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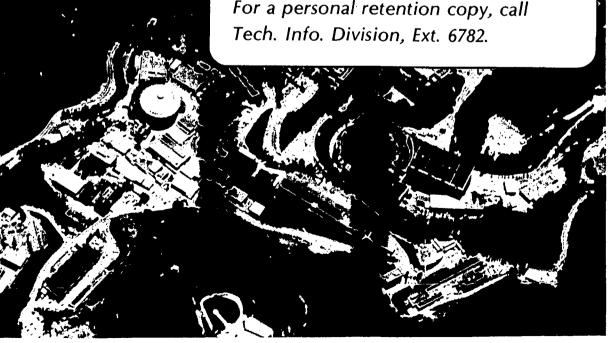
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DIGITAL NEUTRON RADIOGRAPHY USING PLANE CONVERTERS WITH MULTIWIRE PROPORTIONAL CHAMBERS

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INTRODUCTION

The work described here was completed more than three years ago, and represents, in large part the PhD¹) and MS²) thesis research of two of the present authors. Much of it has been reported previously elsewhere³,⁴). It constitutes an effort to develop and study a moderately low cost, moderate resolution, high sensitivity, on-line method for digital neutron radiography, intended for use where neutron fluence was limited by source strength, or received dose. The basic imaging system consisted of a position-sensitive gas proportional chamber together with its associated imaging electronics, and a plane neutron converter. Enriched-boron, gadolinium, and polyethylene (for fast neutrons) converters wer analyzed and tested. Some work was done on digital data enhancement, and efforts to improve spatial resolution included pressurizing the proportional-chamber gas to reduce the track lengths of the neutron-interaction products.

The results of this work are described below.

THE DETECTION SYSTEM

Multiwire Proportional Chamber

The multiwire proportional chamber (MWPC) consisted of three parallel wire planes, a central (anode) plane, and two outer (cathode) planes. Each plane was a parallel-wire grid mounted on a glass epoxy frame. The anode wires were 12.5-µmeter gold-plated tungsten and were spaced 1.5-mm apart. The cathode wires were made from 37-µmeter gold-plated molybdenum and were spaced 1-mm apart. The wires axes in the two cathode planes were mutually perpendicular. Interplane spacing was 3 mm, the cathodes being 6 mm apart. A converter plate can be mounted on either the front or back of the detector with its face supported 0.5 mm from the cathode plane. A schematic blowup of the detector assembly is shown in Figure 1. For most of the measurements described herein, only a back converter was used.

One side of each cathode plane was capacitively coupled to an electro-magnetic delay line. Position information was derived by measuring the time delay between a prompt anode pulse and a delayed cathode pulse. The two cathodes, having their wire planes mutually perpendicular, permitted simultaneous position measurement along two orthogonal axes.

The detector had a sensitive area 25 cm \times 25 cm, and maximum overall dimensions, when mounted in its pressure chamber, of 47 cm \times 47 cm \times 9 cm.

⁺ Present address

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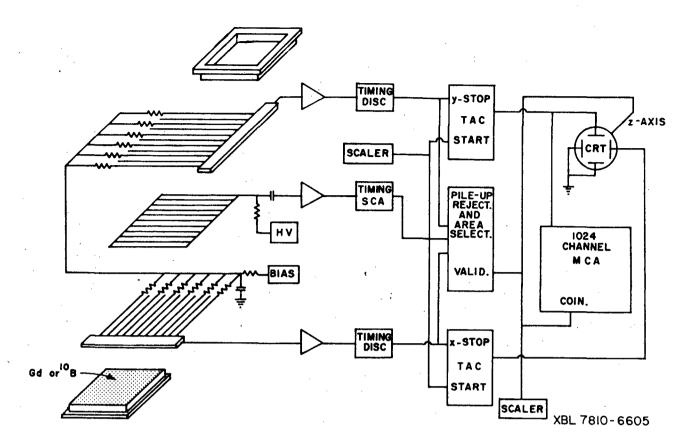


Fig. 1. Schematic diagram of wire chamber and electronics.

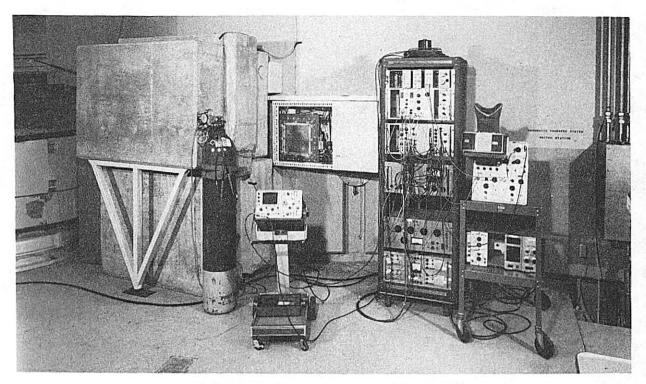
The Analysis System

The anode signal and the two cathode signals were processed through charge-sensitive preamplifiers and timing discriminators. The processed anode pulse then provided a "start" signal for two time-to-amplitude converters (TAC). Each processed cathode pulse provided one "stop" (Fig. 1). An analog image of an interaction (event) in the chamber is derived by placing the TAC outputs into the x-y inputs of an oscilloscope, and a timing, strobe, pulse into the z input. For each event, after sufficient time has elapsed for both TACs to reach their full amplitude (2 μ s), the strobe pulse intensifies a dot on the scope screen. Integration of the dot pattern, either by eye, or on film produces the analog image. Alternatively digital images can be accumulated, stored, and processed by using the same input electronics in conjunction with a two-dimensional analyzer. Figure 1 also shows a one-dimensional-analysis setup for resolution measurements. Figure 2 shows the experimental setup at the neutron beam port.

Neutron Converters

The neutron converters were mounted on a flat substrate of 0.15 cm-thick flat aluminum sheet stock, which was joined to a machined aluminum stiffening frame, either with epoxy, or by electron-beam welding. Both bonding methods produced an adequately flat surface.

The boron converter was made by covering the entire aluminum substrate with pressure-sensitive tape and then dusting 92%-enriched Boron-10 powder onto the resulting adhesive surface. The thickness of the boron layer made in this manner varied between 3 and 4 mg/cm. The gadolinium converter was made by epoxying a 75- μ meter Gd foil onto the substrate. A fast neutron



XBB 742-855

Fig. 2. Exposure facility at the Berkeley Research Reactor. The MWPC is shown mounted in the experiment holder.

converter was made by attaching a 1.5 mm sheet of polyethylene to the substrate with double-sided tape.

EFFICIENCY AND RESOLUTION

Design Considerations

Neutron reaction products will produce relatively long tracks in the low-density gas of the proportional chamber. For example the 70-kev electron from Gd, which has a range of only 50 µmeters in film emulsion, has a range of over 3 cm in proportional-chamber gas (primarily Ar) at STP. The alpha particle from neutron capture, on the other hand has a range of less than 1 cm in Ar. For this reason, although Gd was the converter of choice for photographic-emulsion work, B was our first choice. Figure 3 shows residual-range curves of alpha particles leaving the B converter. The curves were generated by dividing the converting layer onto 25 equal-thickness zones, and then calculating the locus of range end points as a function of emission angle. The numbers appearing on alternate curves are the percent of alphas originating in the zone, that energe. The alphas from all zones appear to emerge from the same point because on the scale of the figure the converter dimensions are negligibly small.

Circular segments on the graph define constant alpha-particle range and are therefore lines of constant energy, or energy deposition. The two segments shown correspond to 0.1 and 1 MeV. If signal-amplitude discrimination is employed, then only those alphas lying on the range curves between energy-defining segments will contribute to a radiographic image. Such energy discrimination can improve spatial resolution, but only at the expense of

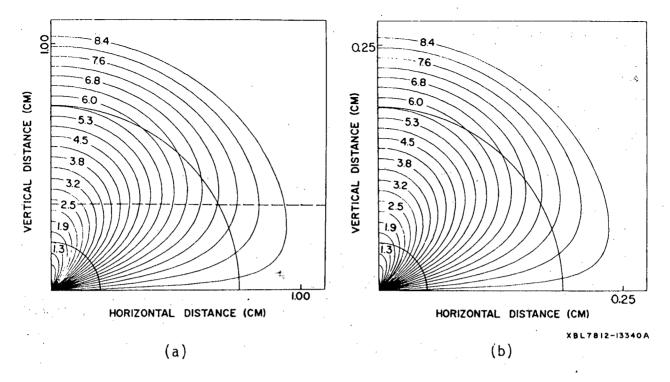


Fig. 3. Family of residual-range curves for α particles emerging from a 10B converter into Ar a) at 1 atm and b) at 4 atm.(--- is anode)

neutron-detection efficiency.

Several other characteristics of the conversion process can be inferred from the figure. If the converter is thinner than the alpha range, then inner curves will disappear, one curve for each 1/25 of the range. Similiarly, if the converter is coated with a thin layer of non-converting material, then outer curves will disappear, one for each 1/25 of the range. This latter effect will also improve resolution, but again at the expense of efficiency. Increasing the pressure of the chamber gas simply changes the abscissa and ordinate scales proportionately. To illustrate this effect, Figure 3b shows the residual range curves for alpha particles at 4 atm chamber pressure. At this pressure the maximum alpha range is less than 0.25 cm, improving resolution with no loss in efficiency. Figure 4 shows a comparison of residual-range curves for the 70-keV electron from Gd-157 at both 1 and 4 atm chamber pressure. Note that the family of curves for the electron at 4 atm appears similar to those for the alpha at 1 atm.

Figure 5 shows residual-range curves for 1-MeV neutrons from a polyethylene converter. Because n-p scattering occurs only in the forward direction, the polyethylene converter must be placed upstream of the chamber. The resolution limit in this case is not entirely determined by the proton range, but merely by that part of the proton track that lies in the chamber. Even for 1-MeV neutrons, most of the proton tracks extend well beyond the 6-mm thickness of the sensitive volume.

Calculated converter efficiencies for thermal neutrons were 15% and 6% respectively for the Gd and B. In both cases the measured values were only about 40% of those calculated. For the polythylene converter an efficiency of 0.1% was calculated for a Pu-B neutron spectrum, very close to what was achieved experimentally.

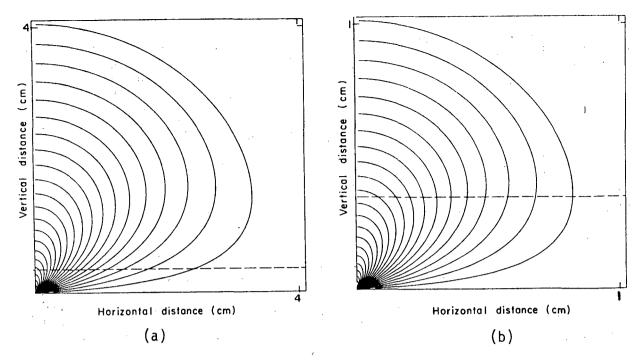


Fig. 4. Residual-range curves for 70-keV electrons emerging from a Gd converter into Ar gas a) at 1 atm and b) at 4 atm. (--- is anode)

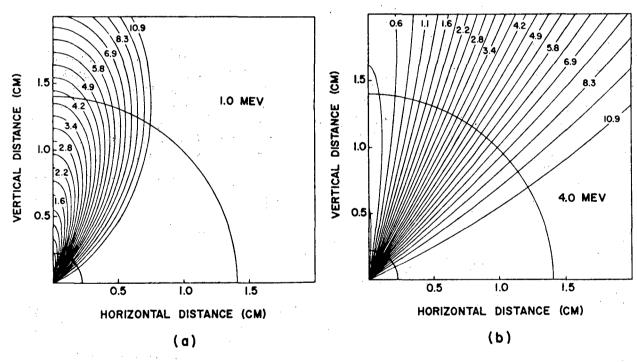
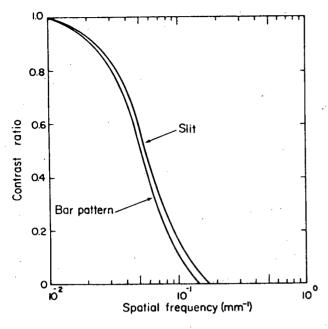


Fig. 5. Residual-range curves for recoil protons ejected from a ${\rm CH}_2$ converter for a) 1 MeV neutrons and b) 4 MeV neutrons.

Measurements

Spatial resolution was determined by calculating modulation transfer functions (MTF) from digital images of Cd bar patterns. Some calculations of MTF's from single-slit images [Line Spread Functions (LSF)] were also made for comparison (Fig. 6).

Figures 7 and 8 show MTF's as a function of chamber pressure for Gd and B respectively. Figure 9 shows critical frequency (the spatial frequency at



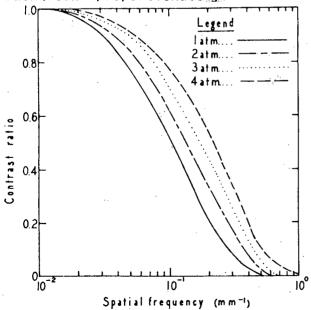
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| Legend | latm... | 2 atm... | 3 atm... | 4 atm... | 4 atm... | 10° | 10° | Spatial frequency (mm⁻¹)

Fig. 6. Comparison of the modulation transfer function (MTF) as measured from a slit image and from a bar pattern image.

Fig. 7. MTF's using the Gd converter at 1,2,3, and 4 atm.

which the contrast ratio falls to 1/e as a function of chamber pressure. The B resolution improved significantly with pressure and reached a maximum value for $\omega_{\rm C}$ of almost 3/mm at 4 atm, which was however less than the four-fold improvement that one might expect from simple scaling. On the other hand, for gadolinium converter there was little improvement in resolution. In both cases there was a 4-fold increase in the background counting rate, suggesting that increasing detector density does, at least, increase gamma background proportionately.



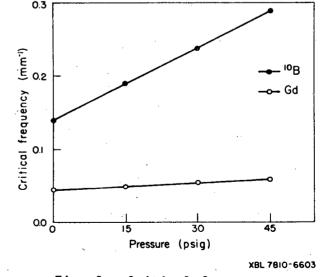
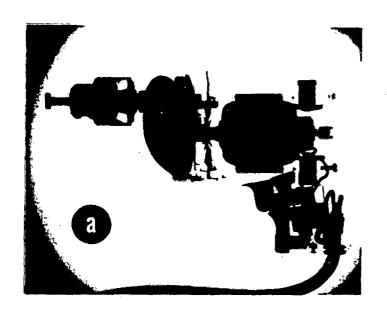
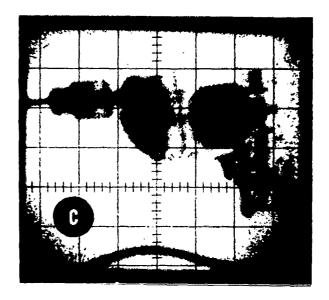
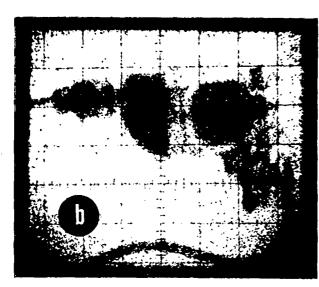


Fig. 8. MTF's using the ¹⁰B converter at 1,2,3, and 4 atm.

Fig. 9. Critical frequency, $\boldsymbol{\omega}_{\text{C}}$, as a function of pressure.







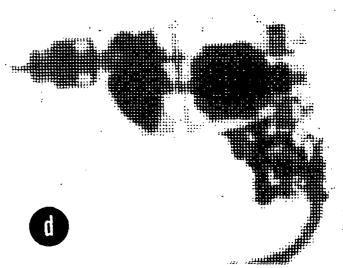
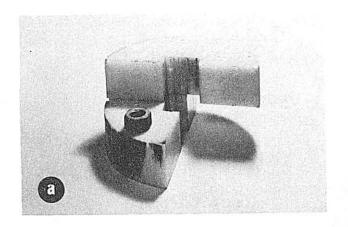
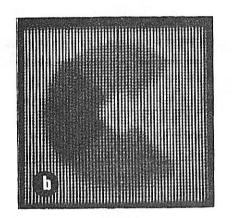
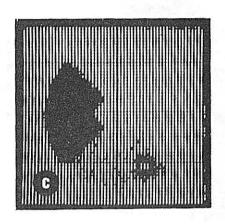


Fig. 10. Neutron Radiographic images of an electric drill on film using a GdO converter, a); as analog oscilloscope displays of neutron interaction densities of 5mm^{-2} , b); and 60 mm⁻², c); and from a reconstruction of digitally stored and normalized data, d). (XBB 758-6522)







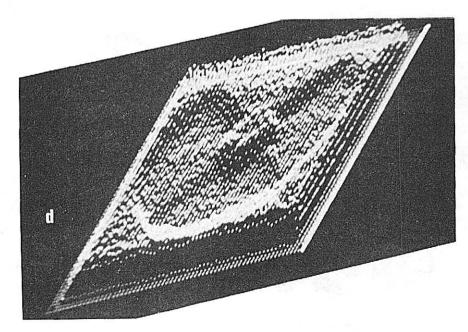


Fig. 11. a) Test object used for fast neutron imaging, b) and c) fast neutron digital radiographs of test object, d) isometric display of digital image. (XBB 742-870)

SOME EXAMPLE IMAGES AND CONCLUSIONS

Figure 10 shows a normal neutron radiograph of an electric drill (10a) together with polaroid photos of analog oscilloscope images (10b,c), and a digitally stored and reconstructed image (10d) of the same drill. While not a likely subject for digital processing, the drill has sufficient structural detail to illustrate the characteristics, including limitations, of this digital imaging system. The direct analog images were made in exposures of 7s and 85s respectively to a thermal-neutron beam of 10^4 n-cm⁻²-s⁻¹ digital image was stored in a two-dimensional array of 2mm x 2mm-area elements, normalized, element-by-element against an object-out background image and then displayed in 32 shades of gray.

Figure 11 shows a test object for fast neutron imaging (11a), together with digital images made using a Pu-Be source and the polythylene converter (11b,c, and d). Various features are enhanced by digital discrimination.

At the time the above work was done we had no on-line computer available for such data processing. The now-standard computer functions were simulated using a two-dimensional 4096-channel pulse-height analyzer. Present technology and cost breakthroughs have probably made digital processing no more difficult nor expensive than analog oscilloscope imaging. So, where the quality of this resolution has application, it can be implemented at relatively modest cost.

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