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**Publication Date**

1980



# Lawrence Berkeley Laboratory

UNIVERSITY OF CALIFORNIA

## Engineering & Technical Services Division

X-RAY POWDER DIFFRACTION PATTERNS FOR ST. LOUIS  
AEROSOL SAMPLES

B. H. O'Connor and J. M. Jaklevic

January 1980

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X-RAY POWDER DIFFRACTION PATTERNS FOR  
ST. LOUIS AEROSOL SAMPLES\*

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The purpose of this report is to present the diffraction pattern data measured in a x-ray powder diffraction study of airborne particulate material which had been collected in the St. Louis area on cellulose ester membrane filters (O'Connor and Jaklevic; 1979a, 1979b).

The St. Louis filter samples were collected with dichotomous samplers operated continuously at 50 l/min over periods of 6 or 12 hours, and producing fine ( $<2.4 \mu\text{m}$  mass median diameter) and course ( $2.4\text{-}20 \mu\text{m}$ ) particle deposits on  $1.2 \mu\text{m}$  pore size cellulose ester membrane filters (Millipore\*\*\* type RAWP) of effective diameter 32 mm and mass/area =  $4 \text{ mg/cm}^2$ . The samples were from stations 103 and 105 (inner city sites), 118 (transitional) and 124 (outer), along a line running in a southerly direction from the city. Details of the sample collection conditions and mass loadings are given in O'Connor and Jaklevic (1979b).

The powder diffractograms were acquired with a conventional Norelco Bragg-Brentano diffractometer, and with a Cu anode x-ray tube operated at 40kV and 20mA and monochromatized with a  $8.4 \mu\text{m}$  Ni filter. The intensity of the diffracted beam was measured with a Xe side-window proportional counter and the detector arm was stepped in increments of  $0.04^\circ$  in  $2\theta$  (2x Bragg angle) from  $10^\circ$  to  $50^\circ$ . A  $1^\circ$  divergence slit was employed with a matching antiscatter slit and a  $0.05^\circ$  receiving slit. The total time for each scan was 23 hours.

The patterns were reduced by manual means to sets of peak positions ( $2\theta$  in degrees) and relative intensity above background (INT). The line data are given in Tables 1 and 2, together with the Bragg spacing (D in Angstrom units) and the uncertainty in the spacing (ERR-D).

The reduced data were subsequently analyzed by the search/match identification system operated by the Interactive Sciences Corporation through the Telenet computer network (see O'Connor and Jaklevic, 1979b). Figures 1 and 2 give the powder diffraction patterns in bar graph form and the line assignments for the selected compounds.

\* This work was supported by the Division of Biomedical and Environmental Research of the U.S. Department of Energy under Contract No. W-7405-ENE-48.

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\*\*\*Reference to a company name or product name does not imply approval or recommendation of the product by the University of California or the United States Department of Energy to the exclusion of others that may be suitable.

REFERENCES

O'Connor, B.H. and Jaklevic, J.M. (1979a) X-ray diffractometry of airborne particulates deposited on membrane filters. Lawrence Berkeley Laboratory -- Report LBL-9041.

O'Connor, B.H. and Jaklevic, J.M. (1979b). Chemical analysis of ambient aerosol samples by x-ray powder diffractometry. Lawrence Berkeley Laboratory -- Report LBL-9496.

Table 1a. Diffraction Data for Station 103 Fine Fraction Samples

SAMPLE I/D : 58771

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 10.03     | 8.816  | .050  | 3.0  |
| 2    | 11.76     | 7.526  | .037  | 4.0  |
| 3    | 12.16     | 7.277  | .034  | 15.0 |
| 4    | 14.00     | 6.324  | .026  | 5.0  |
| 5    | 14.87     | 5.959  | .023  | 3.0  |
| 6    | 18.20     | 4.873  | .015  | 2.5  |
| 7    | 18.78     | 4.725  | .014  | 3.0  |
| 8    | 20.10     | 4.417  | .013  | 5.0  |
| 9    | 20.33     | 4.367  | .012  | 8.0  |
| 10   | 20.56     | 4.319  | .012  | 10.0 |
| 11   | 21.31     | 4.169  | .011  | 6.0  |
| 12   | 22.92     | 3.879  | .010  | 2.0  |
| 13   | 23.56     | 3.777  | .009  | 3.0  |
| 14   | 27.70     | 3.220  | .007  | 8.0  |
| 15   | 28.51     | 3.131  | .006  | 3.0  |
| 16   | 29.31     | 3.047  | .006  | 6.0  |
| 17   | 29.83     | 2.995  | .006  | 2.0  |
| 18   | 32.02     | 2.795  | .005  | 5.0  |
| 19   | 34.49     | 2.600  | .004  | 4.0  |
| 20   | 38.92     | 2.314  | .003  | 1.5  |
| 21   | 40.82     | 2.210  | .003  | 2.0  |

SAMPLE I/D : 73464

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 12.20     | 7.255  | .047  | 5.0  |
| 2    | 16.92     | 5.240  | .025  | 5.0  |
| 3    | 20.20     | 4.396  | .017  | 15.0 |
| 4    | 20.48     | 4.336  | .017  | 27.0 |
| 5    | 21.32     | 4.167  | .015  | 3.0  |
| 6    | 22.84     | 3.893  | .013  | 6.5  |
| 7    | 23.56     | 3.776  | .013  | 3.0  |
| 8    | 27.48     | 3.246  | .009  | 2.0  |
| 9    | 28.48     | 3.134  | .009  | 6.0  |
| 10   | 29.28     | 3.050  | .008  | 9.0  |
| 11   | 29.84     | 2.994  | .008  | 4.0  |
| 12   | 32.08     | 2.790  | .007  | 1.0  |
| 13   | 33.72     | 2.658  | .006  | 1.0  |
| 14   | 34.28     | 2.616  | .006  | 1.5  |
| 15   | 35.48     | 2.530  | .006  | 1.0  |
| 16   | 38.76     | 2.323  | .005  | 1.5  |

SAMPLE I/D : 67765

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT |
|------|-----------|--------|-------|-----|
| 1    | 12.08     | 7.326  | .048  | 3.5 |
| 2    | 20.20     | 4.396  | .017  | 2.5 |
| 3    | 27.52     | 3.241  | .009  | 1.5 |
| 4    | 34.20     | 2.622  | .006  | 1.0 |

SAMPLE I/D : 69476

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 12.16     | 7.278  | .048  | 27.0 |
| 2    | 16.68     | 5.315  | .025  | 4.0  |
| 3    | 16.96     | 5.228  | .024  | 7.5  |
| 4    | 20.12     | 4.413  | .017  | 15.0 |
| 5    | 20.48     | 4.336  | .017  | 30.0 |
| 6    | 22.80     | 3.900  | .014  | 9.0  |
| 7    | 27.52     | 3.241  | .009  | 10.5 |
| 8    | 28.48     | 3.134  | .009  | 4.5  |
| 9    | 29.24     | 3.054  | .008  | 7.5  |
| 10   | 29.80     | 2.998  | .008  | 6.0  |
| 11   | 32.00     | 2.797  | .007  | 5.0  |
| 12   | 34.40     | 2.607  | .006  | 5.0  |
| 13   | 35.60     | 2.522  | .005  | 2.0  |
| 14   | 38.84     | 2.319  | .005  | 3.0  |

SAMPLE I/D : 71102

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 12.20     | 7.255  | .047  | 20.5 |
| 2    | 18.76     | 4.730  | .020  | 3.5  |
| 3    | 20.08     | 4.422  | .017  | 9.0  |
| 4    | 24.76     | 3.596  | .011  | 2.0  |
| 5    | 27.56     | 3.236  | .009  | 11.0 |
| 6    | 32.04     | 2.793  | .007  | 4.5  |
| 7    | 34.36     | 2.610  | .006  | 4.5  |
| 8    | 40.84     | 2.210  | .004  | 2.5  |
| 9    | 42.86     | 2.113  | .004  | 2.0  |
| 10   | 45.80     | 1.981  | .003  | 1.0  |

|    |       |       |      |     |
|----|-------|-------|------|-----|
| 15 | 40.80 | 2.212 | .004 | 2.0 |
| 16 | 41.68 | 2.167 | .004 | 1.5 |
| 17 | 42.80 | 2.113 | .004 | 1.5 |
| 18 | 45.88 | 1.978 | .003 | 1.0 |

Table 16. Diffraction Data for Station 105 Fine Fraction Samples

SAMPLE I/D : 53652

|    | LINE 2-TH(DEC) | D(ANG) | ERR-D | INT  |
|----|----------------|--------|-------|------|
| 1  | 12.05          | 7.346  | .044  | 6.0  |
| 2  | 16.71          | 5.305  | .023  | 8.0  |
| 3  | 17.00          | 5.214  | .022  | 17.0 |
| 4  | 18.75          | 4.732  | .018  | 2.0  |
| 5  | 20.21          | 4.393  | .016  | 40.0 |
| 6  | 20.58          | 4.316  | .015  | 62.0 |
| 7  | 22.91          | 3.882  | .012  | 24.0 |
| 8  | 28.45          | 3.137  | .008  | 12.0 |
| 9  | 28.60          | 3.122  | .008  | 11.0 |
| 10 | 29.25          | 3.053  | .007  | 24.0 |
| 11 | 29.83          | 2.995  | .007  | 15.0 |
| 12 | 32.02          | 2.795  | .006  | 2.0  |
| 13 | 33.12          | 2.705  | .006  | 3.0  |
| 14 | 33.70          | 2.660  | .006  | 6.0  |
| 15 | 34.35          | 2.610  | .005  | 3.0  |
| 16 | 35.52          | 2.527  | .005  | 5.0  |
| 17 | 38.80          | 2.321  | .004  | 7.0  |
| 18 | 41.06          | 2.198  | .004  | 3.0  |
| 19 | 41.57          | 2.172  | .004  | 4.0  |

SAMPLE I/D : 67105

|    | LINE 2-TH(DEC) | D(ANG) | ERR-D | INT  |
|----|----------------|--------|-------|------|
| 1  | 16.96          | 5.228  | .018  | 9.0  |
| 2  | 20.23          | 4.390  | .012  | 31.0 |
| 3  | 20.57          | 4.317  | .012  | 44.0 |
| 4  | 22.87          | 3.889  | .010  | 18.0 |
| 5  | 28.49          | 3.133  | .006  | 10.0 |
| 6  | 28.60          | 3.121  | .006  | 7.0  |
| 7  | 29.29          | 3.049  | .006  | 15.0 |
| 8  | 29.75          | 3.003  | .006  | 8.0  |
| 9  | 33.70          | 2.659  | .004  | 3.0  |
| 10 | 34.34          | 2.612  | .004  | 2.0  |
| 11 | 35.60          | 2.522  | .004  | 5.0  |
| 12 | 38.75          | 2.324  | .003  | 4.0  |
| 13 | 41.05          | 2.199  | .003  | 3.0  |
| 14 | 41.56          | 2.173  | .003  | 4.0  |

SAMPLE I/D : 69762

|    | LINE 2-TH(DEC) | D(ANG) | ERR-D | INT  |
|----|----------------|--------|-------|------|
| 1  | 12.08          | 7.328  | .035  | 42.0 |
| 2  | 16.50          | 4.796  | .015  | 4.5  |
| 3  | 18.62          | 4.766  | .015  | 5.5  |
| 4  | 19.99          | 4.441  | .013  | 27.0 |
| 5  | 20.39          | 4.355  | .012  | 13.0 |
| 6  | 21.20          | 4.191  | .011  | 2.0  |
| 7  | 22.75          | 3.909  | .010  | 3.0  |
| 8  | 27.45          | 3.249  | .007  | 18.5 |
| 9  | 28.37          | 3.146  | .006  | 3.5  |
| 10 | 29.23          | 3.056  | .006  | 4.5  |
| 11 | 29.68          | 3.009  | .006  | 2.0  |
| 12 | 30.26          | 2.954  | .005  | 2.0  |
| 13 | 30.77          | 2.905  | .005  | 1.5  |
| 14 | 31.86          | 2.888  | .005  | 9.5  |
| 15 | 33.13          | 2.764  | .005  | 3.0  |
| 16 | 34.22          | 2.621  | .004  | 11.0 |
| 17 | 35.48          | 2.530  | .004  | 1.5  |
| 18 | 37.08          | 2.424  | .004  | 2.0  |
| 19 | 38.00          | 2.368  | .003  | 1.5  |
| 20 | 38.57          | 2.334  | .003  | 2.0  |
| 21 | 40.64          | 2.220  | .003  | 5.5  |
| 22 | 41.44          | 2.179  | .003  | 2.0  |
| 23 | 42.59          | 2.123  | .003  | 3.0  |
| 24 | 45.57          | 1.991  | .002  | 3.0  |
| 25 | 49.58          | 1.838  | .002  | 1.5  |
| 26 | 50.16          | 1.819  | .002  | 2.5  |

SAMPLE I/D : 58832

|    | LINE 2-TH(DEC) | D(ANG) | ERR-D | INT  |
|----|----------------|--------|-------|------|
| 1  | 12.10          | 7.312  | .035  | 12.5 |
| 2  | 16.98          | 5.222  | .018  | 3.0  |
| 3  | 18.76          | 4.731  | .014  | 2.5  |
| 4  | 20.25          | 4.386  | .012  | 9.5  |
| 5  | 20.53          | 4.325  | .012  | 15.5 |
| 6  | 21.28          | 4.175  | .011  | 5.0  |
| 7  | 22.89          | 3.886  | .010  | 5.0  |
| 8  | 27.59          | 3.233  | .007  | 4.0  |
| 9  | 28.45          | 3.137  | .006  | 3.5  |
| 10 | 29.31          | 3.047  | .006  | 5.0  |
| 11 | 29.83          | 2.996  | .006  | 2.5  |
| 12 | 31.89          | 2.806  | .005  | 2.5  |
| 13 | 33.72          | 2.658  | .004  | 1.5  |
| 14 | 34.36          | 2.610  | .004  | 2.0  |
| 15 | 40.66          | 2.219  | .003  | 1.5  |
| 16 | 40.89          | 2.207  | .003  | 1.5  |
| 17 | 41.58          | 2.172  | .003  | 2.0  |

Table 1c. Diffraction Data for Station 118 Fine Fraction Samples

SAMPLE I/D : 58309

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 12.20     | 7.255  | .034  | 9.0  |
| 2    | 16.67     | 5.317  | .018  | 3.0  |
| 3    | 16.96     | 5.228  | .018  | 6.0  |
| 4    | 20.23     | 4.390  | .012  | 14.0 |
| 5    | 20.51     | 4.329  | .012  | 19.0 |
| 6    | 22.87     | 3.889  | .010  | 5.0  |
| 7    | 27.57     | 3.235  | .007  | 5.0  |
| 8    | 28.43     | 3.139  | .006  | 4.0  |
| 9    | 29.29     | 3.049  | .006  | 8.0  |
| 10   | 29.81     | 2.998  | .006  | 5.0  |
| 11   | 31.93     | 2.803  | .005  | 3.0  |
| 12   | 33.65     | 2.664  | .004  | 2.0  |
| 13   | 34.34     | 2.612  | .004  | 3.0  |
| 14   | 35.60     | 2.522  | .004  | 2.0  |
| 15   | 36.69     | 2.327  | .003  | 2.0  |
| 16   | 40.87     | 2.208  | .003  | 2.0  |

SAMPLE I/D : 66930

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 11.63     | 7.689  | .052  | 6.5  |
| 2    | 16.15     | 5.488  | .027  | 6.5  |
| 3    | 17.87     | 4.963  | .022  | 48.0 |
| 4    | 19.11     | 4.644  | .019  | 14.5 |
| 5    | 20.23     | 4.389  | .017  | 2.0  |
| 6    | 20.71     | 4.289  | .016  | 8.0  |
| 7    | 23.35     | 3.810  | .013  | 12.5 |
| 8    | 23.55     | 3.778  | .013  | 16.0 |
| 9    | 25.05     | 3.555  | .011  | 3.0  |
| 10   | 26.27     | 3.392  | .010  | 29.5 |
| 11   | 26.63     | 3.347  | .010  | 16.5 |
| 12   | 29.15     | 3.063  | .008  | 3.0  |
| 13   | 30.51     | 2.930  | .008  | 16.0 |
| 14   | 32.91     | 2.722  | .006  | 2.0  |
| 15   | 33.35     | 2.687  | .006  | 2.0  |
| 16   | 35.67     | 2.517  | .005  | 3.5  |
| 17   | 36.39     | 2.469  | .005  | 3.0  |
| 18   | 40.47     | 2.229  | .004  | 3.0  |
| 19   | 40.87     | 2.208  | .004  | 3.0  |

SAMPLE I/D : 65720

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 12.07     | 7.333  | .035  | 5.0  |
| 2    | 16.71     | 5.304  | .018  | 3.0  |
| 3    | 16.94     | 5.233  | .018  | 2.0  |
| 4    | 20.27     | 4.381  | .012  | 8.0  |
| 5    | 20.50     | 4.332  | .012  | 12.0 |
| 6    | 22.91     | 3.882  | .010  | 3.0  |
| 7    | 26.64     | 3.347  | .007  | 2.0  |
| 8    | 27.50     | 3.244  | .007  | 4.0  |
| 9    | 28.41     | 3.141  | .006  | 4.0  |
| 10   | 29.27     | 3.051  | .006  | 5.0  |
| 11   | 29.79     | 2.999  | .006  | 5.0  |
| 12   | 31.91     | 2.804  | .005  | 2.0  |
| 13   | 33.17     | 2.700  | .005  | 2.0  |
| 14   | 33.69     | 2.660  | .004  | 2.0  |
| 15   | 34.32     | 2.613  | .004  | 3.0  |
| 16   | 35.64     | 2.519  | .004  | 2.0  |
| 17   | 38.79     | 2.321  | .003  | 2.0  |
| 18   | 41.60     | 2.171  | .003  | 2.0  |
| 19   | 43.67     | 2.073  | .003  | 2.0  |
| 20   | 44.47     | 2.037  | .002  | 2.0  |

SAMPLE I/D : 66933

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 12.08     | 7.327  | .035  | 5.0  |
| 2    | 16.67     | 5.319  | .018  | 12.0 |
| 3    | 17.01     | 5.212  | .017  | 17.0 |
| 4    | 17.93     | 4.947  | .016  | 11.0 |
| 5    | 19.08     | 4.652  | .014  | 2.0  |
| 6    | 20.28     | 4.379  | .012  | 47.0 |
| 7    | 20.51     | 4.330  | .012  | 58.0 |
| 8    | 20.97     | 4.237  | .011  | 10.0 |
| 9    | 22.92     | 3.886  | .010  | 15.0 |
| 10   | 23.61     | 3.769  | .009  | 7.0  |
| 11   | 26.47     | 3.367  | .007  | 50.0 |
| 12   | 28.48     | 3.134  | .006  | 12.0 |
| 13   | 28.65     | 3.115  | .006  | 5.0  |
| 14   | 29.34     | 3.044  | .006  | 21.0 |
| 15   | 29.86     | 2.992  | .006  | 11.0 |
| 16   | 30.55     | 2.927  | .005  | 4.0  |
| 17   | 32.15     | 2.784  | .005  | 3.0  |
| 18   | 32.95     | 2.718  | .005  | 3.0  |
| 19   | 33.70     | 2.659  | .004  | 9.0  |
| 20   | 34.39     | 2.608  | .004  | 3.0  |
| 21   | 35.65     | 2.518  | .004  | 6.0  |
| 22   | 37.77     | 2.382  | .003  | 3.0  |
| 23   | 38.80     | 2.321  | .003  | 6.0  |
| 24   | 41.04     | 2.199  | .003  | 3.0  |
| 25   | 41.61     | 2.170  | .003  | 5.0  |
| 26   | 42.53     | 2.125  | .003  | 5.0  |

Table 1c-cont. Diffraction Data for Station 118 Fine Fraction Samples

SAMPLE I/D : 69707

|    | LINE 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|----|----------------|--------|-------|------|
| 1  | 11.89          | 7.445  | .045  | 4.0  |
| 2  | 16.19          | 5.475  | .024  | 7.0  |
| 3  | 17.94          | 4.945  | .020  | 54.0 |
| 4  | 18.59          | 4.772  | .019  | 2.5  |
| 5  | 19.10          | 4.646  | .018  | 17.5 |
| 6  | 23.33          | 3.812  | .012  | 9.5  |
| 7  | 23.62          | 3.766  | .011  | 31.0 |
| 8  | 26.32          | 3.386  | .009  | 50.0 |
| 9  | 26.61          | 3.349  | .009  | 16.0 |
| 10 | 30.48          | 2.933  | .007  | 23.0 |
| 11 | 32.96          | 2.718  | .006  | 5.0  |
| 12 | 35.58          | 2.523  | .005  | 5.0  |
| 13 | 36.24          | 2.479  | .005  | 5.0  |
| 14 | 40.39          | 2.233  | .004  | 4.5  |
| 15 | 40.90          | 2.206  | .004  | 5.0  |

SAMPLE I/D : 70472

|    | LINE 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|----|----------------|--------|-------|------|
| 1  | 12.15          | 7.284  | .048  | 3.0  |
| 2  | 16.87          | 5.255  | .025  | 4.5  |
| 3  | 20.19          | 4.398  | .017  | 13.0 |
| 4  | 20.51          | 4.330  | .017  | 19.5 |
| 5  | 22.79          | 3.902  | .014  | 7.0  |
| 6  | 28.43          | 3.139  | .009  | 3.0  |
| 7  | 29.27          | 3.051  | .008  | 6.0  |
| 8  | 29.79          | 2.999  | .008  | 3.0  |
| 9  | 33.15          | 2.702  | .006  | 1.5  |
| 10 | 33.71          | 2.659  | .006  | 2.0  |
| 11 | 34.35          | 2.611  | .006  | 1.5  |
| 12 | 35.55          | 2.525  | .005  | 2.0  |
| 13 | 38.79          | 2.321  | .005  | 2.0  |

Table 1d. Diffraction Data for Station 124 Fine Fraction Samples

SAMPLE I/D : 58022

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 12.14     | 7.289  | .048  | 3.0  |
| 2    | 16.67     | 5.317  | .025  | 6.0  |
| 3    | 16.96     | 5.228  | .024  | 11.0 |
| 4    | 20.28     | 4.378  | .017  | 25.0 |
| 5    | 20.52     | 4.329  | .017  | 38.0 |
| 6    | 22.75     | 3.908  | .014  | 12.0 |
| 7    | 28.49     | 3.133  | .009  | 8.0  |
| 8    | 28.60     | 3.121  | .009  | 6.0  |
| 9    | 29.29     | 3.049  | .008  | 14.0 |
| 10   | 29.80     | 2.998  | .008  | 10.0 |
| 11   | 33.71     | 2.659  | .006  | 4.0  |
| 12   | 35.60     | 2.522  | .005  | 2.0  |
| 13   | 38.75     | 2.324  | .005  | 4.0  |
| 14   | 41.56     | 2.173  | .004  | 3.0  |

SAMPLE I/D : 67353

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 12.10     | 7.315  | .048  | 4.0  |
| 2    | 17.89     | 4.958  | .022  | 16.0 |
| 3    | 19.09     | 4.648  | .019  | 6.0  |
| 4    | 23.62     | 3.766  | .013  | 11.0 |
| 5    | 26.32     | 3.386  | .010  | 14.0 |
| 6    | 26.61     | 3.350  | .010  | 7.0  |
| 7    | 30.51     | 2.930  | .008  | 6.0  |
| 8    | 35.61     | 2.521  | .005  | 2.0  |
| 9    | 36.30     | 2.475  | .005  | 2.0  |
| 10   | 40.32     | 2.237  | .004  | 2.0  |
| 11   | 40.77     | 2.213  | .004  | 2.0  |

SAMPLE I/D : 58604

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 12.31     | 7.188  | .033  | 8.0  |
| 2    | 20.23     | 4.390  | .012  | 5.0  |
| 3    | 20.92     | 4.247  | .012  | 7.0  |
| 4    | 22.98     | 3.870  | .010  | 2.0  |
| 5    | 23.44     | 3.795  | .009  | 4.0  |
| 6    | 26.77     | 3.331  | .007  | 6.0  |
| 7    | 27.68     | 3.222  | .007  | 10.0 |
| 8    | 29.75     | 3.003  | .006  | 6.0  |
| 9    | 32.16     | 2.784  | .005  | 4.0  |
| 10   | 33.19     | 2.699  | .005  | 4.0  |
| 11   | 34.22     | 2.620  | .004  | 3.0  |
| 12   | 37.09     | 2.424  | .004  | 2.0  |
| 13   | 43.74     | 2.069  | .003  | 5.0  |
| 14   | 44.54     | 2.034  | .002  | 4.0  |
| 15   | 45.81     | 1.981  | .002  | 2.0  |

SAMPLE I/D : 67355

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 12.02     | 7.362  | .044  | 2.0  |
| 2    | 17.92     | 4.949  | .020  | 15.0 |
| 3    | 19.16     | 4.632  | .017  | 5.0  |
| 4    | 23.53     | 3.781  | .012  | 18.0 |
| 5    | 26.23     | 3.398  | .009  | 15.0 |
| 6    | 26.59     | 3.352  | .009  | 9.0  |
| 7    | 30.38     | 2.942  | .007  | 7.0  |
| 8    | 32.86     | 2.726  | .006  | 2.0  |
| 9    | 35.62     | 2.520  | .005  | 2.0  |
| 10   | 40.72     | 2.216  | .004  | 2.0  |

SAMPLE I/D : 69276

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 16.16     | 5.486  | .019  | 7.0  |
| 2    | 17.82     | 4.976  | .016  | 42.0 |
| 3    | 19.09     | 4.649  | .014  | 15.0 |
| 4    | 20.47     | 4.338  | .012  | 6.0  |
| 5    | 23.58     | 3.773  | .009  | 33.0 |
| 6    | 26.28     | 3.391  | .007  | 36.0 |
| 7    | 26.57     | 3.354  | .007  | 16.0 |
| 8    | 30.49     | 2.932  | .005  | 26.0 |
| 9    | 32.90     | 2.722  | .005  | 3.0  |
| 10   | 35.66     | 2.517  | .004  | 5.0  |
| 11   | 36.30     | 2.475  | .004  | 3.0  |
| 12   | 38.77     | 2.322  | .003  | 2.0  |
| 13   | 40.38     | 2.233  | .003  | 2.0  |
| 14   | 40.90     | 2.206  | .003  | 3.0  |
| 15   | 43.43     | 2.083  | .003  | 1.0  |
| 16   | 48.15     | 1.890  | .002  | 2.0  |

SAMPLE I/D : 62226

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT |
|------|-----------|--------|-------|-----|
| 1    | 12.21     | 7.251  | .034  | 5.0 |
| 2    | 26.66     | 3.344  | .007  | 3.0 |
| 3    | 27.69     | 3.221  | .007  | 5.0 |
| 4    | 29.76     | 3.002  | .006  | 3.0 |
| 5    | 32.28     | 2.773  | .005  | 2.0 |
| 6    | 33.31     | 2.690  | .004  | 2.0 |
| 7    | 43.75     | 2.069  | .003  | 2.0 |

Table 2a. Diffraction Data for Station 103 Coarse Fraction Samples

SAMPLE I/D : 17268

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 11.62     | 7.615  | .052  | 3.0  |
| 2    | 18.90     | 4.695  | .020  | 4.0  |
| 3    | 20.62     | 4.307  | .017  | 3.0  |
| 4    | 22.90     | 3.883  | .013  | 2.0  |
| 5    | 23.66     | 3.760  | .013  | 5.0  |
| 6    | 26.46     | 3.368  | .010  | 6.0  |
| 7    | 26.66     | 3.344  | .010  | 13.0 |
| 8    | 27.38     | 3.257  | .009  | 2.0  |
| 9    | 28.06     | 3.180  | .009  | 4.0  |
| 10   | 29.14     | 3.064  | .008  | 4.0  |
| 11   | 29.42     | 3.036  | .008  | 14.0 |
| 12   | 30.90     | 2.894  | .007  | 2.0  |
| 13   | 31.62     | 2.830  | .007  | 2.0  |
| 14   | 39.42     | 2.286  | .004  | 2.0  |
| 15   | 47.54     | 1.913  | .003  | 2.0  |
| 16   | 48.58     | 1.874  | .003  | 2.0  |

SAMPLE I/D : 20518

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 20.72     | 4.287  | .016  | 3.0  |
| 2    | 26.66     | 3.343  | .010  | 28.0 |
| 3    | 29.43     | 3.035  | .008  | 20.0 |
| 4    | 30.81     | 2.962  | .007  | 5.0  |
| 5    | 35.89     | 2.562  | .005  | 2.0  |
| 6    | 36.42     | 2.467  | .005  | 1.0  |
| 7    | 37.54     | 2.396  | .005  | 1.0  |
| 8    | 39.34     | 2.290  | .004  | 5.0  |
| 9    | 43.22     | 2.093  | .004  | 4.0  |
| 10   | 47.63     | 1.909  | .003  | 2.0  |

SAMPLE I/D : 20533

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 16.44     | 5.393  | .028  | 3.0  |
| 2    | 20.31     | 4.373  | .018  | 9.0  |
| 3    | 20.48     | 4.336  | .018  | 14.0 |
| 4    | 22.72     | 3.914  | .015  | 6.0  |
| 5    | 23.67     | 3.760  | .013  | 4.0  |
| 6    | 25.35     | 3.513  | .012  | 3.0  |
| 7    | 26.50     | 3.363  | .011  | 9.5  |

SAMPLE I/D : 17765

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 16.83     | 5.268  | .025  | 8.0  |
| 2    | 18.23     | 4.866  | .021  | 3.0  |
| 3    | 19.39     | 4.578  | .019  | 4.0  |
| 4    | 20.91     | 4.248  | .016  | 5.0  |
| 5    | 23.71     | 3.753  | .012  | 17.0 |
| 6    | 25.47     | 3.497  | .011  | 6.0  |
| 7    | 26.63     | 3.347  | .010  | 10.0 |
| 8    | 29.43     | 3.035  | .008  | 13.0 |
| 9    | 31.35     | 2.853  | .007  | 2.0  |
| 10   | 37.99     | 2.368  | .005  | 1.5  |
| 11   | 39.35     | 2.290  | .004  | 2.0  |
| 12   | 43.23     | 2.093  | .004  | 2.0  |
| 13   | 45.35     | 2.000  | .003  | 3.0  |

SAMPLE I/D : 21102

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 20.64     | 4.303  | .016  | 3.0  |
| 2    | 21.74     | 4.087  | .015  | 1.0  |
| 3    | 23.02     | 3.863  | .013  | 3.0  |
| 4    | 14.52     | 6.100  | .036  | 1.0  |
| 5    | 26.67     | 3.342  | .010  | 12.0 |
| 6    | 29.40     | 3.038  | .008  | 19.0 |
| 7    | 30.92     | 2.892  | .007  | 2.0  |
| 8    | 32.88     | 2.724  | .006  | 2.0  |
| 9    | 35.57     | 2.524  | .005  | 1.0  |
| 10   | 39.36     | 2.289  | .004  | 3.0  |
| 11   | 43.22     | 2.093  | .004  | 3.0  |
| 12   | 47.53     | 1.913  | .003  | 2.0  |
| 13   | 48.58     | 1.874  | .003  | 2.0  |

SAMPLE I/D : 19476

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 26.66     | 3.344  | .010  | 16.5 |
| 2    | 29.42     | 3.036  | .008  | 6.0  |
| 3    | 31.18     | 2.868  | .007  | 1.5  |

Table 2b. Diffraction Data for Station 105 Coarse Fraction Samples

SAMPLE I/D : 3652

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 11.60     | 7.628  | .052  | 4.0  |
| 2    | 20.84     | 4.262  | .016  | 5.0  |
| 3    | 26.64     | 3.346  | .010  | 17.0 |
| 4    | 29.44     | 3.034  | .008  | 10.0 |
| 5    | 30.88     | 2.896  | .007  | 2.5  |
| 6    | 36.56     | 2.458  | .005  | 2.5  |
| 7    | 39.44     | 2.285  | .004  | 2.5  |

SAMPLE I/D : 20118

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 14.58     | 6.074  | .024  | 11.0 |
| 2    | 26.68     | 3.341  | .007  | 13.0 |
| 3    | 29.49     | 3.028  | .006  | 8.5  |
| 4    | 31.79     | 2.815  | .005  | 23.0 |
| 5    | 34.43     | 2.605  | .004  | 13.0 |
| 6    | 36.26     | 2.477  | .004  | 26.0 |
| 7    | 39.47     | 2.283  | .003  | 2.5  |
| 8    | 47.39     | 1.918  | .002  | 7.0  |

SAMPLE I/D : 12934

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 26.76     | 3.331  | .007  | 8.5  |
| 2    | 29.46     | 3.032  | .006  | 10.5 |
| 3    | 31.81     | 2.884  | .005  | 3.5  |
| 4    | 31.81     | 2.813  | .005  | 12.0 |
| 5    | 36.00     | 2.495  | .004  | 1.5  |
| 6    | 39.44     | 2.285  | .003  | 2.0  |
| 7    | 43.17     | 2.096  | .003  | 1.5  |
| 8    | 45.40     | 1.998  | .002  | 3.0  |
| 9    | 47.47     | 1.915  | .002  | 1.5  |
| 10   | 48.50     | 1.877  | .002  | 1.5  |

SAMPLE I/D : 21018

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 26.89     | 4.252  | .012  | 5.5  |
| 2    | 23.07     | 3.855  | .009  | 2.5  |
| 3    | 26.68     | 3.341  | .007  | 19.0 |
| 4    | 27.43     | 3.252  | .007  | 1.5  |
| 5    | 29.49     | 3.028  | .006  | 27.5 |
| 6    | 30.93     | 2.891  | .005  | 6.0  |
| 7    | 35.34     | 2.540  | .004  | 1.5  |
| 8    | 36.03     | 2.493  | .004  | 2.5  |
| 9    | 39.47     | 2.283  | .003  | 5.5  |
| 10   | 40.96     | 2.203  | .003  | 1.5  |
| 11   | 43.14     | 2.097  | .003  | 3.5  |
| 12   | 47.04     | 1.932  | .002  | 1.5  |
| 13   | 47.39     | 1.918  | .002  | 2.5  |
| 14   | 48.42     | 1.880  | .002  | 3.0  |
| 15   | 50.02     | 1.823  | .002  | 1.5  |

SAMPLE I/D : 15927

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 26.66     | 3.343  | .007  | 16.0 |
| 2    | 29.41     | 3.037  | .006  | 8.0  |
| 3    | 30.79     | 2.904  | .005  | 3.0  |
| 4    | 35.38     | 2.537  | .004  | 2.0  |
| 5    | 39.39     | 2.287  | .003  | 2.0  |
| 6    | 43.06     | 2.100  | .003  | 1.5  |
| 7    | 49.94     | 1.826  | .002  | 2.5  |

SAMPLE I/D : 19776

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT |
|------|-----------|--------|-------|-----|
| 1    | 26.64     | 3.346  | .007  | 7.0 |
| 2    | 29.16     | 3.062  | .006  | 2.0 |
| 3    | 29.45     | 3.033  | .006  | 6.0 |
| 4    | 30.82     | 2.901  | .005  | 2.5 |
| 5    | 32.55     | 2.751  | .005  | 4.0 |
| 6    | 35.36     | 2.543  | .004  | 2.0 |

Table 2c. Diffraction Data for Station 118 Coarse Fraction Samples

SAMPLE I/D : 8961

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 21.82     | 4.072  | .011  | 2.0  |
| 2    | 26.70     | 3.339  | .007  | 12.5 |
| 3    | 29.45     | 3.033  | .006  | 8.5  |
| 4    | 30.83     | 2.900  | .005  | 2.5  |
| 5    | 39.37     | 2.288  | .003  | 2.0  |
| 6    | 43.16     | 2.096  | .003  | 1.0  |

SAMPLE I/D : 20480

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 20.81     | 4.268  | .016  | 5.0  |
| 2    | 26.65     | 3.345  | .010  | 16.0 |
| 3    | 29.45     | 3.033  | .008  | 34.0 |
| 4    | 30.81     | 2.902  | .007  | 7.0  |
| 5    | 39.45     | 2.284  | .004  | 3.0  |
| 6    | 43.17     | 2.096  | .004  | 2.0  |
| 7    | 47.57     | 1.911  | .003  | 1.5  |
| 8    | 48.53     | 1.876  | .003  | 1.5  |

SAMPLE I/D : 19707

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 20.91     | 4.248  | .015  | 5.0  |
| 2    | 23.17     | 3.838  | .012  | 5.0  |
| 3    | 26.67     | 3.343  | .009  | 33.0 |
| 4    | 29.51     | 3.027  | .007  | 43.0 |
| 5    | 30.82     | 2.901  | .007  | 9.0  |
| 6    | 35.99     | 2.495  | .005  | 5.0  |
| 7    | 39.42     | 2.286  | .004  | 6.0  |
| 8    | 41.02     | 2.200  | .004  | 3.0  |
| 9    | 43.13     | 2.097  | .003  | 4.0  |
| 10   | 47.50     | 1.914  | .003  | 3.0  |
| 11   | 48.45     | 1.879  | .003  | 4.0  |
| 12   | 50.05     | 1.822  | .002  | 3.0  |

SAMPLE I/D : 21352

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 20.94     | 4.243  | .011  | 6.0  |
| 2    | 23.06     | 3.857  | .009  | 2.0  |
| 3    | 23.75     | 3.746  | .009  | 2.0  |
| 4    | 26.73     | 3.335  | .007  | 22.0 |
| 5    | 29.48     | 3.030  | .006  | 5.0  |
| 6    | 30.86     | 2.897  | .005  | 1.0  |
| 7    | 34.87     | 2.573  | .004  | 1.0  |
| 8    | 36.48     | 2.463  | .004  | 1.0  |
| 9    | 39.35     | 2.290  | .003  | 2.5  |
| 10   | 49.96     | 1.826  | .002  | 2.0  |

SAMPLE I/D : 20472

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 20.86     | 4.258  | .016  | 6.0  |
| 2    | 26.66     | 3.344  | .010  | 30.0 |
| 3    | 29.42     | 3.036  | .008  | 18.0 |
| 4    | 30.94     | 2.890  | .007  | 6.0  |
| 5    | 31.62     | 2.830  | .007  | 2.0  |
| 6    | 32.54     | 2.752  | .007  | 4.0  |
| 7    | 39.42     | 2.286  | .004  | 3.0  |
| 8    | 43.22     | 2.093  | .004  | 2.0  |
| 9    | 47.10     | 1.929  | .003  | 2.0  |
| 10   | 47.54     | 1.913  | .003  | 2.0  |
| 11   | 48.54     | 1.875  | .003  | 2.0  |

SAMPLE I/D : 23518

| LINE | 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|------|-----------|--------|-------|------|
| 1    | 26.61     | 3.350  | .009  | 5.0  |
| 2    | 29.47     | 3.030  | .007  | 4.0  |
| 3    | 31.75     | 2.818  | .006  | 20.0 |
| 4    | 45.36     | 1.999  | .003  | 4.0  |

Table 2d. Diffraction Data for Station 124 Coarse Fraction Samples

SAMPLE I/D : 7717

| LINE 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|----------------|--------|-------|------|
| 1              | 26.98  | 3.305 | .007 |

SAMPLE I/D : 8612

| LINE 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|----------------|--------|-------|------|
| 1              | 26.66  | 3.344 | .007 |
| 2              | 29.47  | 3.031 | .006 |
| 3              | 39.45  | 2.284 | .003 |

SAMPLE I/D : 14780

| LINE 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|----------------|--------|-------|------|
| 1              | 20.84  | 4.262 | .012 |
| 2              | 26.69  | 3.339 | .007 |
| 3              | 29.39  | 3.039 | .006 |
| 4              | 30.82  | 2.901 | .005 |
| 5              | 39.48  | 2.282 | .003 |
| 6              | 49.98  | 1.825 | .002 |

SAMPLE I/D : 16029

| LINE 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|----------------|--------|-------|------|
| 1              | 20.93  | 4.244 | .011 |
| 2              | 26.67  | 3.343 | .007 |
| 3              | 29.48  | 3.030 | .006 |
| 4              | 36.59  | 2.456 | .004 |
| 5              | 39.40  | 2.287 | .003 |
| 6              | 42.38  | 2.139 | .003 |
| 7              | 43.19  | 2.095 | .003 |
| 8              | 47.43  | 1.917 | .002 |
| 9              | 48.40  | 1.880 | .002 |
| 10             | 50.01  | 1.824 | .002 |

SAMPLE I/D : 16674

| LINE 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|----------------|--------|-------|------|
| 1              | 21.18  | 4.194 | .016 |
| 2              | 26.92  | 3.312 | .010 |
| 3              | 29.73  | 3.005 | .008 |
| 4              | 36.84  | 2.440 | .005 |
| 5              | 39.65  | 2.273 | .004 |
| 6              | 42.63  | 2.121 | .004 |
| 7              | 43.44  | 2.083 | .004 |
| 8              | 47.69  | 1.907 | .003 |
| 9              | 48.66  | 1.871 | .003 |
| 10             | 50.27  | 1.815 | .003 |

SAMPLE I/D : 19276

| LINE 2-TH(DEG) | D(ANG) | ERR-D | INT  |
|----------------|--------|-------|------|
| 1              | 26.60  | 3.351 | .007 |
| 2              | 27.00  | 3.302 | .007 |

FIGURE CAPTIONS

Figure 1. Diffraction patterns in bar graph form for the fine particle samples.

(a) Station 103 (b) Station 105 (c) Station 118 (d) Station 124.

Figure 1. Diffraction patterns in bar graph form for the coarse particle samples.

(a) Station 103 (b) Station 105 (c) Station 118 (d) Station 124.

## Station 103 (Fine Fraction)

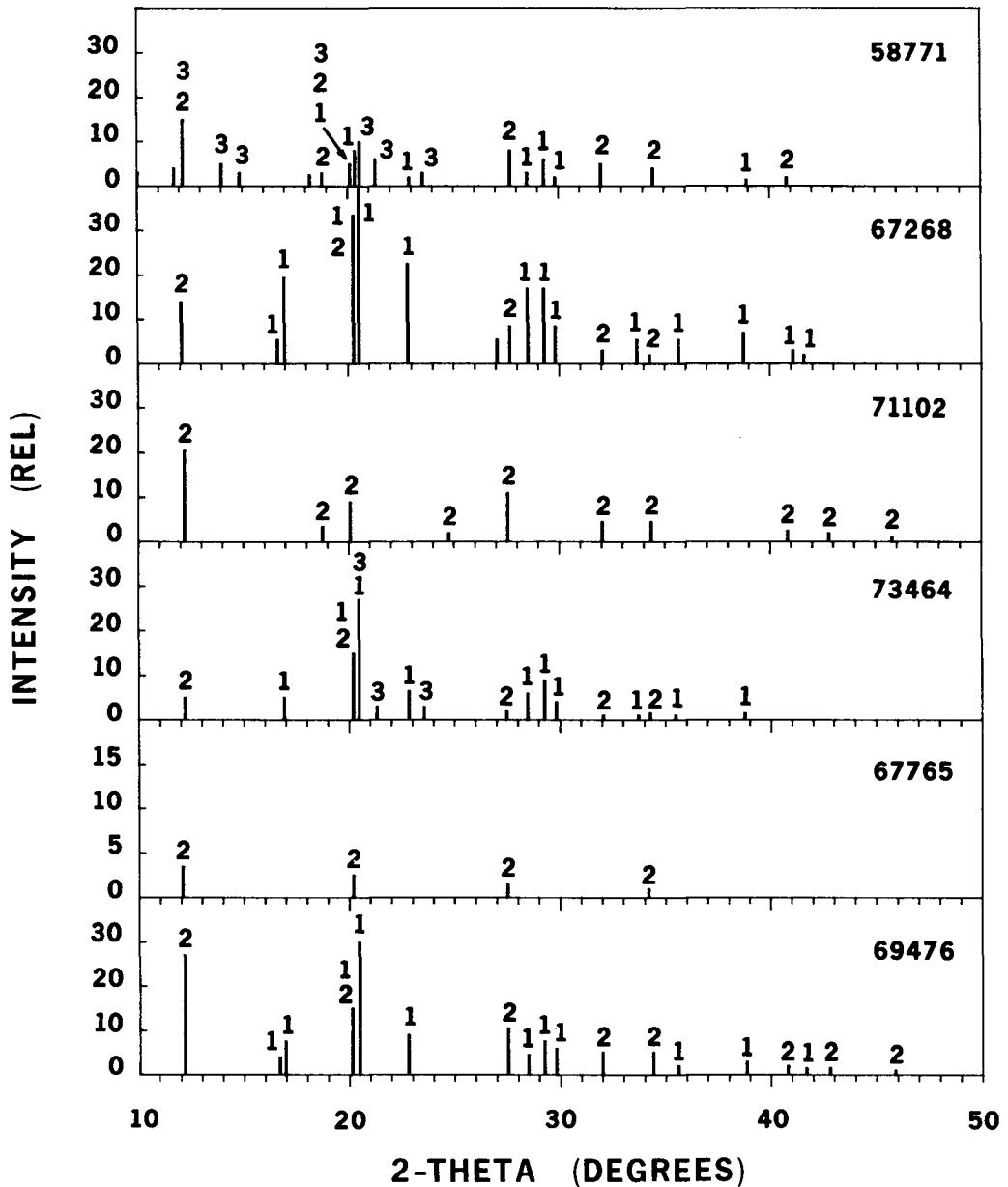
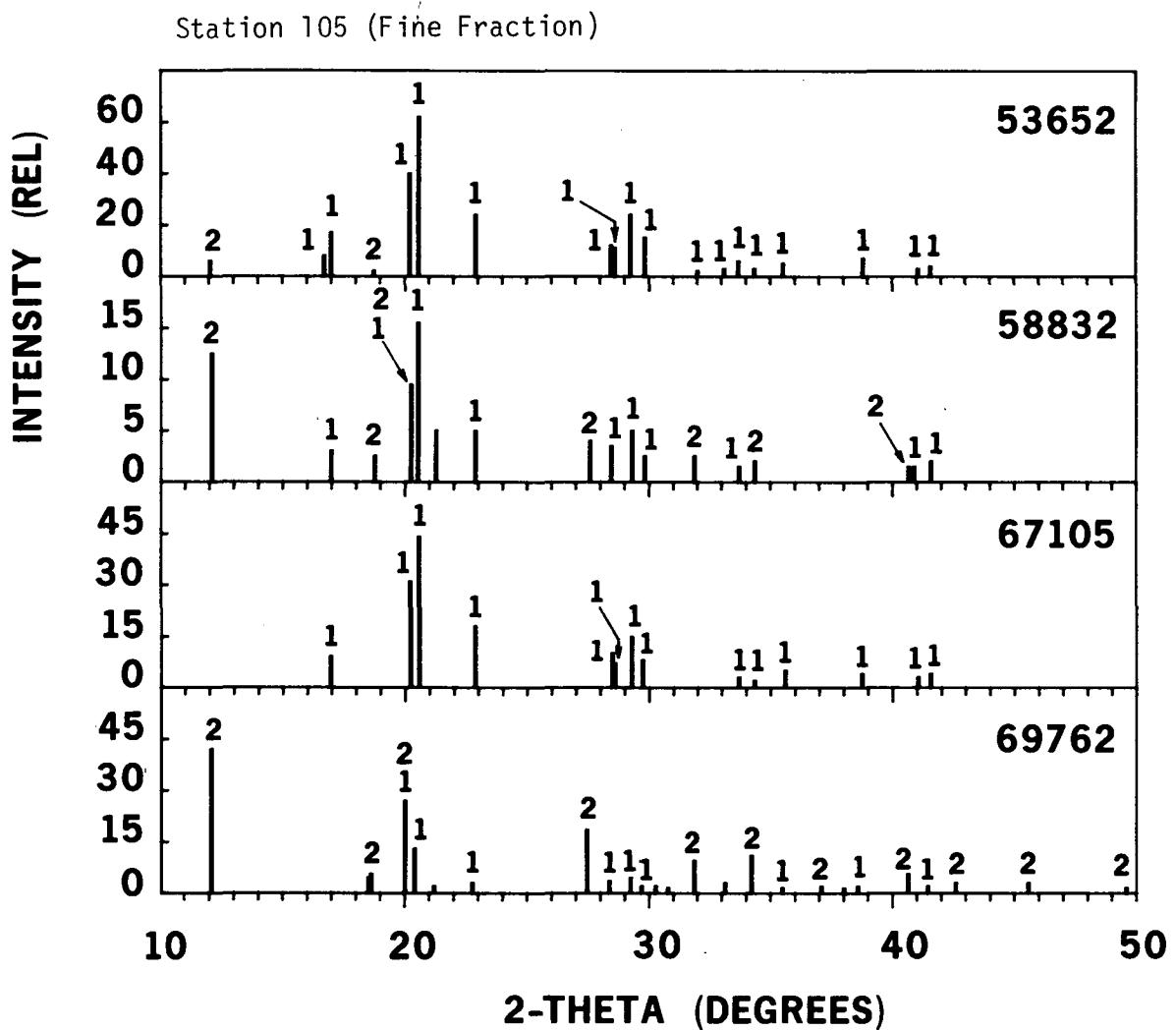
 $1 = (\text{NH}_4)_2\text{SO}_4$  $2 = (\text{NH}_4)_2\text{SO}_4 \cdot \text{PbSO}_4$  $3 = (\text{NH}_4)_2\text{SO}_4 \cdot \text{ZnSO}_4 \cdot 6\text{H}_2\text{O}$

Fig. 1b



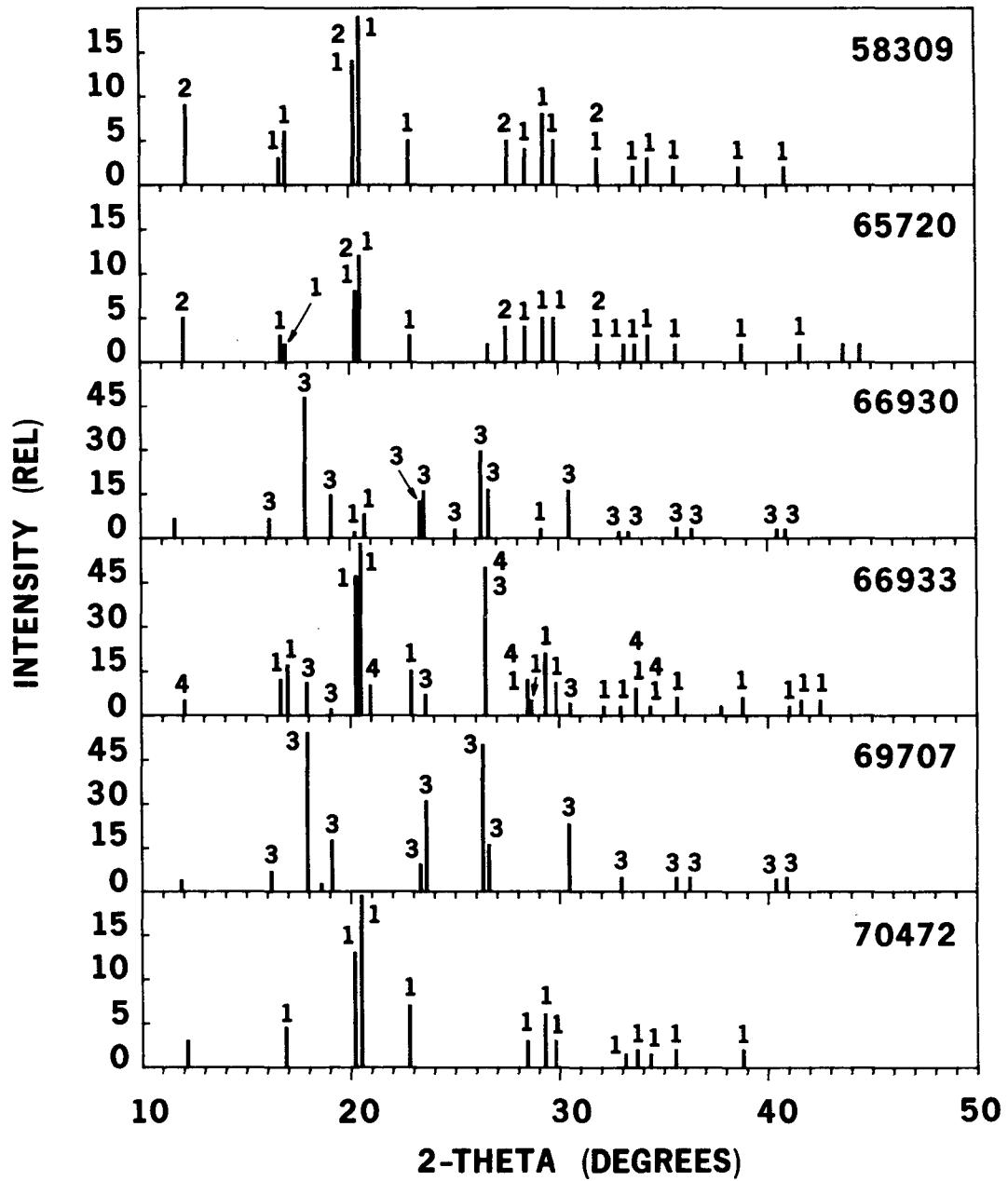
$$1 = (\text{NH}_4)_2\text{SO}_4$$

$$2 = (\text{NH}_4)_2\text{SO}_4 \cdot \text{PbSO}_4$$

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Fig. 1c

Station 118 (Fine Fraction)



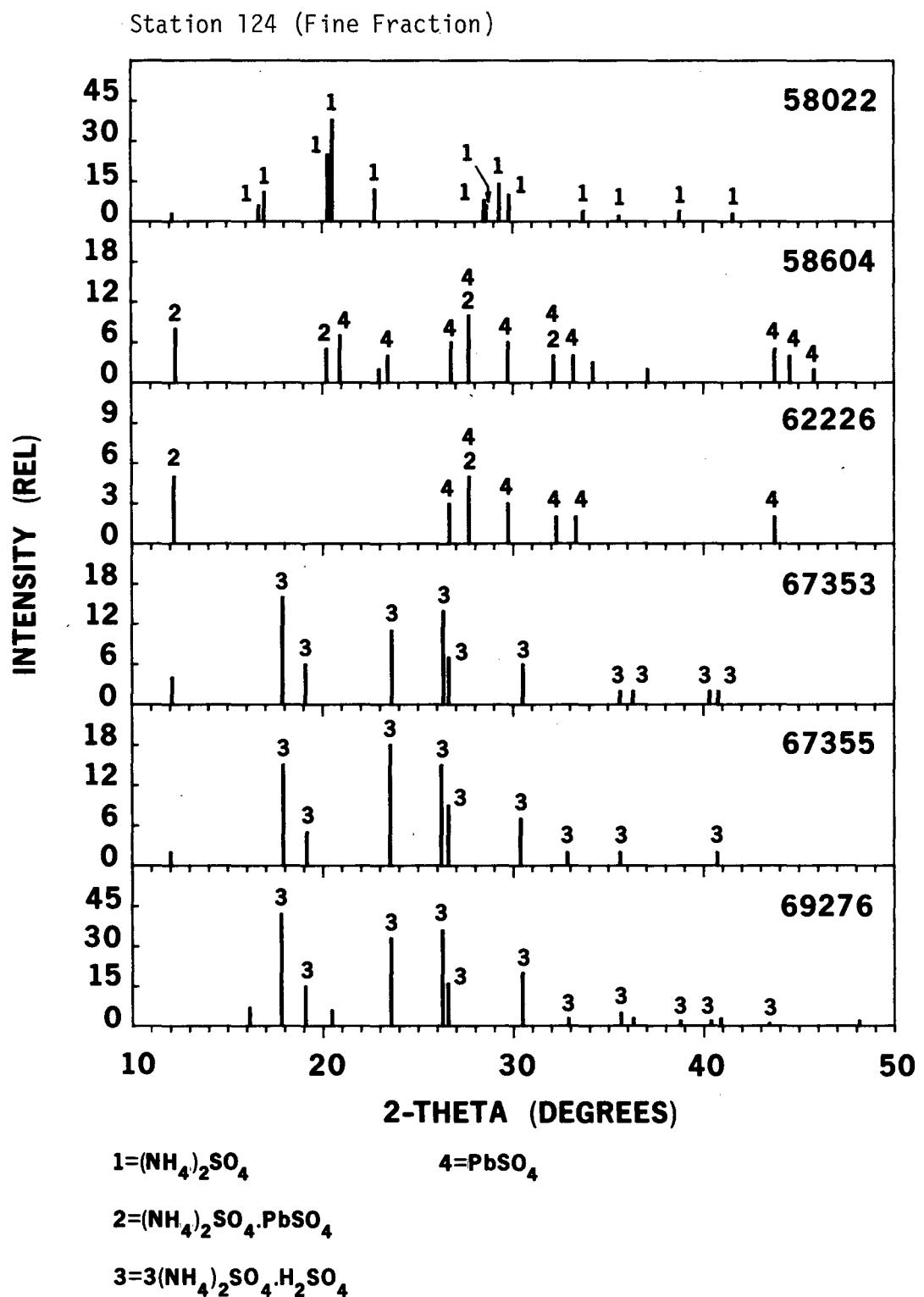
1= $(\text{NH}_4)_2\text{SO}_4$

4= $\text{CaAl}_2\text{Si}_2\text{O}_{16} \cdot 4\text{H}_2\text{O}$

2= $(\text{NH}_4)_2\text{SO}_4 \cdot \text{PbSO}_4$

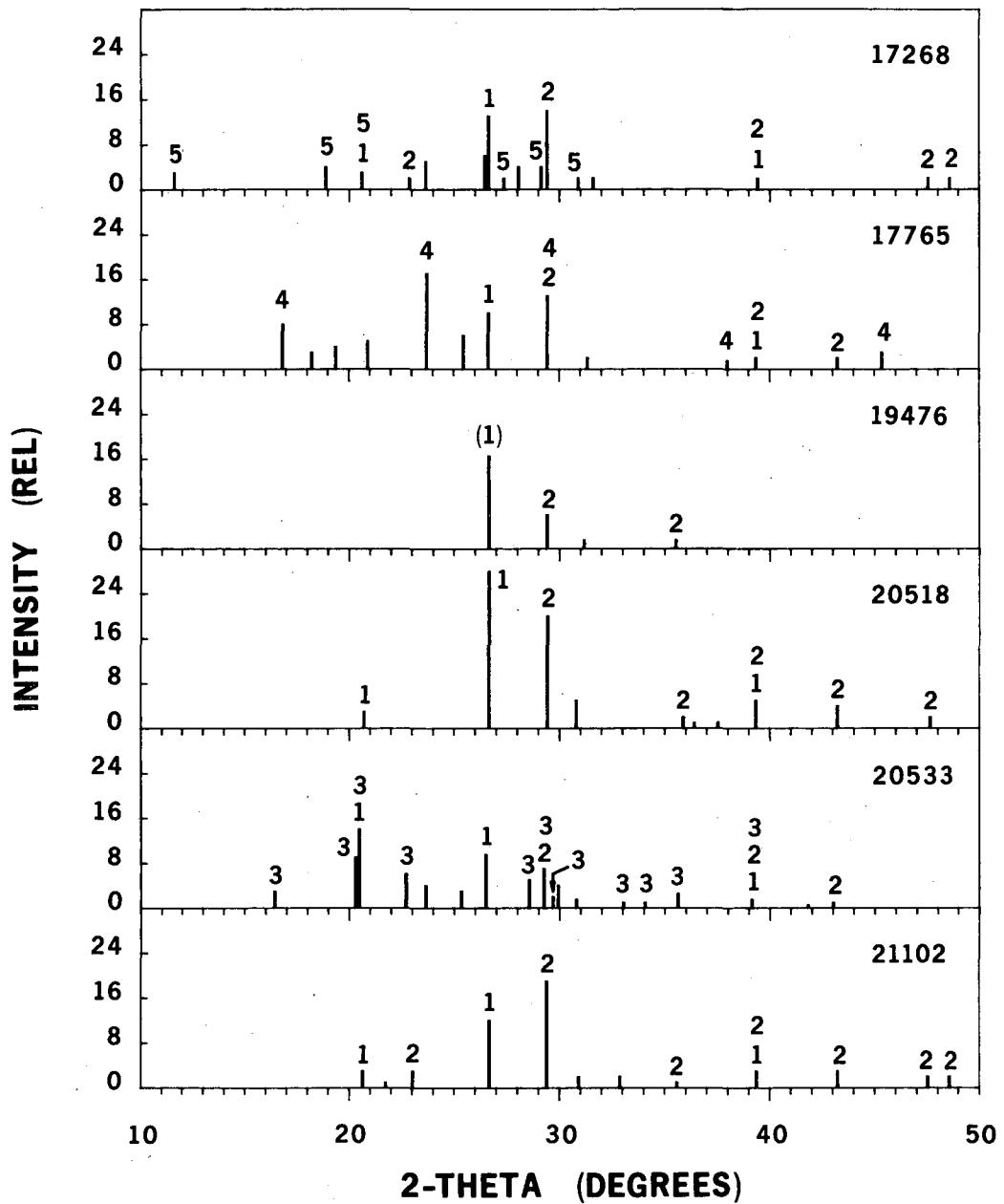
3= $3(\text{NH}_4)_2\text{SO}_4 \cdot \text{H}_2\text{SO}_4$

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Station 103 (Coarse Fraction)



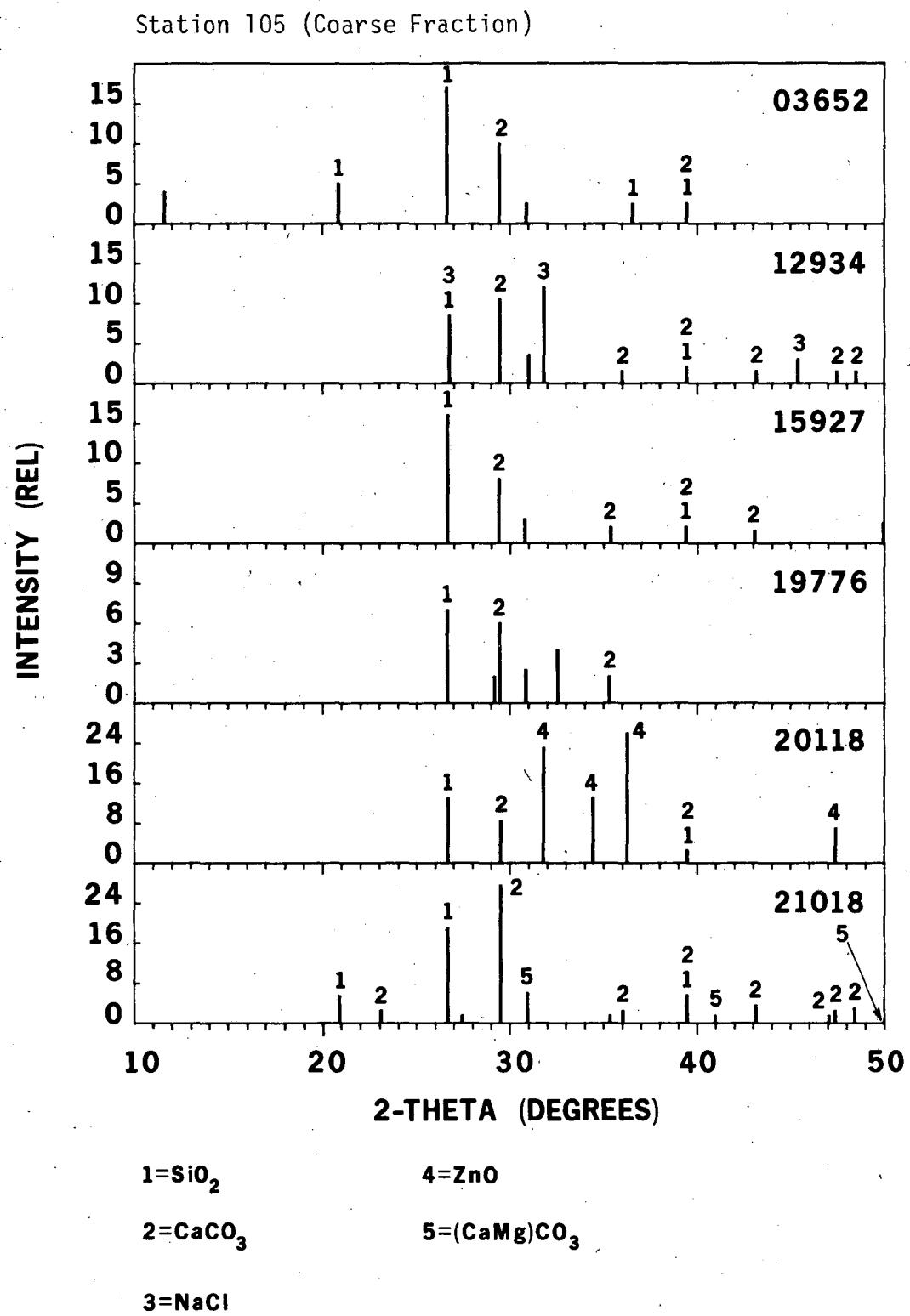
1=SiO<sub>2</sub>

4=(0.7NH<sub>4</sub>H<sub>2</sub>PO<sub>4</sub>). (0.3KH<sub>2</sub>PO<sub>4</sub>)

2=CaCO<sub>3</sub>

5=CaAl<sub>2</sub>Si<sub>2</sub>O<sub>16</sub>.4H<sub>2</sub>O

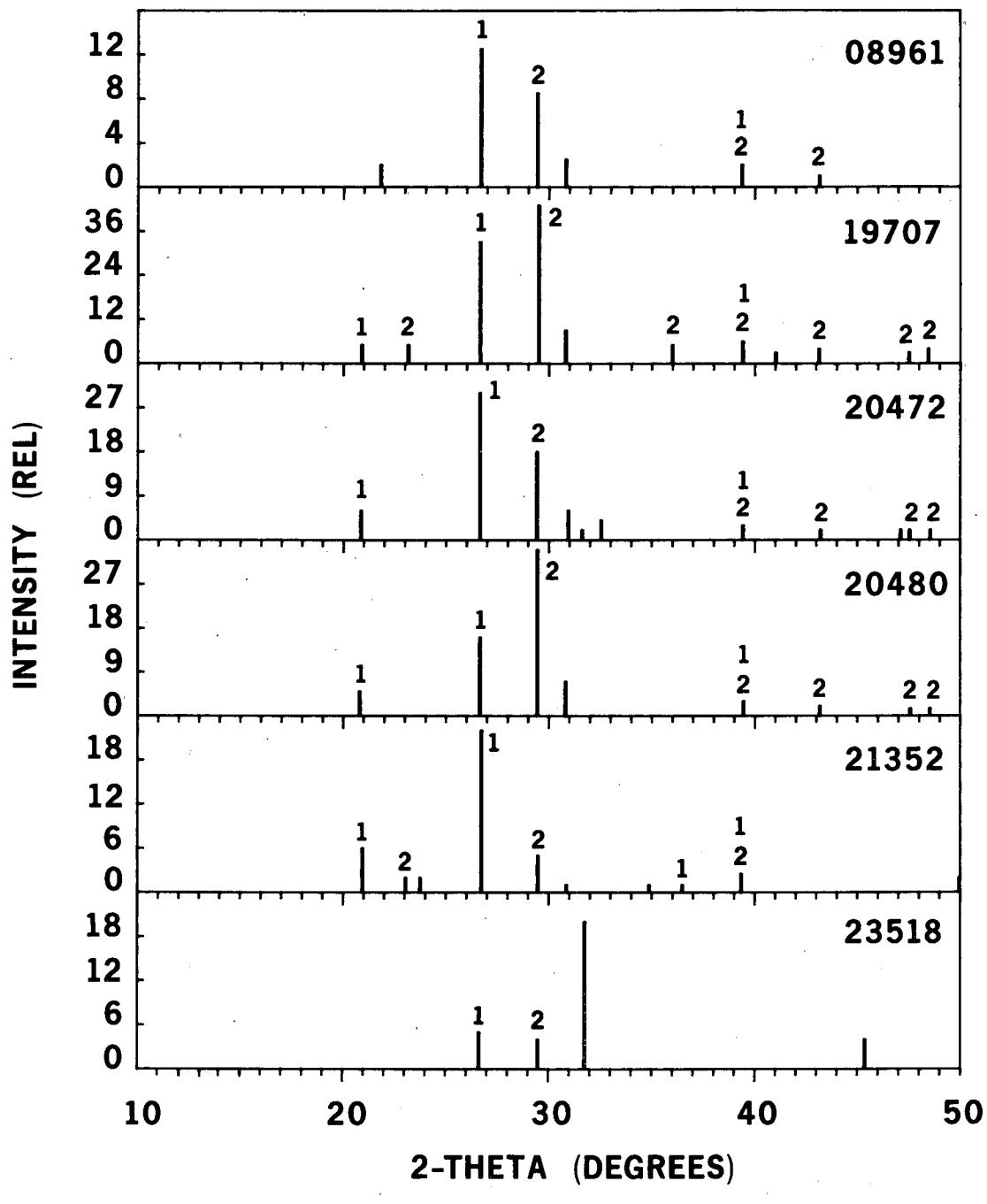
3=(NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>



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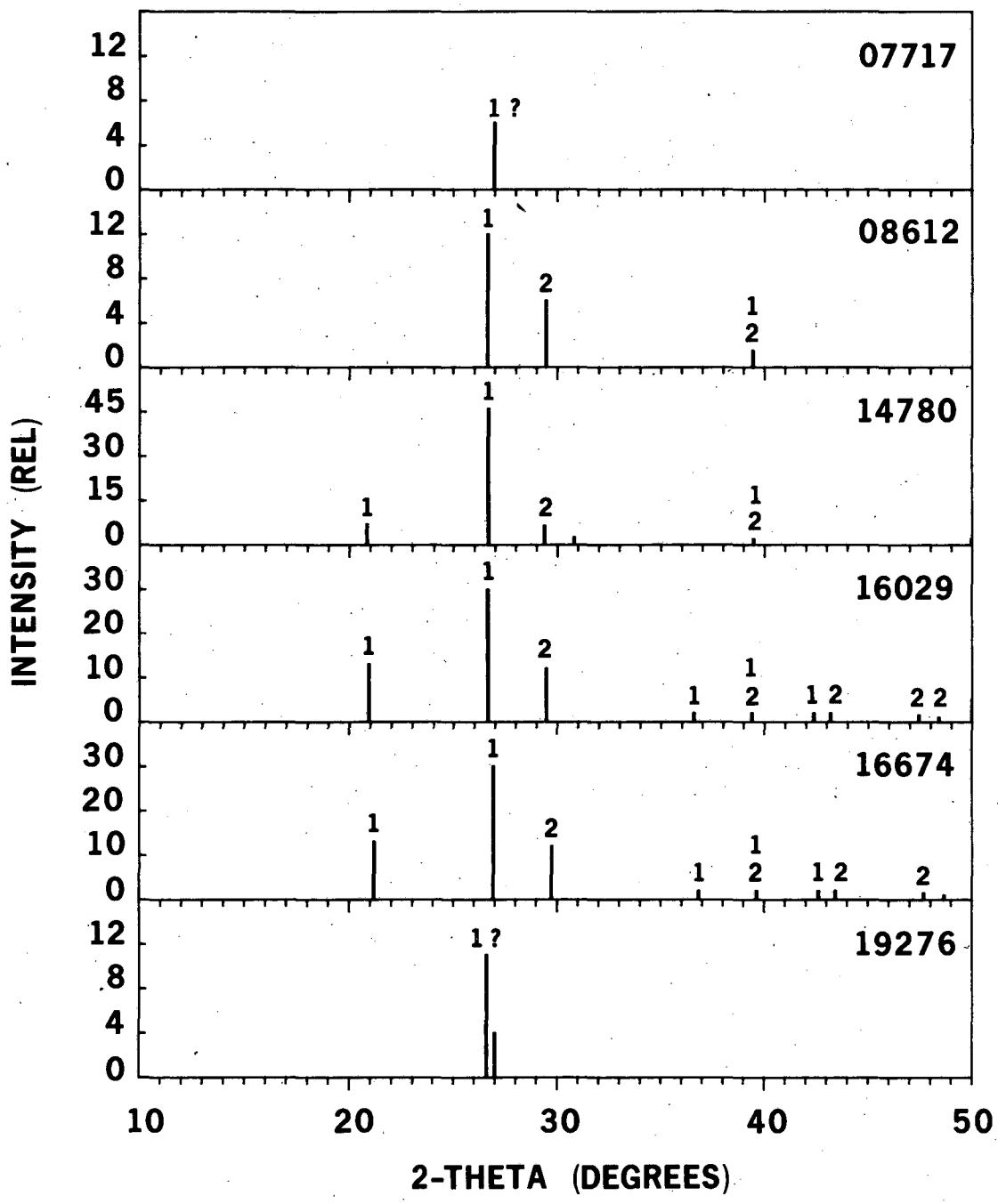
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## Station 118 (Coarse Fraction)

1= $\text{SiO}_2$ 2= $\text{CaCO}_3$ 

XBL 7910-12600

Station 124 (Coarse Fraction)



1= $\text{SiO}_2$

2= $\text{CaCO}_3$

XBL 7910-12595

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