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### Article MBD-Based Machining Feature Recognition and Process Route Optimization

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Abstract: Machining feature recognition is considered the key connecting technique to the integration of Computer-Aided Design (CAD) and Computer-Aided Process Planning (CAPP), and decisionmaking of the part processing scheme and the optimization of process route can effectively improve the processing efficiency and reduce the cost of product machining cost. At present, for the recognition of machining features in CAD models, there is a lack of a systematic method to consider process information (such as tolerance and roughness) and an effective process route optimization method to plan part processing procedures. Here we represent a novel model processing feature recognition method, and, on the basis of feature processing plan decision, realize the optimization of the process route. On the basis of a building model Attributed Adjacency Graph (AAG) based on model geometry, topology, and process information, we propose an AAG decomposition and reconstruction method based on Decomposed Base Surface (DBS) and Joint Base Surface (JBS) as well as the recognition of model machining features through Attributed Adjacency Matrix-based (AAM) feature matching. The feature machining scheme decision method based on fuzzy comprehensive evaluation is adopted, and the decision is realized by calculating the comprehensive evaluation index. Finally, the Machining Element Directed Graph (MEDGraph) is established based on the constraint relationship between Machining Elements (MEs). The improved topological sorting algorithm lists the topological sequences of all MEs. The evaluation function is constructed with the processing cost or efficiency as the optimization objective to obtain the optimal process route. Our research provides a new method for model machining feature recognition and process route optimization. Applications of the proposed approach are provided to validate the method by case study.

**Keywords:** machining feature recognition; process route optimization; machining elements directed graph (MEDGraph); improved topology sorting algorithm

#### 1. Introduction

Automatic Feature Recognition (AFR) refers to the extraction of feature information with specific engineering significance from part models. A CAD model of a part is composed of low-level graphic elements such as surface, line, and point, while CAPP information is generated based on high-level features with engineering semantics. Feature recognition is an intelligent interface between CAD and CAPP. AFR can identify the corresponding features according to specific process requirements, which is the basis of process planning and the most important step in transforming design information into manufacturing process information. With the help of AFR, the structure feature can be identified according to specific process information, which is considered the most crucial technique to turn design information into a manufacturing process [1].

In recent years, feature recognition has developed rapidly, but the traditional feature recognition methods based on model topology and surface geometry recognition do not take model process information into account. If the roughness and tolerance grade of



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**Copyright:** © 2022 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). the assembly surface of two models with identical topology and geometric dimensions are quite different, their processing technology may be completely different. Therefore, machining feature recognition based on machining information has become a problem that must be considered.

Model-Based Definition (MBD) is a model-based product data definition method that adds tolerance, annotation, and other process information on the basis of model topology and geometric data. Based on the geometric and process information in the MBD model, the processing feature recognition based on MBD lays a foundation for the subsequent feature processing scheme decision and process route optimization.

The paper plans to solve the problems of machining feature recognition, machining scheme decision, and process route optimization in the MBD model. On the basis of extracting the model geometry and process information, the model Attributed Adjacency Graph (AAG) is established and decomposed to obtain a feature subgraph, and then the feature subgraph is matched with predefined machining features to realize machining feature recognition. The decision-making method of the model feature processing scheme based on fuzzy comprehensive evaluation is adopted. By analyzing the influencing factors of the feature processing scheme, the subordinate relationship between each influencing factor and the processing scheme is established. A multi-factor comprehensive evaluation model is established according to the single-factor evaluation results, and the optimization of feature processing schemes is realized by calculating the comprehensive evaluation index vector. Finally, based on the constraint relationship between the processing elements, a Machining Elements Directional Graph (MEDGraph) is established. The improved topological sorting algorithm lists all the topological sequences of the processing elements, takes the processing cost or efficiency as the optimization objective, constructs an evaluation function, and obtains the optimal process route.

The remainder of the paper is organized as follows. Section 2 reviews the literature relating to feature recognition. In Section 3, the method of information extraction from MBD is introduced. Model AAG-based machining feature recognition method is constructed in Section 4. In Section 5, the feature processing scheme is decided. In Section 6, the model process route is optimized. The proposed methods are validated through a case study in Section 7, followed by a conclusion in Section 8.

#### 2. Literature Review

In order to achieve feature recognition and process route optimization based on the CAD model, scholars carried out research in the fields of machining feature recognition and process route optimization.

#### 2.1. Machining Feature Recognition

The purpose of machining feature recognition is to realize the conversion from design features to machining features. The concept of feature recognition was first proposed by Kyprianou [2], and its main research object is the geometric topology classification of models. Since then, various types of feature recognition methods have emerged, including graph-based methods, volume decomposition-based methods, neural network-based methods, trace-based methods, rule-based methods, and hybrid methods combining various methods [3].

The graph-based method is considered to be the most successful method. This method describes the feature recognition problem as a graph matching problem. The B-rep model is converted into a graph representation. Joshi and Chang first proposed the feature recognition method of AAG [4]. By acquiring the geometric topological relationship between surfaces and edges of the model, AAG is constructed, and then the machining features are identified by subgraph matching. However, in its research, only the concave-convex attributes of surfaces and edges are considered, and the model information is not fully expressed. Li [5] adds other attributes of vertices on the basis of AAG to form an Extended Attributed Adjacency Graph (EAAG). Marefat and Kashyap proposed the

concept of virtual connection and tried to recover the boundary information lost due to the intersection of features [6]. This method realized the recognition of intersection features. However, the virtual connection construction is difficult, and the method is not universal.

Armstrong first proposed feature recognition based on unit decomposition [7]. Sakurai et al. conducted more in-depth research and made great progress [8–10]. This method can effectively identify intersection features and provide multiple interpretations [11]. However, this method is low efficient, so it needs to be further filtered. Campana and Mele proposed a rule-based feature recognition method [12], which needs to formulate predefined rules for each type of feature to be recognized. However, the definition of feature rules is not unique, and the calculation of feature recognition methods is large. Requicha et al. proposed a feature recognition method based on traces [13], which mainly studies the traces generated when different features intersect inside the part. Sunil and Pande proposed a feature recognition method based on neural networks [14], which can effectively recognize intersection features. However, due to the problem of data source, the accuracy of its recognition results cannot be guaranteed.

Hybrid feature recognition methods combine the advantages of two or more traditional feature recognition methods. Li et al. used the hybrid feature recognition method to improve the recognition reliability of rib features [15]. Gao and Shah proposed an intersection feature recognition method based on the mixture of graph and rule [16]. Fougeres and Ostrosi adopted a hybrid representation combining framework, syntax, and diagrams for the representation of features [17].

Liu et al. proposed a hybrid feature recognition method based on graph decomposition and feature factor clustering [18]. Zhang et al. input the geometric topology information of the model into the improved BP neural network for feature recognition by reading the step neutral file [19]. Duan et al. proposed a feature recognition method based on feature layering for cabin parts [20]. Luo et al. proposed a hybrid feature recognition method based on the combination of graph and rule-based reasoning [21].

The above feature recognition technologies have the defect of insufficient correlation between the identified features and model process information, which is not conducive to the processing of later process information.

#### 2.2. Feature Processing Scheme Decision

Feature processing scheme decision-making is an important step in process design, which requires comprehensive consideration of many factors, such as material, type of processing features, and processing accuracy. The application of novel decision-making methods, such as the production rule decision-making method, method based on decision table or decision tree, fuzzy reasoning decision-making method, and neural network decision-making method, greatly improves the decision-making efficiency of the processing scheme compared with the traditional method based on process manual.

Berenji et al. proposed a decision-making method based on production rules to determine the processing scheme through the selection structure of judgment [22]. Huang established a mathematical model of fuzzy comprehensive evaluation for the decision-making of feature processing schemes and realized the decision-making process by synthesizing the fuzzy relations [23]. Ma et al. analyzed the fuzzy mapping relationship between feature attributes and the processing scheme and established a processing scheme decision model based on fuzzy reasoning [24]. Hu et al. established a feature processing scheme decision-making model based on Tsukamoto fuzzy reasoning and realized the optimization of feature processing schemes according to the membership degree of each processing scheme [25]. Zhong [26] and Zhao [27] used the neural network method to make feature processing scheme decisions. Guan et al. combined a genetic algorithm and Analytic Hierarchy Process (AHP) to realize the decision of the processing scheme [28]. Hu et al. used particle swarm optimization to optimize processing schemes with the goal of product benefits and product quality [29].

#### 2.3. Process Route Optimization

The formulation of process route is the key to product production, which determines the machining process and cost of parts [30]. The traditional process route formulation method is inefficient and difficult to achieve optimization. With the development of computer technology such as artificial intelligence and data mining, the application of various intelligent algorithms makes it possible to formulate product process plans with high efficiency, low energy consumption, and low cost [31].

Chen et al. studied the CAPP system based on the feature parameter model and realized the process route decision by extracting the geometric feature parameters on the model and matching them with the template base [32]. Peng et al. extracted the feature factors of gear blanks using the fault tree analysis method and obtained the manufacturing process route with the best ecological efficiency [33]. Krishna et al. proposed a novel heuristic ant colony algorithm to search for the global optimal process route, constructed the optimal objective function model, and verified its progressiveness [34]. Salehi et al. proposed a two-level planning process route optimization method [35]. Zhou et al. built a multi-objective model to optimize the low-carbon-based process route optimization method, which determines the minimum carbon emissions and processing time as the objective of optimizing the process route [36].

Cheng et al. integrated the ant colony algorithm and bacterial foraging algorithm and designed two search phases of manufacturing resources and processing element sequence [37]. An et al. proposed an optimization algorithm combining intuitionistic fuzzy sets and the second generation of intensity Pareto to construct a multi-objective function with the lowest replacement cost of processing resources to realize the optimization of the process route [38]. Based on the genetic algorithm, Guo et al. introduced feasible process sequences to improve the genetic algorithm, and the convergence speed and global optimization ability of the genetic algorithm were improved [39–41]. Liu et al. combined polychromatic set theory and genetic algorithm and took the shortest auxiliary time as the optimization goal, realizing the work step sequencing in the machining center [42].

#### 3. MBD-Based Model Information Extraction

MBD model data express product design and manufacturing information, including 3D model data, datum, coordinate system, annotation information, and other data, which can provide information support for subsequent process planning of products. Currently, MBD has become a general model definition method. Every mainstream 3D product design software has established a data conversion interface to STEP files and also developed corresponding customized development functions, such as Creo Toolkit of Creo, UG Open provided by UG, and CATIA CAA of CATIA.

The identification of model machining features mainly involves solid model information and annotation information in the MBD model [43]. The solid model reflects the product geometry and is composed of the basic geometric elements through topological connection, including model geometry information and auxiliary geometry information. Auxiliary geometric information is associated with geometric elements such as points, lines, and faces. Annotation information includes dimension, tolerance, roughness, and other elements related to machining requirements. The dimension information expresses the topological relationship between geometric elements, and the relative position between geometric elements can be determined by the dimension. Tolerance and roughness together express the machining accuracy requirements of parts.

Currently, there are two main expression schemas of 3D models, which are CSG and B-Rep. B-Rep representation mainly expresses geometric and topological information. The former is composed of position, coordinate, curve equation, etc., and the latter is formed by point, edge, contour, surface, and logical relationship among them. Most current modeling software supports B-Rep representation.

#### 3.1. MBD Model Data Structure

Geometric elements are topologically connected to form a solid model. From the perspective of data structure, it is mainly composed of surfaces and edges. Annotation information expresses process information of the model and is the basis for formulating machining route. Most 3D modeling software use surfaces, contours, and edges to describe solid models. Surfaces and edges are the main carriers of model information, and contours, as auxiliary geometric elements, play a transitional role between surfaces and edges. The annotation information of the MBD model mainly includes dimension, tolerance, and surface roughness, which are attached to the model geometry.

The model elements involved in feature recognition mainly include surface, edge, dimension, tolerance, and roughness. Structure arrays are defined to represent model elements, as shown in Table 1. Among them, the arrays surface [], edge [], contour [], surfinish [], gtol [], and dimension [], respectively store the information on surfaces, edges, contours, tolerances, and dimensions of the model.

Table 1. Structure arrays for the storage of MBD model.

Structure Array	Surface []	Edge [ ]	Contour []	Surfinish [ ]	Gtol []	Dimension []
	ID	ID	Type	Symbol	Symbol	Symbol
	Туре	Туре	Edge ID	Value	Туре	Туре
	Concavity-convexity	Concavity-convexity	_/	Related surface ID	Value	Value
Structure member	Adjacent surface ID	Adjacent surface ID	/	/	Related surface ID	Upper deviation
	Edge ID	Inner contour attribute	/	/	Datum ID	Lower deviation
	Contour information	/	/	/	/	Related surface ID
	Roughness	/	/	/	/	/
	Tolerance	/	/	/	/	/

The contour is divided into inner contour and outer contour. The inner contour is a closed loop formed by the end-to-end connected edges inside the model surface. There can be multiple inner contours on a surface. The outer contour is a closed loop formed by the end-to-end connected edges on the outermost side of the model surface. There is only one outer contour on a surface. Each edge has two or more adjacent faces, and the inner contour properties of some edges on different faces are different. It is specified that if an edge appears as an inner contour edge on an adjacent face, the edge is an inner contour edge.

#### 3.2. Extraction of MBD Model Information

The geometry and topology information and annotation information contained in the MBD model are the data basis for subsequent machining feature recognition and process route optimization. There are mainly two methods to extract model data. The first method is to extract information from neutral format files [44], and the other method is through customized development tools provided by commercial CAD modeling software [45]. In this paper, the latter method is used to develop an automatic model data extraction system and construct the data foundation of a machining feature recognition system based on MBD. This paper will take Creo software as an example to extract model information through Creo Toolkit.

The geometry and topology information of the model includes geometric information and topology information. Among them, geometric information describes the geometric data of vertices, edges, and faces; topology information describes the connection between vertices, edges, and faces. According to the above description of model information, when extracting geometric information, the extracted surface data includes ID and type of the surface and the contour information on it. The extracted edge data is the ID and type of the edge. The extracted topological information is mainly the connection relationship between model surfaces and edges, including the concavity–convexity of surfaces and edges and their adjacent surfaces. When extracting model information, first use the Creo Toolkit interface function to access the model. Then traverse the model surfaces, and record their ID, type, concavity–convexity of the surface, and the adjacent surface ID in sequence. Traverse the contours on the surface, judge the type of the contours and record its constituent edges. Finally, traverse the edges of the model, and record its ID, type, concavity–convexity, and the ID of the adjacent surface in turn.

Take the Creo model as an example, and build its geometry and topology information extraction flow chart, as shown in Figure 1. The main functions related to model geometry and topology information extraction in Creo Toolkit are shown in Table 2.

The pseudo-code of the geometric and topology information extraction algorithm is shown in Appendix A Algorithm A1.

The extracted model annotation information mainly includes dimension, tolerance, and roughness. Dimension information includes dimension symbols, types, values, deviations, and IDs of associated geometric elements. Tolerance information includes tolerance symbols, types, values, IDS of associated geometric elements, and datums; The surface roughness includes roughness value and associated surface ID. The above information is obtained by traversing the surface dimensions, tolerances, and roughness.

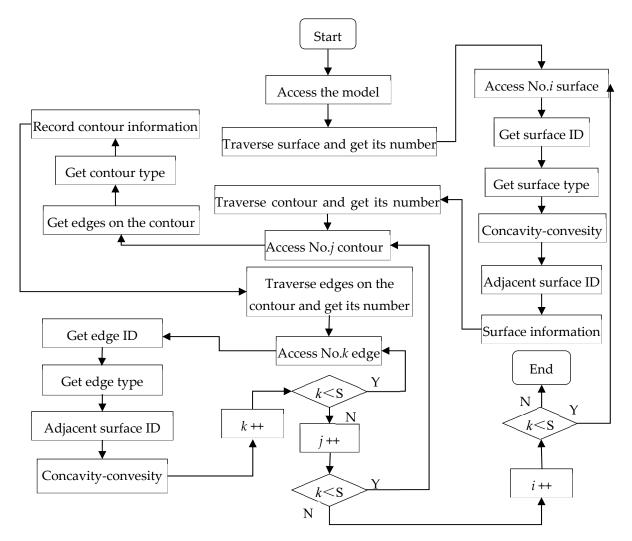


Figure 1. Flow chart of model geometric topology information extraction.

No.	Name	Function
1	ProMdlCurrentGet	Get the handle of current model
2	ProSolidSurfaceVisit	Traverse the model surfaces
3	ProSurfaceContourVisit	Traverse the contour on the surface
4	ProContourEdgeVisit	Traverse the edge on the contour
5	ProContourTraversalGet	Get the type of contour
6	ProSurfaceIdGet	Get the surface ID
7	ProSurfaceTypeGet	Get the type of the surface
8	ProSurfaceDataGet	Get the surface data
9	ProEdgeIdGet	Get the edge ID
10	ProEdgeTypeGet	Get the edge type

Table 2. Functions of geometric and topology information extraction.

#### 4. Machining Feature Recognition Based on AAM

Based on the preceding MBD model information extraction, a machining feature recognition algorithm based on Attributed Adjacency Matrix (AAM) is proposed. The model AAG is constructed by extracting the model information and then decomposed into feature subgraphs and converted into AAM, which is matched with the predefined features to realize the recognition of machining features.

In the process of machining feature recognition based on AAM, a model AAG is constructed according to the geometric and topology information of the model, and it is decomposed based on Decomposition Base Surface (DBS) and Joint Base Surface (JBS). Then match the decomposed AAG subgraph with predefined features to identify machining features. The process is shown in Figure 2.

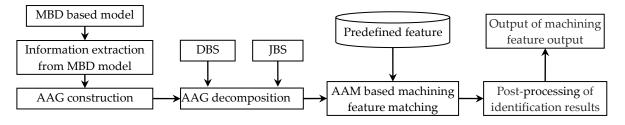


Figure 2. Flow chart of machining feature recognition.

The related concepts involved in the research process are as follows.

DBS [46] refers to the surface containing one or more inner contours in a 3D model. As shown in Figure 3, the top surface f of the hexahedron contains an inner contour composed of four model edges, and the surface f is a DBS.

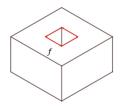


Figure 3. DBS.

Feature Base Surface (FBS) refers to a concave plane in a 3D model, and there is no entity of the model along the normal direction of the surface. As shown in Figure 4, the bottom plane of the keyway is an FBS, which belongs to the concave plane, and there is no entity of the model along its normal direction.

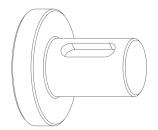


Figure 4. FBS.

JBS refers to two unconnected model surfaces, which need to be processed as the same surface when machining. When two surfaces have the same equation expression, and at least one of them is concave, the two surfaces are JBSs, such as  $f_3$  and  $f_4$ , in Figure 5.

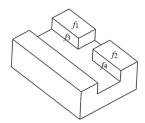


Figure 5. Joint base surface.

The Maximum Concave Connection Subgraph (MCCS) [18] of a node is the maximum connected graph that can be obtained by taking this node as the starting node and extending outward along the node line of the concave attribute in an AAG.

#### 4.1. Construction of Model AAG

In the process of machining feature recognition based on AAG, the B-Rep information of the model is expressed by AAG, which can accurately describe the topological structure of the model surfaces and edges. Conventional AAG uses nodes to represent surfaces, and lines represent the intersecting edges of two surfaces. When the intersecting edge is convex, it is represented by the number 1, and when it is concave, it is represented by the number 0. This representation that does not include other attributes has certain limitations. Sometimes, AAG cannot accurately express the model.

When constructing the model AAG, the attributes of model surfaces and edges are extracted and used to enhance the expression ability of AAG. The node of AAG represents the model surface, and its attributes include type, concavity–convexity, DBS attribute, FBS attribute, and JBS attribute; its definition is shown in Table 3. The line between AAG nodes represents model edges, and its attributes include type, concavity–convexity, and inner contour edges; its definition is shown in Table 4.

Attribute Name	Type of Variable	Attribute Definition			
Туре	int	1Planar Plane2Cylinder3Conical surface4other surface			
Concavity-convexity	int	$\begin{cases} -1 & \text{Concave surface} \\ 1 & \text{Convex surface} \end{cases}$			
DBS attribute	bool	{ true DBS { false Not DBS			
FBS attribute	bool	∫ true FBS ) false Not FBS			
JBS attribute	int	/			

Table 3. Attribute of AAG nodes.

Attribute Name	Type of Variable	Attribute Definition
Туре	int	{1 Straight edge 2 Arc edge 3 Other edge
Concavity-convexity	int	{-1 Concave edge 0 Smooth edge 1 Convex edge
Inner contour	bool	{ true Inner contour edge { false No inner contour edge

Table 4. Attribute definition of node connection in AAG.

#### 4.1.1. Concavity–Convexity Judgment of Model Edge

The concavity–convexity of model edges is an important attribute of AAG, which determines the properties of model features. Zhou defined edge concavity–convexity as two adjacent surfaces on the mode; when the angle outside the solid is less than  $180^\circ$ , the intersection line is a concave edge. When the angle outside the solid is greater than  $180^\circ$ , the intersection line is convex [47]. According to the above definition, the edge *l* in Figure 6a is concave, and *l'* in Figure 6b is convex.

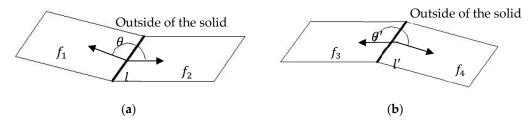


Figure 6. The definition of edge concavity–convexity. (a) *l* is concave; (b) *l'* is convex.

The preceding method defines the concavity–convexity of the intersection line when the plane intersects with the plane, but does not involve the concavity–convexity judgment of the intersection edge between the surface and planar plane or between two surfaces. According to the extraction of model information in this paper, we propose the definition of model edge concavity–convexity is as follows: when the adjacent surface of the edge is a plane, and the included angle of the non-solid side of the model is in the interval ( $\pi$ ,  $2\pi$ ), this edge is convex. When the included angle is in the interval (0,  $\pi$ ), this side is concave. When the adjacent surfaces are not all planar planes, and the included angle between the tangent plane of the surface at one point and another plane (or the tangent plane of the surface) on the non-solid side is in the interval (0,  $\pi$ ), this edge is concave. When the included angle is in the interval ( $\pi$ ,  $2\pi$ ), this side is concave. When the included angle is in the interval ( $\pi$ ,  $2\pi$ ), this side is concave. When the included angle is in the interval ( $\pi$ ,  $2\pi$ ), this side is concave. When the included angle is in the interval ( $\pi$ ,  $2\pi$ ), this side is convex, and when the included angle is equal to  $180^{\circ}$ , this side is smooth, as shown in Figure 7.

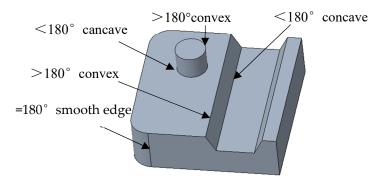


Figure 7. Examples of concavity and convexity of edges in the model.

The concavity–convexity of an edge is determined by the included angle of two planes where the edge is located. Luo [21] proposed a method to solve the included angle by using the arccosine of the plane normal vector, as shown in Formula (1).

$$\theta = \arccos \frac{n_1 \cdot n_2}{|n_1| |n_2|} \tag{1}$$

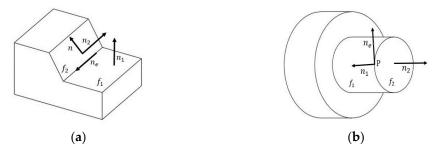
where,  $\theta$  is the angle between two planes,  $n_1$  and  $n_2$  is the normal vector of the plane.

The included angle that can be calculated in Formula (1) ranges from 0 to  $\pi$ , which can only be applied to the calculation of concave edges. A method to define the included angle between two surfaces is proposed, which can be used to solve the included angle of any angle between two planes or surfaces. The algorithm is as follows:

(1) When the adjacent surfaces of the edges are all planar planes, select one as the base plane, define the edge direction vector as the vector product of the base plane normal vector and the non-base plane normal vector, define the reference direction vector as the vector product of the edge direction vector and the non-base plane normal vector, and the angle between the reference direction vector and the base plane normal vector is  $\theta$ . When  $\cos(\theta) > 0$ , the edge is concave. When  $\cos(\theta) < 0$ , the edge is convex.

(2) When the adjacent surfaces of the edge are not all planar planes, first, take a point P on the edge. If the adjacent surfaces are planes, then select this plane as the base plane, and the tangent plane of the surface at point P is the non-base plane. If the adjacent surfaces are all curved surfaces, the tangent plane of any curved surface at point P is taken as the base surface, and the tangent plane of the other curved surface is taken as the non-base surface. It is defined that the tangent vector at point P is the vector product of the normal vector of the base plane and the normal vector of the non-base plane, the reference direction vector is the vector product of the tangent vector at point P and the normal vector of the base plane, and the angle between the reference direction vector and the normal vector of the base plane is  $\theta$ . When  $\cos(\theta) > 0$ , the edge is concave. When  $\cos(\theta) < 0$ , the edge is convex. When  $\cos(\theta) = 0$ , the edge is smooth.

Take Figure 8 as an example to judge the concavity–convexity of the edges. In (a),  $f_1$  and  $f_2$  are planar planes, and their normal vectors are  $n_1$  and  $n_2$ . Take  $f_1$  as the base plane, the direction vector of the straight side e is  $n_e = n_1 \times n_2$ , and the reference direction vector is  $n = n_e \times n_2$ . The included angle of n and  $n_1$  is  $\theta$ . Because of  $cos\theta > 0$ , the edge is concave. In (b),  $f_1$  is a surface,  $f_2$  is planar,  $f_2$  is taken as the base plane, and then take a point P on the intersection of two surfaces.  $n_1$  is the normal vector of the intersection at point P,  $n_2$  is the normal vector of  $f_2$ , the tangent vector of the intersection at point P is  $n_e = n_2 \times n_1$ , and the reference direction vector is  $n = n_e \times n_1$ . The angle between n and  $n_2$  is  $\theta$ . Because of  $cos(\theta) < 0$ , the edge e is convex.



**Figure 8.** Concavity–convexity judgment of model edge. (**a**) shows the intersection line of two planar planes; (**b**) shows the intersection line of planar plane and curved surface.

#### 4.1.2. Concavity–Convexity Judgment of Model Surface

Guo's definition of surface concavity–convexity is as follows [48]. If all the edges of the outer contour are convex, the face is convex, and if not, it is concave. But in Figure 9, the outer contour edges of  $f_1$  and  $f_2$  contain concave edges, and according to the above

definition, both surfaces are concave. However, it is generally considered that  $f_1$  is convex. So, the above definition is not accurate enough to express the topological information of the model and is only applicable to the model without convex features.

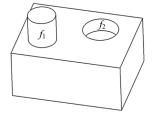


Figure 9. Concavity-convexity judgment of model surface.

A new method to define the surface convexity–concavity is proposed. The rules are as follows: (1) For a planar plane, when all its outer contour edges are convex, the surface is convex, and when the outer contour edges of the surface are not all convex, the surface is concave. (2) For a quadric surface, its concavity–convexity is judged according to whether the normal vector at any position on the surface is on the same side as the curvature circle at that point. When it is on the same side, the surface is concave; otherwise, it is convex. This is shown in Figure 10.

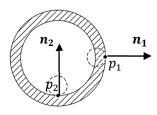


Figure 10. Judgment of curvature of surface.

#### 4.1.3. Construction of AAG

Based on the preceding model information extraction method and attribute research, the model AAG is constructed by taking the model surface as the node, taking the intersection line as the edge, and adding the attributes of surface and line. Its process is shown in Figure 11, and the main steps are as follows.

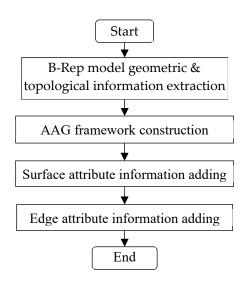


Figure 11. AAG construction flow.

(1) Extract B-Rep model information. Taking Creo models as examples, the Creo Toolkit is used to traverse the model surfaces and lines to extract their attribute.

(2) Model AAG framework is established, which is based on the geometric information and topological relationship between surface and line. AAG nodes are created based on model surfaces, and AAG edges are created based on the topological relationship between surfaces and edges.

(3) Add model surface attribute information. Traverse AAG nodes and add their attribute information.

(4) Add model edge attribute information. Traverse AAG edges and add their attribute information.

Based on the preceding research on model information extraction and AAG construction, the serialization of model AAG is realized by building structure arrays and assigning values to the structure members. The main steps are as follows:

(1) Access the structure arrays surface [], edge [], and contour [], which were assigned in the previous information extraction.

(2) Construct node structure array node [] and line structure array line [], and establish the corresponding relationship between surface [] and node [] and between edge [] and line [].

(3) Traverse and extract the data in surface [], and define the relevant attributes of node []. The data in edge [] is extracted to define the relevant attributes of the node connection line [].

After the above operations, the model AAG is serialized in the form of a structure array, and its pseudo-code is shown in Appendix A Algorithm A2.

#### 4.2. AAG Decomposition and Reconstruction Based on DBS and JBS

The essence of machining feature recognition based on AAG is to search for isomorphic subgraphs matching predefined features in model AAG [49]. Graph matching is a typical NP-complete problem. So far, there is no suitable method to solve it. The usual countermeasure is to decompose the AAG and then match the subgraphs obtained after decomposition with predefined features. In most of the previous studies, AAGs are decomposed according to the concavity–convexity of the model edges, which has high accuracy for concave feature recognition. However, for convex features, it is not ideal.

An AAG decomposition and reconstruction algorithm based on DBS and JBS is proposed. According to the node attributes, AAG is decomposed to realize the recognition of various features, and the features with the same JBS are reconstructed into subgraphs to merge the segmented features. The basic principle is as follows. AAG is searched for nodes with DBS attributes, and according to the concavity–convexity attributes of the inner contour edges, the subgraphs with concave and convex features are extracted respectively. It is further judged whether the convex feature subgraphs still contain concave feature subgraphs, and the nodes corresponding to the non-machining surfaces in the remaining AAG are deleted. The MCCS with the FBS attribute is extracted. Finally, the nodes with JBS attributes are searched and merged to realize the subgraph reconstruction within the model. The main steps are as follows.

(1) AAG decomposes based on DBS. Traverse AAG to find DBS in the model and delete the inner contour on it. If the edge of the inner contour is a convex edge, the decomposed subgraph is merged into the concave feature subgraph set MAAG. Otherwise, the subgraph is merged into the convex feature subgraph set TAAG.

(2) If a concave edge exists in the convex feature subgraph TAAG-*i*, the MCCS CAAG-*i* is extracted with the adjacent face of the edge as the starting node, and CAAG-*i* and the remaining graphs are merged into the feature subgraph set MAAG. Otherwise, TAAG-*i* is set as an independent feature and is merged into the feature subgraph set MAAG.

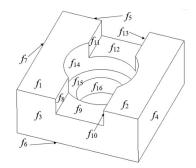
(3) Delete the surface of the non-machining feature. AAG is updated to AAG-1, and the node with the convex surface attribute in AGG-1 and the edges connected with this node are deleted.

(4) AAG decomposes based on FBS. AAG-1 is updated to AAG-2, the nodes with FBS attribute are taken as start nodes, and the MCCS is extracted, which is put into the feature subgraph set MAAG.

(5) Subgraph reconstructs based on JBS. Search for nodes with the same JBS attribute in the feature subgraph set MAAG and merge them to obtain the reconstructed feature subgraph.

The pseudo-code of the preceding algorithm is shown in Appendix A Algorithm A3.

Taking the model shown in Figure 12 as an example, the process of AAG decomposition and reconstruction based on DBS and JBS will be described. According to the method in Section 4.2, its AAG is constructed as shown in Figure 13. There are 16 nodes and 35 lines in the graph, which represent the number of model surfaces and edges, respectively. The numbers on the line represent the edge concavity–convexity, "1" represents the convex edge, and "-1" represents the concave edge. The red lines represent the inner contour edge attribute, the red nodes represent FBS attribute, the orange nodes represent DBS attribute, and the green nodes represent JBS attribute.



**Figure 12.** MBD model. Where,  $f_1$ - $f_{16}$  represent the 16 surfaces of the model.

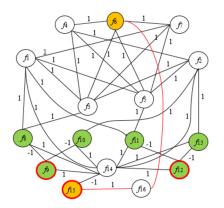
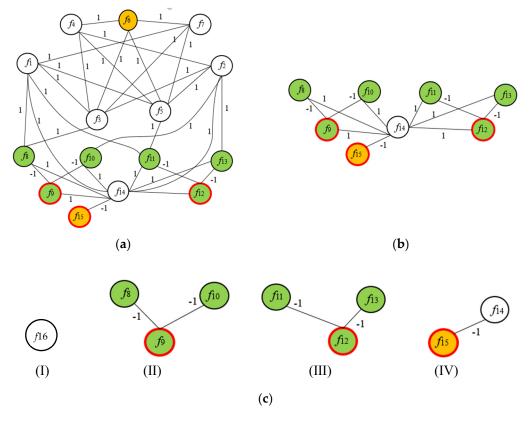


Figure 13. Model AAG.

The AAG decomposition process of the above model is shown in Figure 14. First, search for the nodes with DBS attribute, which are  $f_{15}$  and  $f_6$ . Search for lines that are connected to  $f_{15}$  and  $f_6$  and have inner contour attributes, which are the two red lines in the AAG, and delete them. Since  $f_6$  has convex edge attribute, the subgraph (I) is composed of a single node  $f_6$ , which is a concave characteristic subgraph. Then, update AAG to get AAG-1, as shown in (a). Delete the node with the convex attribute in AAG-1 and the line connected with the node, and update to get AAG-2, as shown in (b). Search AAG-2 for nodes with FBS attribute, which are  $f_9$ ,  $f_{12}$ , and  $f_{15}$ . Finally, the MCCSs of nodes  $f_9$ ,  $f_{12}$ , and  $f_{15}$  are extracted, respectively, to obtain the feature subgraph (II) composed of nodes  $f_8$ ,  $f_9$ , and  $f_{10}$ ; the feature subgraph (III) composed of nodes  $f_{14}$  and  $f_{15}$ . After decomposition, a total of four feature subgraph (IV) composed of nodes  $f_{14}$  and  $f_{15}$ . After decomposition, a total of four feature subgraphs are obtained, as shown in (c), which are the through-hole feature where  $f_{16}$  is located, the blind-hole feature where  $f_{15}$  is located.



**Figure 14.** AAG decomposition based on DBS. (**a**) shows the updated AAG-1; (**b**) shows the updated AAG-2; (**c**) shows the four decomposed subgraphs.

Surface  $f_9$  and  $f_{12}$  are JBSs, and they will generally be processed as a feature when machining. However, it is now divided due to the intersection of features, so two feature subgraphs are generated through the decomposition of AAG. According to the AAG reconstruction method based on JBS described above, it is found that three groups of nodes,  $f_8$  and  $f_{11}$ ,  $f_9$  and  $f_{12}$ , and  $f_{10}$  and  $f_{13}$ , have the same JBS attribute. Through subgraph reconstruction, the two features corresponding to nodes  $f_8$ ,  $f_9$ ,  $f_{10}$  and  $f_{11}$ ,  $f_{12}$ ,  $f_{13}$  are merged into one through slot feature, as shown in Figure 15.

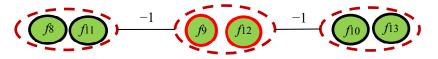


Figure 15. Subgraph reconstruction based on JBS.

#### 4.3. Machining Feature Matching Based on AAM

Generally, feature matching is accomplished by the isomorphism of graphs. Its principle is as follows: after the decomposition of AAG, the feature subgraph is isomorphically matched with the predefined features. If the two have the same topology, it indicates that the feature matching is successful, and the feature object is recognized as the corresponding processing feature; if the matching fails, the feature type is undefined or does not exist. In order to overcome the shortcomings of the existing feature matching methods, a machining feature matching method based on AAM is proposed.

#### 4.3.1. Machining Feature Matching Method Based on AAM

Aiming at the problem of feature matching, a feature matching algorithm based on AAM is proposed. The decomposed feature subgraph is constructed as AAM and matched with the predefined feature to realize the recognition of machining features. The advantage

of this method is that it only needs to match the features of the constituent elements of AAM and avoids the similarity transformation of AAM.

The AAM constructed by AAG is a square matrix whose order is equal to the number of nodes in the feature subgraph. Diagonal elements represent the attributes of nodes in the feature subgraph, and non-diagonal elements represent the attributes of edges in the feature subgraph. The AAM of a feature subgraph is shown in Formula (2).

$$M[n][n] = \begin{bmatrix} m_{11} & m_{12} & \cdots & m_{1n} \\ m_{21} & m_{22} & \cdots & m_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ m_{n1} & m_{n2} & \cdots & m_{nn} \end{bmatrix}$$
(2)

where, *n* represents the number of nodes of the feature subgraph,  $m_{ij}$  ( $i \neq j$ ) indicates the attribute of edge,  $m_{ii}$  indicates the attribute of the node.

The node attribute is composed of concavity–convexity, type, and FBS attribute of the surface. It is expressed as a positive integer containing three digits. It is recorded as  $m_{ii} = abc$ , and the values of each attribute are shown in Formulas (3)–(5).

$$a = \begin{cases} 1 & \text{Convexity surface} \\ 0 & \text{Concavity surface} \end{cases}$$
(3)

$$b = \begin{cases} 1 & \text{Planar plane} \\ 2 & \text{Cylinder} \\ 3 & \text{conical surface} \\ 4 & \text{other surface} \end{cases}$$
(4)

$$c = \begin{cases} 1 & \text{FBS} \\ 2 & \text{Non FBS} \end{cases}$$
(5)

The edge attribute consists of concavity–convexity and the type of the edge, which is represented by a positive integer containing two digits and is recorded as  $m_{ij} = de$ . The values of each attribute are shown in Formulas (6) and (7).

$$d = \begin{cases} 1 & \text{Concavity edge} \\ 2 & \text{Convexity edge} \\ 3 & \text{smooth edge} \end{cases}$$
(6)

$$e = \begin{cases} 1 & \text{Staight edge} \\ 2 & \text{Arc edge} \\ 3 & \text{other edge} \end{cases}$$
(7)

The node and edge attributes are stored in the structure array node [][] and line [][], respectively. Node attribute can be assessed through node [][].node\_at, node[][].node\_ type and node[][].node\_ f\_face. Edge attribute can be obtained through line[][].line\_ at and line[][].line\_type.

If the geometric information and topological structure of the nodes and edges in the predefined feature and feature subgraph are the same, it means that they match, which should meet the requirement of the same order of the matrix, same diagonal elements, and the similarity of each row element set. The similarity of each row element set means that each row element of the AAM of the feature subgraph has a one-to-one mapping relationship with each row element of the predefined AAM.

The main process of the AAM-based feature matching algorithm is as follows.

(1) Judge whether the order of the feature subgraph AAM and the predefined AAM are the same.

(2) Judge whether diagonal elements are equal.

(3) Judge whether the sets formed by each row element are similar. If any of the conditions are not met, the matching is unsuccessful.

(4) If the matching is not successful, the sub-feature is exported, and whether they are machining features will be judged by human–computer interaction. If so, they will be added to the predefined feature library.

Table 5 shows typical machining features and their predefined AAMs, in which the green area is the machining feature. The algorithm in this paper can effectively identify through hole, blind-hole, closed key slot, open key slot, through groove, cylinder extrusion, blind groove, step, and other machining features.

No.	Feature Name	Graphical Representation	AAM
1	Through-hole		[220]
2	Blind-hole		$\begin{bmatrix} 220 & 21 \\ 21 & 110 \end{bmatrix}$
3	Closed key slot		$\begin{bmatrix} 220 & 13 & 0 & 13 & 21 \\ 13 & 210 & 13 & 0 & 11 \\ 0 & 13 & 220 & 13 & 21 \\ 13 & 0 & 13 & 210 & 11 \\ 21 & 11 & 21 & 11 & 110 \end{bmatrix}$
4	Open key slot		$\begin{bmatrix} 110 & 11 & 21 & 11 \\ 11 & 210 & 13 & 0 \\ 21 & 13 & 220 & 21 \\ 11 & 0 & 21 & 210 \end{bmatrix}$
5	Through groove		$\begin{bmatrix} 210 & 11 & 0 \\ 11 & 110 & 11 \\ 0 & 11 & 210 \end{bmatrix}$
6	Cylinder extrusion		$\begin{bmatrix} 111 & 22\\ 22 & 221 \end{bmatrix}$
7	Blind groove		$\begin{bmatrix} 210 & 11 & 0 & 11 \\ 11 & 110 & 11 & 11 \\ 0 & 11 & 210 & 11 \\ 11 & 11 & 11 & 110 \end{bmatrix}$
8	Step		$\begin{bmatrix} 210 & 11\\ 11 & 210 \end{bmatrix}$
9	Rectangular blind cavity		$\begin{bmatrix} 210 & 11 & 0 & 11 & 11 \\ 11 & 210 & 11 & 0 & 11 \\ 0 & 11 & 210 & 11 & 11 \\ 11 & 0 & 11 & 210 & 11 \\ 11 & 11 & 11 & 11 & 110 \end{bmatrix}$
10	Rectangular through cavity		$\begin{bmatrix} 210 & 11 & 0 & 11 \\ 11 & 210 & 11 & 0 \\ 0 & 11 & 210 & 11 \\ 11 & 0 & 11 & 210 \end{bmatrix}$

Table 5. Typical machining features.

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#### 4.3.2. AAM Establishment Algorithm

For a characteristic subgraph t, the structure arrays of the nodes and edges are node[t][n] and line[t][n]. Traverse the members of the node array node[][].node\_at,

node[][].node\_type and node[][].node\_f\_face and get the node properties. Traverse the edge array members line[][].line\_ at and line[][].line\_type and get the edge properties. The establishment process of AAM is shown in Figure 16.

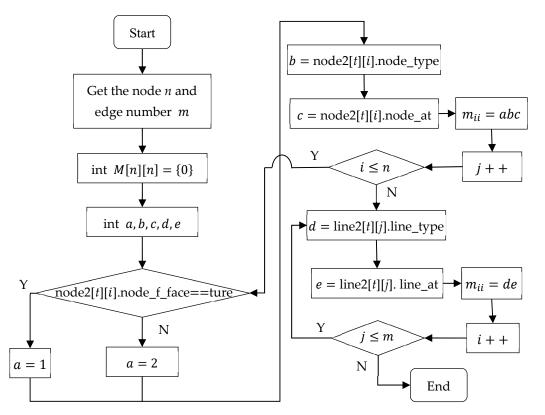


Figure 16. The AAM construction process.

The main steps are as follows, and the pseudo-code of the algorithm is shown in Appendix A Algorithm A4.

(1) Access the data of line2[t][] and node2[t][], and define matrix M[n][n], and assign the initial value of each element to 0.

(2) Determine the value of m<sub>ii</sub>. If node2[t][i].node\_f\_face = true, then a = 1. If node2[t][i].node\_f\_face = false, then a = 2. Determine the value of b as follows: b = node2[t][i].node\_type. Determine the value of c as follows: c = node2[t][i].node\_at.
(3) Assign the data of m<sub>ii</sub> as follows: d = line2[t][j].line\_type and e = line2[t][j].line\_at.

#### 4.3.3. AAM Matching Algorithm

A matching method of feature subgraph AAM and predefined feature AAM is proposed. The feature subgraph AAM to be matched is represented by matrix A[n][n], and the predefined feature AAM is represented by matrix B[m][m]. The main process of matching between them is as follows.

(1) If n = m, go on; otherwise, the matching is unsuccessful.

(2) Define set  $S_1$  and  $S_2$ , and assign the values of diagonal elements of A[n][n] to  $S_1$ , and the value of B[m][m] diagonal element to  $S_2$ . If  $S_1 = S_2$ , go on; otherwise, the matching is not successful.

(3) Define set  $S_{Ai}$  and  $S_{Bj}$  and assign the valve of No.*i* row of a [*n*] [*n*] to set  $S_{Ai}$ , the valve of No.*j* row of a [*n*] [*n*] to set  $S_{Bj}$ . If each set  $S_{Ai}$  can find the set  $S_{Bj}$  that is equal to it and does not repeat, the matching is successful and the machining feature is recognized; otherwise, the matching is unsuccessful.

The flow chart of feature subgraph matching is shown in Figure 17, and the pseudocode of the algorithm is shown in Appendix A Algorithm A5.

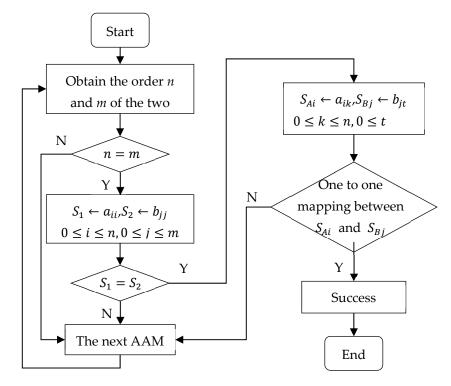


Figure 17. AAM matching process.

#### 5. Decision Making of Feature Processing Scheme Based on Fuzzy Comprehensive Evaluation

The determination of the feature processing scheme is a complex decision-making process and also the premise of process route optimization. Based on the recognition of MBD model machining features, a feature processing scheme decision method based on fuzzy comprehensive evaluation is proposed. By analyzing the influencing factors of processing scheme selection, the mapping relationship between the influencing factors and processing schemes is established. A multi-factor comprehensive evaluation model is established according to the single-factor evaluation results. By calculating the comprehensive evaluation index vector, the optimization of feature processing schemes is realized. The processing scheme decision-making process based on fuzzy comprehensive evaluation is shown in Figure 18. The main steps are as follows:

(1) Establish the factor set that affects the decision-making of the processing scheme. The set is shown as follows

$$U = \{u_1, u_2, \cdots, u_i\} \tag{8}$$

where,  $u_i$  is the No.*i* factor affecting the evaluation object.

(2) Determine the weight of each influencing factor. In the evaluation of processing methods, the importance of each influencing factor is different. The weight of the influencing factor  $u_i$  is expressed as  $w_i$ . Therefore, the weight set of influencing factors is established as shown in the following formula

$$W = \{w_1, w_2, \cdots, w_i\} \tag{9}$$

(3) Establish an alternative set of processing schemes. The alternative set of processing schemes is the set of all possible results of the evaluation object.

(4) Single-factor fuzzy evaluation. The fuzzy comprehensive evaluation matrix R is obtained according to the fuzzy relationship matrix between each influencing factor and the alternative set of the processing scheme.

(5) Calculate the fuzzy comprehensive evaluation index vector  $B = W \cdot R$ . Select the largest evaluation index  $b_i$  as the final result.

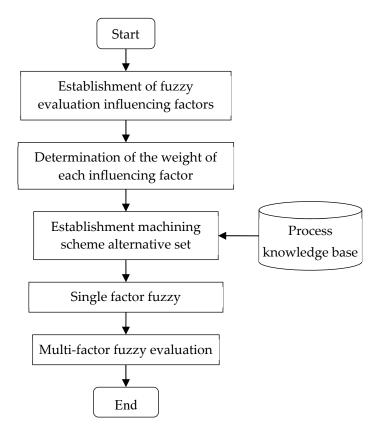


Figure 18. Decision of feature processing method based on fuzzy comprehensive evaluation.

According to the process characteristics of parts, the features are divided into face features and hole features. We take face features as an example and carry out fuzzy comprehensive evaluation of feature processing schemes on the basis of studying its single factor fuzzy evaluation.

#### 5.1. Establishment of Alternative Sets for Fuzzy Evaluation of Surface Features

The main influencing factors of the surface feature process scheme include workpiece material, feature type, processing accuracy, roughness, and other process requirements. The fuzzy evaluation influencing factor set is shown in the following formula

$$U_1 = \{M, F, IT, R_a\} \tag{10}$$

where, *M* stands for workpiece material, *F* stands for feature type, *IT* stands for machining accuracy and  $R_a$  stands for surface roughness. The workpiece material *M* is specifically expressed as:

$$M = \{m_1, m_2, m_3\} \tag{11}$$

where,  $m_1 \sim m_3$  represent steel, cast iron, and non-ferrous metals, respectively. Feature type *F* is represented by the set shown in the following formula

$$F = \{f_1, f_2, f_3, f_4, f_5, f_6, f_6\}$$
(12)

where,  $f_1 \sim f_6$  denote plane, step, blind step, through groove, blind groove, cavity, and boss, respectively.

The alternative set of fuzzy evaluation of feature processing schemes is the set of all possible feature processing schemes. The type, processing size, material, and accuracy requirements of features are the main factors to be considered in formulating processing schemes. The typical processing scheme set of surface processing features is shown in Table 6.

No.	Processing Scheme	Machining Accuracy	Surface Roughness <i>Ra</i> /µm	Scope of Application
1	Rough planing	IT11~13	12.5~50	
2	Rough planing—fine planing Rough planing—fine	IT8~10	3.2~6.3	Plane processing of ferrous and nonferrous metals
3	planing—wide blade fine planing	IT6~7	0.8~1.6	
4	Rough milling	IT11~13	6.3~25	Plane, through groove, step, and
5	Rough milling—finish milling	IT8~10	1.6~6.3	other features of ferrous and non-ferrous metals
6	Rough milling—finish milling—fine grinding	IT6~7	0.8~1.6	Plane of ferrous metal

Table 6. Typical processing scheme of surface features.

A fuzzy evaluation candidate set of face features is established according to the above processing scheme, as shown below

$$X = \{x_1, x_2, x_3, x_4, x_5, x_6\}$$
(13)

where,  $x_1 \sim x_6$  represent typical processing schemes of surface features, which are rough planing, rough planing fine planing, rough planing fine planing, rough milling, rough milling, rough milling, rough milling fine milling, rough milling fine milling.

### 5.2. Determination of Weight of Each Influencing Factor

In order to ensure the objectivity of the weights of the influencing factors of fuzzy evaluation, the method of combining the Analytic Hierarchy Process (AHP) and expert consultation [50] is used to establish the weight set of the influencing factors of area characteristics, as shown below

$$W = \{w_1, w_2, w_3, w_4\}$$
(14)

where,  $w_1 \sim w_4$  represent the weight of processing material, feature type, processing accuracy, surface roughness, and  $\sum_{i=1}^{4} w_i = 1$ .

Because each factor has a different influence on the feature processing scheme, according to the scale of AHP shown in Table 7, a comparison matrix A of surface features is established, as shown in Formula (15).

$$\begin{bmatrix} a_{ij} \end{bmatrix}_{4 \times 4} = \begin{bmatrix} 1 & 2 & 3 & 3 \\ \frac{1}{2} & 1 & 3 & 3 \\ \frac{1}{3} & \frac{1}{3} & 1 & 1 \\ \frac{1}{3} & \frac{1}{3} & 1 & 1 \end{bmatrix}$$
(15)

where,  $a_{ij} = C_i / C_j$ ,  $a_{ij} > 0$ ,  $a_{ij} = 1 / a_{ij}$ .

Table 7. Scale table
----------------------

Scale Value	Meaning
1	$C_i$ is as important as $C_i$
3	$C_i$ is slightly more important than $C_j$
5	$C_i$ is more important than $C_j$
7	$C_i$ is significantly more important than $C_i$
9	$C_i$ is extremely more important than $C_i$
2, 4, 6, 8	Preceding adjacent median
Reciprocal of scale value	Contrary to the above comparison between $C_i$ and $C_j$

In order to ensure the rationality of the comparison matrix, the consistency test is carried out. The consistency verification ratio *CR* of the comparison matrix is shown as follows

$$CR = CI/RI \tag{16}$$

where, CI is the consistency index of comparison matrix, which is defined as follows

$$CI = (\lambda - n)/(n - 1) \tag{17}$$

where, *n* is the order of the comparison matrix, and *RI* is the random consistency index. The values of RI are shown in Table 8.

Table 8. Random consistency index.

п	1	2	3	4	5	6	7	8	9
RI	0	0	0.58	0.90	1.12	1.24	1.32	1.41	1.51

If CR < 0.1, it is considered that the consistency of the comparison matrix is satisfactory, and its normalized eigenvector can be used as the weight vector. Through calculation, the maximum eigenvalue of the comparison matrix A of surface features is 5.0606, and the consistency verification ratio of its comparison matrix *CR* is 0.0224, which is less than 0.1. Therefore, the consistency is satisfactory. Normalize the feature vector of a to obtain the weight set of influencing factors  $W = \{0.444, 0.312, 0.122, 0.122\}$ .

#### 5.3. Single Factor Fuzzy Mapping of Machining Schemes for Surface Features

For surface feature processing schemes, according to the set of influencing factors for fuzzy evaluation, a fuzzy mapping relationship model with each influencing factor is established, as shown in Figure 19.

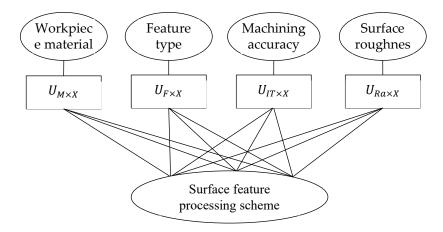


Figure 19. Fuzzy mapping model between machining scheme and influencing factors.

In the preceding figure,  $U_{M \times X}$ ,  $U_{F \times X}$ ,  $U_{IT \times X}$ , and  $U_{Ra \times X}$  are the fuzzy relations between workpiece material, feature type, machining accuracy, surface roughness, and surface feature machining scheme.

#### 5.3.1. Fuzzy Mapping between Workpiece Material and Machining Schemes

According to the application scope of the machining scheme of each surface feature, the corresponding relationship between the workpiece material and the machining scheme is shown in Table 9.

No.	$x_1$	<i>x</i> <sub>2</sub>	<i>x</i> <sub>3</sub>	$x_4$	<i>x</i> <sub>5</sub>	<i>x</i> <sub>6</sub>
$m_1$		$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	
$m_2$	$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$		$\checkmark$
$m_3$	$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	$\checkmark$	

Table 9. Correspondence between workpiece material and surface feature processing scheme.

When the workpiece material  $m_i$  can be processed by the processing scheme  $x_j$ , the membership degree of  $(m_i, x_j)$  is set to 1; otherwise, it is set to 0. According to the preceding correspondence, the fuzzy mapping expression between the material type and the surface feature processing scheme is obtained, as shown below

$$f_{M\times X}(m_i, x_j) = \begin{cases} f_{M\times X}(m_1, x_j) = \left\{ \frac{1}{x_1}, \frac{1}{x_2}, \frac{1}{x_3}, \frac{1}{x_4}, \frac{1}{x_5}, \frac{1}{x_6} \right\} \\ f_{M\times X}(m_2, x_j) = \left\{ \frac{1}{x_1}, \frac{1}{x_2}, \frac{1}{x_3}, \frac{1}{x_4}, \frac{1}{x_5}, \frac{1}{x_6} \right\} \\ f_{M\times X}(m_3, x_j) = \left\{ \frac{1}{x_1}, \frac{1}{x_2}, \frac{1}{x_3}, \frac{1}{x_4}, \frac{1}{x_5}, \frac{0}{x_6} \right\} \end{cases}$$
(18)

From the above formula, the fuzzy relationship between the workpiece material set M and the surface feature machining scheme set X can be obtained, which is represented by fuzzy matrix  $R_{M \times X}$ , as shown in Equation (19).

where,  $r_{ij} = \mu_{M \times X}(m_i, x_j)$  indicates the possibility of selecting a processing scheme  $x_j$  when the workpiece material is  $m_i$ .

#### 5.3.2. Fuzzy Mapping between Feature Types and Machining Schemes

The corresponding relationship between the feature types and the processing schemes of the features of each surface is shown in Table 10.

Table 10. Correspondence between feature type and surface feature processing scheme.

No.	$x_1$	<i>x</i> <sub>2</sub>	<i>x</i> <sub>3</sub>	$x_4$	$x_5$	<i>x</i> <sub>6</sub>
$f_1$	$\checkmark$	$\checkmark$	$\checkmark$		$\checkmark$	
$f_2$	$\checkmark$	$\checkmark$	$\checkmark$			$\checkmark$
<i>f</i> 3 <i>f</i> .	/	/	/			/
14 f5	V	V	V			V
$f_6$				$\sqrt[4]{}$	$\sqrt[v]{}$	
$f_7$				$\checkmark$	$\checkmark$	

When the processing feature of type  $f_i$  can be processed with processing scheme  $x_j$ , the membership degree of  $(f_i, x_j)$  is set to 1; otherwise, it is set to 0. According to the corresponding relationship, the fuzzy mapping expression between the feature type and the surface feature processing scheme is obtained, as shown below.

$$\begin{cases} f_{F \times X}(f_1, x_j) = \begin{cases} \frac{1}{x_1}, \frac{1}{x_2}, \frac{1}{x_3}, \frac{1}{x_4}, \frac{1}{x_5}, \frac{1}{x_6} \\ f_{F \times X}(f_2, x_j) = \begin{cases} \frac{1}{x_1}, \frac{1}{x_2}, \frac{1}{x_3}, \frac{1}{x_4}, \frac{1}{x_5}, \frac{1}{x_6} \\ f_{F \times X}(f_3, x_j) = \begin{cases} \frac{0}{x_1}, \frac{0}{x_2}, \frac{0}{x_3}, \frac{1}{x_4}, \frac{1}{x_5}, \frac{0}{x_6} \\ f_{F \times X}(f_4, x_j) = \begin{cases} \frac{1}{x_1}, \frac{1}{x_2}, \frac{1}{x_3}, \frac{1}{x_4}, \frac{1}{x_5}, \frac{1}{x_6} \\ f_{F \times X}(f_5, x_j) = \begin{cases} \frac{0}{x_1}, \frac{0}{x_2}, \frac{0}{x_3}, \frac{1}{x_4}, \frac{1}{x_5}, \frac{0}{x_6} \\ f_{F \times X}(f_6, x_j) = \begin{cases} \frac{0}{x_1}, \frac{0}{x_2}, \frac{0}{x_3}, \frac{1}{x_4}, \frac{1}{x_5}, \frac{0}{x_6} \\ f_{F \times X}(f_7, x_j) = \begin{cases} \frac{0}{x_1}, \frac{0}{x_2}, \frac{0}{x_3}, \frac{1}{x_4}, \frac{1}{x_5}, \frac{0}{x_6} \\ \frac{0}{x_1}, \frac{0}{x_2}, \frac{0}{x_3}, \frac{1}{x_4}, \frac{1}{x_5}, \frac{0}{x_6} \\ \end{cases} \end{cases} \end{cases}$$
(20)

According to Formula (20), the fuzzy relationship between the feature type set *F* and the surface feature processing scheme set *X* can be obtained, which is expressed by the fuzzy matrix  $R_{F \times X}$ , as shown below

where,  $r_{ij} = \mu_{F \times X}(f_i, x_j)$ , which indicates the possibility of selecting machining scheme  $x_j$  when the machining feature type is  $f_i$ .

5.3.3. Fuzzy Mapping between Machining Accuracy and Machining Schemes

The machining accuracy range of feature machining scheme  $x_j$  is  $ITn \sim ITm$ , n < m. The following assumptions are made in this paper:

(1) When *IT* is less than ITn - 2, the scheme  $x_j$  cannot meet the processing requirements, so the possibility of scheme selection is 0.

(2) When *IT* is greater than *ITm*, although this scheme can meet the processing requirements, its economy is poor, so the possibility of selecting this scheme is 0.

(3) When *IT* is in the range of  $ITn - 2 \sim ITn$ , the possibility of selecting this scheme is 0.8~1.

(4) When *IT* is in the range of  $ITn \sim ITm$ , the possibility of selecting this scheme is 1.

The membership function of the fuzzy mapping between the machining accuracy and the scheme is defined using the piecewise function method, as shown in Formula (22).

$$\mu(IT, x_j) = \begin{cases} 0 & IT < ITn - 2\\ 1 - \frac{(ITn - IT)}{5(ITm - ITn)} & ITn - 2 \le IT < ITn\\ 1 & ITn \le IT \le ITm\\ 0 & IT > ITm \end{cases}$$
(22)

According to  $\mu(IT, x_j)$ , the fuzzy relationship between the machining accuracy *IT* and the surface feature machining scheme set *X* is obtained, which is expressed by the fuzzy matrix  $R_{IT \times X}$ , as shown below

$$R_{IT \times X} = \left[ r_{1j} \right]_{1 \times 6} \tag{23}$$

where,  $r_{1j}$  represents the possibility of selecting the machining scheme  $x_j$  when the machining feature accuracy requirement is *IT*.

#### 5.3.4. Fuzzy Mapping between Surface Roughness and Machining Scheme

When the surface roughness is greater than the upper limit of the roughness obtained by the machining scheme, the machining scheme cannot meet the requirement, and the selectivity of the machining scheme is 0. When the surface roughness is between the upper and lower limits of the scheme roughness, the processing scheme can meet the requirements, and the optional range of the scheme is 0.8~1. When the surface roughness is less than the lower limit of the scheme roughness, the machining scheme can meet the requirements, but the economy is reduced, so its selectivity is zero. The membership function of the surface roughness is shown below

$$(R_a, x_j) = \begin{cases} 0 & R_a < a \\ 1 - \frac{(logb - logR_a)}{5(logb - loga)} & a \le R_a \le b \\ 0 & R_a > b \end{cases}$$
(24)

where,  $R_a$  is the surface roughness required by the machining feature, a is the minimum roughness that can be achieved by the machining scheme, and b is the maximum. Since the surface roughness standard series is approximately an equal ratio series, and its common ratio is  $\sqrt{10}$ , the logarithm of the surface roughness value is taken [25].

According to the membership function of the surface roughness  $\mu(R_a, x_j)$ , the fuzzy relationship between the surface roughness and the processing scheme set *X* can be obtained, which is expressed by the fuzzy matrix  $R_{Ra \times X}$ , as shown below

$$R_{Ra \times X} = \left[ r_{1j} \right]_{1 \times 6} \tag{25}$$

where,  $r_{1j}$  represents the possibility of selecting the machining scheme  $x_j$  when the machining surface roughness requirement is Ra.

#### 5.4. Fuzzy Comprehensive Evaluation of Feature Processing Scheme

The fuzzy comprehensive evaluation of feature machining scheme is a decisionmaking process of the machining scheme, which comprehensively considers various influencing factors. According to the fuzzy relation matrix of each single-factor, the final fuzzy comprehensive evaluation matrix can be obtained, as shown in Equation (26).

$$R = [R_M, R_F, R_{IT}, R_{Ra}]^T$$
(26)

where,  $R_M$  is workpiece material fuzzy matrix,  $R_F$  is feature type fuzzy matrix,  $R_{IT}$  is machining accuracy fuzzy matrix, and  $R_{Ra}$  is surface roughness fuzzy matrix.

The calculation of fuzzy comprehensive evaluation index vector is shown in Formula (27).

$$B = W \cdot R \tag{27}$$

where, *W* is weight vector of influencing factors and *R* is fuzzy comprehensive evaluation matrix.

According to the calculation results, the candidate set element corresponding to the maximum evaluation index  $b_i$  is selected as the processing scheme. The pseudo-code of the feature processing scheme decision algorithm based on fuzzy comprehensive evaluation is shown in Appendix A Algorithm A6.

#### 6. Process Route Optimization Based on MEDGraph

The process route optimization of the feature machining scheme is a problem of optimizing the Machining Element (ME) sequence. On the basis of analyzing the constraint relationship among the MEs, a model machining process route optimization method based on MEDGraph is proposed. First, MEDGraph is established based on the constraint relationship among the MEs, and then the topology sequence of all the MEs is listed by the improved topology sorting algorithm. Finally, the evaluation function is constructed with the machining cost or efficiency as the optimization objective to obtain the optimal process route.

#### 6.1. Description of Process Route Optimization Problem

The optimization of the process route is to sort the processes in the machining scheme according to the process rules and optimization objectives and obtain the optimal or near-optimal processing route. A part to be machined can be regarded as a set of multiple machining features. It is assumed that a part has n machining features, which is represented as follows

$$Part = \{f_1, f_2, \cdots, f_n\}$$
(28)

where,  $f_i$  is the No.*i* machining feature in the part.

Each machining feature is usually formed through a plurality of processes, which correspond to the machining scheme of the machining feature. Dou et al. [40] defines the information entities related to feature processing as ME, which is represented as a six tuple, as shown below

$$me = (ID, f_i, S, M, T, TAD)$$
<sup>(29)</sup>

where, *ID* is the ME number;  $f_i$  is the characteristics processed by ME; *S* is the processing name, such as rough turning and fine turning; *M* is the machine tool used for processing; *T* is the required tools; and *TAD* is the tool approach direction.

The machining process of a part can be expressed as a set of MEs, as shown below

$$ME = \{me_1, me_2, \cdots, me_n\}$$
(30)

where, *me<sub>i</sub>* is the No.*i ME* in the processing element set.

On the basis of the preceding definition, the optimization of the process route is transformed into the optimization of the processing elements sorting in *ME*. That is, the evaluation function is established with the processing cost or production efficiency as the optimization objective, and the processing element ranking result with the best target value is obtained under the condition that the relevant process rules are met.

Structure array me[] is constructed, which is used to store relevant information of processing elements. Its members include me\_id, stage, TAD, feature\_id, operation\_name, t\_id, and m\_id, which are used to store ME ID, processing stage, TAD, machined feature, processing name, tool ID, and machine ID, respectively. Among them, the processing stages to which the processing element belongs are represented by 1, 2, 3, and 4, which are rough processing, semi-finishing, finish processing, and finishing processing, respectively.

#### 6.2. The Construction of MEDGraph

In order to ensure the processing quality, the formulation of the process route needs to comply with the relevant rigid process rules and give priority to meeting the additional rules. Rigid process rules are mainly as follows: benchmark first, rough machining before finish machining, surface machining before hole, and process the main surface first and then the other surface. Additional rules are recommended rules during processing, mainly including: (1) Adjacency rule. The process execution sequence of certain machining features is preferably adjacent. (2) Clustering rules. Features on the same surface, features of the same type, or features that need to be processed with the same tool are best arranged for processing together.

Based on the constraint relationship between the processing elements, the process flow represented by the directed graph is called Machining Element Directed Graph (MED-Graph) [51], which is defined as

$$G = (V, E) \tag{31}$$

where, *V* is the node of the digraph, representing the MEs set, and its definition is shown as Formula (32); *E* is the set of directed edges, which indicates the priority relationship between MEs. Its definition is shown as Formula (33).

$$V = ME = \{me_0, me_1, me_2, \cdots, me_n\}$$
(32)

$$E = \left\{ e(me_i, me_j) \middle| 0 \le i, j \le n, i \ne j \right\}$$
(33)

The processing element directed graph is established according to the constraint relationship between processing elements. The establishment process is as follows: traverse all processing elements, randomly select two of them, create corresponding nodes, judge the constraint relationship between the two processing elements, and create a directed edge between nodes according to their priority order until all processing elements have created corresponding nodes. The process element digraph is represented by an adjacency matrix, and its definition is shown in Equation (34).

$$\mathbf{E}[n][n] = \begin{bmatrix} e_{11} & e_{12} & \dots & e_{1n} \\ e_{21} & e_{22} & \dots & e_{1n} \\ \vdots & \ddots & \vdots \\ e_{n1} & e_{n2} & \dots & e_{nn} \end{bmatrix}$$
(34)

where, *n* is the number of nodes in MEDGraph,  $e_{ii}$  is machining element  $me_i$ ,  $e_{ij}$  is the constraint relationship between  $me_i$  and  $me_j$ . The value rules of  $e_{ij}$  are as follows: when  $me_i$  takes precedence over  $me_j$ ,  $e_{ij} = 1$ ,  $e_{ji} = -1$ ; if there is no priority constraint relationship between  $me_i$  and  $me_j$ .

The construction process of the MEDGraph matrix is shown in Figure 20, and its main steps are as follows:

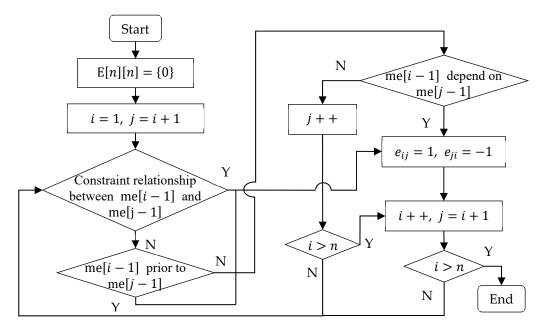


Figure 20. Construction of MEDGraph matrix.

(1) Assign an initial value of 0 to the element  $e_{ij}$  of E[n][n],  $1 \le i \le n$ ,  $1 \le j \le n$ .

(2) Let i = 1, j = i + 1, and judge whether there is a benchmark relationship between me[i-1].feature and me[j-1].feature If me[j-1].feature is based on me[i-1].feature, let  $e_{ij} = 1, e_{ji} = -1$ ; otherwise, go to (3).

(3) If me[i-1].stage < me[j-1].stage, let  $e_{ij} = 1$ ,  $e_{ji} = -1$ ; otherwise, go to (4).

(4) Judge whether there is a dependency between me[i-1].feature and me[j-1].feature. If me[j-1].feature depends on me[i-1].feature, let  $e_{ij} = 1$ ,  $e_{ji} = -1$ ; otherwise, go to step 5. (5) Let j + +, and return to (2) until j = n + 1 and go to (6).

(6) let i + i + j = i + 1, return to (2) until i = n + 1, and end the program.

#### 6.3. Acquisition of ME Topological Sequence Based on Improved Topology Sorting Algorithm

The MEDGraph constructed by the preceding method is a Directed Acyclic Graph (DAG). Using a topological sorting algorithm, all vertices in the DAG can be arranged into a linear sequence so that any pair of nodes u and v in the graph, if  $\langle u, v \rangle \in E(DAG)$ , u appears before v in the linear sequence. Such a linear sequence is called a topological sequence. The basic principles of the topology sorting algorithm are as follows: (1) select a node with a degree of 0 from the digraph and output it. (2) Delete this node and all directed edges from it from the directed graph. (3) Repeat the above steps until there are no more nodes with a degree of 0 in the digraph. The algorithm is shown in Figure 21.

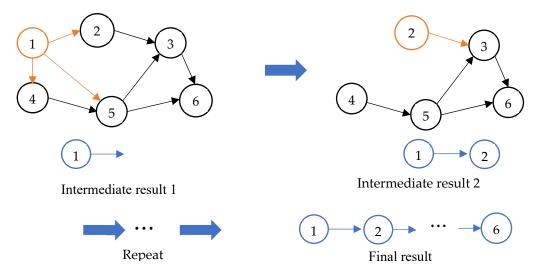


Figure 21. Topology sorting algorithm.

The results of the topological sorting of digraphs are not unique, and the conventional topological sorting algorithm can only obtain one result at random. By combining the topological sorting algorithm with the backtracking method, an improved topological sorting algorithm is proposed to obtain all the MEs topological sequences. The basic principle is as follows: after outputting a topological sequence, trace back to the previous node, and output nodes different from the previous topological sequence at this level. If there are no different nodes, continue to trace back to the previous level and finally realize the output of all topological sequences; its flow chart is shown in Figure 22, and the process is as follows:

(1) Read the MEDGraph.

(2) Find all the nodes in the current digraph with an indegree of 0, which constitute the node set S(j), and set the set index i = 0. Go to (3) if the set is not empty; otherwise, go to 4.

(3) If i < length(S(j)), take S(j)[i] as the value of the current topological sequence element result[j], and add 1 to i. Delete all the directional edges starting from result[j], and mark the deleted directional edges so that they can be recovered during backtracking. Return to (2) and continue to obtain the value of the current topology sequence element result[j + 1].

If i > length(S(j)), trace back to the last topological sequence element result[j - 1], and change its value to the next value in the corresponding set S(j - 1). Before using this value, recover all directed edges starting from S(j - 1)[n] and turn to (2). If n is equal to the number of elements in the set S(j - 1), the backtracking continues. Subtract 1 from j, and recover the deleted edge to obtain a new value. When j is equal to -1, it ends.

(4) If the number of elements in the current topology sequence is equal to the number of nodes, output it, go to (3), and continue to find other possible topology sequences.

Through the improved topological sorting algorithm, the topological sequence of all MEs is obtained.

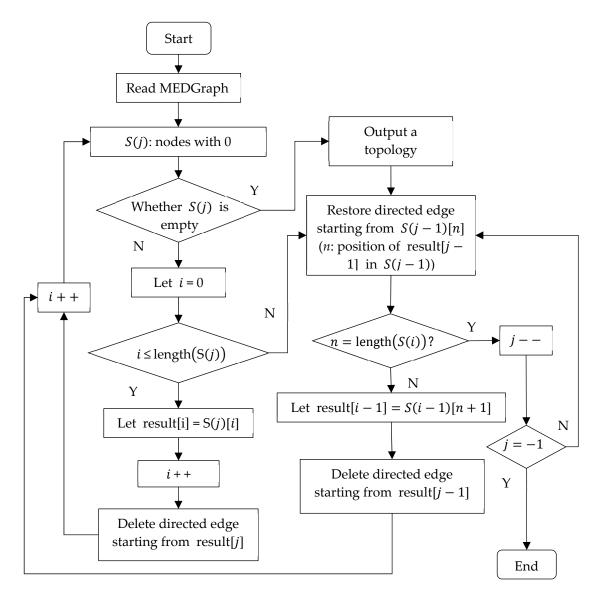


Figure 22. Improved topology sorting algorithm.

6.4. Acquisition of Optimal Machining Element Topological Sequence

All the ME topological sequences are obtained by using the improved topological sorting algorithm mentioned above, and each of them can be converted into a feasible process route. An optimal route will be selected according to cost, efficiency, and other factors. Therefore, it is necessary to build an evaluation function and select the optimal ME topological sequence according to the value of the function. Considering that frequent replacement of manufacturing resources in the machining process will increase process error and reduce quality and efficiency, the evaluation function of the processing element sequence is constructed with the minimum number of replacements of manufacturing resources as the optimization objective, as follows

$$F = \gamma_1 F_1 + \gamma_2 F_2 + \gamma_3 F_3 \tag{35}$$

where,  $F_1$ ,  $F_2$ , and  $F_3$  are machine tool transformation function, fixture transformation function, and tool transformation function, respectively, and  $\gamma_1$ ,  $\gamma_2$ , and  $\gamma_3$  are the weight coefficients of the above functions.

Different ME may use different machine tools, but frequent replacement of the machine tools during the machining process will increase the auxiliary time. At the same time, because the workpiece needs to be relocated when replacing the machine tool, the machining accuracy will be affected. The MEs using the same machine tool shall be arranged in adjacent positions as far as possible. The machine transformation function is defined as follows:

$$F_1 = \sum_{1}^{n-1} \partial_1(\text{me}[i].\text{m_id}, \text{me}[i+1].\text{m_id})$$
(36)

Similarly, different processing elements may use different fixtures and tools, and changing fixtures and tools will also increase auxiliary time and reduce accuracy. The processes using the same fixtures and tools shall be arranged in adjacent positions as far as possible. The fixture and tool transformation functions are shown in Formulas (37) and (38).

$$F_{2} = \sum_{1}^{n-1} \partial_{2}(\partial_{1}(\text{me}[i].\text{m_id}, \text{me}[i+1].\text{m_id}), \partial_{1}(\text{me}[i].\text{TAD}, \text{me}[i+1].\text{TAD}))$$
(37)

$$F_{3} = \sum_{1}^{n-1} \partial_{2}(\partial_{1}(\text{me}[i].\text{m_id}, \text{me}[i+1].\text{m_id}), \partial_{1}(\text{me}[i].\text{t_id}, \text{me}[i+1].\text{t_id}))$$
(38)

where,  $\partial(x, y)$  is defined as follows:

$$\partial_1(x,y) = \begin{cases} 1 \ x \neq y \\ 0 \ x = y \end{cases}$$
(39)

$$\partial_2(x,y) = \begin{cases} 1 & \text{other} \\ 0 & x = y = 0 \end{cases}$$
(40)

The pseudo-code for obtaining the optimal machining element sequence is shown in Appendix A Algorithm A7.

### 7. Case Study

To validate the proposed machining feature recognition and process route optimization algorithm, a case study is performed in collaboration with a machinery enterprise. When developing product process flow, the enterprise first uses the machining feature recognition method proposed by us to traverse the machining features in the model, then makes the feature machining method decision, and finally optimizes the process route. We have established a prototype system, and its architecture is shown in Figure 23, which includes a human–computer interaction layer, functional layer, and database layer. The functions of each part are as follows:

Human-computer interaction layer

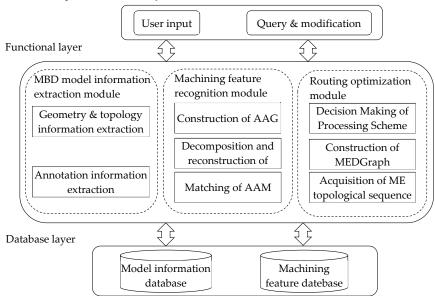


Figure 23. Prototype system architecture.

In order to verify the system functions, take the MBD model shown in Figure 24 as an example to verify the method proposed in this paper. First, extract the model information, as shown in Figures 25 and 26. The former figure shows the geometry and topology information of the model, and the latter shows the annotation information. A total of 71 faces and 219 edges of the model are extracted.

The extracted information is serialized in the Access database. With the tables of "surface\_ data", "edge\_ data", "dimension\_ Data", and "gtol roughness", the database stores the model information of surface, edge, dimension, tolerance, and roughness information, respectively, as shown in Figure 27.

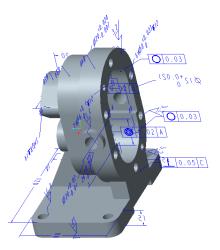


Figure 24. Example model.

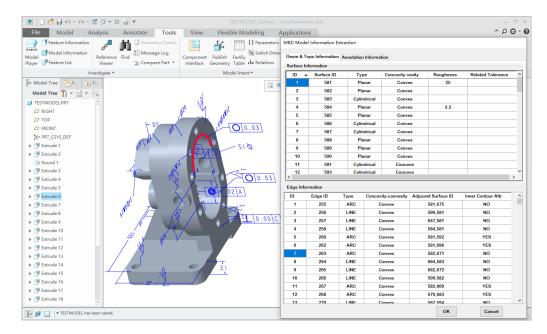


Figure 25. Extraction of model geometry and topology information.

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Figure 26. Extraction of model annotation information.

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1	581	PLANAR	convex	25		1	255	ARC	Convex	581,675	NO
2	582	PLANAR	convex			2	256	LINE	Convex	599, 581	NO
3	583	CYLINDRICAL	convex			3	257	LINE	Convex	647, 581	NO
4	584	PLANAR	convex	3.2		4	258	LINE	Convex	584, 581	NO
5	585	PLANAR	convex			5	260	ARC	Convex	581, 592	YES
6	586	CYLINDRICAL	convex			6	262	ARC	Convex	581,696	YES
7	587	CYLINDRICAL	convex			7	263	ARC	Convex	582, 671	NC
8	588	PLANAR	convex			8	264	LINE	Convex	684, 583	NO
9	589	PLANAR	convex			9	265	LINE	Convex	682, 672	NO
10	590	PLANAR	convex			10	266	LINE	Convex	599, 582	NO
11	591	CYLINDRICAL	concave			11	267	ARC	Convex	582, 669	YES
12	593	CYLINDRICAL	concave			12	268	ARC	Convex	670, 683	YE
13	595	CYLINDRICAL	concave			13	270	LINE	Convex	587, 594	NO
14	597	CYLINDRICAL	concave	6.3		14	272	LINE	Concave	588, 598	NO
15	599	PLANAR	CONVEX			15	273	LINE	Convex	589, 584	NO
16	600	PLANAR	CONVEX			16	274	ARC	Concave	651, 583	NC
17	603	PLANAR	CONVEX			17	275	LINE	Convex	590, 676	NO
18	604	CYLINDRICAL	convex			18	276	ARC	Convex	635, 584	NC
19	605	CYLINDRICAL	convex			19	277	LINE	Convex	603, 587	NC
20	606	PLANAR	concave			20	278	ARC	Convex	604, 610	YE:
21	607	PLANAR	concave			21	279	LINE	Convex	605, 611	NC
22	608	PLANAR	concave			22	280	LINE	Convex	606, 612	NC
23	610	PLANAR	CONAGX			23	281	ARC	Concave	607, 586	YE
24	611	CYLINDRICAL	CONVEX			24	282	LINE	Convex	608, 668	NC
25	612	PLANAR	convex			25	284	LINE	Convex	652, 584	NC
26	614	PLANAR	convex			26	284	LINE	Convex	610, 584	NC
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AD116 AD119 AD122	Type - I Linear Linear Linear	120 80 44		Lover Devia 0.1	340, 350 352, 288 369, 367		• Symbo GP2	1 ▼ 2 Co	Type - Tol Val axiality 0.0	3 660	
AD116 AD119 AD122 AD125	Type - I Linear Linear	120 80	per Deviation - 1		340, 350 352, 288 369, 367 256, 358	/ ID 1 2	<ul> <li>Symbo GP2 GP3</li> </ul>	1 ▼ 2 Co 3 Cin	Type • Tol Val axiality 0.0 ccularity 0.0	3 660 5 637	
AD116 AD119 AD122 AD125 AD131	Type - I Linear Linear Linear Linear Diameter	120 80 44 5	per Deviation - 1 0.1	0.1	340, 350 352, 288 369, 367 256, 358 346		• Symbo GP2	1 ▼ 2 Co 3 Cin	Type - Tol Val axiality 0.0	3 660 5 637	
AD116 AD119 AD122 AD125	Type I Linear Linear Linear Linear	120 80 44 5 9 8	per Deviation - 1 0.1 0.2	0.1	340, 350 352, 288 369, 367 256, 358	ID 1 2 3	<ul> <li>Symbo GP2 GP3 GP4</li> </ul>	1 - Co 2 Co 3 Cin 4 Cin	Type • Tol Val axiality 0.0 rcularity 0.0 rcularity 0.0	3 660 5 637 5 635	6
AD116 AD119 AD122 AD125 AD131 AD133	Type - I Linear Linear Linear Linear Diameter Diameter	120 80 44 5 9	per Deviation - 1 0.1	0.1	340, 350 352, 288 309, 367 256, 358 346 659	ID 1 2 3 4	<ul> <li>Symbo GP2 GP3 GP4 GP5</li> </ul>	1 - Co 2 Co 3 Cin 4 Cin 5 Co	Type • Tol Val axiality 0.0 ccularity 0.0 ccularity 0.0 axiality 0.0	3 660 5 637 5 635 3 639	6
AD116 AD116 AD122 AD122 AD125 AD131 AD133 AD134	Type - I Linear Linear Linear Linear Diameter Diameter Diameter	120 80 44 5 9 8 8	0.1 0.2 0.05	0.1 0.2 0	340, 350 352, 288 309, 367 256, 358 346 659 294	ID 1 2 3 4 5	<ul> <li>Symbo GP3 GP3 GP4 GP5 GP5</li> </ul>	1 - Co 2 Co 3 Cin 4 Cin 5 Co 5 Ven	Type - Tol Val axiality 0.0 rcularity 0.0 rcularity 0.0 axiality 0.0 rticality 0.0	3         660           5         637           5         635           3         639           5         584	6
AD116 AD119 AD122 AD125 AD131 AD133 AD134 AD136	<ul> <li>Type - I Linear Linear Linear Diameter Diameter Diameter Radius Radius</li> </ul>	120 80 44 5 9 8 8 6 40 34	0.1 0.2 0.05	0.1 0.2 0	340, 350 352, 288 369, 367 256, 358 346 659 294 302	Z ID 1 2 3 4 5 6	<ul> <li>Symbo</li> <li>GP2</li> <li>GP3</li> <li>GP4</li> <li>GP5</li> <li>GP6</li> <li>SF0</li> </ul>	1 - Co 2 Co 3 Cin 4 Cin 5 Co 5 Ven 0 Re	Type - Tol Val axiality 0.0 ccularity 0.0 ccularity 0.0 axiality 0.0 cuticality 0.0 oughness 6.3	3         660           5         637           5         635           3         639           5         584           5         598	6
Symbol           AD116           AD119           AD122           AD125           AD131           AD133           AD134           AD136           AD137           AD138           AD139	<ul> <li>Type - I Linear Linear Linear Diameter Diameter Diameter Radius Radius</li> </ul>	120 80 44 5 9 8 8 8 6 40 34 20	0.1 0.2 0.05	0.1 0.2 0	340, 350 352, 288 399, 307 256, 358 346 659 294 302 611 615 645	ID 1 2 3 4 5	<ul> <li>Symbo GP3 GP3 GP4 GP5 GP5</li> </ul>	1 - Co 2 Co 3 Cin 4 Cin 5 Co 5 Ven 0 Re	Type - Tol Val axiality 0.0 rcularity 0.0 rcularity 0.0 axiality 0.0 rticality 0.0	3         660           5         637           5         635           3         639           5         584	6
Apilo AD116 AD122 AD122 AD125 AD131 AD133 AD134 AD136 AD137 AD138 AD139 AD140	<ul> <li>Type - I Linear Linear Linear Diameter Diameter Diameter Radius Radius Radius Radius</li> </ul>	120 80 44 5 9 8 8 6 40 34 20 6	0.1 0.2 0.05	0.1 0.2 0	340, 350 352, 288 309, 367 256, 358 346 659 294 302 611 615 645 647	ID 1 2 3 4 4 5 6 6 7	<ul> <li>Symbo</li> <li>GP2</li> <li>GP3</li> <li>GP4</li> <li>GP4</li> <li>GP5</li> <li>GP6</li> <li>SP0</li> <li>SP1</li> </ul>	1 ▼ 2 Co 3 Cin 4 Cin 5 Co 5 Ven 0 Ro 1 Ro	Type         Tol Val           axiality         0.0           ccularity         0.0           axiality         0.0           axiality         0.0           outlarity         0.1           outlarity         0.2           outlarity         0.3	3         660           5         637           5         635           3         639           5         584           5         598           582         582	6
Symbol           AD116           AD119           AD122           AD125           AD131           AD133           AD134           AD136           AD137           AD138           AD139           AD140	<ul> <li>Type - I Linear Linear Linear Diaaeter Diaaeter Diameter Radius Radius Radius Radius</li> </ul>	120 80 44 5 9 8 8 6 40 34 20 6 11	per Deviation - ) 0.1 0.2 0.05 0.1	0.1 0.2 0	340, 350 352, 288 399, 367 256, 358 346 655 294 302 611 615 645 645 647 013	ID 1 2 3 4 4 5 6 6 7 8	<ul> <li>Symbo</li> <li>GP2</li> <li>GP3</li> <li>GP4</li> <li>GP5</li> <li>GP6</li> <li>SF0</li> <li>SF1</li> <li>SF2</li> </ul>	1 - Co 2 Co 3 Cin 4 Cin 5 Co 5 Ven 6 Ven 0 Ro 1 Ro 2 Ro	Type • Tol Val axiality 0.0 ccularity 0.0 axiality 0.0 axiality 0.0 ticality 0.0 oughness 6.3 bughness 3.2	3         060           5         637           5         635           3         639           5         584           598         582           621         621	6
April 6 AD116 AD119 AD122 AD125 AD131 AD133 AD134 AD136 AD137 AD138 AD139 AD140 AD145 AD146	<ul> <li>Type - I Linear Linear Linear Diameter Diameter Diameter Radius Radius Radius Radius Radius Diameter</li> </ul>	120 80 44 5 9 8 8 6 40 34 20 6 11 12	0.1 0.2 0.05	0.1 0.2 0	340, 350 352, 288 309, 307 256, 358 659 294 302 011 015 045 045 045 045 043 013	L ID 1 2 3 4 4 5 6 6 7 7 8 9	<ul> <li>Symbo</li> <li>GP2</li> <li>GP3</li> <li>GP4</li> <li>GP5</li> <li>GP6</li> <li>SP1</li> <li>SP2</li> <li>SP4</li> </ul>	1         -           2         Co           3         Cin           4         Cin           5         Co           6         Ven           0         R           2         R           4         R	Type     Tol Val       axiality     0.0       rcularity     0.0       axiality     0.0       axiality     0.0       obughness     6.3       oughness     25       oughness     3.2       oughness     3.2	3         660           5         637           5         635           3         639           5         584           5         582           621         637	6
Symbol           AD116           AD119           AD122           AD125           AD131           AD133           AD134           AD136           AD137           AD138           AD138           AD1440           AD145           AD145	<ul> <li>Type - I</li> <li>Linear</li> <li>Linear</li> <li>Linear</li> <li>Linear</li> <li>Diameter</li> <li>Diameter</li> <li>Diameter</li> <li>Radius</li> </ul>	120 80 44 5 9 8 8 8 6 40 34 20 6 11 11 12 10	per Deviation - 1 0.1 0.2 0.05 0.1 0.2	0.1 0.2 0 0	340, 350 352, 288 369, 367 256, 358 846 659 294 611 645 645 647 613 622 337, 373	ID 1 2 3 4 4 5 6 6 7 8	<ul> <li>Symbo</li> <li>GP2</li> <li>GP3</li> <li>GP4</li> <li>GP5</li> <li>GP6</li> <li>SP1</li> <li>SP2</li> <li>SP4</li> </ul>	1         -           2         Co           3         Cin           4         Cin           5         Co           6         Ven           0         R           2         R           4         R	Type • Tol Val axiality 0.0 ccularity 0.0 axiality 0.0 axiality 0.0 ticality 0.0 oughness 6.3 bughness 3.2	3         660           5         637           5         635           3         639           5         584           5         582           621         637	6
AD116 AD116 AD119 AD122 AD125 AD131 AD133 AD134 AD136 AD137 AD138 AD139 AD140 AD145 AD145 AD155 AD158	Type - I Linear Linear Linear Diaaeter Diaaeter Diaaeter Radius Radius Radius Radius Radius Radius Diaaeter Linear Diaaeter	120 80 44 5 9 8 8 6 40 34 20 6 11 11 12 10 30	per Deviation - 1 0.1 0.2 0.05 0.1 0.2 0.1	0.1 0.2 0 0	340, 350 352, 288 309, 307 256, 358 340 659 294 302 611 615 645 647 613 622 337, 373 498	L ID 1 2 3 4 4 5 6 6 7 7 8 9	<ul> <li>Symbo</li> <li>GP2</li> <li>GP3</li> <li>GP4</li> <li>GP5</li> <li>GP6</li> <li>SP1</li> <li>SP2</li> <li>SP4</li> <li>SP5</li> </ul>	1         -           2         Co           3         Cin           5         Co           5         Ver           5         Ver           6         Ver           2         R           4         R           4         R           5         R	Type - Tol Val axiality 0.0 ccularity 0.0 crularity 0.0 cticality 0.0 cticality 0.0 cticality 0.0 cticality 0.0 cughness 2.5 cughness 3.2 cughness 3.2 cughness 1.6	3         660           5         637           5         635           3         639           5         584           5         582           621         637           639         639	6
ymbol AD116 AD119 AD122 AD125 AD131 AD133 AD134 AD136 AD136 AD137 AD138 AD139 AD140 AD145 AD146 AD158 AD160	Type - I Linear Linear Linear Linear Diameter Diameter Diameter Radius Radius Radius Radius Radius Radius Diameter Diameter Diameter	120 80 44 5 9 8 8 8 6 40 34 20 6 11 12 10 30 20	per Deviation - 1 0.1 0.2 0.05 0.1 0.2 0.2 0.1 0.03	0.1 0.2 0 0 0.1 0.1	340, 350 352, 288 369, 367 256, 358 659 294 611 615 615 617 617 617 613 622 337, 373 498 485	ID 1 1 2 3 4 4 5 6 6 7 7 8 9 9 1 ( 11	<ul> <li>Symbo</li> <li>GP2</li> <li>GP3</li> <li>GP4</li> <li>GP5</li> <li>GP6</li> <li>GP6</li> <li>SP1</li> <li>SP2</li> <li>SP4</li> <li>SP5</li> <li>SP6</li> <li>SP6</li> </ul>	1         -           2         Co           3         Cin           4         Cin           5         Co           6         Ven           7         R           1         R           2         R           4         R           5         R           5         R	Type     • Tol Val       axiality     0.0       ccularity     0.0       ccularity     0.0       axiality     0.0       uginess     6.3       oughness     3.2       oughness     3.2       oughness     3.2       oughness     1.6       oughness     1.6	3         660           5         637           5         638           5         584           5         584           5         582           621         637           639         582           637         639           638         689           5         584           637         639           660         639	6
AD116 AD116 AD122 AD125 AD125 AD133 AD134 AD136 AD137 AD136 AD137 AD138 AD139 AD140 AD145 AD146 AD155 AD155 AD155 AD160 AD161	Type - I Linear Linear Linear Diaaeter Diaaeter Diaaeter Radius Radius Radius Radius Radius Diaaeter Diaaeter Diaaeter Diaaeter	120 80 9 8 8 8 6 40 34 20 6 11 12 12 10 30 20 20	per Deviation - 1 0.1 0.2 0.05 0.1 0.2 0.1	0.1 0.2 0 0	340, 350 352, 288 309, 307 256, 358 659 294 302 011 015 045 045 045 045 047 013 022 337, 373 498 485	D 10 1 2 3 3 4 4 5 5 6 6 7 7 8 9 9 9 10 11 11	<ul> <li>Symbo</li> <li>GP2</li> <li>GP4</li> <li>GP4</li> <li>GP5</li> <li>GP6</li> <li>GP6</li> <li>SP6</li> <li>SP7</li> <li>SP6</li> <li>SP6</li> <li>SP6</li> <li>SP6</li> <li>SP6</li> <li>SP7</li> </ul>	1         -         Co           2         Co         Co           3         Cin         Cin           5         Co         Co           5         Ver         Co           6         Ver         Co           0         R         Co           1         R         Co           2         R         Co           4         R         Co           5         R         Co           6         R         Co           7         R         R	Type     Tol Val       axiality     0.0       ccularity     0.0       axiality     0.0       axiality     0.0       axiality     0.0       axiality     0.0       ughness     3.2       uughness     3.2       uughness     1.6       uughness     1.6       uughness     6.3	3         660           5         637           5         635           3         639           5         584           582         621           637         639           600         637           639         639           5         582           621         637           639         660           640         642	6
AD116 AD119 AD122 AD125 AD125 AD131 AD133 AD134 AD133 AD137 AD138 AD137 AD138 AD139 AD140 AD140 AD155 AD158 AD158 AD158 AD161 AD161	Type I Linear Linear Linear Diaaeter Diaaeter Diaaeter Radius Radius Radius Radius Radius Radius Diaaeter Diaaeter Diaaeter Diaaeter Diaaeter Linear	120 80 44 5 9 8 8 6 40 34 40 34 40 34 10 12 10 20 20 20	per Deviation - 1 0.1 0.2 0.05 0.1 0.2 0.2 0.1 0.03	0.1 0.2 0 0 0.1 0.1	340, 350 352, 288 369, 367 256, 358 659 294 611 613 645 645 645 622 337, 873 498 485 485 486 279, 410	ID 1 1 2 3 4 4 5 6 6 7 7 8 9 9 1 ( 11	<ul> <li>Symbo</li> <li>GP2</li> <li>GP4</li> <li>GP4</li> <li>GP5</li> <li>GP6</li> <li>GP6</li> <li>SP6</li> <li>SP7</li> <li>SP7</li> <li>SP6</li> <li>SP6</li> <li>SP6</li> <li>SP6</li> <li>SP7</li> </ul>	1         -         Co           2         Co         Co           3         Cin         Cin           5         Co         Co           5         Ver         Co           6         Ver         Co           0         R         Co           1         R         Co           2         R         Co           4         R         Co           5         R         Co           6         R         Co           7         R         R	Type     • Tol Val       axiality     0.0       ccularity     0.0       ccularity     0.0       axiality     0.0       uginess     6.3       oughness     3.2       oughness     3.2       oughness     3.2       oughness     1.6       oughness     1.6	3         660           5         637           5         635           3         639           5         584           582         621           637         639           600         637           639         639           5         582           621         637           639         660           640         642	6
AD116 AD119 AD122 AD122 AD125 AD131 AD133 AD134 AD137 AD138 AD137 AD138 AD140 AD146 AD155 AD146 AD158 AD164 AD164 AD167	Type - I Linear Linear Linear Linear Linear Diaaeter Diaaeter Radius Radius Radius Radius Radius Radius Radius Radius Radius Linear Linear Linear Linear	120 80 9 8 8 6 40 34 20 6 6 11 12 12 10 30 20 20 20 20 22	per Deviation - 1 0.1 0.2 0.05 0.1 0.2 0.2 0.1 0.03	0.1 0.2 0 0 0.1 0.1	340, 350 352, 288 309, 307 256, 358 340 659 294 302 011 015 045 045 045 045 047 013 022 337, 373 498 485 485 485 485 486 279, 410	D 10 1 2 3 3 4 4 5 5 6 6 7 7 8 9 9 9 10 11 11	<ul> <li>Symbo GP2</li> <li>GP3</li> <li>GP4</li> <li>GP6</li> <li>GP6</li> <li>SP7</li> <li>SP7</li> <li>SP6</li> <li>SP6</li> <li>SP7</li> <li>SP7&lt;</li></ul>	1         -         Co           2         Co         Co           3         Cin         Co           5         Co         Co           5         Co         Co           6         Ven         Co           0         R         Co           1         R         Co           2         R         Co           4         R         Co           5         R         Co           6         R         Co           7         R         R           8         R         R	Type - Tol Val axiality 0.0 ccularity 0.0 crularity 0.0 viality 0.0 pughness 25 pughness 3.2 pughness 3.2 pughness 1.6 pughness 1.6 pughness 1.6 pughness 3.2	3         660           5         637           5         635           5         584           5         582           621         637           639         682           621         637           639         600           642         642           584         584	6
AD116 AD119 AD125 AD125 AD131 AD133 AD134 AD136 AD136 AD137 AD138 AD138 AD140 AD145 AD146 AD155 AD146 AD155 AD160 AD161 AD161 AD167 AD170	Type - 1 Linear Linear Linear Linear Diameter Diameter Radius Radius Radius Radius Radius Linear Diameter Diameter Diameter Diameter Linear Linear Linear	120 80 44 5 9 8 8 8 6 40 34 20 6 11 12 10 30 20 20 20 20 20 20 20 20	per Deviation - 1 0.1 0.2 0.05 0.1 0.2 0.2 0.1 0.03	0.1 0.2 0 0 0.1 0.1	340, 350 352, 288 369, 367 256, 358 459 294 302 611 615 647 647 647 647 647 647 647 647	ID           1           2           3           4           5           6           7           8           9           10           11           12           13           14	<ul> <li>Symbo</li> <li>GP2</li> <li>GP3</li> <li>GP4</li> <li>GP6</li> <li>GP6</li> <li>SP7</li> <li>SP7</li> <li>SP6</li> <li>SP6</li> <li>SP7</li> <li>SP7</li></ul>	1         -         Co           2         Co         Cin           3         Cin         Cin           4         Cin         Cin           5         Co         Co           6         Ven         Co           7         Rd         Rd           7         Rd         Rd           8         Rd         Rd	Type Tol Val axiality 0.0 ccul arity 0.0 axiality 0.0 axiality 0.0 axiality 0.0 axiality 0.0 axiality 0.0 axiality 0.0 sughness 3.2 sughness 3.2 sughness 3.2 sughness 1.6 sughness 6.3 sughness 6.3	3         660           5         637           5         638           5         584           5         582           2         621           3         639           6         637           6         582           2         621           639         660           4         642           5         584           5         654	6
AD119 AD122 AD125 AD133 AD134 AD136 AD136 AD139 AD139 AD140 AD145 AD140 AD145 AD146 AD158 AD160 AD161 AD161 AD161 AD161 AD161 AD170 AD171	Type - I Linear Linear Linear Linear Linear Diaaeter Diaaeter Radius Radius Radius Radius Radius Diaaeter Diaaeter Diaaeter Diaeter Linear Linear Linear	120 80 44 5 9 8 8 8 8 6 40 34 20 0 0 11 12 10 10 30 20 20 20 20 22 20 22 22 20 22 22 20 22 22	per Deviation - 1 0.1 0.2 0.05 0.1 0.2 0.2 0.1 0.03	0.1 0.2 0 0 0.1 0.1	$\begin{array}{c} 340, 350\\ 352, 288\\ 309, 307\\ 256, 358\\ 340\\ 659\\ 294\\ 3002\\ 011\\ 015\\ 045\\ 045\\ 045\\ 045\\ 045\\ 045\\ 045\\ 04$	2 ID 1 2 3 4 5 6 6 7 8 9 1 1 1 2 3 1 4 5 1 1 1 2 3 3 4 4 5 1 1 1 2 3 3 4 4 5 1 1 1 2 3 3 4 4 5 1 1 1 1 2 3 3 4 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1	<ul> <li>Symbo</li> <li>GP2</li> <li>GP3</li> <li>GP4</li> <li>GP5</li> <li>GP6</li> <li>SP6</li> <li>SP7</li> <li>SP6</li> <li>SP7</li> <li>SP7</li></ul>	1         Co           2         Co           3         Cin           5         Co           5         Ver           6         Ver           6         R           7         R           6         R           6         R           7         R           8         R           9         R           00         R	Type Tol Val axiality 0.0 rcularity 0.0 rcularity 0.0 rticality 0.0 rtic	3         600           5         637           5         638           5         588           5         582           637         637           6         637           6         637           6         637           6         600           6         642           5         584           604         655	6
AD116 AD116 AD125 AD122 AD125 AD131 AD133 AD134 AD136 AD137 AD138 AD139 AD140 AD145 AD146 AD145 AD158 AD158 AD158 AD158 AD164 AD164 AD164 AD164 AD167 AD171 AD174	Type - 1 Linear Linear Linear Linear Linear Diaaeter Diaaeter Radius Radius Radius Radius Radius Diaaeter Linear Diaaeter Linear Linear Linear Linear Linear Linear	120 80 44 5 9 9 8 8 8 0 40 34 20 6 11 12 10 0 0 20 20 20 20 20 20 20 22 8	per Deviation - 1 0.1 0.2 0.05 0.1 0.2 0.2 0.1 0.03	0.1 0.2 0 0 0.1 0.1	340, 350 352, 288 369, 367 256, 358 459 294 302 611 615 643 643 643 643 643 643 643 643	ID           1           2           3           4           5           6           7           8           9           10           11           12           13           14	<ul> <li>Symbo</li> <li>GP2</li> <li>GP3</li> <li>GP4</li> <li>GP5</li> <li>GP6</li> <li>SP6</li> <li>SP7</li> <li>SP6</li> <li>SP7</li> <li>SP7</li></ul>	1         Co           2         Co           3         Cin           5         Co           5         Ver           6         Ver           6         R           7         R           6         R           6         R           7         R           8         R           9         R           00         R	Type Tol Val axiality 0.0 ccul arity 0.0 axiality 0.0 axiality 0.0 axiality 0.0 axiality 0.0 axiality 0.0 axiality 0.0 sughness 3.2 sughness 3.2 sughness 3.2 sughness 1.6 sughness 6.3 sughness 6.3	3         600           5         637           5         638           5         588           5         582           637         637           6         637           6         637           6         637           6         600           6         642           5         584           604         655	6
AD116 AD116 AD122 AD125 AD125 AD131 AD134 AD136 AD138 AD138 AD138 AD138 AD138 AD138 AD140 AD140 AD140 AD140 AD140 AD155 AD155 AD155 AD155 AD160 AD161 AD160 AD161 AD167 AD170 AD177	Type - I Linear Linear Linear Linear Linear Diaaeter Diaaeter Diaaeter Radius Radius Radius Radius Diaaeter Diaaeter Diaaeter Linear Linear Linear Linear	120 80 80 44 5 5 8 8 8 8 8 8 8 40 34 20 6 11 12 10 30 20 20 20 20 20 20 22 20 20 22 8 8 8	per Deviation - ) 0.1 0.2 0.05 0.1 0.2 0.1 0.2 0.1 0.03 0.03	0.1 0.2 0 0.1 0.1 0.5 0.02 0.02	$\begin{array}{c} 340, 350\\ 352, 288\\ 309, 307\\ 256, 358\\ 340\\ 659\\ 294\\ 3002\\ 011\\ 015\\ 045\\ 045\\ 045\\ 045\\ 045\\ 045\\ 045\\ 04$	2 ID 1 2 3 4 5 6 6 7 8 9 1 1 1 2 1 3 1 4 5 1 1 1 2 3 3 4 4 5 1 1 1 2 3 3 4 4 5 1 1 1 2 3 3 4 4 5 1 1 1 1 2 3 3 4 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1	<ul> <li>Symbolic GP2</li> <li>GP3</li> <li>GP4</li> <li>GP5</li> <li>GP6</li> <li>SP6</li> <li>SP7</li> <li>S</li></ul>	1         Co           2         Co           3         Cin           5         Co           5         Co           60         Ven           61         R           65         R           65         R           65         R           65         R           65         R           66         R           67         R           68         R           69         R           60         R           72         R	Type Tol Val axiality 0.0 rcularity 0.0 rcularity 0.0 rticality 0.0 rtic	3         660           5         637           5         638           5         584           5         582           637         637           6         637           6         637           6         637           6         637           6         637           6         637           6         637           6         642           5         584           6         642           5         584           6         694           6         625	6
AD116 AD116 AD125 AD122 AD125 AD131 AD133 AD134 AD136 AD137 AD138 AD139 AD140 AD145 AD146 AD145 AD158 AD158 AD158 AD158 AD164 AD164 AD164 AD164 AD167 AD171 AD174	Type - 1 Linear Linear Linear Linear Linear Diaaeter Diaaeter Radius Radius Radius Radius Radius Diaaeter Linear Diaaeter Linear Linear Linear Linear Linear Linear	120 80 44 5 9 9 8 8 8 0 40 34 20 6 11 12 10 0 0 20 20 20 20 20 20 20 22 8	per Deviation - 1 0.1 0.2 0.05 0.1 0.2 0.2 0.1 0.03	0.1 0.2 0 0 0.1 0.1	340, 350 352, 288 369, 367 256, 358 459 294 302 611 615 643 643 643 643 643 643 643 643	2 ID 1 2 3 4 4 5 6 6 7 8 9 10 11 12 13 14 16 16 16 16 16 16 16 16 16 16	<ul> <li>Symbo</li> <li>GP2</li> <li>GP3</li> <li>GP4</li> <li>GP5</li> <li>GP6</li> <li>SF1</li> <li>SF2</li> <li>SF4</li> <li>SF5</li> <li>SF5</li> <li>SF5</li> <li>SF1</li> <li>SF1</li> <li>SF1</li> <li>SF1</li> <li>SF1</li> </ul>	1         Co           2         Co           3         Cin           4         Cin           5         Co           6         Ven           0         R           1         R           2         R           6         R           7         R           8         R           9         R           00         R           2         R           3         R           3         R           3         R	Type - Tol Val axiality 0.0 ccularity 0.0 crularity 0.0 rticality 0.0 pticality 0.0 underss 2.5 pughness 3.2 pughness 3.2 pughness 1.6 pughness 1.6 pughness 1.6 pughness 3.2 pughness 3.2 pughness 3.2 pughness 3.2 pughness 3.2 pughness 3.2	3         660           5         637           5         638           5         584           5         582           637         637           6         637           6         637           6         637           6         637           6         637           6         637           6         637           6         642           5         584           6         642           5         584           6         694           6         625	- Datum 6: 6: 5:

**Figure 27.** Storage of model information. (a) Surface information; (b) Edge information; (c) Dimension information; (d) Tolerance and roughness information.

AAG decomposition method based on DBS and JBS is adopted to identify machining features, and the results are shown in Figure 28. A total of 28 machining features were identified, and the results were automatically imported into the Excel database to complete serialization, as shown in Figure 29.

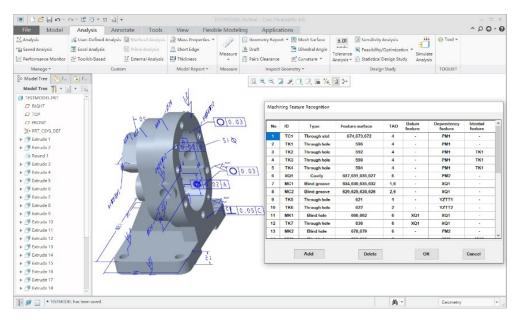


Figure 28. Recognition of machining features.

	Α	В	С	D	E	F	G	Н
1	No.	ID	Туре	Feature surface	TAD	Datum feature	Dependency feature	Idential feature
2	1	TC1	Through slot	674,673,672	4	-	PM1	-
3	2	TK1	Through hole	596	4	-	PM1	-
4	3	TK2	Through hole	592	4	-	PM1	TK1
5	4	TK3	Through hole	598	4	-	PM1	TK1
6	5	TK4	Through hole	594	4	-	PM1	TK1
7	6	XQ1	Cavity	637,631,635,627	6	-	PM2	-
8	7	MC1	Blind groove	634,630,635,632	1,6	-	XQ1	-
9	8	MC2	Blind groove	629,625,628,626	2,6	-	XQ1	-
10	9	TK5	Through hole	621	1	-	YZTT1	-
11	10	TK6	Through hole	622	2	-	YZTT2	-
12	11	MK1	Blind hole	660,662	6	XQ1	XQ1	-
13	12	TK7	Through hole	636	6	XQ1	XQ1	-
14	13	MK2	Blind hole	678,679	6	-	PM2	-
15	14	MK3	Blind hole	692,683	6	-	PM2	MK2
16	15	MK4	Blind hole	690,682	6	-	PM2	MK2
17	16	MK5	Blind hole	694,684	6	-	PM2	MK2
18	17	MK6	Blind hole	688,681	6	-	PM2	MK2
19	18	MK7	Blind hole	686,680	6	-	PM2	MK2
20	19	MK8	Blind hole	696,697	6	-	PM2	-
21	20	MKQ	Blind hole	699 700	6	_	PM2	MK 8

Figure 29. Serialization of recognition result.

Set the material attribute of the model as cast iron, and use the feature processing scheme decision based on fuzzy comprehensive evaluation to make the feature processing scheme decision. The result is shown in Figure 30. Serialize the decision results.

According to the machining feature recognition and processing scheme decision results, the ME sequence is generated and stored in the database, as shown in Figure 31. The manufacturing resource information involved is shown in Table 11.

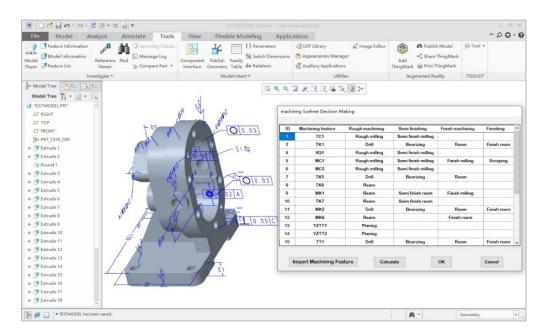


Figure 30. Decision results of machining scheme.

m-eleme	nt					
ID	✓ Machining fe •	ME -	Process nam •	Machine available 🗸	Tools availal 🗸	TAD -
1	TC1	me1	Rough mill	M2,M3,M4	X3,X4	4
2	TK1	me2	Drill	M1,M3	Z1	4
3	TK1	me3	Ream	M1,M3	J1	4
4	XQ1	me4	Rough mill	M2,M3	X3	6
5	XQ1	me5	Finish mill	M2,M3	X5	6
6	MC1	теб	Rough mill	M2,M3,M4	X3,X4	1,6
7	MC2	me7	Rough mill	M2,M3,M4	X3,X4	2,6
8	TK5	me8	Drill	M1	Z1,Z2	1
9	TK5	me9	Ream	M1	J1	1
10	TK6	me10	Drill	M1	Z1,Z2	2
11	TK6	me11	Ream	M1	J1	2
12	MK1	me12	Drill	M1	Z2	6
13	MK1	me13	Rough ream	M1	J1	6
14	MK1	me14	Finish ream	M1	J2	6
15	TK7	me15	Drill	M1	Z2	6
16	TK7	me16	Rough ream	M1	J1	6
17	TK7	me17	Finish ream	M1	J2	6
18	MK2	me18	Drill	M1,M3	Z1	6
19	MK2	me19	Ream	M1,M3	J1	6
20	MK8	me20	Drill	M1,M3	Z1	6
21	MK8	me21	Ream	M1,M3	J1	6
22	YZTT1	me22	Rough mill	M3	X3	1
23	YZTT2	me23	Rough mill	M3	X3	2
24	TT1	me24	Rough mill	M3	X3	5
25	MK10	me25	Drill	M1	Z2	5
26	MK10	me26	Bearizing	M1	KZ1	5
27	MK10	me27	Ream	M1	J1	5
28	MK11	me28	Drill	M1	Z1	5
29	MK11	me29	Rough ream	M1	J1	5
30	MK11	me30	Finish ream	M1	J2	5
31	PM1	me31	Rough mill	M2,M3,M4	X1,X2	4
32	PM2	me32	Rough mill	M2,M3,M4	X1,X2	6
33	PM2	me33	Finish mill	M2,M3,M4	X6	6

Figure 31. MEs sequence.

No.	Туре	Name	Resource	No.	Туре	Name	Resource
1		M1	drilling machine	1		Z1, Z2, Z3	Twist drill
2	machine	M2	Vertical milling machine	2	tool	J1, J2	Reamer
3	machine	M3	CNC milling machine	3	1001	KZ1	Counterbore drill
4		M4	Horizontal milling machine	4		X1, X2, X3, X4, X5, X6	Milling cutter

 Table 11. Manufacturing resource information.

Fifty-three topological sequences of ME are obtained by optimizing the ME sorting, among which the evaluation function value of the optimal sequence:  $F = 1 \times 0.530 + 9 \times 0.297 + 21 \times 0.163 = 6.626$ ; this sequence is the optimal process route for this part machining, as shown in Figure 32.

	А	В	С	D	E	F
1	No.	ME	Name	Machine	TAD	Tool
2	1	me31	Rough mill	M3	4	X1
3	2	me1	Rough mill	M3	4	X3
4	3	me32	Rough mill	M3	6	X1
5	4	me33	Finish mill	M3	6	X6
6	5	me4	Rough mill	M3	6	X3
7	6	me5	Finish mill	M3	6	X5
8	7	meб	Rough mill	M3	6	X3
9	8	me7	Rough mill	M3	6	X3
10	9	me22	Rough mill	M3	1	X3
11	10	me23	Rough mill	M3	2	X3
12	11	me24	Rough mill	M3	5	X3
13	12	me28	Drill	M1	5	Z1
14	13	me25	Drill	M1	5	Z2
15	14	me26	Bearizing	M1	5	KZ1
16	15	me27	Ream	M1	5	J1
17	16	me29	Rough ream	M1	5	J1
18	17	me30	Fine ream	M1	5	J2
19	18	me2	Drill	M1	4	Z1
20	19	me3	Ream	M1	4	J1
21	20	me8	Drill	M1	1	Z1
22	21	me9	Ream	M1	1	J1
23	22	me10	Drill	M1	2	Z1
24	23	me11	Ream	M1	2	J1
25	24	me12	Drill	M1	6	Z2
26	25	me15	Drill	M1	6	Z2
27	26	me18	Dril1	M1	6	Z1
28	27	me20	Drill	M1	6	Z1
29	28	me13	Rough ream	M1	6	J1
30	29	me16	Rough ream	M1	6	J1
31	30	me19	Ream	M1	6	J1
32	31	me21	Ream	M1	6	J1
33	32	me14	Fine ream	M1	6	J2
34	33	me17	Fine ream	M1	6	J2

Figure 32. Optimal ME sequence.

#### 8. Conclusions

In summary, aiming at the problem of machining feature recognition and process route optimization in the MBD model, we propose a feature matching algorithm based on model AAM after studying the model AAG decomposition based on DBS and JBS, which first constructs the decomposed feature subgraph as AAM, and then realizes machining feature recognition by matching with predefined feature AAM. A feature processing scheme decision-making method based on fuzzy comprehensive evaluation is proposed. By analyzing the influencing factors of processing scheme selection, the mapping relationship between the influencing factors and the processing scheme is established. Based on the single-factor evaluation results, a multi-factor comprehensive evaluation model is established. By calculating the comprehensive evaluation index, the optimization of the feature processing scheme is realized. Based on the optimized scheme, a model processing route optimization method based on MEDGraph is proposed. Based on the constraint relationship between MEs, the MEDGraph is established. The improved topological sorting algorithm is applied to list the topological sequence of all MEs. Finally, the evaluation function is constructed to obtain the optimal process route. Our research realized the recognition of machining features in parts and the determination of the optimal process route without complex similarity transformation of AAM. The application of our research can provide a premise for enterprise intelligent manufacturing on the basis of automatic recognition of model machining features.

Our future work will focus on the recognition of machining features, including freeform surfaces and complex intersection features, as well as the optimization of process routes considering other factors, such as machining parameters and process tolerance allocation.

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#### Appendix A

Algorithm A1. Geometric & topology information extraction algorithm 1. Input: MBD model 2. Output: Store geometric & topology information in computer memory 3./\*Definition of structure array\*/ 4. struct Surface\_data 5. { 6. ElemType surf\_id 7. ElemType *surf\_type* 8. ElemType *surf\_at* 9. vector< ElemType > *adj\_surf\_id* 10. vector< ElemType > *edge\_id* 11. vector< ElemType > *cont\_data* 12. ElemType *surffinish\_value* 13. vector< ElemType > gtol\_data 14. } 15. struct Contour\_data 16. { 17. vector< ElemType > edge\_id 18. ElemType contour\_type 19. } 20. struct Edge\_data 21. { 22. ElemType *edge\_id* 23. ElemType edge\_type 24. ElemType *edge\_at* 25. vector<ElemType > adja\_suf 26. ElemType *edge\_in* 

27. }

Algorithm A1. Cont.						
28./*Define structure array*/						
29. Surface_data surf[num1], Contour_data contour[num2], Edge_data edge[num3]						
$30. k \leftarrow 0, h \leftarrow 0$						
31. Call ProMdlCurrentGet() to get the handle of the current model						
32. Call ProSolidSurfaceVisit() to traverse surface and obtain and output surface[]						
33. <b>Call</b> ProArraySizeGet() to get the length of surf[], which is <i>m</i>						
34. for $(i = 0; i < m; i + +)$ do						
35. Call ProSurfaceIdGet() to get the ID of No.i+1 surface and write it to surf[i].surf_id						
36. Call ProSurfaceTypeGet() to get the type of No.1+1 surface and write to surf[i]. surf_type						
37. Call ProSurfaceAtGe () to get the concavity-convexity of No.1+1 surface						
38. Write to surface[ <i>i</i> ]. <i>surf_at</i>						
39. <b>Call</b> ProSurfaceContourVisit() to traverse the contour and write them to Contour[]						
40. <b>Call</b> ProArraySizeGet() to get the length of Contour[], which is <i>n</i>						
41. <b>for</b> $(j = 0; j < n; j + +)$ <b>do</b>						
42. <b>Call</b> ProContourTraversalGet() to get the type of contour and write to						
contour[k].contour_type						
43. <b>Call</b> ProContourEdgeVisit() to traverse the edges of contour and write to Edge[]						
44. <b>Call</b> ProArraySizeGet() to get the length of edge[], which is <i>e</i>						
45. <b>for</b> $(t = 0; t < e; t ++)$ <b>do</b>						
46. <b>Call</b> ProEdgeIdGet() to get the ID of edge						
47. Write it to $edge[h].edge_id$ , contour [k].edge_id						
48. <b>if</b> $(edge[h].edge_id \notin surface[i].edge_id)$ <b>then</b>						
49. Write to surface[ <i>i</i> ]. <i>edge_id</i>						
50. end if						
<ul> <li>51. Call ProEdgeTypeGet() to get type of edge and write to edge[h].edge_type</li> <li>52. Call ProEdgeAtGet() to get concavity-convexity and write to edge[h].edge_at</li> </ul>						
0 () 0 ) 0 1 0 1						
54.Write to $edge[h].adja\_suf$ 55.if $(edge[h].adja\_suf \notin surface[i].edge\_id)$ then						
55. If $(edge[n].uuju_suj \notin surface[i].edge_uu )$ then 56. Write to $surface[i]. adj_surf_id$						
57. end if						
58. <i>h</i> ++						
59. end for						
60. Write contour[k] to surface[i].cont_data						
61.   k++						
62. end for						
63. end for						

#### Algorithm A2. AAG construction

- 1. Input: MBD model information structure array surface[], edge[] and contour[]
- 2. Output: line[num1], node[num2]
- 3./\*Define structure array node[num2] and line[num1], num1 and num2 is the number of model edge and surface\*/
- 4. struct Node
- 5. {
- 6. ElemType *surface\_id*
- 7. vector< ElemType > adj\_line
- 8. ElemType *node\_type*
- 9. ElemType node\_at
- 10. ElemType *d\_face*

#### Algorithm A2. Cont. 11. ElemType *f\_face* 12. ElemType *c\_face* 13. } node[num2] 14. struct Line 15. { 16. ElemType edge\_id ElemType node1 17. 18. ElemType node2 19. ElemType line\_type 20. ElemType *line\_at* 21. ElemType in\_contour 22. } line[num1] 23./\*Assign the id of line and surface \*/ 24. for (i = 0; i < num1; i + +) do 25. line[*i*]. *edge\_id* $\leftarrow$ edge[*i*].*edge\_id* 26. end for 27. **for** (*i* = 0; *i* < num2; *i* ++) **do** 28. node[*j*]. *surface\_id* ← surface[*j*].*surface\_id* 29. end for 30./\* Determine the connection relationship between nodes and edges\*/ 31. **for** (*i* = 0; *i* < num2; *i* ++) **do** 32. **for** (*j* = 0; *j* < num1; *j* ++) **do** 33. **for** (*k* = 0; *k* < surface[*i*].edge\_id.size(); *k* ++) **do** 34. **if** (line[*j*]. *edge\_id* == surface[*i*].edge\_id[*k*]) **then** 35. Add line[*j*] to node[*i*]. *adj\_line* 36. if (line[j].node1==NULL) then 37. line[*j*].*node*1 $\leftarrow$ node[*i*] 38. else 39. line[*j*].*node*2 $\leftarrow$ node[*i*] 40. end if 41. end if 42. end for 43. end for 44. end for 45./\*Add node attribute\*/ 46. **for** (*i* = 0; *i* < num2; *i* ++) **do** 47. /\*Assign the type\*/ 48. if (surface[*i*].*type* == planar) then node[*i*].*node\_type* $\leftarrow$ 1 end if 49. if (surface[*i*].*type* == cylinder) then node[*i*].*node\_type* $\leftarrow$ 2 end if 50. if (surface[*i*].*type* == conical) then node[*i*].*node\_type* $\leftarrow$ 3 end if 51. if (surface[*i*].*type* == other) then node[*i*].*node\_type* $\leftarrow$ 4 end if 52. /\*Assign the concavity-convexity of surface\*/ 53. if (surface[i].concavity-convexity ==concave) then node[*i*].*node\_at* $\leftarrow -1$ 54. 55. else $\mathsf{node}[i].\mathit{node}\_at \gets 1$ 56. 57. end if /\*Assign the DBS attribute\*/ 58. 59. if (surface[i].contour\_information == inner) then 60. node[*i*].*d\_face* $\leftarrow$ true 61. else 62. node[*i*].*d\_face* $\leftarrow$ false 63. end if /\*Assign the FBS attribute\*/ 64.

65. Calculation the extrusion of  $f_i$ , which is  $V_h$ 

Algorithm A2. Cont.

if (surface[i].type == planar && surface[i].concavity-convexity == convex 66. &&  $V_h \cap part = \emptyset$  then 67. node[i].*f\_face*  $\leftarrow$  true 68. else 69.  $node[i].f_face \leftarrow false$ 70. end if 71. end for 72./\*Traverse the JBS\*/ 73. **for** (*i* = 0; *i* < num2; *i* ++) **do** 74. **for** (*j* = 0; *j* < num2; *j* ++) **do** 75. if (surface[*i*] and surface[*j*] == JBS) then 76.  $node[i].c_face \leftarrow node[j].c_face \leftarrow k$ 77. *k*++ 78. end if 79. end for 80. end for 81./\*Add edge attribute\*/ 82. **for** (*i* = 0; *i* < num1; *i* ++) **do** /\*Assign the type\*/ 83. if (edge[i].type == straight) then  $line[i].line_type \leftarrow 1$  end if 84. 85. if (edge[i].type == arc) then  $line[i].line_type \leftarrow 2$  end if 86. if (edge[i].type == other) then  $line[i].line_type \leftarrow 3$  end if 87. if (edge[i].type == straight) then  $line[i].line_type \leftarrow 1$  end if 88. /\*Assign the concavity-convexity\*/ 89. if (edge[i].concavity-convexity == concavity) then  $line[i].line_at \leftarrow -1$  end if 90. if (edge[i].concavity-convexity == convexity) then  $line[i].line_at \leftarrow 1$  end if 91. if (edge[*i*].concavity-convexity == smooth) then line[*i*].line\_at  $\leftarrow$  0 end if 92. /\*Assign the inner contour attribute\*/ 93. if (edge[i].inner\_contour == true) then 94. line[*i*]. *in\_contour*  $\leftarrow$  true 95. else 96. line[*i*]. *in\_contour*  $\leftarrow$  false 97. end if 98. end for

Algorithm A3. AAG decomposition and reconstruction based on DBS and JBS

```
1. Input: line[num1] and node[num2]
```

2. Output: line1[n][] and node1[n][], which represent the edge and node after reconstruction

```
3./*Decomposition based on DBS*/
```

4. Nsign[i]  $\leftarrow 0$ 

```
5. for (i = 0; i < \text{num2}; i + +) do
```

```
6. if (node[i].d_face == ture) then
```

```
7. for (j = 0; j < \text{num1}; j ++) do
```

```
8. if (\text{line}[i].node1 == \text{node}[i] \mid | \text{line}[i].node2 = \text{node}[i]) then
```

- 9. **if** (line[*j*].*in\_contour* == true && line[*j*].*line\_at* == -1) **then**
- 10.  $Nsign[i] \leftarrow -1$
- 11.  $line[j] \leftarrow NULL$
- 12. end if

13. **if** (line[j].*in\_contour* == false && line[*j*].*line\_at* == 1) **then** 

- 14. Nsign  $[i] \leftarrow 1$
- 15.  $\operatorname{line}[i] \leftarrow \operatorname{NULL}$
- 16. end if
- 17. end if

```
18. end for
```

- 19. end if
- 20. end for
- -0. cita 101

Algorithm A3. Cont. 21. **for** (*i* = 0; *i* < num2; *i* ++ ) **do** 22. **if** (node[*i*] ==-1) **then** 23. Extract the information of node[] and line[] adjacent to node[i] 24. if (line ].*line\_at* = -1) then 25. line[]  $\leftarrow$  NULL 26. Assign the value of node[] to corresponding node1[][] 27. Obtain the value of line1[][] according to node1[][] 28. else 29 Store the corresponding node1[ ][ ] and line1[ ][ ] 30. end if 31. end if 32. **if** (node[*i*] ==1) **then** 33. Extract the information of node[] and line[] adjacent to node[i], and store them to node1[ ][ ] and line1[ ][ ] 34. end if 35. Delete line[] and node[] 36. end for 37./\*Delete non-machining surface\*/ 38. **for** (*i* = 0; *i* < node[].size; *i* ++) **do** 39. **if** (node[*i*].*node\_at* == 1) **then** 40.  $node[i] \leftarrow NULL$ 41. Delete line[] adjacent to node[i].adj\_line 42. Update line[] and node[] 43. end if 44. end for 45./\*Extract the MCCS on FBS\*/ 46. **for** (*j* = 0; *j* < node[].size; *j* ++) **do** 47. if (node[j].f\_face == true) then 48. **for** (*k* = 0; *k* < node[*j*].adj\_line.size; *k* ++) **do** 49. if  $(node[j].adj_line[k].line_at == -1)$  then 50. Extract the node adjacent to node[*j*].adj\_line[*k*] 51. if (extracted node has concave edge) then 52. Continue to extract nodes adjacent to the concave edges 53. end if 54. end if end for 55. 56. end if 57. Store node[] to node1[][] and then get the corresponding line1[][] 58. end for 59./\*Search the node with the same JBS attribute\*/ 60. c\_sign[n][]  $\leftarrow 0$ 61. **for** (*i* = 0; *i* < n; *i* ++) **do for** (*j* = 0; *j* < node1[*i*][].size; *j* ++) **do** 62. 63. if  $(node1[i][j].c_face \neq \emptyset$  then 64.  $c\_sign[i][j] \leftarrow node1[i][j].c\_face$ 65. end if 66. end for 67. end for 68. **for** (*k* = 0; *k* < n; *k* ++) **do** 69. **for** (*s* = 0; *s* < n; *s* ++) **do** 70. if (c\_sign[*k*][] and c\_sign[*s*][] have the same element) then 71. Merge line1[*s*][] to line1[*k*][] 72. Merge node1[s][] to node1[k][] 73. end if 74. end for 75. end for

Algorithm A4. AAM establishment algorithm 1. Input: line2[m][] and node2[m][] 2. Output: The AAM of machining feature to be identified 3.  $sg \leftarrow 0$ , M[n][n]  $\leftarrow 0$ 4. **for** (*t* = 0; *t* < m; *t* ++) **do for** (*i* = 0; *i* < node[*t*][].size; *i* ++) **do** 5.  $a \leftarrow 2, b \leftarrow c \leftarrow 0$ 6. 7.  $c \leftarrow node2[t][i].node_at$ 8.  $b \leftarrow node2[t][i].node_type$ 9. **if** (node2[*t*][*i*].node\_ f\_face == true) **then** 10.  $a \leftarrow 1$ end if 11. 12.  $M[sg][sg] \leftarrow a*100+b*10+c$ 13. sg++14. end for 15. end for 16. for (w = 0; w < m; w ++) do 17. **for** (*j* = 0; *j* < line2[*w*][].size; *j* ++) **do**  $\dot{d} \leftarrow 0, e \leftarrow 0$ 18 19.  $d \gets line2[w][j].line\_type$  $e \leftarrow line2[w][j].line_at$ 20. Search node2[ ][ ] for line2[w][j].node1 21. 22. Search node2[ ][ ] for line2[w][j].node2 23. Determine the position of line2[*w*][*j*] in AAM according to node2[][] 24.  $M[k][h] \leftarrow M[h][k] \leftarrow d*10+e$ 25. end for 26. end for

Algorithm A5. Matching between feature subgraph AAM and predefined feature AAM

1. Input: feature subgraph AAM to be identified represented by matrix A[n][n], and predefined feature AAM represented by matrix B[m][m] 2. Output: matching result 3./\* Define the function SetJudgment(matrix1, matrix2) to determine whether matrix1 and matrix2 is identical \*/ 4. SetJudgment(matrix1, matrix2) 5. { 6.  $k \leftarrow 0$ 7. **for** (*i* = 0; *i* < matrix1.size; *i* ++) **do for** (j = 0; j < matrix2.size; j + +) $j \leftarrow 0$  to matrix2.size **do** 8. 9. **if** (matrix1[*i*] == matrix2[*j*]) **then** 10. *k*++ 11. matrix2  $\leftarrow$  matrix2.erase(matrix2.begin()+*j*) 12. break 13. end if end for 14. 15. end for 16. if (k == n) then 17.  $result \gets true$ 18. else 20.  $result \gets false$ 21. end if 22. return result 23. } 24. for (i = 0; i < f; i + +) do//f is the number of feature subgraphs 25. if  $(n \neq m)$  then

Algo	Algorithm A5. Cont.				
26.	Get next AAM				
27.	else				
28.	vector <int> <math>S_1</math>, vector<int> <math>S_2</math></int></int>				
29.	<b>for</b> $(i = 0; i < n; i ++)$ <b>do</b>				
30.	$S_1 \leftarrow A[i][i]$				
31.	$S_2 \leftarrow B[i][i]$				
32.	end for				
33.	result1 = SetJudgment( $S_1$ , $S_2$ )				
34.	if (!result1) then				
35.	Get next AAM				
36.	else				
37.	vector <int> <math>S_{Ai}</math>, vector<int> <math>S_{Bi}</math></int></int>				
38.	<b>for</b> ( <i>i</i> = 0; <i>i</i> < n; <i>i</i> ++) <b>do</b>				
39.	$S_{Ai} \leftarrow A[i][$ ]				
40.	$S_{Bi} \leftarrow B[i][$ ]				
41.	end for				
42.	$index \leftarrow 0$				
43.	<b>for</b> ( $w = 0$ ; $w < n$ ; $w ++$ ) <b>do</b>				
44.	<b>for</b> $(u = 0; u < n; u ++)$ <b>do</b>				
45.	result2=SetJudgment( $S_{Aw}$ , $S_{Bu}$ )				
46.	if (!result2) then				
47.	Get next AAM				
48.	else				
49.	$S_{Bu} \leftarrow 0$				
50.	index ++				
51.	break				
52.	end if				
53.	end for				
54.	end for				
55.	if $(index \neq n)$ then				
56.	Get next AAM				
57.	else				
58.	success				
59.	end if				
60.	end if				
61. <b>er</b>	nd for				

Algorithm A6. Decision algorithm of feature machining scheme

1. Input: machining feature information

2. Output: Optimal processing scheme

3. Call ProMaterialDataGet( ) to get the material properties, which is Mat

4. **for** (i = 0; i < n; i + +) **do**//n is the number of processing features

5. if (feature[i]  $\neq$  hole feature) then//Processing scheme decision

6. /\* Calculate fuzzy matrix of each influencing factor for surface features\*/

7. **for** (j = 0; j < 6; j ++) **do** 

8. **if** (x[j] is suitable for Mat) **then**  $RM[j] \leftarrow 1$  **end if** 

9. **if**  $(x[j] \text{ is suitable for feature}[i].feature_type)$  **then** RF $[j] \leftarrow 1$  **end if** 

10. GetSchemeIT(x[j])//Obtain the precision range ITn~ITm of scheme x[j]

11. **if** (feature [i].IT < ITn - 2 || feature [i].IT > ITm) **then** RIt $[j] \leftarrow 0$  **end** if

12. **if**  $(ITn \le feature[i].IT \le ITm)$  **then**  $RIt[j] \leftarrow 1$  **end if** 

13. **if**  $(ITn - 2 \le feature[i].IT < ITn)$  **then**  $RIt[j] \leftarrow 1-((ITn-feature[i].IT)/(5*(ITm-ITn)))$ 

end if

14. GetSchemeRa(x[j])//Obtain the roughness range a~b of scheme x[j]

15. **if** feature[*i*].Ra < a || feature[*i*].Ra > b **then** RRa[*j*]  $\leftarrow$  0 **end** if

Algorithm A6. Cont. 16. if  $a \leq \text{feature}[i]$ .Ra  $\leq$  b then RRa[j]  $\leftarrow$  1-(log(b)-log(feature[i].Ra))/5(log(b)-log(a)) end if 17. end for 18. /\*Calculating fuzzy comprehensive evaluation matrix R1[ ][ ]\*/ 19. **for** (*k*1 = 0; *k*1 < 6; *k*1 ++) **do** 20.  $R1[0][k1] \leftarrow RM[k1]$ end for 21. **for** (*k*2 = 0; *k*2 < 6; *k*2 ++) **do** 22. 23.  $R1[1][k2] \leftarrow RF[k2]$ 24. end for 25. **for** (*k*3 = 0; *k*3 < 6; *k*3 ++) **do** 26.  $R1[2][k3] \leftarrow RIt[k3]$ 27. end for 28. **for** (*k*4 = 0; *k*4 < 6; *k*4 ++) **do** 29.  $R1[3][k4] \leftarrow RRa[k4]$ 30. end for 31 /\*Calculating fuzzy comprehensive evaluation index vector B[]\*/ 32. **for** (*num* = 0; *num* < 6; *num* ++) **do** 33 **for** (*i* = 0; *i* < 6; *i* ++) **do for** (*j* = 0; *j* < 4; *j* ++) **do** 34. 35.  $B[num] \leftarrow B[num] + W[j] * R1[i][j]$ 36. end for 37. end for 38. end for 39. Take x[] corresponding to element with largest value in B[] as the scheme [*i*] 40. end if 41. **if** (feature[*i*] == hole feature) **then** 42. **for** (*w* = 0; *w* < 13; *w* ++) **do** 43. if (y[w] is suitable for *Mat*) then  $RM[w] \leftarrow 1$  end if 44. GetFeatureD()//Get the diameter *D* of hole feature 45. if (y[w] is suitable for D) then  $RD[w] \leftarrow 1$  end if 46. GetSchemeIT(y[w]) //Get the precision range ITn ~ ITm of scheme y[w]47. if (feature[i].IT < ITn - 2 || feature[i].IT > ITm) then  $\text{RIt}[j] \leftarrow 0$  end if 48. if  $(ITn \leq feature[i], IT \leq ITm)$  then  $RIt[i] \leftarrow 1$  end if 49. if  $(ITn - 2 \le feature[i].IT < ITn)$  then RIt[j] $\leftarrow 1 - \left((ITn - feature[i].IT) / (5 * (ITm - ITn))\right) \text{ end if}$ 50. GetSchemeRa(y[w]) //Get the roughness range a ~ b of scheme y[w]end if 51. 52. if (feature[i].Ra < a || feature[i].Ra > b) then  $RRa[w] \leftarrow 0$  end if 53. if (feature[i].Ra < a || feature[i].Ra > b) then 54.  $RRa[w] \leftarrow 1-(\log(b)-\log(feature[i].Ra))/5(\log(b)-\log(a))$ 55. end if 56. end for 57. /\* Calculate fuzzy comprehensive evaluation matrix R2[ ][ ] of hole feature\*/ 58. **for** (*s*1 = 0; *s*1 < 13; *s*1 ++) *do* 59.  $R2[0][s1] \leftarrow RM[s1]$ 60. end for **for** (*s*2 = 0; *s*2 < 13; *s*2 ++) **do** 61. 62.  $R2[1][s2] \leftarrow RD[s2]$ 63. end for 64. **for** (*s*3 = 0; *s*3 < 13; *s*3 ++) **do** 65.  $R2[2][s3] \leftarrow RIt[s3]$ 66. end for 67. for (*s*4 = 0; *s*4 < 4; *s*4 ++) do 68.  $R2[3][s4] \leftarrow RRa[s4]$ 69. end for

Algorithm A6. Cont.				
70.	/*Calculate fuzzy comprehensive evaluation index vector B[ ]*/			
71.	<b>for</b> ( <i>num</i> = 0; <i>num</i> < 13; <i>num</i> ++) <b>do</b>			
72.	<b>for</b> ( <i>i</i> = 0; <i>I</i> < 13; <i>i</i> ++) <b>do</b>			
73.	<b>for</b> $(j = 0; j < 4; j ++)$ <b>do</b>			
74.	$B[num] \leftarrow B[num] + W[j] * R2[i][j]$			
75.	end for			
76.	end for			
77.	end for			
78.	Take y[] corresponding to the element with largest value in B[] as the scheme $[i]$			
79.	end if			
80. en	d for			

Algorithm A7. acquisition of optimal machining element sequence

1. **Input:** all the MEs sequence TS[*i*][] 2. Output: optimal sequence OTS[] 3.  $max \leftarrow 0$ ,  $op \leftarrow 0$ ,  $F[] \leftarrow 0$ 4. for (i = 0; i < n; i + +) do//n is the number of sequences  $diff_m \leftarrow 0, diff_t \leftarrow 0, diff_D \leftarrow 0$ 5. for (j = 0; j < m-1; j + +) do//m is the number of machining element 6. 7.  $num \leftarrow TS[i][i]$ 8. if  $(me[num].m_id \neq me[num+1].m_id)$  then  $diff_m++$  end if 9. if  $(me[num].m_id \neq me[num+1].m_id \mid \mid me[num].t_id \neq me[num+1].t_id)$  then 10.  $diff_t++$ end if 11. 12. if  $(me[num].m_id \neq me[num+1].m_id \mid | me[num].TAD \neq me[num+1].TAD)$  then 13.  $diff_D++$ 14. end if 15. end for 16.  $F[i] \leftarrow 0.53^* \text{ diff}_m + 0.163^* \text{ diff}_t + 0.297^* \text{ diff}_D$ 17. end for 18. **for** (*s* = 0; *s* < n; *s* ++) **do** 19. if (F[s] > max) then 20.  $max \leftarrow F[s]$ 21.  $op \leftarrow s$ 22. end if 23. end for 24. **for** (*k* = 0; *k* < n; *k* ++) **do** 25.  $OTS[k] \leftarrow TS[op][k]$ 26. end for

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