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### Title

Agarose-Based Hydrogels as Suitable Bioprinting Materials for Tissue Engineering

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1 Agarose-based hydrogels as suitable bioprinting materials

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1 **Abstract**

2           Hydrogels are useful materials as scaffolds for tissue engineering applications. The solid  
3 content used for hydrogels require a balance between scaffold stiffness and nanoporosity, which  
4 impacts nutrient diffusion into cell-laden scaffolds. Using hydrogels with additive manufacturing  
5 techniques has been a challenge, due to inconsistencies in print fidelity. In this study, agarose-  
6 based hydrogels commonly used for cartilage tissue engineering were compared to Pluronic, a  
7 hydrogel with established printing capabilities. Moreover, new material mixtures were developed  
8 for bioprinting by combining alginate and agarose. We compared mechanical and rheological  
9 properties, including yield stress, storage modulus, and shear thinning, to determine parameters  
10 that may predict better extrusion-based printability and to assess their potential as a bioink for  
11 cell-based tissue engineering. We found that all gels demonstrated shear-thinning behavior, yet  
12 recovered immediately upon the absence of a shear stress. Print fidelity of agarose-based gels  
13 improved with the addition of alginate, which did not significantly alter yield strength ( $p > 0.1$ ).  
14 Alginate-agarose composites prepared with 5% w/v (3:2 agarose to alginate ratio) demonstrated  
15 high print fidelity with excellent cell viability that was maintained over a 28-day culture period  
16 ( $> \sim 70\%$  cell survival at day 28). Therefore, agarose-alginate mixtures showed the greatest  
17 potential as an effective bioink for additive manufacturing of biological materials for cartilage  
18 tissue engineering.

19

20 **Keywords**

21 Additive manufacturing, Bioprinting, hydrogels, 3D printing, bioinks, agarose, alginate

## 1 Introduction

2 Osteoarthritis of articular cartilage leads to chronic pain and reduced joint mobility<sup>1</sup>. The  
3 gold-standard treatment strategy for osteoarthritis is total-joint arthroplasty, where the native  
4 cartilage and some of the underlying boney tissue are removed and replaced with metal and  
5 polymer components. While successful in reducing joint pain, the mismatch in material stiffness  
6 between native tissues (0.5-1.0 MPa for cartilage<sup>2, 3</sup>) and implanted materials (0.9 GPa for ultra-  
7 high molecular weight polyethylene<sup>4</sup>) causes long-term problems, including increased  
8 degradation of the surrounding healthy tissue<sup>5</sup>. Alternatively, tissue-engineering strategies aim to  
9 recapitulate the function of healthy cartilage in the laboratory to develop implantable  
10 biomaterials for cartilage repair and replacement.

11 Hydrogels have become common scaffolds for cartilage tissue engineering, because of  
12 their ability to promote production of extra cellular matrix components in three-dimensional (3D)  
13 culture. Popular hydrogels for matrix production include sodium alginate and agarose. Agarose  
14 has been particularly successful in cultivating engineered cartilage constructs with biochemical  
15 and mechanical properties comparable to native values within eight weeks of culture<sup>6</sup>. Hydrogel  
16 selection is largely based on biocompatibility, nanoporosity, support for matrix deposition, and  
17 material behavior under specific temperature ranges or loading conditions (*e.g.*, static *vs.*  
18 dynamic loading)<sup>7</sup>.

19 Casting is the preferred fabrication method for thermoset hydrogels, with individual  
20 constructs being created with diameters that are typically less than 10 mm<sup>8-11</sup>. Implanting  
21 standard casted constructs will require surface shaping to match the patient's native curvature.  
22 However, matrix deposition does not occur evenly throughout the construct, with the construct  
23 periphery receiving more nutrients, resulting in greater matrix deposition. Therefore, resurfacing

1 an engineered construct during implantation will weaken the implanted material, altering  
2 stress distributions between engineered and native tissues, which may affect long-term  
3 durability. Recent studies have shown that clinical images (*i.e.*, magnetic resonance images or  
4 computed tomography) can be used to develop molds for larger engineered cartilage surfaces  
5 with subject-specific topography<sup>2, 15</sup>. However, cultivating larger constructs is difficult, due to  
6 the increase in nutrient path-length between nutrients surrounding the construct and cells at the  
7 center of the construct, hindering matrix production and affecting long-term cell viability<sup>12, 13, 14</sup>.

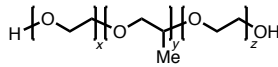
8 Extrusion-based 3D printing represents an attractive alternative to casting because of the  
9 increased versatility in construct design and ability to incorporate macropores throughout the  
10 scaffold design<sup>16, 17</sup>. However, 3D printing of hydrogels with high shape fidelity has been  
11 difficult due to issues during extrusion and material spreading after being dispensed from the  
12 nozzle. Useful materials for extrusion-based printing must demonstrate shear thinning behavior  
13 (*i.e.*, non-Newtonian behavior), where viscoelastic properties are shear-rate dependent. That is,  
14 these materials must stop flowing once deposited onto the print platform to minimize spreading  
15 and maintain shape fidelity.

16 Recent work by Mouser *et al.* demonstrated that yield strength was an important material  
17 property for determining printability, where materials with higher yield strength had better shape  
18 fidelity. Thermoset hydrogels are ideal for this purpose, as material properties are tunable based  
19 on the concentration of solids in the mixture. Previous studies have also printed hydrogels into a  
20 cooling cryogenic liquid (cryoprinting) or into an ion bath to induce crosslinking and improve  
21 print fidelity. However, increasing the solid composition and crosslinking affects nanoporosity,  
22 which will alter nutrient diffusion and tissue growth. Furthermore, cryoprinting may negatively  
23 impact long-term cell viability, if temperature gradients are not carefully controlled throughout

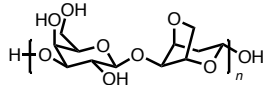
1 the construct. Therefore, there is a need to develop bioinks that are able to maintain high shape  
2 fidelity with extrusion-based printing, without compromising their ability to support *de novo*  
3 matrix growth.

4 The objective of this study was to identify a suitable non-crosslinked hydrogel for  
5 bioprinting. Specifically, we investigated mechanical properties of various concentrations and  
6 combinations of biocompatible polymers, including agarose (Type VII) and sodium alginate,  
7 which were compared to Pluronic F-127, a gel with known printing capabilities (Figure 1).  
8 Agarose and sodium alginate have been used extensively for cartilage engineering, because of  
9 their ability to promote cell proliferation and matrix production<sup>22-28</sup>. Pluronic was used as a  
10 control material for 3D printing; however, it is not considered an ideal bioink for scaffold  
11 formation, due to issues with long-term cell viability and stability in aqueous solutions<sup>8, 10, 30-32</sup>.  
12 Printable gels were then tested to confirm biocompatibility with cartilage chondrocytes for tissue  
13 engineering applications.

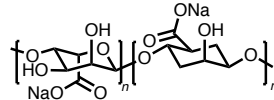
Pluronic F-127:



Agarose:



Sodium alginate:



14

15 **Figure 1.** Molecular structure of evaluated materials (Pluronic, agarose, and sodium alginate).

16

## 17 **Materials and Methods**

### 18 *Hydrogel Preparation*

19 Agarose hydrogels were prepared by mixing agarose in 0.15 M phosphate buffered saline  
20 (PBS) for final concentrations of 2%, 3%, or 4% weight by volume (w/v; Type VII powder,  
21 Sigma Aldrich, St. Louis, MO). Alginate-agarose hydrogels were prepared by mixing a 3:2 ratio

1 of agarose and sodium alginate in 0.15 M PBS (total solid content = 3.75% or 5% w/v). All  
2 agarose-based hydrogels were mixed and sterilized in a bench-top autoclave (120 °C for 25  
3 minutes). Pluronic® F-127 hydrogels were prepared at a final concentration of 30% w/v in 0.15  
4 M PBS and mixed in an ice bath until a homogeneous clear liquid formed. All solutions gelled  
5 within 10 minutes at room temperature.

### 6 *Rheology and Mechanical Testing*

7 Four experiments were performed to evaluate temperature-dependent and strain rate-  
8 dependent mechanical properties (Anton Paar MCR302 rheometer, Ashland, VA). Samples  
9 (~0.35 g; n = 5 per group) were loaded onto the Peltier plate and a steel plate was lowered to  
10 compress the gel sample (conical plate diameter = 25 mm; trimming gap = 64 µm; final gap = 54  
11 µm). Agarose-based gels were re-melted by increasing the temperature of the Peltier plate to 65  
12 °C, then allowed to gel at room temperature before each test.

13 In the first experiment, the temperature of the Peltier plate was increased at a rate of 5  
14 °C/min under a constant oscillatory stress (1 Pa at 1 Hz). A smoothing function was used to  
15 eliminate random peaks in measurements (average of every 5 points). Storage modulus, loss  
16 modulus, and phase angle were recorded.

17 In the second experiment, shear rate was increased from 0.01 to 10.00 s<sup>-1</sup> and viscosity  
18 was measured (temperature = 37 °C). Shear thinning gels were defined as those that followed a  
19 power law relationship ( $y = \alpha e^{\beta}$ ); therefore, exhibiting a linear decrease in viscosity with  
20 temperature when plotted on logarithmic scale. The parameters  $\alpha$  and  $\beta$  were used to calculate  
21 shear rate at the extruder wall using a power law relationship for non-Newtonian fluids (Equation  
22 1).<sup>33</sup> In Equation 1,  $R$  and  $L$  are the radius and length of the extruder needle, respectively,  $\gamma_w$  is

1 the shear rate at the extruder wall, and  $\Delta P$  is the pressure difference between the extruder and the  
2 atmosphere.

$$3 \quad \gamma_w = \left(\frac{R\Delta P}{2\alpha L}\right)^{\frac{1}{\beta+1}} \quad (1)$$

4 The third experiment consisted of applying the calculated shear rate at the extruder wall  
5 ( $\gamma_w$ ) for 1000 s at 37°C. The shear yield point was defined as the maximum shear stress measured  
6 in that range. The fourth and final experiment consisted of three steps: first, a constant oscillation  
7 was applied at 1 Hz for 100 s. Then, the calculated shear rate at the extruder wall was applied for  
8 800 s to induce yield, followed by a constant oscillation (1 Hz, 30 minutes, at 37 °C). Storage  
9 ( $G'$ ) and loss ( $G''$ ) moduli were measured during oscillations. The time value where storage  
10 modulus was greater than loss modulus during the second oscillation step was defined as the  
11 recovery time of the 3D hydrogel network after yielding.

12 Compressive modulus of agarose-based gel mixtures was determined under unconfined  
13 compression testing. Gels were cast into slabs between two glass slides separated with a rubber  
14 border (thickness = 2.27 mm). A 6 mm biopsy punch was used to create cylindrical samples from  
15 the slab. A monotonic ramp test to 90% strain at a rate of 0.3 %/s was applied to calculate yield  
16 strength ( $n = 10$  samples per group; Instron A620-325, Norwood, MA), which was defined as the  
17 stress at the end of the linear portion of the stress-strain curve.

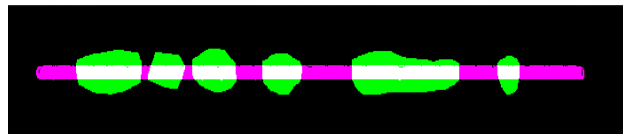
### 18 *Acellular and Cell-Based Printing*

19 To evaluate print fidelity, a commercially available 3D printer was used to print simple  
20 line and honeycomb structures (BioBots, Philadelphia, PA). Two-dimensional geometries were  
21 created using computer-aided design (CAD; AutoCad 2016, Autodesk, San Francisco, CA),  
22 converted to 3D stereolithography files (STL, 360 Fusion by Autodesk), which was then  
23 converted into g-code to be interpreted by the 3D printer (Repetier software, Willich, Germany).



1 Hydrogels were loaded into a 10 mL syringe and placed into a heated canister to maintain 37 °C  
2 during printing. Gels were extruded through a 30-gauge needle by applying 65–75 psi of  
3 pressure with an air compressor. Printed constructs were photographed next to a ruler for scale.

4 To quantify shape fidelity, a custom algorithm was developed that overlaid the CAD  
5 model with pictures of the printed construct and output the amount of (a) overlap between pixels  
6 from the printed gel and the CAD model, (b) gel pixels outside of the model area, and (c) model  
7 pixels not covered by the gel ( $n > 8$ ; MATLAB, Mathworks, Natick, MA). A printing parameter,  
8  $p$ , was defined as the percentage of correctly placed (overlapping) pixels minus the percentage of  
9 incorrectly placed (overhanging plus uncovered model) pixels ( $p = (a - b - c) * 100$ ; Figure 2).



10  
11 **Figure 2.** Example output of overlaid images from MATLAB code. The code separates gel and  
12 model pixels into one of three groups: gel pixels that do not overlap with the model are shown in  
13 green, model pixels not covered by printed gel are highlighted in magenta, and overlapping  
14 pixels are shown in white.

15  
16 Based on the results from acellular prints, agarose-alginate mixtures appeared to be the  
17 most promising gel formulation for maintaining print integrity; therefore, only agarose-alginate  
18 gel mixtures were used to evaluate cell viability after printing. Chondrocytes were acquired from  
19 juvenile bovine stifle joints within 24 hours of death. Articular cartilage was digested overnight  
20 with Type 4 collagenase (Worthington, Lakewood, NJ). Approximately 20 M cells/mL were  
21 encapsulated within agarose-alginate hydrogels for a final concentration of 3.75% (2.25%  
22 agarose + 1.5% alginate) and 5% w/v (3% w/v agarose + 2% w/v alginate) before printing.  
23 Constructs were printed as single lines (print width = 0.5 mm, length = 30 mm), cultured for 28  
24 days with chemically-defined media containing growth factors (TGF- $\beta$ ).

1           On days 0, 7, 14, 21, and 28, samples were stained and imaged to assess cell viability (n  
2 > 5 per group; Live/Dead kit, Life Technologies, Carlsbad, CA). Images were collected as a z-  
3 stack (Swept Field Confocal microscope, Praire Technologies; 10X objective), and a custom  
4 written MATLAB algorithm was used to count the number of living (green channel) and dead  
5 (red channel) cells. The percentage of living cells was calculated as the number of living cells  
6 divided by the total number of cells. Cell viability values greater than 80% were defined as  
7 successful.

#### 8 *Biochemical assay*

9           Samples were obtained at days 7, 21, and 28 to measure glycosaminoglycan (GAG)  
10 composition (n > 7 per group). Samples were lyophilized (Labconco, Kansas City, MO) for 48  
11 hours to determine dry weight and digested overnight at 56°C with Protенаise K enzyme (MP  
12 Biomedical, Burlingame, CA). GAG content was determined using the colorimetric dimethyl  
13 methylene blue (DMMB) assay and normalized by the samples initial wet weight. Data was  
14 normalized to the average GAG content at day 7 to assess tissue growth with culture time.

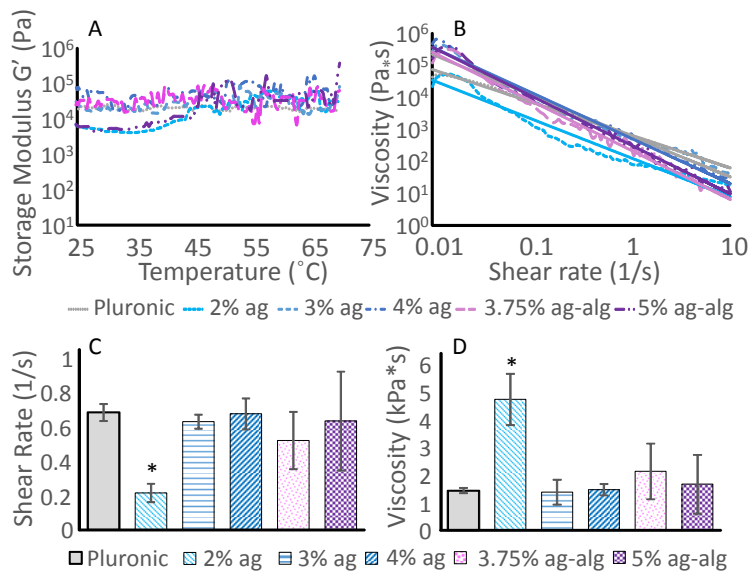
#### 15 *Statistics*

16           A one-way analysis of covariance (ANOVA) was performed on the print fidelity  
17 parameter, mechanical properties, and cell viability. Significance was assumed at  $p < 0.05$ . When  
18 significance was found, a Bonferroni post-hoc test was performed to compare each agarose or  
19 alginate-agarose mixture with the control (Pluronic). Finally, the percentage difference between  
20 print parameters for the control and agarose-based gels was calculated.

#### 21 **Results**

22           Storage modulus changed slightly with temperature over the range of 25-70 °C (Figure  
23 3A). At physiological temperature of 37°C, 2% agarose had significantly lower storage modulus

1 values than Pluronic, while there was no significant difference for 3% & 4% agarose or 3.75%  
 2 and 5% agarose-alginate (Figure 4A). All gels exhibited shear-thinning behavior, with a  
 3 logarithmically linear decrease in viscosity at higher shear rates (Figure 3B). The shear rate at the  
 4 wall ( $\alpha$ ) and viscosity ( $\beta$ ) parameters for each gel mixture are presented in Table 1. The  
 5 magnitude of the slope ( $\beta$ ) was lowest for Pluronic and increased with solid concentration in  
 6 agarose-only gels, but not agarose-alginate mixtures. The 2% agarose showed significantly lower  
 7 shear rate and significantly higher viscosity at the extruder wall when compared to Pluronic, and  
 8 no other gel showed significant differences in either parameter (Figure 3C&D). No clear  
 9 relationship between viscosity and solid concentration was observed for the range of solid  
 10 composition evaluated here.



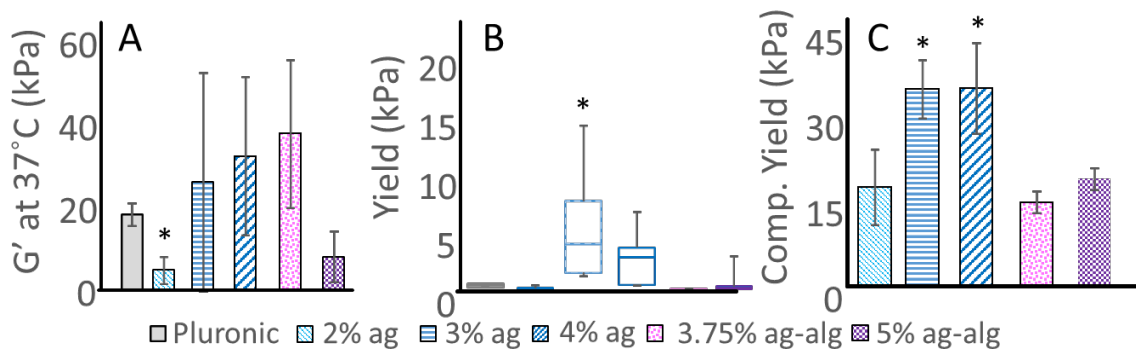
11  
 12 **Figure 3.** Mechanics: A) Storage Modulus vs Temperature, B) Viscosity vs Shear Rate, C) Shear  
 13 rate felt by gel at extruder wall, and D) Viscosity at extruder wall for all gels. \* represents  
 14 significant difference ( $p < 0.05$ ) to Pluronic.

15  
 16  
 17

Gel	R <sup>2</sup>	$\alpha$	$\beta$
Pluronic	0.99	654	-1.0
2% agarose	0.95	127	-1.2
3% agarose	0.97	613	-1.3
4% agarose	0.99	522	-1.4
3.75% agarose-alginate	0.98	221	-1.5
5% agarose-alginate	0.99	320	-1.5

**Table 1.** Power fit parameters for viscosity versus shear rate.

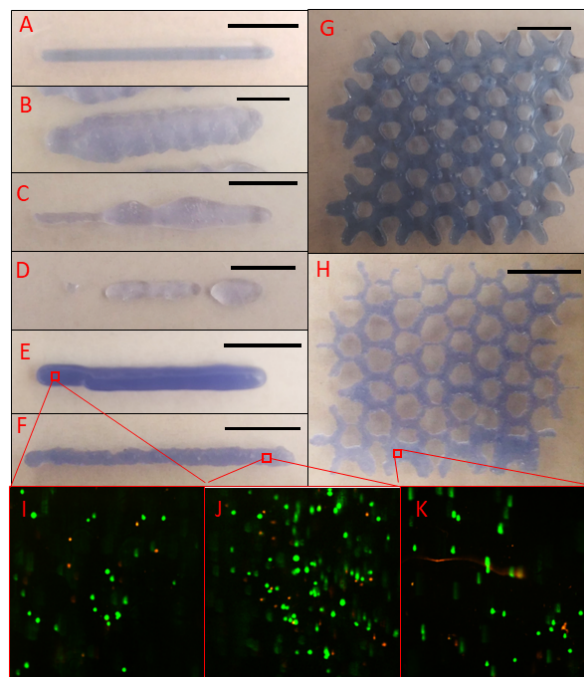
The shear yield strength for 3% agarose gels was significantly greater than the shear yield strength of Pluronic (Figure 5B). There were no other significant differences in shear yield strength, but there was high variation in yield strength measured for higher w/v agarose-only gels (3 & 4% agarose). Relaxation experiments showed that recovery after yielding was instantaneous for all gels (Figure 4). Unconfined compression could not be performed on Pluronic because the hydrogel was too soft to test. Agarose gels with 3% w/v and 4% w/v had similar compressive yield strengths, which was greater than 2% w/v agarose and the agarose-alginate mixtures (Figure 4C;  $p < 0.001$ ).



14

1 **Figure 4.** Mechanics: A) Storage modulus values at 37°C and B) Shear yield strength for  
2 all gels. \*represents significant difference ( $p < 0.05$ ) when compared to Pluronic. C)  
3 Compressive yield strength for agarose based gels. \* represents significant difference  
4 ( $p < 0.05$ ) to other groups.  
5

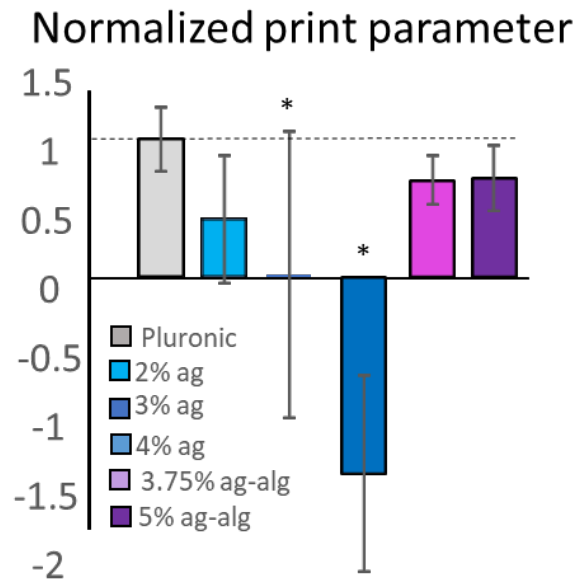
6  
7 Most gels showed limited shape fidelity, meaning that the construct was not similar to the  
8 initial model (Figure 5A-F). Smooth printed lines were achieved with Pluronic, as expected  
9 (Figure 5A). However, printability of agarose-based gels varied significantly depending on the  
10 agarose concentration and whether it was mixed with alginate (Figure 5B-F). 2% w/v agarose  
11 and 3.75% w/v agarose-alginate gels tended to spread beyond the specified print area (Figure 5A  
12 & C), while 3% w/v and 4% w/v agarose were too tough to extrude continuously (Figure 5B &  
13 D). The calculated print parameter for gels with a greater agarose concentration (*i.e.*, 3 & 4%)  
14 were significantly different from the control (Figure 6;  $p < 0.001$ ). Based on the results from  
15 printed lines, printing of more complex shapes (*e.g.*, honeycombs) was only attempted with  
16 Pluronic and agarose-alginate mixtures (Figure 5G-H).



17

1 **Figure 5.** 3D printed lines with A) Pluronic, B) 2% agarose, C) 3% agarose, D) 4% agarose, E)  
 2 3.75% agarose-alginate, and F) 5% agarose-alginate. Honeycombs printed with G) Pluronic and  
 3 H) 5% agarose-alginate. Cell viability for I) 3.75% agarose-alginate and J) 5% agarose-alginate  
 4 printed lines, and from a honeycomb print with K) 5% agarose-alginate at Day 0. Scale bars = 10  
 5 mm.

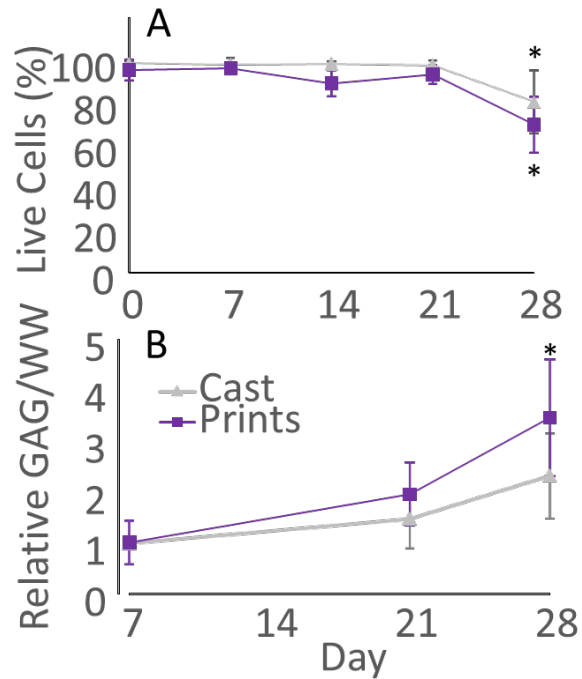
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7

8 **Figure 6.** Printing parameter results. Numbers above each group represent percentage difference  
 9 to Pluronic. Groups with an asterisks (\*) were significantly different from Pluronic ( $p < 0.001$ ).

10 Cell viability of agarose-alginate gels fabricated through 3D printing or more established  
 11 casting techniques showed predominantly living cells throughout the first three weeks of culture  
 12 (Figure 5I-K, Figure 7A). At day 28, there was a ~20% decrease in cell viability of casted  
 13 constructs (day 0 =  $97.4 \pm 0.3\%$ , day 28 =  $80.3 \pm 14.8\%$ ) and a 25% decrease in cell viability of  
 14 printed constructs (day 0 =  $93.3 \pm 4.3\%$ , day 28 =  $69.6 \pm 13.1\%$ ; Figure 7). Cell viability of  
 15 printed constructs was comparable to casted constructs, except that cell viability of printed  
 16 constructs started to decrease earlier than casted constructs (Figure 7A – day 21). GAG content  
 17 of all constructs increased with time, with printed constructs containing more than 3 times as  
 18 much GAG in Day 28 as in Day 7 (Figure 7B).



1  
 2 **Figure 7.** A) Cell viability for 5% agarose-alginate (ag-alg) scaffolds. No differences were  
 3 observed in cell viability between 3D printed lines and traditional casting, except at Day 21 ( $p >$   
 4 0.2). B) Glycosaminoglycan (GAG) content over sample wet weight (WW) normalized by Day 7  
 5 GAG/WW. Error bars represent standard deviation. \* represents significant difference to first  
 6 group.

7  
 8 **Discussion**

9 We evaluated whether hydrogels, that have been successful in developing *de novo*  
 10 cartilage, have ideal properties as unmodified bioinks for extrusion-based 3D printing.  
 11 Rheological properties and printability five variations of agarose-based gels were analyzed and  
 12 compared to Pluronic, a gel with known printing capabilities<sup>8</sup>. Agarose mixed with alginate  
 13 demonstrated similar shear thinning properties, and yield strength to Pluronic and improved  
 14 print-shape fidelity when compared to agarose-only gels. Based on print integrity and cell  
 15 viability results, 5% agarose-alginate mixture was determined to be a suitable material for 3D  
 16 bioprinting for cartilage tissue engineering. 3D printed agarose-alginate constructs demonstrated  
 17 excellent cell viability for up to 21 days in culture, as well as improved GAG production.

1 Many variables factor into print outcomes for extrusion based printing, including print  
2 pressure, gel temperature, and gel mechanics. Previous studies have highlighted the importance  
3 of extruded materials to have shear thinning properties and a low yield strength. Rheology  
4 experiments suggested that 2% agarose, 3.75% agarose-alginate, and 5% agarose could be  
5 continuously extruded and therefore printable. All gels exhibited shear thinning behavior defined  
6 as a decrease in viscosity when exposed to shear stress (Figure 4). Such behavior has been  
7 determined as necessary to extrude from a nozzle and deposit material on a printing bed.  
8 However, another requirement that has been previously reported for extrusion is the presence of  
9 a shear yield point below 5 kPa. Our results are consistent with these findings, as gels that  
10 consistently filled the model area showed yield strengths of that magnitude (Figure 5). Gels that  
11 showed limited success with extrusion-based printing had yield strengths significantly higher  
12 than Pluronic (3% & 4% agarose; Figures 5 & 7).

13 To quantify print integrity observations we developed an analysis that resulted in a  
14 printing parameter that includes an assessment of the gel's ability to print within the specified  
15 print area, accounting for missed areas or overspreading. The addition of a printing parameter  
16 suggested that gels that were able to be extruded (2% agarose, 3.75% agarose-alginate, and 5%  
17 agarose-alginate) printed with suitable shape fidelity (Figure 7). The print parameter calculated  
18 for these gels was not statistically different from Pluronic, nor was it significantly different  
19 between gels once normalized by the control (Figure 7). However, it became apparent that 2%  
20 agarose and 3.75% agarose-alginate showed significant spreading of gel outside the model area  
21 (Figure 6). We initially believed this was due to a delayed recovery of the gel network after  
22 extrusion, but rheology experiments showed that all gels maintained an intact network during  
23 shearing (Figure 4). Percentage difference between 2% agarose and Pluronic was almost twice as



1 large as that between agarose-alginate gels and Pluronic (Figure 6). For this reason, 5% agarose-  
2 alginate was chosen as the best candidate for cell experiments.

3 The agarose-alginate mixture (5% w/v) showed excellent cell viability for up to 21 days  
4 in culture, as well as production of GAG over a 28 day period in both casted and printed  
5 constructs (Figure 8 & 9). Casted constructs have been used extensively in cartilage engineering  
6 applications and have been shown to promote matrix production. The absence of significant  
7 differences in cell viability between casted constructs and printed constructs agrees with work by  
8 Blaeser et al that the printing process does not cause immediate damage to cells. Printed  
9 constructs also showed a slightly higher GAG content than casted constructs, although there was  
10 no significant difference when compared to printed constructs (Figure 9; p-value). We believe  
11 that this difference was influenced by geometric reasons, as printed lines are thinner (~0.5mm  
12 wide) than casted constructs (diameter = 2.27 mm) and as such there is less distance for nutrients  
13 in the media to travel. The similarities in GAG production between casts and prints lead us to  
14 believe that the 5% w/v agarose-alginate gel is a suitable bioink.

15 Rheological properties for all gels were evaluated at physiological temperature (37°C)  
16 instead of a wider range to match the temperature during cell-based printing.. Given that agarose  
17 is a thermoset material, it remains plausible that agarose-only gels can produce constructs with  
18 high shape fidelity under different temperature conditions. The findings in this study did not  
19 show a definitive rheological property that correlated to print integrity, but our results are  
20 consistent with previous findings that suggest yield strength and shear-thinning are factors in  
21 being able to extrude a material continuously (Figure 4 & 5). The primary focus of cell-based  
22 test in this study was to evaluate cell viability. Future work will evaluate matrix production of  
23 other constituents, such as collagen, and evaluate tissue mechanics over time.

1 **Conclusions**

2           In conclusion, the 5% w/v agarose-alginate mixture was ideal for extrusion-based  
3 bioprinting of 3D cartilage constructs. The mixture was able to print high shape fidelity  
4 structures comparable to Pluronic without the necessity of additional crosslinking or printing  
5 inside sacrificial materials, a technique that may affect long-term performance by including  
6 additional steps in the fabrication process. Moreover, the agarose-alginate mixture maintained  
7 excellent cell viability and supported GAG production. Therefore, extrusion-based printing may  
8 provide researchers with an easy-to-manufacture technique for developing complex engineered  
9 tissues.

10

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8 **Competing interests statement**

9 The authors have no competing interests to declare.

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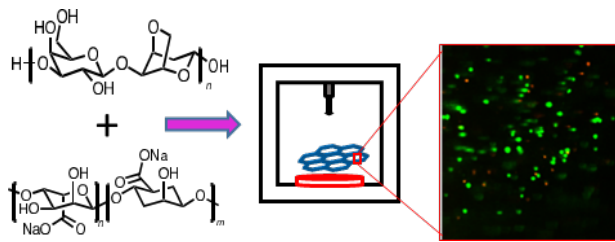
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7 **For Table of Contents Only:**



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TOC Graphic: Agarose-alginate bioinks