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Theoretical Study of the Benefit of Long Axial Field-of-View PET on Region of Interest Quantification

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Abstract

The aim of this study is to evaluate the benefit of long axial field-of-view (AFOV) PET scanners on region of interest (ROI) quantification. We simulated a series of PET scanners with an AFOV ranging from 22 cm to 220 cm. A theoretical framework was used to predict the contrast recovery coefficient (CRC) and the variance of ROI quantification in penalized maximum likelihood (ML) image reconstruction, in which the resolution and noise tradeoff was controlled by a regularization parameter with a quadratic penalty function. The characterization was based on the converged penalized ML reconstruction with an accurate system model. We examined quantification of a 2-mm ROI and 10-mm ROI in a clinically relevant scan range of 110 cm. Multiple bed positions with 50% overlap were used for scanners with shorter AFOV to provide a relatively uniform sensitivity across the 110 cm axial range. A uniform water cylinder of 20 cm in diameter and 230 cm in length was chosen to model the attenuation and background activity. We computed the variance reduction factor at fixed resolution. Effects of different detector capabilities, including TOF (time-of-flight) resolution (320 ps, 500 ps, and non-TOF) and DOI (depth-of-interaction) resolution (4 mm, 10 mm, and no DOI), were evaluated. The results show that at a normal activity level (370 MBq), the 220-cm AFOV scanner offers a ~ 17-fold variance reduction for the 2-mm ROI and ~26-fold variance reduction for the 10-mm ROI (both measured at CRC=0.5) over the 22-cm AFOV scanner when both using detectors with 500 ps TOF resolution no DOI capability. The variance reduction factors of trues-only are higher than those of including scatters and randoms. Combining 320 ps TOF and 4-mm DOI, the 220-cm long scanner offers a ~45-fold variance reduction over the 22-cm long reference scanner (500 ps TOF, no DOI) for imaging 2-mm and 10-mm ROIs. The variance reduction factors are higher at a lower activity level due to lower random fraction. In conclusion, our study demonstrates that a long AFOV scanner can greatly improve the quantitative accuracy of PET imaging compared to current state-of-the-art clinical PET scanners.

Keywords

positron emission tomography; long axial field of view; ROI quantification

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1. Introduction

Positron emission tomography (PET) is a major imaging modality for high-sensitivity molecular imaging to visualize and track biochemical process of interest using radiotracers (Cherry 2004). It has been widely used for clinical diagnosis (e.g. oncology, neurology and cardiology), biomedical research, and translational medicine. However, the image quality of PET is mainly limited by the number of coincidence photon pairs that are recorded in each PET scan due to low sensitivity and concerns regarding radiation dose. To overcome the limitation of current PET scanners and explore new applications of PET, we are building a 2-meter long PET scanner, called the EXPLORER (<http://explorer.ucdavis.edu>) that will dramatically improve the photon detection efficiency for long axial FOV (AFOV) scans (Badawi *et al* 2013, Cherry *et al* 2017, Badawi *et al* 2018, Zhang *et al* 2018b). In addition to the improved sensitivity, it can cover the entire human body and will provide total-body high temporal resolution dynamic PET scans for the first time (Zhang *et al* 2014a). The EXPLORER project has stimulated growing interest in developing long AFOV PET scanners, with several alternative versions of the EXPLORER under development (Karp *et al* 2017, Viswanath *et al* 2017). To date we have built a small-scale version of the EXPLORER scanner (called mini-EXPLORER) using Siemens Biograph mCT PET detector modules (Berg *et al* 2018a, Berg *et al* 2018b). It has a ring diameter of 44 cm and an AFOV of 45 cm and can perform extended AFOV PET imaging of non-human primates and medium-size animals. High-quality images have been obtained for low-dose high-temporal-resolution dynamic imaging (Zhang *et al* 2017b). A second device (mini-EXPLORER-II) with broadly similar geometry but smaller crystals and better timing resolution has also been developed by United Imaging Healthcare (UIH) (Lv *et al* 2017).

Simulation studies have been performed to examine the benefit of extended axial FOV for PET imaging. Most of these studies were based on the noise equivalent count rate (NECR) (MacDonald *et al* 2017, Poon *et al* 2012, Isnaini *et al* 2014). In particular, Poon *et al* (Poon 2013, Badawi *et al* 2013) have shown that a 2-meter long scanner provides a factor of 40-fold gain in TOF-weighted NECR (Conti 2006) compared to a Siemens mCT PET using simulation models of the mCT scanner (Poon 2015). However, NECR (including TOF-weighted NECR) is only a function of count rates for true, scattered and random events. It does not take into account the spatial resolution of the detectors and hence may not truly reflect image quality. Surti *et al* (Surti *et al* 2013, Surti *et al* 2015) evaluated image quality in terms of lesion detectability, but only for simulated scanners with an AFOV up to 75 cm.

In this work, we evaluate the benefit of long AFOV scanners for region of interest (ROI) quantification with modeling of geometric sensitivity, detector resolution, and TOF resolution. We focus on a clinically relevant scan range of 110 cm for oncologic PET. We study a series of PET scanners with AFOV ranging from 22 cm to 220 cm. Contrast recovery coefficient (CRC) and variance of ROI quantification are analyzed using theoretical formulae that have been developed and validated for converged penalized maximum likelihood image reconstruction on typical whole-body scanner geometries (Qi and Leahy 1999, Qi and Leahy 2000, Qi and Huesman 2006). Benefits of using detectors with better time-of-flight (TOF) resolution and depth-of-interaction (DOI) capability have also been

examined to provide guidance for the future development of long AFOV scanners. The performance gain as a function of injected activity level has also been studied.

2. Materials and Methods

2.1. Scanner configurations

We examine a series of PET scanners with a range of AFOVs (Zhang *et al* 2017c). The simulated configurations are broadly based on the detector modules of a Siemens Biograph mCT PET scanner (Jakoby *et al* 2011). The ring diameter of the scanners is fixed at 83.5 cm. Each detector ring is formed by 48 detector blocks (48B). Each detector block consists of a 13×13 array of 4.0×4.0×20 mm³ lutetium-yttrium oxyorthosilicate (LYSO) scintillator crystals and has dimensions of 52 mm×52 mm. The energy resolution is set at 11.7% and energy window is 435-650 (keV). We did not model detector dead-time or pulse pile-up effects. Each PET scanner is made of multiple detector rings with a 4-mm axial air gap between adjacent detector rings. In total we simulated 4 designs with 4, 8, 20, and 40 block detector rings, which we refer to as 4R, 8R, 20R, and 40R in the following discussion. Table 1 shows the axial FOV of the simulated designs together with their respective solid angle coverage for a point at the center of the FOV.

2.2. ROI quantification

We use the theoretical formulae derived for converged penalized maximum likelihood (PML) image reconstruction to compute the CRC and variance of ROI quantification. These formulae have been verified extensively against Monte Carlo reconstructions (Qi and Leahy 1999, Qi and Leahy 2000, Qi and Huesman 2006). While previous validations were performed for typical whole-body PET geometries, we expect that the accuracy of the formulae holds for the central 110-cm axial range inside the 40R scanner, where the resolution and variance are relatively uniform (see figure 3(b)). Applying these formulae to regions near the axial ends of the 40R scanner may require further validation.

For completeness, we briefly describe the formulae and refer readers to the references for more details. We focus on the penalized likelihood image reconstruction that estimates the unknown PET tracer distribution x from the measured data y by

$$\hat{x} = \arg \max L(y|x) - \beta x' R x \quad 1$$

where $L(y|x)$ is the log Poisson likelihood function, β is a regularization parameter, and R is the second-order derivative of the penalty function. The expectation of the PET data \bar{y} are given by

$$\bar{y} = E[y|x] = P x + \bar{s} + \bar{r} \quad 2$$

where P is the system matrix that models the probability of detecting an event originated from each image voxel in each line of response (LOR), \bar{s} and \bar{r} are the expectations of scatters and randoms, respectively.

Let f_I be the indicator function of an ROI. The mean activity inside the ROI can be calculated by

$$A = \frac{1}{|f_I|} \hat{x}' f_I \quad 3$$

where $|f_I|$ denotes the number of voxels in the ROI. The performance of the ROI quantification can be measured by the bias and variance of A . When the background activity is known (or can be estimated accurately), the bias of the ROI is directly related to the contrast recovery coefficient (CRC) that is defined as

$$\text{CRC} = \frac{A/B - 1}{A^{\text{true}}/B - 1} \quad 4$$

where A^{true} is the true activity inside the ROI and B is the background activity. Using the formulae derived previously (Qi and Huesman 2006), the CRC and variance of an ROI can be approximated by

$$\text{CRC} \approx \frac{1}{|f_I|} f'_I [F + \beta R]^{-1} F f_I \quad 5$$

$$\text{Var} \approx f'_I [f + \beta R]^{-1} F [F + \beta R]^{-1} f_I \quad 6$$

where F is the Fisher information matrix (FIM) that is given by

$$F = P' \text{diag}\{1/\bar{y}\} P \quad 7$$

Direct inversion of the Fisher information matrix is difficult because of its large size. Fortunately, for a small ROI, the above equations can be evaluated by using the locally shift-invariant approximation and fast Fourier transform (Qi and Leahy 2000). The formulae become

$$\text{CRC} \approx \frac{1}{N|f_I|} \sum_{i=0}^{N-1} \frac{\lambda_i |\gamma_i|^2}{\lambda_i + \beta \mu_i} \quad 8$$

$$\text{Var} \approx \frac{1}{N} \sum_{i=0}^{N-1} \frac{\lambda_i |\gamma_i|^2}{(\lambda_i + \beta \mu_i)^2} \quad 9$$

where λ and μ are the Fourier transform of the images formed by the column vectors of \mathbf{F} and \mathbf{R} corresponding to the ROI location, respectively, and γ is the Fourier transform of image of f_f . N is the number of voxels in each image. Equations (5) and (6) were used to compute the CRC vs. variance tradeoff of ROIs located along the central axis of each scanner. CRC and variance curves were calculated by varying the regularization parameter β of the PML reconstruction and the variance reduction factors of long AFOV scanners over the 22-cm 4R scanner were computed at fixed CRC values.

To compute one column of the FIM, $F e_f = P' \text{diag}\{1/\bar{y}\} P e_f$, where e_f is a unit vector with one at the center of the ROI and zero elsewhere, we need three operations: (i) calculation of the forward projection of a point source at the center of the ROI, $P e_f$, (ii) calculation of the forward projection of the background, \bar{y} , and (iii) backprojection of the ratio between $P e_f$ and \bar{y} . SimSET (Harrison *et al* 2006) was used to estimate the point source projection by tracking annihilation photons emitted from the point source for all scanner configurations. The forward projection of the uniform background and backprojection operation were performed using a pre-computed system matrix. The system matrix \mathbf{P} was computed using a multi-ray-tracing projector that divides each detector crystal into $4 \times 4 \times 20$ sub-elements and traces all the possible lines connecting the elements of two detectors after weighting by the crystal attenuation (Zhou and Qi 2011). It models the spatially variant point spread function (PSF) and LOR-dependent detection response. We used an image dimension of $135 \times 135 \times 1119$ with $2 \times 2 \times 2$ mm³ voxels to cover a FOV of 27 cm transaxially and 223.8 cm axially. To model the background, we first simulated a point source at various locations inside an XCAT 2.0 phantom (Segars *et al* 2010) and plotted the central sensitivity ratio over the 4R reference scanner as a function of axial FOV in figure 1(a). Clearly the sensitivity curve varies substantially from location to location due to attenuation effect. To simplify the comparison, we used a uniform water cylinder to model the attenuation and background activity, and fitted the diameter of the cylinder to match the average sensitivity curve of the XCAT phantom. Figure 1(b) shows that the fitted water cylinder (20 cm diameter and 220 cm long) provides a sensitivity curve that matches very well to the average of the XCAT phantom for scanners with an AFOV from 22 cm to 220 cm.

2.3. Evaluation studies

We focus on the clinical whole-body oncology imaging scenario to image an extended axial scan range of 110 cm. This corresponds to an “vertex to thighs” FDG scan protocol frequently used in cancer imaging. Quantification performance for single-bed imaging scenario can be found in our previous work (Zhang *et al* 2017c). In the experiments, we did not restrict the maximum acceptance ring difference and all detected events from each scanner were used. For scanners with a shorter axial FOV, multiple bed positions with 50% axial overlap were used. Specifically, the number of bed positions were 11 for 4R, 6 for 8R, 2 for 20R, and 1 for 40R. We did not include the 20R single-bed scan, because its sensitivity drops to zero at the edge of the 110-cm scan range. Figure 2 illustrates the scan protocols of the extended 110-cm scan range imaging. The total scan time was kept the same. In all imaging scenarios, we evaluated the CRC versus variance curve for quantifying a 2-mm ROI (one cubic voxel) and 10-mm ROI ($5 \times 5 \times 5$ cubic voxels) at the radial center, but different axial positions. Because the relative performance between scanners is independent of the

ROI contrast according to the theoretical equations, we set the activity ratio between each ROI and the background to 2:1 in all comparisons. Two TOF resolutions (500 ps and 320 ps) and two DOI resolutions (10 mm and 4 mm) were simulated and compared with the non-TOF and no DOI scanners. The 500 ps TOF was commonly available in commercial PET scanners (Jakoby *et al* 2011) and 320 ps TOF has also been reported in recent published work (Peng *et al* 2015, Miller *et al* 2015, Zhang *et al* 2018a). The choice of DOI resolutions also covered the range that had been reported in the literature (Du *et al* 2018, Zhang *et al* 2013a, Zhang *et al* 2013b). Two different activity levels, 20 MBq and 370 MBq, were investigated to represent a low dose and a regular clinical dose studies, respectively.

2.4. Scatters and randoms estimation

We used SimSET software package to estimate the scatter mean. Because of the relatively smooth nature of the scatter sinogram, we grouped the detected scatter events in detector block pairs, used a coarse TOF bin (225 ps), and then interpolated between adjacent LORs (and TOF bins) to calculate the mean \bar{s} for each event (Zhang *et al* 2014b, Zhang *et al* 2017a).

We use a Poisson random variable with the mean $R_{ij} = 2\tau_{ij}S_iS_j$ to simulate the randoms rate in each LOR, where S_i and S_j are the singles rates of crystals i and j , respectively, and $2\tau_{ij}$ is a ring-difference dependent variable coincidence timing window (CTW) which we used to reduce the number of random events in nonTOF data along the oblique LORs. To calculate the CTW for an event with ring difference L , we use the formula $\tau_{ij} = \sqrt{D^2 + L^2}/c$, where D is the diameter of transaxial FOV (e.g. 60 cm), and c is the speed of light in a vacuum. The resulting CTWs for the events with ring difference of 4R, 8R, 20R, and 40R are 4.26, 4.96, 8.35, and 15.20 ns, respectively. The CTW for the 4R scanner is similar to the value used in the Siemens mCT scanner (Jakoby *et al* 2011). For TOF data, the formula of random mean in each timing bin is $R_{ij}^{TOF} = \tau\Delta S_iS_j$ with $\tau\Delta$ as the timing bin size which is 25 ps in our simulated study. Note that this singles rate based formula assumes taking all possible coincidence pairs in case of multiple (>2) hits within a CTW.

To estimate the singles rates, we ran a SimSET simulation in ‘SPECT’ mode and then doubled the event rates to get the singles rates for PET. The ^{176}Lu source in L(Y)SO cannot be simulated directly using SimSET. Instead we used a measured singles rate of 105 cps/cc (within the energy window of 435 to 650 keV) based on Siemens mCT block detectors (Berg *et al* 2016). Therefore, the singles rate from L(Y)SO background is about 33.6 cps per crystal (volume of 0.32 cm³), which was added to the singles rates from the emission object.

3. Results

3.1. Axial sensitivity

Figure 3 shows the comparison of sensitivity along the axial axis provided by different scanners for imaging an extended axial scan range of 110 cm without and with object attenuation. All the curves are normalized to the maximum sensitivity of the 4-ring scanner (4R). Figure 3(b) shows the relatively uniform sensitivity across the 110-cm axial FOV for

40R, and is due to the attenuation effect through the long cylinder phantom. Overall, the 40R geometry offers ~30-fold higher sensitivity over the 4R scanner for the 110 cm scan range, and ~10 and 1.4~2.8-fold higher sensitivity over the 8R and 20R scanners, respectively. Note that the axial sensitivity profiles of 20R and 40R scanners do not follow a triangular shape for a single bed position even without consideration of object attenuation (see (Zhang *et al* 2017c)) because the solid angle is not a linear function of the axial length. As a result, there are noticeable variations in the 20R sensitivity profile with 50% bed overlap. While a 30% bed overlap would improve the axial uniformity of the 20R scanner, this would reduce the overall sensitivity within the 110-cm scan range and hence the overall performance of the 20R scanner. For a comprehensive comparison, we evaluated the quantification performance for an ROI located at both the maximum (best) and minimum (worst) sensitivity locations inside the 110-cm axial scan range for each scanner.

3.2. ROI quantification

We first consider detectors with 500 ps TOF and no DOI. Figure 4(a) shows the CRC vs. variance of the 4 scanners for imaging the 2-mm ROI in the cylinder with 370 MBq total activity. Each curve was obtained by varying the regularization parameter β and represents the performance of the PML reconstruction at convergence. All prompt events (trues + scatters + randoms) were included for analysis. We can see almost overlapping curves for the 40R at center and 55-cm axial offset, indicating that the 2-meter long scanner can provide very uniform image quality over the central 110-cm axial scan range. The performance of the 20R is worse than that of the 40R scanner. The best and worse CRC vs. variance curves of the 20R with 2 beds have a large gap, due to the sensitivity variation shown in figure 3(b). While the gap can be reduced by using a 30% bed overlap, the average performance would also be reduced due to the reduction in the overall sensitivity in the 110-cm scan range.

For an easier comparison, figure 4(b) plots the variance reduction factor of different scanners over the 4R scanner. We can see that the 40R has a ~ 19-fold gain over the 4R for the 2-mm ROI at CRC level of 0.1 and this gain reduces to ~ 16 at a CRC level of 0.6. The decrease is due to the fact that LORs with larger ring difference suffer more crystal penetration effect and have worse axial resolution than LORs with less ring difference. As a result, they are less useful for high resolution (2-mm ROI with high CRC) imaging.

Figure 4(c) shows the CRC vs. variance curves of the 4 scanners for imaging the 10-mm ROI, and Figure 4(d) shows the variance reduction factor curves. We can see that for imaging the 10-mm ROI across an extended axial FOV, the 40R has a ~26-fold gain over the 4R, ~8-fold gain over the 8R, and 1.2~2.4-fold gain over the 20R. The variance reduction gain is higher for the larger 10-mm ROI than that for the 2-mm ROI due to less impact from the axial parallax error of oblique LORs.

3.3. Effect of DOI

Figure 5 shows the CRC vs. variance curves and the variance reduction factor curves for the scanners using detectors with 500 ps TOF and 4-mm DOI. Adding DOI information does not change the performance of 8R and 4R scanners because the ROIs are at the radial center.

However, the performance of 20R and 40R scanners is substantially improved by using DOI detectors, especially for the 2-mm ROI. The variance reduction factors of the 40R scanner increased from 17 (no DOI) to 24 (4-mm DOI) for imaging the 2-mm ROI (CRC=0.5) and the difference between 40R and 20R also becomes larger. We can see that even though the ROI is located at the radial center, DOI can still improve the ROI quantification by reducing axial parallax error.

Since the variance reduction factor remains relatively stable over a wide range of CRC values, we will show only the variance reduction factor at CRC=0.5 hereinafter. We also used the average of the best and worse cases of each scanner for easy comparison.

3.4. Effect of scatters and randoms

Figure 6 shows the scatter fraction ($SF=S/(T+S)$) and random fraction ($RF=R/(T+S+R)$) as a function of block ring difference. The random fraction was examined at two activity levels (20 MBq and 370 MBq). As described in Section 2.4, random event rate was calculated using the ring-difference dependent CTW. We see that both scatter fraction and random fraction increase as the block ring difference increases and LORs with block ring difference greater than 20 mostly contain random events, even at low activity level (20 MBq) due to ^{176}Lu background radiation.

To evaluate the effect of the scatters and randoms, we computed the CRC and variance using events of trues-only, trues + scatters, trues + scatters + randoms, separately. Figure 7 shows the variance reduction factors for the 10-mm ROI using the 500 ps TOF scanners without DOI. The total activity was 370 MBq and the 4R scanner was used as the reference. Clearly the variance reduction factors of trues-only are higher than those of including scatters and randoms. The performance gain of long AFOV scanners reduces slightly when scatters and randoms are included due to higher scatter and random fractions in more oblique LORs as shown in figure 6.

3.5. Effects of TOF and DOI

Using the 4R scanner with 500 ps TOF and no DOI (similar to Siemens mCT scanner) as the reference, we evaluated the performance gain of long AFOV scanners with different TOF and DOI resolutions, for all prompt events. Figure 8 plots the variance reduction factors for imaging a 2-mm ROI and 10-mm ROI over the 110-cm axial scan range using different scanners. The effect of TOF is more substantial than that of DOI, especially for larger ROIs. Furthermore, TOF improvement is nearly independent of ROI size and the length of the scanner: 320 ps TOF achieves ~3-fold variance reduction ratio over nonTOF, and ~1.6-fold over 500 ps TOF. In comparison, better DOI resolution produces higher gain for longer scanners than for shorter scanners. This is due to the reduction of the axial parallax error for oblique LORs with DOI. Combining 320 ps TOF and 4 mm DOI, the 220-cm long scanner offers a ~44-fold variance reduction over the 22-cm reference scanner (500 ps TOF, no DOI) for imaging a 2-mm ROI and ~47-fold variance reduction for imaging a 10-mm ROI.

3.6. Effect of activity level

In addition to the normal activity level of 370 MBq, we also simulated low-dose imaging with 20 MBq total activity. The results are shown in Figure 8 for comparison. We can see that the performance gains of long AFOV scanners over the 22-cm long scanner are slightly higher at the low activity (20 MBq) than at the normal activity (370 MBq) level because the random fractions are lower at the low activity level. However, due to the intrinsic background radiation of ^{176}Lu in the L(Y)SO crystal, the effect of randoms cannot be completely eliminated by further reducing the injected activity.

4. Discussion

In this paper, we used theoretical analysis to evaluate the PET quantification performance gain of long AFOV scanners for a clinically relevant scan range. For a specific TOF and DOI resolution, the 220-cm long scanner offers a 17~28-fold variance reduction for imaging an extended 110-cm axial scan range over the 22-cm scanner. The 220-cm long scanner also offers a 1.2~2.4-fold improvement over a 110-cm long scanner (2 beds). These theoretical results are congruent with our previous Monte Carlo simulation studies comparing the EXPLORER scanner with a 4-ring scanner, where we obtained a variance reduction factor of ~4.2 for static torso imaging and ~47 for total-body imaging (Zhang *et al* 2017a). The larger gain in the referenced study is because a longer scan range of 2-m was examined in the comparison.

There are some limitations in this study. Firstly, we only investigate the ROI along the central axial axis of the FOV. This setup is sufficient for the evaluation of relative performance between long AFOV scanners and short AFOV scanners. While the radially centered ROIs do not suffer parallax error in the transaxial plane, we can still observe the benefit of DOI in long AFOV scanners. However, the importance of DOI is underestimated for this reason. To completely understand the importance of DOI, radially off-centered ROIs should also be considered. Secondly, dead-time and pulse pile-up effect were not modeled and we assumed the prompts and singles rates are linearly related to the total activity, excluding the intrinsic LSO background radiation. This assumption is valid for the simulated activity level (~3.7 kBq/cc) according to published data for mCT scanners (Jakoby *et al* 2011, Poon *et al* 2012). Although this may not hold for higher activity levels, we expect these detector level effects are independent of the AFOV of a scanner and hence do not affect the performance gain of long AFOV scanners. Thirdly, we used a 20-cm diameter uniform cylinder as the background to match the average sensitivity gain of the XCAT phantom. However, the sensitivity gain, as well as scatters and randoms, will be dependent on surrounding tissues and organs in a real patient. Therefore, the variance reduction factor obtained in this paper should be treated as a rough estimate of the average performance gain and the exact the variance reduction factor in a real scan will depends on a number of factors, including spatial location, activity distribution, and attenuation of surrounding tissue. Lastly, equations (5)–(9) are for fully converged penalized ML reconstruction with an accurate system model. In practice, reconstruction algorithms may be terminated before convergence due to various reasons. The effects of early termination and modeling error are not examined in this study.

5. Conclusion

In this work, we have theoretically evaluated the benefit on ROI quantification for long axial FOV scanners. The comparison results show that the 220-cm scanner with 320-ps TOF and 4-mm DOI offers up to a factor of ~45-fold variance reduction for imaging the 2-mm and 10-mm ROI within an extended 110-cm axial scan range over an existing 22-cm long scanner with 500-ps TOF and no DOI. The TOF gain is nearly independent on the scanner axial length and ROI size, while the DOI capability mostly benefits small ROIs. Our future work will include further validation using experimental data.

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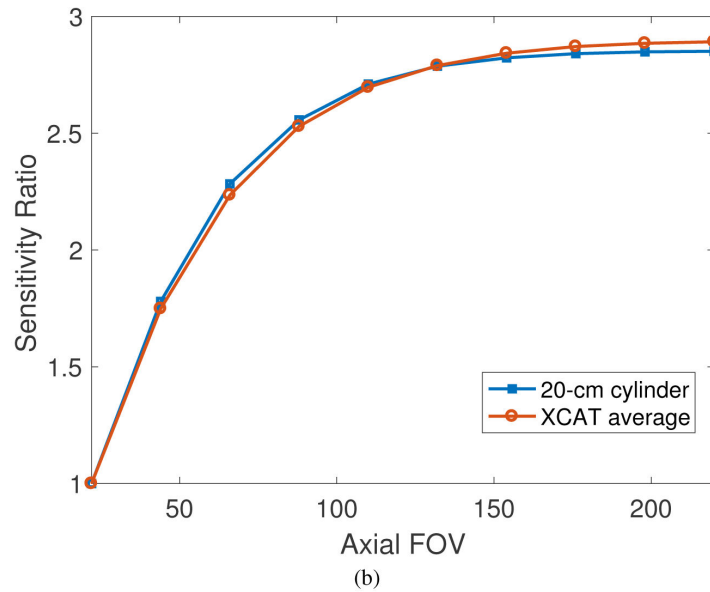
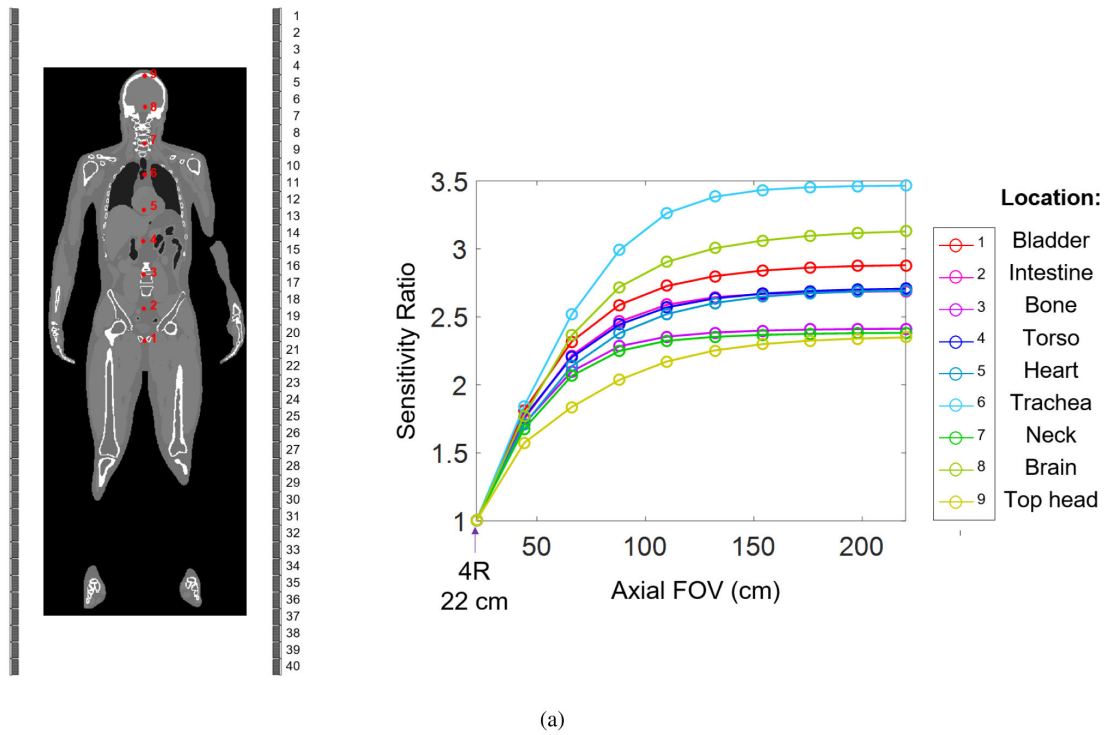


Figure 1:
 (a) Sensitivity ratio of nine ROIs (red dots) in the XCAT phantom as a function of axial FOV. (b) Sensitivity ratio of XCAT simulation (averaged over the nine ROIs) and water cylinder phantom ($D=20$ cm) as a function of axial FOV. The reference scanner is the 22-cm long 4R scanner.

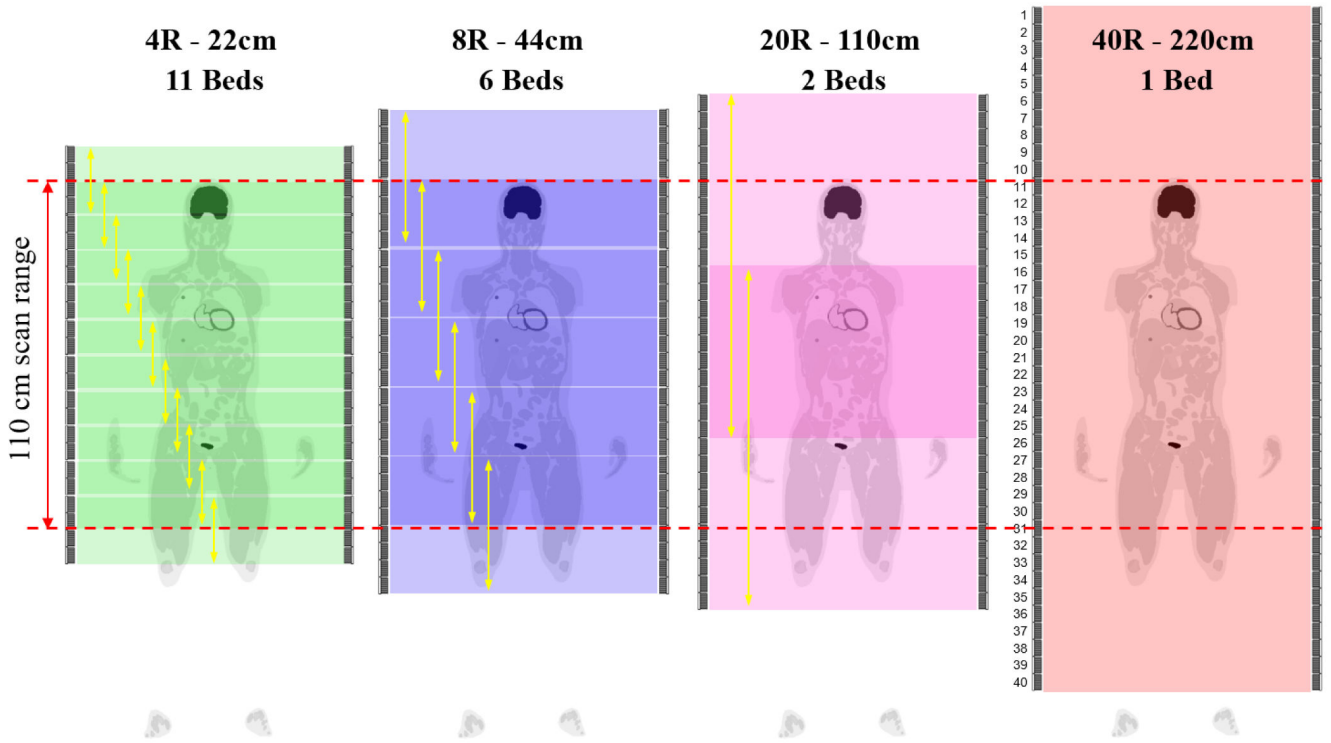


Figure 2:
 Comparison studies of extended 110 cm scan range imaging using 4, 8, 20, 40 block rings (4R, 8R, 20R, 40R). Multiple-bed scan protocol (50% overlap) were used for shorter scanners.

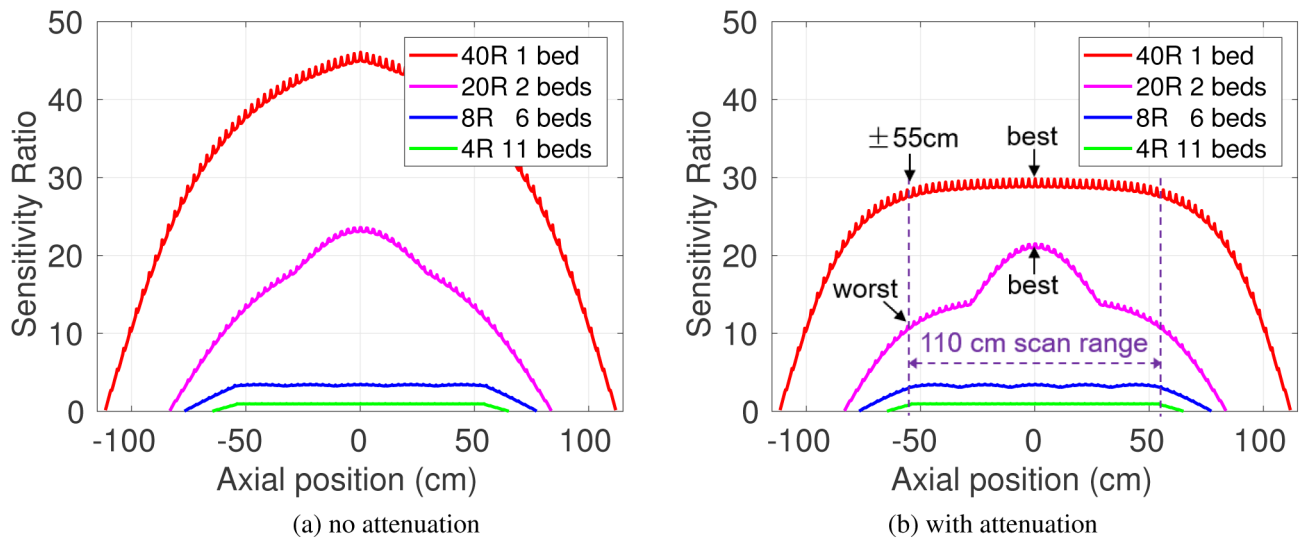


Figure 3: Sensitivity ratio along axial axis (absolute values were scaled to that of 4R): (a) source in air (without attenuation), and (b) source in cylinder phantom. The relative flat sensitivity in 40R is due to the attenuation effect through the long water cylinder.

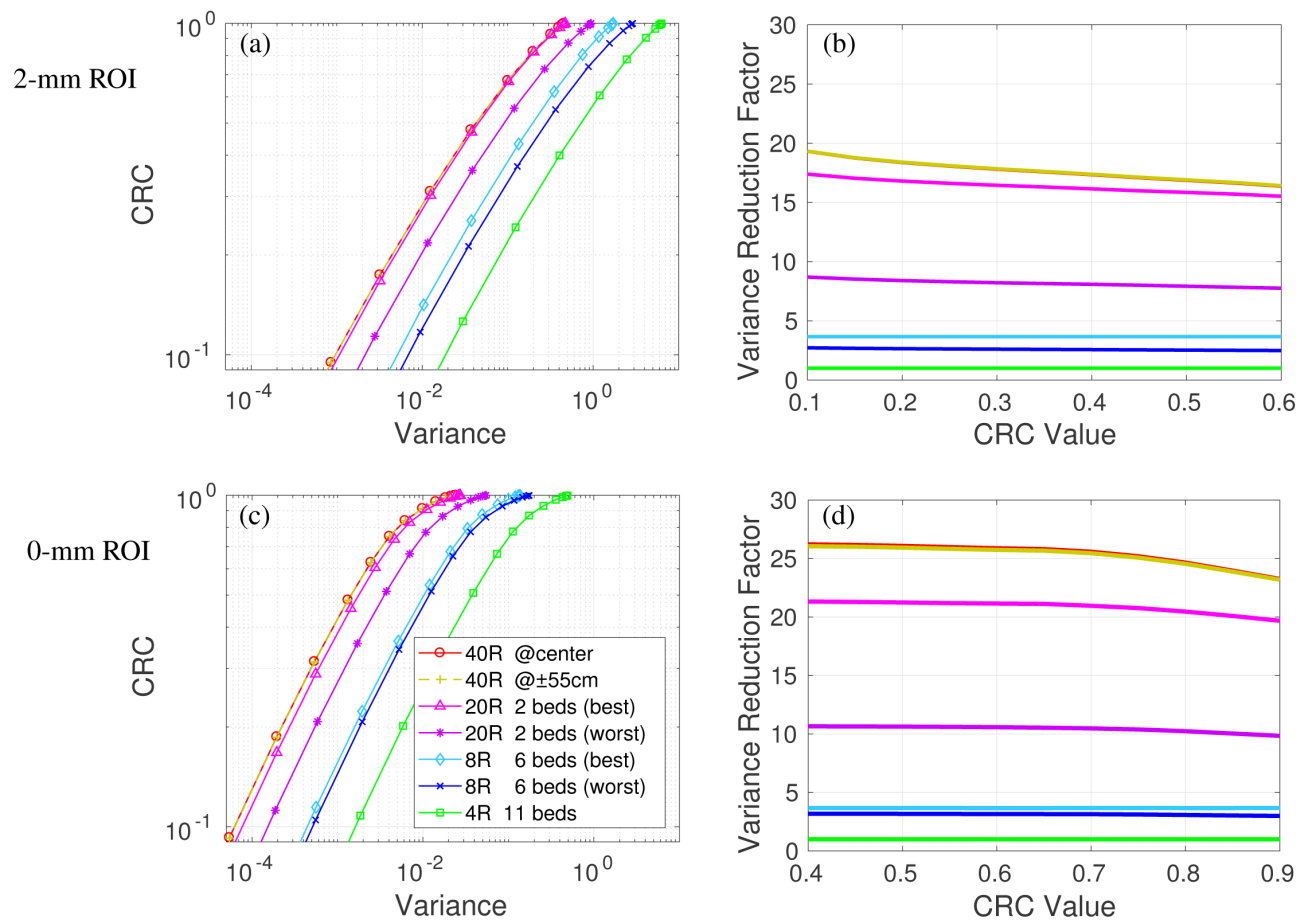


Figure 4: Quantification performance of the four scanners with 500 ps TOF and no DOI detectors. All prompt events (true+scatters+randoms) are considered. CRC vs. variance curves of a 2-mm ROI (a) and 10-mm ROI (c); Variance reduction factor for different scanners over the 4R reference scanner for 2-mm ROI (b) and 10-mm ROI (d).

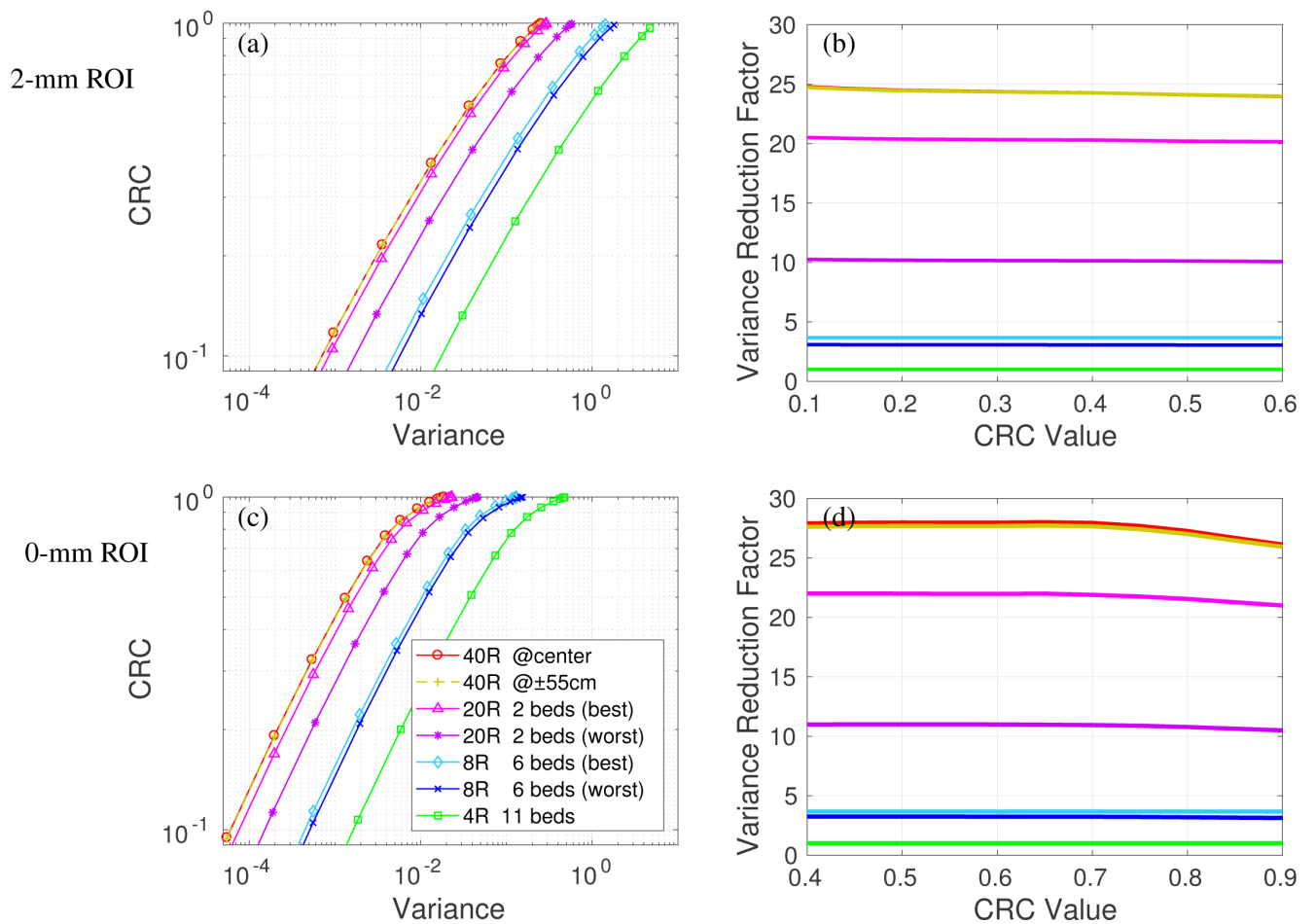


Figure 5: Quantification performance of the four scanners with 500 ps TOF and 4-mm DOI detectors. All prompt events (true+scatters+randoms) are considered. CRC vs. variance curves of 2-mm ROI (a) and 10-mm ROI (c); Variance reduction factor of different scanners over the 4R reference scanner for 2-mm ROI (b) and 10-mm ROI (d).

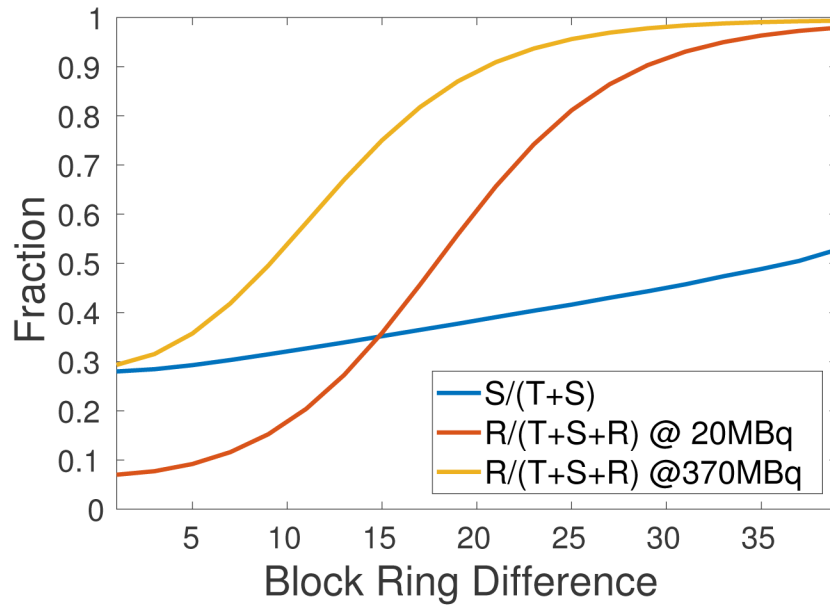


Figure 6: Scatter fraction ($SF=S/(T+S)$) and random fraction ($RF=R/(T+S+R)$) as a function of block ring difference. Random fraction was examined at two activity levels (20 MBq and 370 MBq).

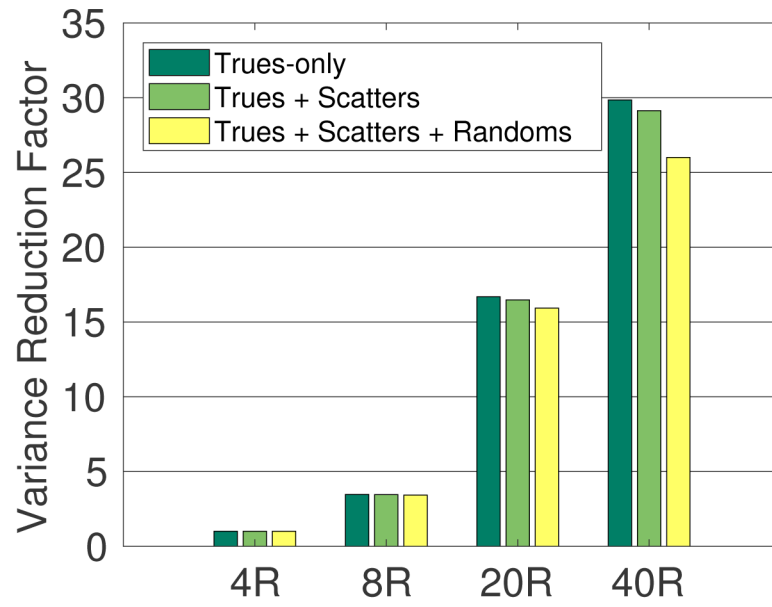


Figure 7: Variance reduction factor (CRC=0.5) of 8R, 20R, 40R scan over the 4R scan for trues-only, trues + scatters, and trues + scatters + randoms, respectively, for 10-mm ROI. All scanners are with 500 ps TOF and no DOI.

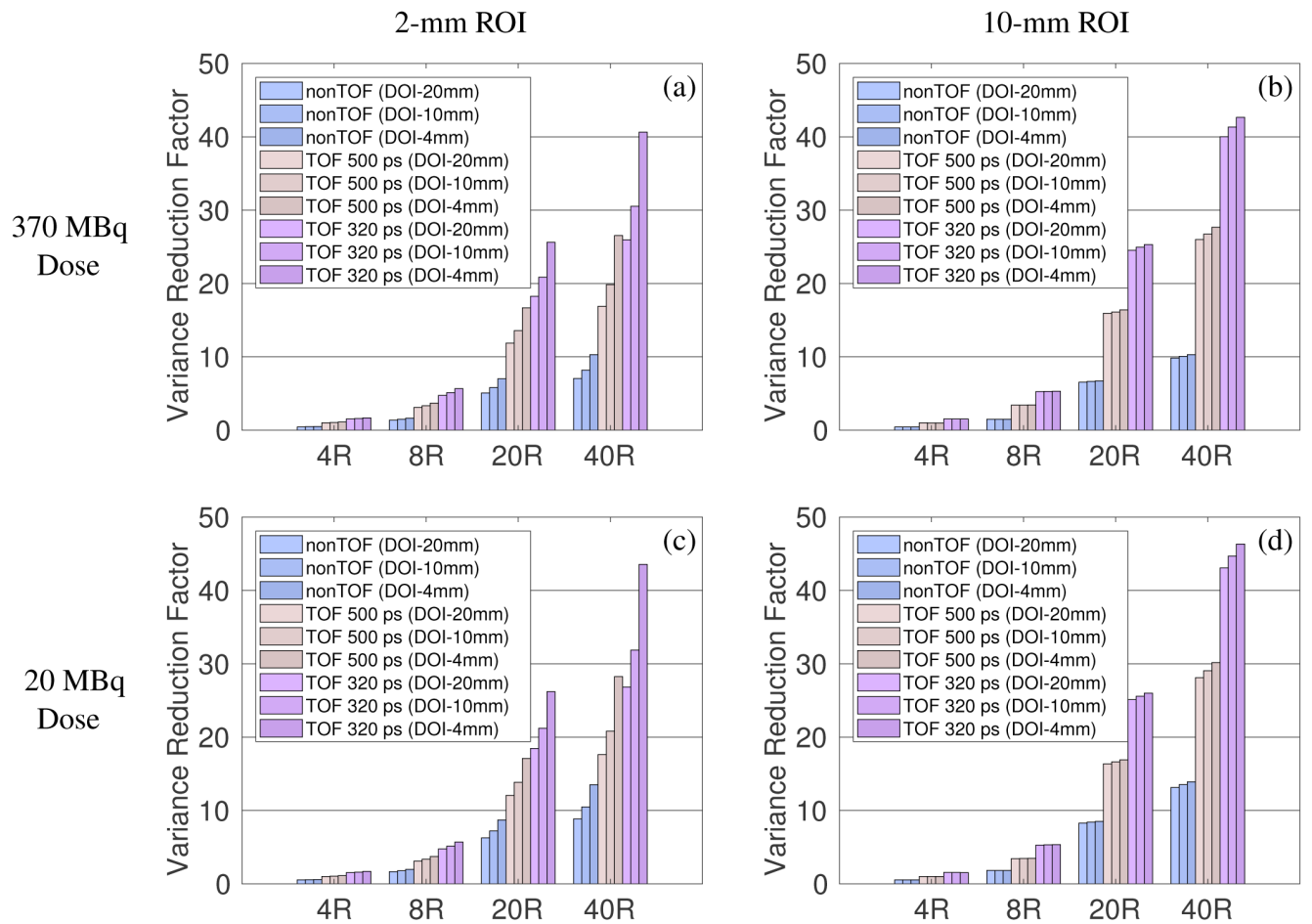


Figure 8: Variance reduction factor for imaging a 2-mm ROI (left) and 10-mm ROI (right) across the 110-cm axial scan range using different scanners over the 4R 500 ps non-DOI reference scanner. Top row: 370 MBq total activity. Bottom row: 20 MBq total activity.

Table 1:

Four scanner designs and their solid angle coverage of a point source at the center.

Design	AFOV (cm)	$\Omega/4\pi$	ratio over 4R
4R	22.0	0.255	1.00
8R	44.4	0.469	1.84
20R	111.6	0.801	3.14
40R	223.6	0.937	3.68

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