### **Lawrence Berkeley National Laboratory**

### **Recent Work**

### **Title**

A DETERMINATION OF THE CRYSTAL STRUCTURE OF XENON TETRAFLUORIDE

### **Permalink**

https://escholarship.org/uc/item/63s2q4n5

### **Authors**

Templeton, David H. Zalkin, Allan Forrester, J.D. et al.

### **Publication Date**

1963-04-01

## University of California

## Ernest O. Lawrence Radiation Laboratory

# A DETERMINATION OF THE CRYSTAL STRUCTURE OF XENON TETRAFLUORIDE

TWO-WEEK LOAN COPY

This is a Library Circulating Copy which may be borrowed for two weeks. For a personal retention copy, call Tech. Info. Division, Ext. 5545

### **DISCLAIMER**

This document was prepared as an account of work sponsored by the United States Government. While this document is believed to contain correct information, neither the United States Government nor any agency thereof, nor the Regents of the University of California, nor any of their employees, makes any warranty, express or implied, or assumes any legal responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by its trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof, or the Regents of the University of California. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof or the Regents of the University of California.

UNIVERSITY OF CALIFORNIA

Lawrence Radiation Laboratory Berkeley, California

Contract No. W-7405-eng-48

A DETERMINATION OF THE CRYSTAL STRUCTURE OF XENON TETRAFLUORIDE\*

David H. Templeton, Allan Zalkin, J. D. Forrester and Stanley M. Williamson

April 1963

A Determination of the Crystal Structure of Xenon Tetrafluoride\*

David H. Templeton, Allan Zalkin, J. D. Forrester and Stanley M. Williamson

Department of Chemistry and Lawrence Radiation Laboratory

University of California, Berkeley, California

April, 1963

The crystal and molecular structure of XeF<sub>li</sub> has been determined by single-crystal x-ray diffraction techniques. The intensities of Mo Ka x-rays diffracted by the crystal were measured with a scintillation counter. The monoclinic unit cell dimensions are a = 5.050 Å, b = 5.922 Å, c = 5.771 Å (each  $\pm 0.003 \text{ Å}$ ), and  $\beta$  =  $99.6^{\circ} \pm 0.1^{\circ}$ . The space group is P2<sub>1</sub>/n with two molecules per unit cell. The xenon atoms occupy the corners and body centers so that the molecular packing is pseudo body-centered cubic. The molecule has a square planar configuration. The Xe-F bond distance is  $1.93 \pm 0.02 \text{ Å}$ , after a correction of  $\pm 0.02 \text{ Å}$  for thermal vibration effects; the F-Xe-F bond angle is a right angle  $\pm 0.02 \text{ Å}$  within the accuracy of the determination.

### INTRODUCTION

This paper is an extended and slightly modified version of our earlier report which described our determination of the crystal and

<sup>\*</sup>This work was done in part under the auspices of the U. S. Atomic Energy Commission.

<sup>(1)</sup> D. H. Templeton, A. Zalkin, J. D. Forrester and S. M. Williamson, J. Am. Chem. Soc. 85, 242 (1963).

molecular structure of XeF,.

The earliest x-ray study of this compound was by Siegel and Gebert<sup>2</sup> who determined the cell dimensions and space group. The atomic coordinates were determined simultaneously by Ibers and Hamilton<sup>3</sup> and ourselves<sup>1</sup> by x-ray diffraction. There and Hamilton used photographic data from precession films, while we used stationary scintillation counter data. This work was soon followed by a neutron-diffaction study by Burns, Agron and Levy<sup>1</sup> which gives somewhat higher precision for the fluorine coordinates than is feasible with the x-ray data.

### EXPERIMENTAL

Xenon tetrafluoride was prepared by heating the elements to 300° in a flow system. Subsequently a slightly modified procedure was adopted. A 4 to 1 molar ratio mixture of F<sub>2</sub> and Xe was mixed well in a half liter copper chamber which contained baffles with twice as much helium, which acted as a carrier gas. The gas mixture then flowed through a copper U-trap at -120° into a 12 in. length of 3/4 in. nickel tubing. The nickel and copper were joined by a silver-soldered connection. The last six inches of the reactor tube was heated to 350° by an electric furnace. The reactor ended with 4 in. of 1/2 in. copper tubing so that there was a thermal gradient before the copper-to-glass seal. A glass U-trap was then either sealed to the glass of the copper-to-glass seal or connected through an ungreased ground joint. The joint was used if the XeF<sub>1</sub> sample was to be transferred to other containers in a dry-box and the seal was used if the trap were equipped with

<sup>(2)</sup> S. Siegel and E. Gebert, J. Am. Chem. Soc. 85, 240 (1963).

<sup>(3)</sup> J. A. Ibers and W. C. Hamilton, Science 139, 106 (1963).

<sup>(4)</sup> J. H. Burns, P. A. Agron, and H. A. Levy, Science

a break-seal so that the sample could be transferred into a vacuum system. The trap was cooled with solid  ${\rm CO}_2$  and the other end went by tubing directly to a hood. The glass from the copper-to-glass seal to the  ${\rm CO}_2(s)$  level was maintained at about  $75^\circ$  by means of a heating tape to prevent condensation upstream from the trap. Good conversion of the Xe to  ${\rm XeF}_{l_1}$  was attained with a flow rate such that the residence time in the reactor was one minute. The apparatus is very similar in design to that of Holloway and Peacock except that our apparatus had only one trap. This procedure yielded the material described by Gunn and Williamson for which the chemical analysis was close to theoretical for  ${\rm XeF}_{l_1}$ . Our x-ray studies of material prepared in this way detected crystals only of the structure described here, except when samples had been exposed to water.

In some of our earlier work we attempted quick transfers of the material in damp air into capillaries, but the resulting samples survived only long enough for a few preliminary x-ray patterns. It was only when the capillaries were loaded by sublimation under vacuum that we obtained stable specimens. The capillaries were thin-walled vitreous silica of 0.5 mm diameter. During the investigation of the final crystal, it is estimated to have undergone about 10 hours of irradiation with no evidence of decomposition, and in fact the crystal continued to grow at the expense of other crystals in the capillary. A few weeks after the experiment, the crystal disappeared by sublimation to regrow in another location in the capillary. Four months later it was still there. Photographs of the crystal taken the day following

<sup>(5)</sup> J. H. Holloway and R. D. Peacock, Proc. Chem. Soc. 1962, 389.

<sup>(6)</sup> S. R. Gunn and S. M. Williamson, Science 140, 177 (1963).

the intensity measurements are shown in Fig. 1. The crystal diameter ranged from 0.13 to 0.24 mm in various directions. Eleven faces of the pseudo-cubic dodecahedron were developed; the twelfth surface was attached to the curved surface of the capillary.

Molybdenum Ka x-rays were produced with a General Electric XRD-5 unit operated at 25 ma. and 40 kvp. A 0.00l in. Zr foil was used to filter the diffracted radiation just before it entered the scintillation counter. The range of intensities measured was from 1 to 14,000 counts per second. The counter was checked and found to be linear over this range.

The cell dimensions were measured with a take-off angle of  $2^{\circ}$  using the resolved Kc<sub>l</sub> peaks of Mo ( $\lambda$  = 0.70926 Å). The crystal was set on the goniostat with the a\* axis perpendicular to the phi circle; this axis coincides very roughly with the axis of the capillary.

The intensities were measured using the stationary technique and counting each reflection for 20 seconds, with a take-off angle of  $\mu^0$ . A fixed-time count is appropriate for approximately equal weighting of the data in the least-squares analysis. The background, plotted as a function of the diffraction angle 20, was ordinarily applied to the data; in a case where the reflection was a multiple of a strong reflection, the background was checked near the reflection. All of the 293 independent independent reflections up to a 20 angle of  $50^{\circ}$  ( $\sin\theta/\lambda \sim 0.59$ ) were measured; 35 of these were below the detection limit and were recorded as zero. The crystal grew about 30 percent during the measurements (two days), and the data were normalized by repeated measurement of a few standard reflections. The data were corrected for the Lorentz-polarization factor using the formula:  $I_{cor} = I \sin 2\theta/(1+\cos^2 2\theta)$ .

The least-squares program of Gantzel, Sparks and Trueblood was used on an IBM7090; this program minimizes the function  $\sum ||F_0|-|F_c||^2/\sum |F_0|^2$  where  $F_0$  and  $F_c$  are the observed and calculated structure factors. The weighting factors were all unity. The program utilizes a full-matrix calculation for the parameter shifts. Our results are stated in terms of temperature factors of the form  $\exp(-\beta_{11}h^2-2\beta_{12}hk-\ldots)$ , although the program actually uses  $\exp(-B_{11}h^2-B_{12}hk-\ldots)$ .

Scattering factors for the neutral Xe and F atoms were obtained from Tables 3.3.1B and 3.3.1A respectively as given in the International Tables.

Due to an oversight the Xe scattering factors were not corrected for the dispersion correction Af' which is approximately -0.5 electrons.

### STRUCTURE DETERMINATION

Reflections are strong when h+k+l is even and weak when it is odd, showing that the Xe atoms are at 0,0,0 and 1/2,1/2,1/2. Trial coordinates for fluorine atoms were estimated by some simple calculations which in principle were equivalent to making projections of the fluorine electron density down the a and c axes with use of only a few terms in which the effect of the fluorine atoms was large. The electron densities were not actually calculated, but were roughly approximated graphically. For example, reflections 060 and 110 were judged to be stronger than average, while 031 and 200 were weaker than average. In these cases the phases are fixed by xenon. Reflections 012, 014, and 520 were judged to be strong among reflections depending only on fluorine. In these cases phases

<sup>(7)</sup> P. Gantzel, R. Sparks and K. Trueblood, private communication (1961).

<sup>(8) &</sup>lt;u>International Tables for X-ray Crystallography</u>, Vol. 3, Kynoch Press, Birmingham, England (1962).

were chosen in all permutations. These calculations resulted in six coordinates for the two fluorine atoms which in five cases were within 0.05 of the final values. For F(2) the trial value of y was 0.18, in error by 0.15. Refinement by least squares quickly corrected this error.

Eight cycles of least squares refinement using isotropic temperature factors brought the unreliability factor  $R = \sum ||F_0| - |F_c||/\sum |F_0||$  to O.11. Four cycles using anisotropic temperature factors then diminished R to 0.089. Two obvious blunders in data taking were corrected by remeasurement of their intensities, and three more cycles of least squares brought R to 0.076.

Some of the low-angle data appeared to suffer from extinction and/or absorption, so the 7 reflections with  $\sin\theta/\lambda$  less than 0.17 were deleted from the refinement. A final set of refinements of 5 cycles reduced R to our final value of 0.059 for 286 data. The results in Table 1 and Table 2 are from this last calculation. Table 1 lists the final parameters. Table 2 lists the observed and calculated structure factors; those marked with an asterisk were deleted from the final refinement.

Some additional calculations were performed with the 96 non-zero, odd h+k+l data. These reflections are the result of fluorine atoms exclusively. A refinement with isotropic temperature factors resulted in coordinates for fluorine atoms which were the same as those in Table 1 within 0.005 or less. The corresponding R was 0.18.

The data were not corrected for absorption. The dimensions of the crystal correspond to #R of about 0.9. In the approximation of spherical shape, absorption would be almost perfectly compensated by systematic errors in the thermal parameters. We estimate that to compensate for the absorption error the temperature parameters of each atom in Table 1

should be increased by the following amounts:

$\beta_{11}$	β <sub>22</sub>	β <sub>33</sub>	$\beta_{12}$	β <sub>13</sub>	$\beta_{23}$
0.0007	0.0005	0.0005	0.0000	0.0001	0.0000

### DISCUSSION

The space group symmetry requires the molecule to be planar, and within the accuracy of the determination it is square planar. Fig. 2 shows the molecular packing, and Fig. 3 the molecular dimensions before correction for thermal motion. If the fluorine atoms are assumed to ride on the xenon atoms, the Xe-F bond distances should be increased by 0.02 Å to the value 1.93 Å.

In Table 3 are listed interatomic distances, without correction for thermal motion. Each xenon has four fluorine neighbors in other molecules at an average distance of 3.25 Å. Each fluorine atom has 8 fluorine neighbors in other molecules at an average distance of 3.13 Å or 3.15 Å, as well as one xenon neighbor in another molecule. The average intermolecular F-F distance infers a van der Waals radius of 1.57 Å, which is considerably larger than the accepted value of 1.35 Å, perhaps because of the considerable thermal motion of the molecules. Using the smaller value for fluorine, one gets an upper limit of 1.9 Å for the van der Waals radius of xenon in this tetravalent state.

We have three independent sets of results for the structure of this crystal: the neutron diffraction study of Burns, Agron and Levy, 4,10 the photographic x-ray study of Hamilton and Ibers, 3,11 and our own counter x-ray study. There is no significant disagreement with respect to

<sup>(9)</sup> L. Pauling, "The Nature of the Chemical Bond", 3rd Ed., Cornell University Press, Ithaca, N. Y. (1960).

<sup>(10)</sup> J. H. Burns, P. A. Agron and H. A. Levy, private communication.

<sup>(11)</sup> J. A. Ibers and W. C. Hamilton, private communication.

the geometry of the structure; the three sets of coordinates agree in each case within two standard deviations or less. The thermal parameters of the fluorine atoms are in similar agreement. The agreement between the sets of thermal parameters for xenon is as good as for fluorine on an absolute scale, but is poorer than the ostensible precision of the measurements. Systematic errors which are a function of  $\theta$  (for example, absorption) will have equal effect on thermal parameters of heavy and light atoms. We attribute the disagreement to systematic errors which have an effect on the thermal parameters at a level of the order of 0.3 in terms of the equivalent isotropic B value, but we have not identified the precise nature of these errors. We are not surprised that such errors are present; rather, we did not expect them to be so small.

Table 1. Crystal structure data for XeF1

a = 
$$5.050 \pm 0.003 \, \text{Å}$$
 Z = 2  
b =  $5.922 \pm 0.003 \, \text{Å}$  Space group  $P2_1/n \, (c_{2h}^5)$   
c =  $5.771 \pm 0.003 \, \text{Å}$  Molecular weight =  $207.30$   
 $\beta = 99.6 \pm 0.1^{\circ}$  X-ray density =  $4.04 \, \text{g/ml}$   
V =  $170.2 \, \text{Å}^3$ 

### Atomic positions:

Xe: 0, 0, 0; 
$$1/2$$
,  $1/2$ ,  $1/2$ .  
F:  $\pm(x, y, z; 1/2 - x, 1/2 + y, 1/2 - z)$ ,  
F(1):  $x = 0.260 \pm 0.003$  F(2):  $x = 0.229 \pm 0.003$   
 $y = 0.146 \pm 0.002$   $y = 0.033 \pm 0.002$   
 $z = -0.153 \pm 0.002$   $z = 0.297 \pm 0.002$ 

### Anisotropic temperature parameters:

	Хe	F(1)	F(2)
$\beta_{ll}$	0.0208 ± 0.0007	0.044 ± 0.006	0.044 ± 0.006
$\beta_{22}$	0.0097 ± 0.0005	0.025 ± 0.004	0.021 ± 0.004
β <sub>33</sub>	0.0120 ± 0.0005	0.031 ± 0.00h	0.029 ± 0.005
β <sub>12</sub>	0.0012 ± 0.0004	-0.006 ± 0.004	0.00\$ ± 0.004
β <sub>13</sub>	0.007\$\psi 0.0008	0.023 ± 0.005	0.002 ± 0.004
β <sub>23</sub>	0.0000 ± 0.0006	0.004 ± 0.004	0.000 ± 0.004

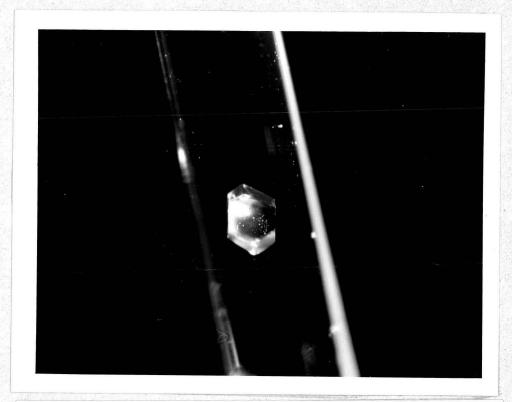
Table 2: Observed and calculated structure factors A An asterisk indicates a reflection

	·					
H.K= 0. 0	L FORS FCAL	-4 44 -40	H.K= 2, 2	-1 71 -69	-4 0 15	-4 26 30
L FCBS FCAL	-5 557 56E	-3 524 481	L FOES FCAL	0 309 321	-3 458 436	-3 486 488
2 550 567	-3 611 605	-2 33 38	-6 344 367	1 33 42	-2 24 -29	-2 50 -49
4 556 545	-1 798 565.	-1 758 740	-5 63 -64	2 310 323	-1 382 367	-1 384 364
6 417 405	1 758 837	C 20 -38	-4 534 " 499		0 0 1	··0 0 <del>-</del> 8
	3 782 792	1 43C 427	<del>-</del> 3 30 26	H•K= 3. C	1 467 472	1 315 344
H,K= 0, 1	5 381 353	2 38 46	-2 814 759	L FCBS FCAL	2 30 -40	2 G 3
L FOBS FCAL	*	3 467 468	-1 129 89	-5 377 390	3 290 296	. 3 289 287
1.641 973•	H,K= 1, 1	4 33 -38	C 599 599	-3 626 621		
2 245 202	L FOBS FCAL	5 320 323	1 48 -42	-1 712 683	H,K± 3, 5	H,K= 4, 4
3. 692 724 4 85 <del>-</del> 70	-6, 344 363 -5 12 5		2 65C 677 3 68 -58	1 681 620 3 353 335	L FGBS FCAL -3 51 57	L FOES FCAL -4 3C4 345
5 393 401	-4 771 740	h,K= 1, 5 L FUBS FCAL	4 362 355	5 309 296	-2 404 396	-3 23 -6
6 C -7	-3 141 105	-4 398 377	5 20 25	7 307 270	-1 53 +56	-2 379 385
	-2 615 551	-3 1C3 -53	, 10 1,	H,K= 3, 1	0 353 354	-1 21 24
H.K= 0. 2	-1 140 -98.	-2 463 444	H.K= 2. 3	L FOBS FCAL	1 42 -32	0 335 340
L FCBS FCAL	.0 734 958.	-1 57 58	L FOBS FCAL	-6 355 384	2 284 309	1 52 -50
C 73C 1052*	1 145 -115+	. C 504 497	-6 18 1G	-5 C 2	•	2 237 259
1 124, 95	2 8C1 943	1 46 43	-5 46C 3449	-4 404 402	H,K= 3, 6	
2 571 616	3 88 65	2 439 435	-4 76 -71	-3 97 -83	L FOBS FCAL	H,K= 4, 5
3 74 66	4 415 404	3 72 -68	-3 428 394	-2 819 776	-1 316 326	L FORS FCAL
4 577 585	5 0 LC	4 292 311	-2 78 75	-1 31 28	0 0 -4	-2 15 -7
5 5C <del>-</del> 53	6 356 339	1. V = 1 C	-1 767 742	0 609 582		-1 298 308 0 0 4
6 333 341	H.K= 1, 2	F.K= 1, 6 L FOBS FCAL	C 0 -13	1 62 54 2 423 428	H,K= 4, 0 L FOBS FCAL	0 0 4
H.K= C. 3	L FC8S FCAL	-3 335 330	2 59 -55	3 21 -28	±4 374 392	H,K= 5, 0
L FCBS FCAL	-6 46 -41	-2 14 10	3 350 361	4 406 370	-2 411 417	L FORS FCAL
1 541 586	-5 447 438	-1 398 383	4 21 25	5 C -9	0 672 610	-3 345 375
2 99 95	-4 64 56	C 23 -23	5 318 313	•	2 329 314	-1 344 347
3 690 724	<del>-</del> 3 663 608	1 376 387	•	H,K= 3, 2	4 263 261	1 281 294
4 61 -61	-2 175 13C	2 14 23	F,K= 2, 4	L FOBS FCAL		
5 328 354	-1 933 1047	3 314 327		26 61	11 11 - 1	
6 C 14		2 22, 22,	L FCBS FCAL	-6 35 41	H,K= 4, 1	H,K= 5, 1
	0 366 -324		-5 29 20	-5 430 444	L FORS FCAL	L FOBS FCAL
	1 499 543	H.K= 2, 0	-5 29 20 -4 410 389	-5 430 444 -4 47 -55	L FORS FCAL -5 333 375	L FOBS FCAL -4 352 395
H,K= 0, 4	1 499 543 2 110 99	H.K= 2. O L FOES FCAL	-5 29 20 -4 410 389 -3 C -6	-5 430 444 -4 47 -55 -3 588 543	L FORS FCAL -5 333 375 -4 50 48	L FOBS FCAL -4 352 395 -3 29 31
H.K= 0. 4 L FCBS FCAL	1 499 543 2 110 99 3 642 650	H.K= 2, 0 L FOBS FCAL =6 305 325	-5 29 20 -4 410 389 -3 C -6 -2 554 509	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92	L FORS FCAL -5 333 375 -4 50 48 -3 483 468	L FOBS FCAL -4 352 395 -3 29 31 -2 314 318
H.K= 0. 4 L FCBS FCAL C 61C 598	1 499 543 2 110 99 3 642 650 4 28 31	H.K= 2, 0 L FOBS FCAL -6 3C5 335 -4 635 650	-5 29 20 -4 410 389 -3 0 -6 -2 554 509 -1 126 -102	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75	L FOBS FCAL -4 352 395 -3 29 31 -2 314 318 -1 13 -10
H,K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130	1 499 543 2 110 99 3 642 650 4 28 31 5 391 380	H.K= 2. 0 L FOBS FCAL -6 3C5 335 -4 635 650 -2 912 977	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135	L FORS FCAL -5 333 375 -4 50 48 -3 483 468	L FOBS FCAL -4 352 395 -3 29 31 -2 314 318
H.K= 0. 4 L FCBS FCAL C 61C 598	1 499 543 2 110 99 3 642 650 4 28 31	H.K= 2, 0 L FOBS FCAL -6 3C5 335 -4 635 650	-5 29 20 -4 410 389 -3 0 -6 -2 554 509 -1 126 -102	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451	L FOBS FCAL -4 352 395 -3 29 31 -2 314 318 -1 13 -10 0 328 353
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528	1 499 543 2 110 99 3 642 650 4 28 31 5 391 380	H•K= 2. 0 L FOES FCAL -6 3C5 335 -4 635 650 -2 912 977 0 417 364	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 £7 83	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9	L FOBS FCAL -4 352 395 -3 29 31 -2 314 318 -1 13 -10 0 328 353 1 22 -23 2 262 272
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528 3 C 21	1 499 543 2 110 95 3 642 65C 4 28 31 5 391 38C 6 18 -2C H.K= 1, 3 L FCBS FCAL	H,K= 2, 0 L FOES FCAL -6 3C5 325 -4 635 650 -2 912 977 0 417 364 2 81C 813 4 472 428	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 87 83 2 473 479	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629 2 40 -46	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9 1 431 460 2 28 26 3 326 306	L FOBS FCAL -4 352 395 -3 29 31 -2 314 318 -1 13 -10 0 328 353 1 22 -23 2 262 272 H, K= 5, 2
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528 3 C 21 4 45C 463 5 14 13	1 499 543 2 110 95 3 642 65C 4 28 31 5 391 38C 6 18 -2C H.K= 1. 3 L FCBS FCAL -6 287 30C	H•K= 2. 0 L FOBS FCAL -6 3C5 335 -4 635 650 -2 912 977 C 417 364 2 81C 813 4 472 428 6 245 253	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 £7 83 2 473 479 3 24 -32 4 268 285	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629 2 40 -46 3 346 341 4 C -13	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9 1 431 460 2 28 26 3 326 306	L FOBS FCAL -4 352 395 -3 29 31 -2 314 318 -1 13 -10 0 328 353 1 22 -23 2 262 272 H, K= 5, 2
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528 3 C 21 4 45C 463 5 14 13	1 499 543 2 110 99 3 642 650 4 28 31 5 391 380 6 18 -20 H.K= 1. 3 L FCBS FCAL -6 287 300 -5 0 13	H,K= 2, 0 L FOES FCAL -6 3C5 325 -4 635 650 -2 912 977 C 417 364 2 81C 813 4 472 428 6 245 253	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 87 83 2 473 479 3 24 -32 4 288 285 b.K= 2, 5	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629 2 40 -46 3 346 341 4 C +13 H.K= 3, 3	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9 1 431 460 2 28 26 3 326 306	L FOBS FCAL -4 352 395 -3 29 31 -2 314 318 -1 13 -10 0 328 353 1 22 -23 2 262 272  H,K= 5, 2 -1 FOES FCAL -4 0 15
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528 3 C 21 4 45C 463 5 14 13 H, K= 0, 5 L FOBS FCAL	1 499 543 2 110 95 3 642 65C 4 28 31 5 391 38C 6 18 -2C H.K= 1. 3 L FCRS FCAL -6 287 30C -5 0 13 -4 557 506	H,K= 2, 0 L FOBS FCAL -6 3C5 325 -4 635 650 -2 912 977 0 417 364 2 81C 813 4 472 428 6 245 253 H,K= 2, 1 L FOBS FCAL	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 £7 83 2 473 479 3 24 -32 4 2£8 285  L FORS FCAL	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629 2 40 -46 3 346 341 4 C +13  H.K= 3, 3 L FOBS FCAL	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9 1 431 460 2 28 26 3 326 306 -4 0 -11  H.K= 4, 2	L FOBS FCAL -4 352 395 -3 29 31 -2 314 318 -1 13 -10 0 328 353 1 22 -23 2 262 272  H, K= 5, 2 -4 0 15 -3 319 353
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528 3 C 21 4 45C 463 5 14 13 H, K= 0, 5 L FCBS FCAL 1 473 478	1 499 543 2 110 95 3 642 65C 4 28 31 5 391 38C 6 18 -2C H.K= 1, 3 L FCBS FCAL -6 287 30C -5 0 13 -4 557 506 -3 17 -11	H.K= 2, 0 L FOBS FCAL -6 3C5 335 -4 635 650 -2 912 977 C 417 364 2 81C 813 4 472 428 6 245 253 H.K= 2, 1 L FOBS FCAL -6 0 -13	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 E7 83 2 473 479 3 24 -32 4 268 285 	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629 2 40 -46 3 346 341 4 C +13 H.K= 3, 3 L FOBS FCAL -5 17 -8	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9 1 431 460 2 28 26 3 326 306 -4 0 -11  H.K= 4, 2 L FORS FCAL	L FOBS FCAL -4 352 395 -3 29 31 -2 314 318 -1 13 -10 0 328 353 1 22 -23 2 262 272  H.K= 5, 2 -4 0 15 -3 319 353 -2 31 25
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528 3 C 21 4 45C 463 5 14 13 H, K= 0, 5 L FCBS FCAL 1 473 478 2 15 -24	1 499 543 2 110 95 3 642 65C 4 28 31 5 391 38C 6 18 -2C H.K= 1, 3 L FCBS FCAL -6 287 30C -5 0 13 -4 557 506 -3 17 -11 -2 746 703	H.K= 2. 0 L FORS FCAL -6 3C5 335 -4 635 650 -2 912 977 0 417 364 2 81C 813 4 472 428 6 245 253 H.K= 2. 1 L FOBS FCAL -6 0 -13 -5 527 515	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 87 83 2 473 479 3 24 -32 4 268 285	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629 2 40 -46 3 346 341 4 C +13  H.K= 3, 3 L FOBS FCAL -5 17 -8 -4 451 448	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9 1 431 460 2 28 26 3 326 306 -4 0 -11  H.K= 4, 2 L FOBS FCAL -5 29 36	L FOBS FCAL  -4 352 395  -3 29 31  -2 314 318  -1 13 -10  0 328 353  1 22 -23  2 262 272  H,K= 5, 2  -4 0 15  -3 319 353  -2 31 25  -1 374 370
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528 3 C 21 4 45C 463 5 14 13 H, K= 0, 5 L FOBS FCAL 1 473 478 2 15 -24 3 431 440	1 499 543 2 110 99 3 642 650 4 28 31 5 391 380 6 18 -20 H.K= 1. 3 L FCBS FCAL -6 287 300 -5 0 13 -4 557 506 -3 17 -11 -2 746 702 -1 19 10	H,K= 2, 0 L FOES FCAL -6 3C5 325 -4 635 650 -2 912 977 C 417 364 2 81C 813 4 472 428 6 245 253 H,K= 2, 1 L FOBS FCAL -6 0 -13 -5 527 515 -4 1C3 -84	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 87 83 2 473 479 3 24 -32 4 288 285	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629 2 40 -46 3 346 341 4 C +13  H.K= 3, 3 L FOBS FCAL -5 17 -8 -4 451 448 -3 0 -9	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9 1 431 460 2 28 26 3 326 306 -4 0 -11  H.K= 4, 2 L FORS FCAL -5 29 36 -4 400 422	L FOBS FCAL  -4 352 395  -3 29 31  -2 314 318  -1 13 -10  0 328 353  1 22 -23  2 262 272  H,K= 5, 2  -4 0 15  -3 319 353  -2 31 25  -1 374 370  0 51 -48
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528 3 C 21 4 45C 463 5 14 13 H, K= 0, 5 L FCBS FCAL 1 473 478 2 15 -24	1 499 543 2 110 95 3 642 65C 4 28 31 5 391 38C 6 18 -2C H.K= 1. 3 L FCBS FCAL -6 287 30C -5 0 13 -4 557 506 -3 17 -11 -2 746 702 -1 19 1C 0 690 733	H.K= 2, 0 L FOBS FCAL -6 3C5 325 -4 635 650 -2 912 977 0 417 364 2 81C 813 4 472 428 6 245 253 H.K= 2, 1 L FOBS FCAL -6 0 -13 -5 527 515 -4 1C3 -84 -3 688 646	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 E7 83 2 473 479 3 24 -32 4 2E8 285	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629 2 40 -46 3 346 341 4 C +13  H.K= 3, 3 L FOBS FCAL -5 17 +8 -4 451 448 -3 0 -9 -2 528 490	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9 1 431 460 2 28 26 3 326 306 -4 0 -11  H.K= 4, 2 L FORS FCAL -5 29 36 -4 400 422 -3 0 -9	L FOBS FCAL  -4 352 395  -3 29 31  -2 314 318  -1 13 -10  0 328 353  1 22 -23  2 262 272  H,K= 5, 2  -4 0 15  -3 319 353  -2 31 25  -1 374 370
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528 3 C 21 4 45C 463 5 14 13 H, K= 0, 5 L FOBS FCAL 1 473 478 2 15 -24 3 431 440 4 C -10	1 499 543 2 110 99 3 642 650 4 28 31 5 391 380 6 18 -20 H.K= 1. 3 L FCBS FCAL -6 287 300 -5 0 13 -4 557 506 -3 17 -11 -2 746 702 -1 19 10	H,K= 2, 0 L FOES FCAL -6 3C5 325 -4 635 650 -2 912 977 C 417 364 2 81C 813 4 472 428 6 245 253 H,K= 2, 1 L FOBS FCAL -6 0 -13 -5 527 515 -4 1C3 -84	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 87 83 2 473 479 3 24 -32 4 288 285	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629 2 40 -46 3 346 341 4 C +13  H.K= 3, 3 L FOBS FCAL -5 17 -8 -4 451 448 -3 0 -9	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9 1 431 460 2 28 26 3 326 306 -4 0 -11  H.K= 4, 2 L FORS FCAL -5 29 36 -4 400 422 -3 0 -9	L FOBS FCAL  -4 352 395  -3 29 31  -2 314 318  -1 13 -10  0 328 353  1 22 -23  2 262 272  H.K= 5, 2  -4 0 15  -3 319 353  -2 31 25  -1 374 370  0 51 -48  1 222 258
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528 3 C 21 4 45C 463 5 14 13 H, K= 0, 5 L FCBS FCAL 1 473 478 2 15 -24 3 431 440 4 C -10	1 499 543 2 110 95 3 642 65C 4 28 31 5 391 38C 6 18 -2C H.K= 1, 3 L FCBS FCAL -6 287 30C -5 0 13 -4 557 506 -3 17 -11 -2 746 702 -1 19 1C 0 690 733 1 21 -25	H.K= 2. 0 L FOBS FCAL -6 3C5 335 -4 635 650 -2 912 977 0 417 364 2 81C 813 4 472 428 6 245 253 H.K= 2. 1 L FOBS FCAL -6 0 -13 -5 527 515 -4 1C3 -84 -3 688 646 -2 212 163	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 67 83 2 473 479 3 24 -32 4 268 285	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629 2 40 -46 3 346 341 4 C -13  H.K= 3, 3 L FOBS FCAL -5 17 -8 -4 451 448 -3 0 -9 -2 528 490 -1 39 -38	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9 1 431 460 2 28 26 3 326 306 -4 0 -11  H.K= 4. 2 L FOBS FCAL -5 29 36 -4 400 422 -3 0 -9 -2 460 441	L FOBS FCAL  -4 352 395  -3 29 31  -2 314 318  -1 13 -10  0 328 353  1 22 -23  2 262 272  H.K= 5, 2  -4 0 15  -3 319 353  -2 31 25  -1 374 370  0 51 -48  1 222 258
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528 3 C 21 4 45C 463 5 14 13 H, K= 0, 5 L FOBS FCAL 1 473 478 2 15 -24 3 431 440 4 C -10 H, K= 0, 6	1 499 543 2 110 95 3 642 65C 4 28 31 5 391 38C 6 18 -2C H.K= 1, 3 L.FCES FCAL -6 287 30C -5 0 12 -4 557 506 -3 17 -11 -2 746 703 -1 19 1C 0 690 733 1 21 -25 2 541 548	H.K= 2. 0 L FORS FCAL -6 3C5 335 -4 635 650 -2 912 977 C 417 364 2 81C 813 4 472 428 6 245 253 H.K= 2. 1 L FORS FCAL -6 0 -13 -5 527 515 -4 1C3 -84 -3 688 646 -2 212 163 -1 874 831	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 87 83 2 473 479 3 24 -32 4 268 285	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629 2 40 -46 3 346 341 4 C -13  H.K= 3, 3 L FOBS FCAL -5 17 -8 -4 451 448 -3 0 -9 -2 528 490 -1 39 -38 0 485 469	L FOBS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9 1 431 460 2 28 26 3 326 306 -4 0 -11  H.K= 4. 2 L FOBS FCAL -5 29 36 -4 400 422 -3 0 -9 -2 460 441 -1 67 -57	L FOBS FCAL  -4 352 395  -3 29 31  -2 314 318  -1 13 -10  0 328 353  1 22 -23  2 262 272  H, K= 5, 2  -4 0 15  -3 319 353  -2 31 25  -1 374 370  0 51 -48  1 222 258  2 0 4
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528 3 C 21 4 45C 463 5 14 13 H, K= 0, 5 L FOBS FCAL 1 473 478 2 15 -24 3 431 440 4 C -10 F, K= 0, 6 L FCBS FCAL C 46C 456 1 66 -73	1 499 543 2 110 95 3 642 65C 4 28 31 5 391 38C 6 18 -2C H.K= 1, 3 L FCES FCAL -6 287 30C -5 0 13 -4 557 506 -3 17 -11 -2 746 702 -1 19 1C 0 690 733 1 21 -25 2 541 548 3 0 -12	H.K= 2, 0 L FOBS FCAL -6 3C5 325 -4 635 650 -2 912 977 C 417 364 2 81C 813 4 472 428 6 245 253 H.K= 2, 1 L FOBS FCAL -6 0 -13 -5 527 515 -4 1C3 -84 -3 688 646 -2 212 163 -1 874 831 C 13	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 £7 83 2 473 479 3 24 -32 4 2£8 285	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629 2 40 -46 3 346 341 4 C +13  H.K= 3, 3 L FOBS FCAL -5 17 -8 -4 451 448 -3 0 -9 -2 528 490 -1 39 -38 0 485 469 1 0 16 2 431 446 3 C -4	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9 1 431 460 2 28 26 3 326 306 -4 0 -11  H.K= 4, 2 L FORS FCAL -5 29 36 -4 400 422 -3 0 -9 -2 460 441 -1 67 -57 0 476 469	L FOBS FCAL -4 352 395 -3 29 31 -2 314 318 -1 13 -10 0 328 353 1 22 -23 2 262 272 H.K= 5, 2 -4 0 15 -3 319 353 -2 31 25 -1 374 370 0 51 -48 1 222 258 2 0 4 H.K= 5, 3 L FOBS FCAL -3 0 -9
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528 3 C 21 4 45C 463 5 14 13 H, K= 0, 5 L FOBS FCAL 1 473 478 2 15 -24 3 431 440 4 C -10 F, K= 0, 6 L FCBS FCAL C 46C 456 1 66 453 2 339 356	1 499 543 2 110 95 3 642 65C 4 28 31 5 391 38C 6 18 -2C  H.K= 1. 3 L.FCBS FCAL -6 287 30C -5 0 12 -4 557 506 -3 17 -11 -2 746 702 -1 19 1C 0 690 733 1 21 -25 2 541 548 3 0 -12 4 4C9 413 5 22 18	H.K= 2, 0 L FOES FCAL -6 3C5 325 -4 635 650 -2 912 977 C 417 364 2 81C 813 4 472 428 6 245 253 H.K= 2, 1 L FOBS FCAL -6 0 -13 -5 527 515 -4 1C3 -84 -3 688 646 -2 212 163 -1 874 831 C 13 4 1 609 649 2 133 -107 3 517 506	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 E7 83 2 473 479 3 24 -32 4 2E8 285 -4 FORS FCAL -4 0 -7 -3 35C 373 -2 26 -26 -1 479 456 C 32 -30 1 422 421 2 0 13 3 3CO 312 H,K= 2, 6	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629 2 40 -46 3 346 341 4 C +13  H.K= 3, 3 L FOBS FCAL -5 17 +8 -4 451 448 -3 0 -9 -2 528 490 -1 39 -38 0 485 469 1 0 16 2 431 446	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9 1 431 460 2 28 26 3 326 306 -4 0 -11  H.K= 4, 2 L FORS FCAL -5 29 36 -4 400 422 -3 0 -9 -2 460 441 -1 67 -57 0 476 469 1 0 -1	L FOBS FCAL  -4 352 395  -3 29 31  -2 314 318  -1 13 -10  0 328 353  1 22 -23  2 262 272  H,K= 5, 2  -4 0 15  -3 319 353  -2 31 25  -1 374 370  0 51 -48  1 222 258  2 0 4  H,K= 5, 3  L FOBS FCAL  -4 0 15  -3 319 353  -2 31 25  -1 374 370  0 51 -48  1 222 258  2 0 4  H,K= 5, 3  L FOBS FCAL  -3 0 -9  -2 314 333
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528 3 C 21 4 45C 463 5 14 13 H, K= 0, 5 L FOBS FCAL 1 473 478 2 15 -24 3 431 440 4 C -10 F, K= 0, 6 L FCBS FCAL C 46C 456 1 66 -73	1 499 543 2 110 95 3 642 65C 4 28 31 5 391 38C 6 18 -2C  H.K= 1. 3 L FCRS FCAL -6 287 30C -5 0 13 -4 557 506 -3 17 -11 -2 746 703 -1 19 1C 0 690 733 1 21 -25 2 541 548 3 0 -12 4 4C9 413 5 22 18  H.K= 1. 4	H.K= 2, 0 L FOES FCAL -6 3C5 325 -4 635 650 -2 912 977 C 417 364 2 81C 813 4 472 428 6 245 253 H.K= 2, 1 L FOBS FCAL -6 0 -13 -5 527 515 -4 1C3 -84 -3 688 646 -2 212 163 -1 874 831 C 13 4 1 609 649 2 133 -107 3 517 506 4 27 29	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 87 83 2 473 479 3 24 -32 4 268 285	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629 2 40 -46 3 346 341 4 C +13  H.K= 3, 3 L FOBS FCAL -5 17 -8 -4 451 448 -3 0 -9 -2 528 490 -1 39 -38 0 485 469 1 0 16 2 431 446 3 C -4 4 309 298	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9 1 431 460 2 28 26 3 326 306 -4 0 -11  H.K= 4, 2 L FORS FCAL -5 29 36 -4 400 422 -3 0 -9 -2 460 441 -1 67 -57 0 476 469 1 0 -1 2 291 305 3 0 18	L FOBS FCAL  -4 352 395  -3 29 31  -2 314 318  -1 13 -10  0 328 353  1 22 -23  2 262 272  H,K= 5, 2  -4 0 15  -3 319 353  -2 31 25  -1 374 370  0 51 -48  1 222 258  2 0 4  H,K= 5, 3  L FORS FCAL  -3 0 -9  -2 314 333  -1 27 5
H, K= 0, 4 L FCBS FCAL C 61C 598 1 140 -130 2 498 528 3 C 21 4 45C 463 5 14 13 H, K= 0, 5 L FOBS FCAL 1 473 478 2 15 -24 3 431 440 4 C -10 F, K= 0, 6 L FCBS FCAL C 46C 456 1 66 453 2 339 356	1 499 543 2 110 95 3 642 65C 4 28 31 5 391 38C 6 18 -2C  H.K= 1. 3 L.FCBS FCAL -6 287 30C -5 0 12 -4 557 506 -3 17 -11 -2 746 702 -1 19 1C 0 690 733 1 21 -25 2 541 548 3 0 -12 4 4C9 413 5 22 18	H.K= 2, 0 L FOES FCAL -6 3C5 325 -4 635 650 -2 912 977 C 417 364 2 81C 813 4 472 428 6 245 253 H.K= 2, 1 L FOBS FCAL -6 0 -13 -5 527 515 -4 1C3 -84 -3 688 646 -2 212 163 -1 874 831 C 13 4 1 609 649 2 133 -107 3 517 506	-5 29 20 -4 41C 389 -3 C -6 -2 554 509 -1 126 -102 C 542 54C 1 E7 83 2 473 479 3 24 -32 4 2E8 285 -4 FORS FCAL -4 0 -7 -3 35C 373 -2 26 -26 -1 479 456 C 32 -30 1 422 421 2 0 13 3 3CO 312 H,K= 2, 6	-5 430 444 -4 47 -55 -3 588 543 -2 118 -92 -1 525 487 0 155 135 1 604 629 2 40 -46 3 346 341 4 C +13  H.K= 3, 3 L FOBS FCAL -5 17 -8 -4 451 448 -3 0 -9 -2 528 490 -1 39 -38 0 485 469 1 0 16 2 431 446 3 C -4	L FORS FCAL -5 333 375 -4 50 48 -3 483 468 -2 81 -75 -1 489 451 0 0 -9 1 431 460 2 28 26 3 326 306 -4 0 -11  H.K= 4, 2 L FOBS FCAL -5 29 36 -4 400 422 -3 0 -9 -2 460 441 -1 67 -57 0 476 469 1 0 -1 2 291 305	L FOBS FCAL  -4 352 395  -3 29 31  -2 314 318  -1 13 -10  0 328 353  1 22 -23  2 262 272  H,K= 5, 2  -4 0 15  -3 319 353  -2 31 25  -1 374 370  0 51 -48  1 222 258  2 0 4  H,K= 5, 3  L FOBS FCAL  -4 0 15  -3 319 353  -2 31 25  -1 374 370  0 51 -48  1 222 258  2 0 4  H,K= 5, 3  L FOBS FCAL  -3 0 -9  -2 314 333

Table 3: Distances in XeF4. The asterisked values are inter-

molecular distances.

Figure 1: Two views of the crystal of XeF<sub>4</sub> used in this structure determination. The two views are approximately 75° rotation apart from each other. The a axis is approximately parallel to the long edge of the crystal.



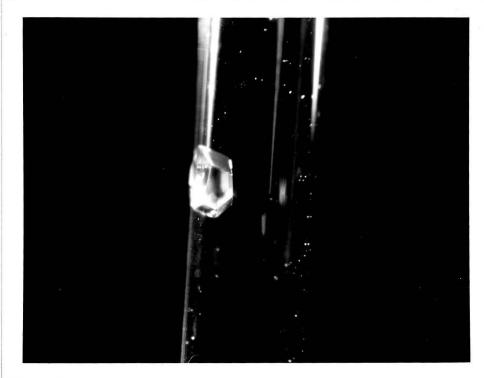


Figure 2: Molecular packing in XeF, as seen in projection down the b axis. The numbers on some of the atoms are b coordinates (x100).

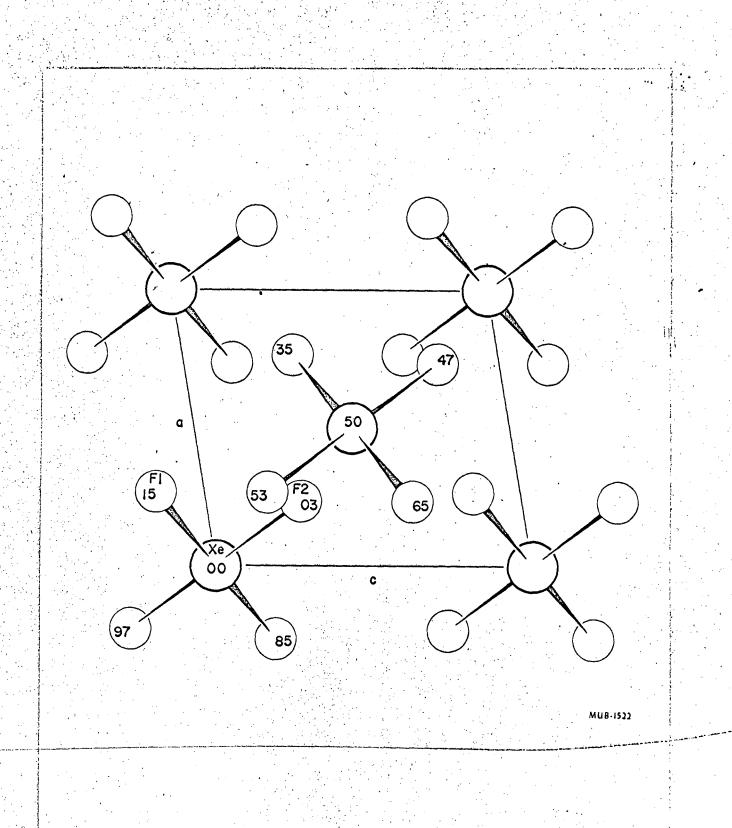
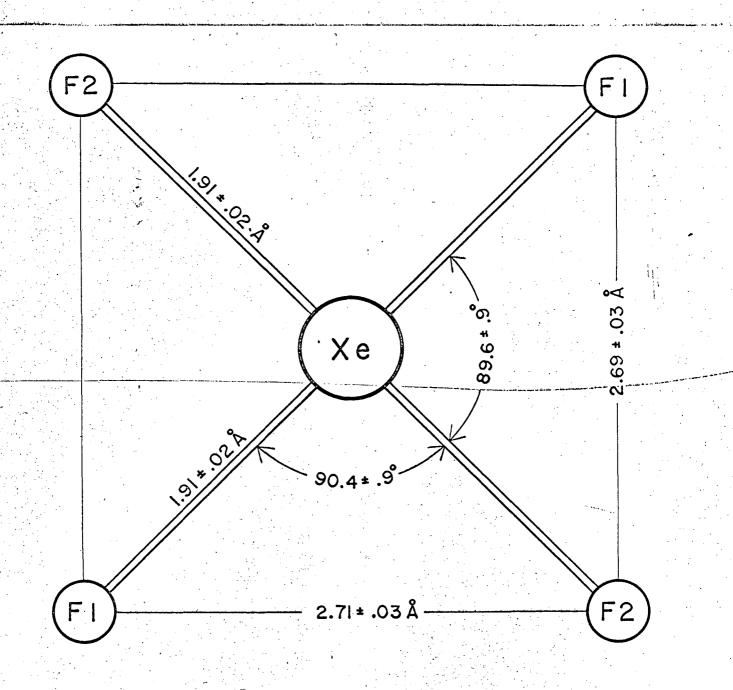


Figure 3: Molecular dimensions in XeF<sub>li</sub>. Distances have not been corrected for thermal vibrations in this figure.



XeF4

