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**LOW FREQUENCY NOISE IN RESONANT JOSEPHSON SOLITON  
OSCILLATORS**

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# LOW FREQUENCY NOISE IN RESONANT JOSEPHSON SOLITON OSCILLATORS.

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## Abstract

The noise in the resonant soliton mode of long and narrow Josephson tunnel junctions (Josephson Transmission Lines, JTLs) has been measured in the frequency range from 0.1 Hz to 25 kHz by means of a dc SQUID. To within a factor of 2 the measured white noise was found to be equal to the Nyquist voltage noise in a resistance equal to the dynamic resistance  $R_D$  of the current-voltage characteristic at the bias point. In contrast, measurements of the linewidth of the microwave radiation from the same JTL showed that the spectral density of the underlying noise voltage scaled as  $R_D^2/R_S$  where  $R_S$  is the static resistance. The origin of the different behavior is not known.

## Introduction

Long, one-dimensional Josephson tunnel junctions (Josephson Transmission Lines, JTL's) are of considerable theoretical and experimental interest because of their highly nonlinear characteristics<sup>1,2</sup>. These devices are slow-wave ( $\bar{c} \approx 0.025c$ ), non-linear transmission lines that support a variety of excitations, such as fluxons, plasmons and breathers, and are modelled by the perturbed, thermal sine-Gordon equation<sup>3,4</sup>. Soliton (fluxon) devices may find applications in radiofrequency oscillators and amplifiers and in digital circuits where the soliton represents one bit of information<sup>5</sup>. The low frequency noise is of interest because it determines the performance of the amplifier and the linewidth of the soliton oscillator. Few noise studies have been reported<sup>6</sup>, however, and here we describe a series of measurements using a dc Superconducting Quantum Interference Device (SQUID).

## JTL model

On a JTL, the soliton is a localized  $2\pi$  "kink" in the phase difference  $\delta(x, t)$  between the two superconducting electrodes on either side of the tunnel barrier. The phase kink corresponds to one quantum of flux,  $\Phi_0 = h/2e$ , (one fluxon or one anti-fluxon) threading the junction in the plane of the barrier. Resonant motion of these fluxons or anti-fluxons produces current singularities in the current-voltage (I-V) characteristics, namely zero-field steps (ZFSs) at voltages  $V_n$

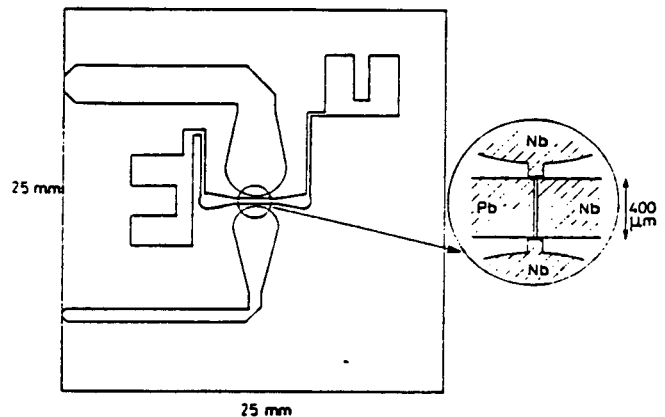


Figure 1. Configuration of Nb-NbO<sub>x</sub>-Pb overlap JTL showing coupling to microstrip antennas.

$= n\Phi_0 \bar{c}/L$ ; here  $n = 1, 2, 3, \dots, L/\lambda_J$ , where  $L$  is the junction length and  $\lambda_J$  is the Josephson penetration depth. On the  $n = 1$  step the fundamental frequency of the pulse train emitted from one end of the JTL is  $f_1 = V_1/2\Phi_0 = \bar{c}/2L$  with a linewidth  $\Delta f_1$ , determined by the fluctuations in the fluxon velocity. Assuming a Nyquist noise spectrum for the junction, one finds<sup>4</sup> the full linewidth at half power for a current-biased JTL to be

$$\Delta f_1 = \pi k_B T R_D^2 / (R_S \Phi_0^2), \quad (1)$$

where  $R_D$  is the dynamic resistance and  $R_S = V/I$ , and  $T$  is the temperature.

The form of Eq. (1) can be understood as follows. The Nyquist noise current associated with the static resistance has spectral density  $4k_B T/R_S$ , and is converted to a voltage spectral density by the factor  $R_D^2$ . The fluctuations in voltage then produce fluctuations in the Josephson frequency.

We are not aware of any calculations of the low frequency white noise. One might expect both mixed-down noise<sup>8</sup> and pair fluctuations arising from photon number fluctuations<sup>9</sup> to give additional contributions to the noise generated at the measurement frequency. Given the lack of a theory for this complicated, nonlinear system, we shall find it convenient to analyze our results in terms of an effective noise resistance  $R^*$ , so that  $S_V(f) = 4k_B T R^*$ .

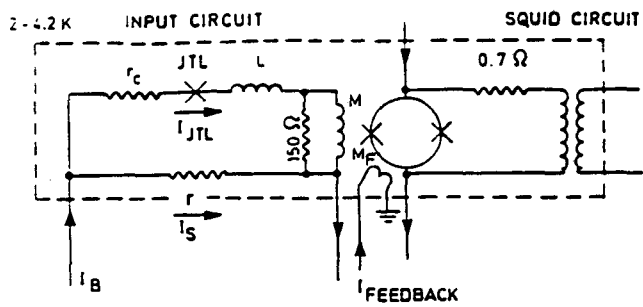


Figure 2. Schematic of dc SQUID amplifier circuit used to measure low frequency voltage noise. Typical circuit parameters were  $r = 0.030 \Omega$ ,  $r_c = 10-40 \text{ m}\Omega$ ,  $L = 9.6 \mu\text{H}$ ,  $M = 15.5 \text{ nH}$  and  $M_F = 37 \text{ pH}$ .

### Experimental details

The JTLs, coupled to microstrip antennas (Fig. 1), were fabricated on Corning 7059 glass at TUD. The Nb-NbO<sub>x</sub>-Pb overlap junctions were  $400 \times 20 \mu\text{m}^2$  with critical current densities in the range 10 to 40 A/cm<sup>2</sup>; the corresponding values of  $\lambda_J$  were 145-75  $\mu\text{m}$ . Four samples were used in this study.

The dc and microwave characteristics were determined at TUD in a carefully screened cryostat with heavily filtered leads. When we changed the bias point from the bottom to the top of a given ZFS, we found the linewidth of the soliton radiation at about 10 GHz varied from about 1 MHz to 2 kHz, always a factor of 2-3 larger than the theoretical prediction obtained with measured values of  $T$ ,  $R_D$  and  $R_S$ .

The low frequency noise was measured at UCB using the dc SQUID amplifier shown in Fig. 2. The 50-turn input coil of the planar SQUID<sup>10,11</sup> was connected in series with the junction and a resistor  $r = 0.026 \Omega$ ;  $r_c$  (10-40 m $\Omega$ ) is the contact resistance of the In pads on the junction. At the low frequencies,  $f$ , at which the measurements were made ( $f < 25 \text{ kHz}$ ) the JTL was voltage biased for  $R_D \gg r$  and current biased for  $r \gg R_D$ ; at the soliton frequencies the JTL was most likely current biased. The SQUID was operated in a conventional flux-locked loop in which the output voltage was proportional to the current in the input coil. Both the SQUID and the JTL were mounted in a Nb cell filled with and immersed in liquid helium, and the cryostat was surrounded by two  $\mu$ -metal shields. The leads were heavily filtered and all circuits were battery powered; a shielded room enclosed the entire experiment.

### Experimental results

The I-V characteristics of each JTL were obtained from plots of the SQUID output vs. the bias current  $I_B$  in the input circuit. A typical I-V characteristic reconstructed from these data is shown in Fig. 3. The noise was measured over the range 0.1 Hz to 25 kHz, and five representative spectra measured at points indicated in Fig. 3 are shown in Fig. 4. Spectrum (a), obtained with zero bias in the JTL, represents

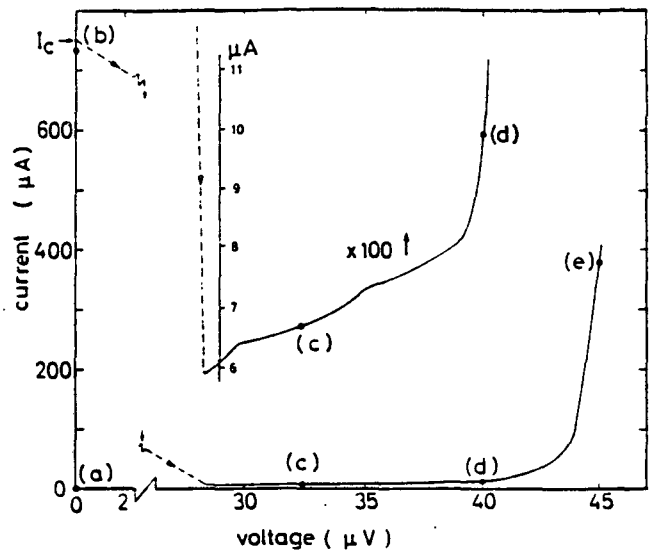


Figure 3. Current-voltage characteristic of JTL at  $T = 4.2 \text{ K}$  showing a ZFS at about  $43 \mu\text{V}$ . Letters (a)-(e) denote bias points at which the noise spectra in Fig. 4 were obtained. Dashed lines are load-lines resulting from the circuit resistance loading the JTL.

the Nyquist noise from the resistance  $r + r_c$ . The roll-off at about 2 kHz corresponds to the low-pass filter knee of the input circuit. Spectrum (b) was obtained with a current of 730  $\mu\text{A}$  in the JTL, which was still in the zero voltage state. The additional noise below about 5 Hz arises from drift in the bias current. In the zero voltage state, we verified that the white noise power scaled with the temperature with a magnitude predicted by the Nyquist formula to within  $\pm 5 \%$ . This result implies that extraneous noise was negligible.

Spectrum (c) was obtained with the JTL biased at about 6.7  $\mu\text{A}$  on the quasiparticle tunneling curve; note that the level of white noise was appreciably lower than in spectra (a) and (b) because the total current resistance increased from  $(r + r_c) = 0.038 \Omega$  to about  $5 \Omega$ . In spectrum (d) we observe a marked peak in the noise at a few kilohertz. This peak arose from random telegraph signals (RTSs) across the JTL with typical magnitude of 10-20 nV. These RTSs are associated with unstable bias points where apparently two different soliton modes compete. Finally, spectrum (e) shows the noise near the top of the first ( $n=1$ ) ZFS, where, typically,  $R_S = 0.1 \Omega$  and  $R_D = 2 \text{ m}\Omega$ . The noise is white at low frequencies ( $f < 10 \text{ Hz}$ ) and between roughly 100 and 700 Hz.

To characterize the noise, we write the spectral density of the noise current in the input circuit as:

$$S_I(f) = 4k_B T (R^* + r + r_c) / (R_D + r + r_c)^2 \quad (2)$$

Here, we have assumed that the voltage noise source of the JTL can be characterized by the effective resistance  $R^*$ , and that the total voltage noise power should be divided by the dynamic resistance of the input circuit to obtain the total current noise power. We note that for bias points near the top of the ZFSs where  $R_D$  is a few milliohms the contribution of the junction noise is small, and the error in its

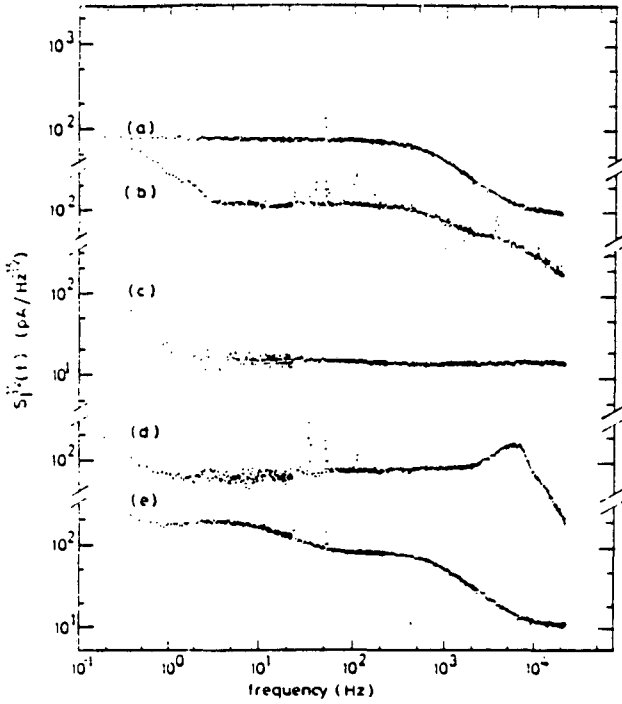


Figure 4. Measured 4.2 K noise spectra  $S_I^{1/2}(f)$  for JTL Letters (a)-(e) refer to the bias points in Fig. 3.

measurement correspondingly large. The results are shown in Fig. 5 where we plot  $R^*/R_D$ , inferred from Eq. (2), vs. current in the JTL. For reference we also plot in Fig. 5 the measured values of  $R_D$ ,  $R_S$ ,  $R_D/R_S$ , and the value of  $R^*$  inferred from the noise measurements and  $R_D$ .

On the quasiparticle curve (filled circles)  $R^*/R_D$  varies from about 2 to 5. Since these results are in the limit  $\hbar f - eV \ll k_B T$ , one would expect the noise power to be given by the Nyquist formula  $4k_B T R_D$ . Thus, it is likely that the excess noise is produced by the dynamics of the long junction; we are not aware of any theory for this noise. On the ZFS, on the other hand,  $R^*/R_D$  is between approximately 1 and 2. Yet, as shown in Fig. 5, over the current range 6 - 380  $\mu A$   $R_D/R_S$  varies from about 1 (low currents) to about 0.02 (high currents). Thus, we conclude that at least at high currents on the ZFS, the effective noise resistance  $R^*$  is not given by  $R_D^2/R_S$  as is the case for the linewidth [Eq.(1)]. Rather, it appears that to a first approximation  $R^* = R_D$ . From this result, we conclude that the noise at low frequencies is higher than one would expect from a naive interpretation of Eq.(1), that is, the factor  $R_D/R_S$  is absent. Since  $R_D/R_S$  is typically 0.03 on the ZFS1 (Fig. 5), the low frequency noise power would be reduced by about 30 if this factor were present.

#### Concluding remarks

We have measured the soliton oscillator linewidth and low frequency noise of a JTL biased on the first ZFS. At an oscillator frequency of 10 GHz, the linewidth is given by  $\alpha k_B T R_D^2 / R_S$  over a current bias range in which  $R_D^2 / R_S$  varies by about a factor of 500. The coefficient  $\alpha$  is typically

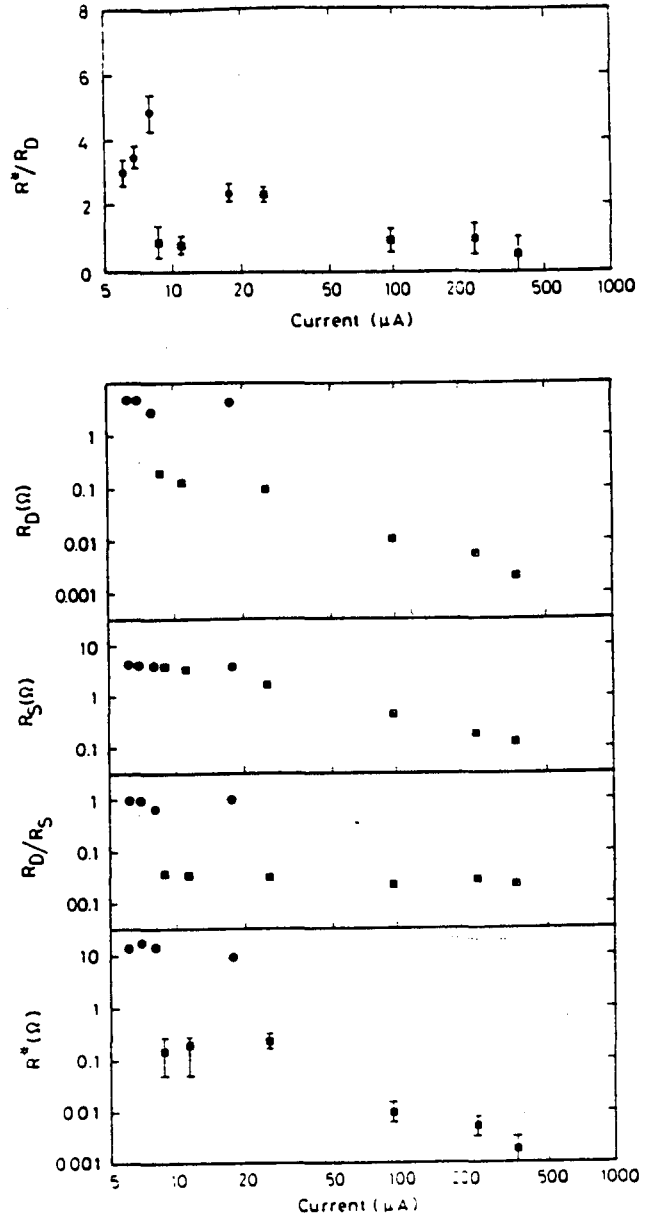


Figure 5. Upper plot shows current-dependence of normalized noise resistance  $R^*/R_D$  calculated from measured data at 4.2 K using Eq. (2). Filled circles refer to quasiparticle curve; filled squares refer to the first ZFS. Lower plot shows current-dependence at 4.2 K of the measured values of  $R_D$ ,  $R_S$  and  $R_D/R_S$  and of the inferred  $R^*$ .

2-3; the reason for this excess linewidth is not known. The spectral density of the low frequency white voltage noise is given by approximately  $\beta 4k_B T R_D$  where  $\beta$  is typically 1-2. Over the range of current studied  $R_S$  varied by about a factor of 50, and thus appears not to enter into the magnitude of the voltage noise. The difference in the dependence of the linewidth and low frequency noise on  $R_S$  is not understood, and it would be of considerable interest to develop a detailed theory for the mechanism of low frequency noise.

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