and  
388 water quality response. Therefore, forecasting load reduction effects  
389 on impairments on a what-if basis are impossible because it cannot  
390 define the relationship of cause and effect.

### 391 **Simple Transient Mass Balance Models**

392 For some TMDL modeling requirements, standard models are not  
393 sufficient, and custom applications need to be developed. In the  
394 majority of cases, these models utilize the concept of mass balance  
395 by first developing a hydrology budget for the three-dimensional  
396 volume representing the system being analyzed. In some cases,  
397 the system volume is subdivided into a number of vertical layers  
398 to improve representation of the interactions between above sur-  
399 face, root zone, shallow, and deep groundwater aquifers. The con-  
400 figuration of the model depends on available data and the chemistry  
401 of the contaminant being regulated. Spreadsheets have been used to  
402 good effect to develop both simple steady-state and transient mass  
403 balance models.

### 404 **Wetland Management Simulator**

405 The Wetland Management Simulator (WETMANSIM) (Quinn  
406 2004) spreadsheet model is an example of a customized monthly  
407 mass balance model of seasonal wetland hydrology and salinity.  
408 The model was developed specifically for managed wetlands that  
409 receive water as canal deliveries in the fall, hold water in shallow  
410 impoundments during the winter, and release the bulk of the ponded  
411 water during spring wetland drawdown. Depending on water avail-  
412 ability, the wetlands are flood irrigated one or more times during the  
413 late spring and early summer months to encourage the growth of  
414 moist soil plants that provide wetland habitat and food resources  
415 for migratory waterfowl. The high clay content of wetland soils that  
416 desiccate and crack during the summer months and swell when wet-  
417 ted required the use of a water displacement infiltration algorithm  
418 rather than the typical Richards equation formulation used by most  
419 models. Monthly time steps were sufficient to provide analysts and  
420 regulators with the necessary relationship between applied water  
421 salinity and the salinity of wetland drainage return flows to the re-  
422 ceiving water body. The simple monthly steady-state spreadsheet  
423 formulation made it easy to adapt the model to create individual  
424 submodels for private wetlands and for State and Federal wildlife  
425 refuges that allowed more local control of salt loading by these en-  
426 tities. WETMANSIM is fairly typical of customized TMDL models  
427 used in TMDL development that are well matched to TMDL objec-  
428 tives and available data.

### **San Joaquin River Input-Output Model**

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The San Joaquin River Input-Output Model (SJRIO) (CVWB 2004)  
is an example of a customized mass balance model where neither a  
monthly nor annual steady-state conceptual model was sufficient for  
analysis of the options being considered by the TMDL. In this case,  
the concept of real-time salinity management was being explored,  
which involved improved coordination of saline drainage return  
flows produced on the west side of the San Joaquin River Basin to  
coincide with reservoir releases of high-quality snowmelt runoff  
from the east side of the Basin. This operational concept became the  
basis of regulatory policy and an amendment to the Basin's water  
quality control plan. For this TMDL modeling approach, the sce-  
nario needed to be tested for a range of river basin hydrologic con-  
ditions and water year types ranging from wet to critically dry. River  
hydrology and water quality are largely determined by releases from  
state and federally-managed reservoirs on the east side of the Basin.  
Hence, another model was needed to simulate the linkage between  
climate and water storage that included the logic behind water re-  
lease policies under various water storage scenarios. This auxiliary  
model was linked to the SJRIO model to develop an implementation  
strategy for the salinity TMDL, and the 30-year hydrologic time  
series it provided allowed the strategy to be tested for a historic se-  
quence of water year types. This is an example of model integration  
and linkage. In this case, linkage of a simple mass balance account-  
ing model with another model capable of creating a historic time  
series of flow and water quality conditions to support the technical  
TMDL methodology.

### **GIS Workflow Models**

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Increased use of GIS and high-resolution remote-sensing analysis  
in support of TMDL modeling has given rise to simple object-  
oriented modeling toolboxes where coverages of land use and other  
measurable data are combined to yield estimates of key decision  
variables. A common application of this methodology is erosion  
modeling. The RUSLE2 example presented previously is a model  
easily adapted to this technique.

Another example is the ArcView Generalized Watershed Load-  
ing Functions (AVGWLF) tool (Evans and Corradini 2016), which  
facilitates the use of the Generalized Watershed Loading Functions  
(GWLF) Model via a GIS software (ArcView) interface. The  
AVGWLF tool is suitable for application to generalized watershed  
loading, source assessment, and seasonal and interannual variabil-  
ity. The AVGWLF tool has been extensively used in the Northeast  
and mid-Atlantic regions. This tool has been adopted by Pennsyl-  
vania as a statewide model for TMDL development and agricultural  
land management (USEPA 2005; Evans and Corradini 2016).

The main advantages of GIS workflow modeling are model  
transparency, the ability to perform operations over a discretized  
model mesh that provides great spatial details, and the appeal of  
the visualization associated with this approach. This technique  
works well with simple models where data such as land use can be  
readily represented in a GIS. The technique is less effective for  
more complex models where the factors are less easily visualized  
or discretized.

### **Summary**

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Simple methods require expert judgment to interpret empirical  
relationships between watershed characteristics and pollutant loads  
to receiving waters. A few of these methods may use existing  
databases and typically can vary in sophistication from a simple

487 spreadsheet program or handheld calculator. In some cases, they  
488 could be in the form of an easy-to-use computer-based numerical  
489 modeling tool. Simple models and methods are often used when  
490 limited data availability and budget or time constraints preclude  
491 the use of more sophisticated methods.

492 Based on the review of several examples of simple models and  
493 analytical procedures, simpler approaches can save time and ex-  
494 pense to support TMDL estimates. Simple approaches also gener-  
495 ally are easier to understand than more detailed analyses by a broad  
496 range of users. The trade-offs associated with using simple ap-  
497 proaches include a potential decrease in forecast accuracy and often  
498 an inability to make predictions at fine geographic and time scales  
499 (e.g., watershed-scale source predictions versus model detailed es-  
500 timates, and annual versus seasonal estimates) (USEPA 1999).

501 The major advantage of simple methods is that these tools can  
502 provide a rapid means of identifying critical loading areas with  
503 minimal effort and data requirements. The major disadvantage of  
504 using simple methods is that only gross estimates of nutrient loads  
505 can be provided, which are of limited value for determining loads  
506 on a seasonal or finer time scale. Another disadvantage is that sim-  
507 ple methods are of limited use for evaluating the effect of non-  
508 point-source control (USEPA 1999).

509 The standard practice in modeling is to identify the dominant  
510 processes and identify the simplest models sufficient to meet the  
511 needs of the project (USEPA 2005). Models include suites of equa-  
512 tions that represent most processes based on the understanding of  
513 real-world setting. Thomann and Mueller (1987) established that  
514 the simplest model sufficient to answer management questions with  
515 confidence should be applied. If data availability does not reach the  
516 level that a detailed model requires, then a simpler model should be  
517 employed.

518 The choice of a water quality model involves trade-offs among  
519 model complexity, required reliability, cost, and time. An adaptive  
520 approach to modeling would start with simpler models at the initial  
521 phases and then progress to more complex frameworks as addi-  
522 tional data are collected and as more focused remedial measures  
523 are assessed (Chapra 2003). Starting with simple analyses and iter-  
524 atively expanding data collection and modeling as the need arises is  
525 the best approach (NRC 2001). Within the limitations of their de-  
526 sign functionality and underlying assumptions, the simple models  
527 and analytical procedure can be useful in the TMDL assessment.

## 528 Acknowledgments

529 The TMDL Analysis and Modeling Task Committee of the  
530 American Society of Civil Engineers' Environmental and Water  
531 Resources Institute was formed to address concerns and challenges  
532 over the current practices of analysis and modeling in the TMDL  
533 development and implementation in terms of analysis technique,  
534 model selection, data requirement, calibration, confirmation test-  
535 ing, and uncertainty reporting. The committee investigated some of  
536 the current practices of analysis and modeling in TMDL develop-  
537 ment and implementation and reported the technical challenges in a  
538 report entitled *Total Maximum Daily Load Analysis and Modeling:  
539 Assessment of the Practice*, published by ASCE Press in 2017.  
540 Authors of this paper are members of the Task Committee, and the  
541 paper is partly based on the findings of the Task Committee and  
542 expansion of original publication.

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