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THE CRYSTAL STRUCTURE OF (XeF⁺) (AsF₆⁻)₁

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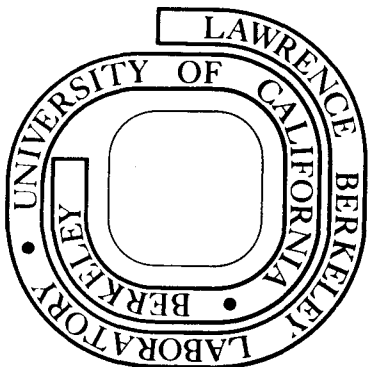
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THE CRYSTAL STRUCTURE OF $[\text{XeF}^+][\text{AsF}_6^-]^1$

Allan Zalkin, Donald L. Ward, Richard N. Biagioni

David H. Templeton*, and Neil Bartlett*

ABSTRACT

Crystals of $\text{XeF}^+\text{AsF}_6^-$ are monoclinic, space group $\text{P2}_1/\text{n}$, $a = 6.308(3)$, $b = 6.275(3)$, $c = 16.023(5)$ Å, $\beta = 99.97(5)^\circ$, $V = 624.66$ Å³, $Z = 4$, $D_x = 3.61$ g cm⁻³, at 24°C. X-ray diffraction data were measured with counter methods and MoK α radiation. With anisotropic temperature factors for all atoms, $R = 0.033$ for 777 independent reflections ($I > 3\sigma$). The structure consists of ion pairs connected by a bridging fluorine atom into FXeFAsF_5 units. The FXeF portion of the molecule is linear (angle = $178.9(7)^\circ$) with $\text{Xe-F} = 1.873(6)$ Å (terminal) and $2.212(5)$ Å (bridging). The FAsF_5 portion of the molecule is roughly octahedral with cis F-As-F angles ranging from $85.3(3)^\circ$ to $94.6(5)^\circ$; the 5 terminal As-F distances range from $1.676(5)$ Å to $1.690(8)$ Å and the bridging As-F distance is $1.813(6)$ Å. The bridge Xe-F-As angle is $134.8(2)^\circ$.

INTRODUCTION

In an earlier paper Sladky *et al.* described² the preparation of the 1:1 $\text{XeF}_2 - \text{AsF}_5$ complex and showed that it lost AsF_5 readily under vacuum at ordinary temperatures to yield a 2:1 complex. The crystal structure of the 2:1 complex has already been described³ and is consistent with formulation as the salt $\text{Xe}_2\text{F}_3^+\text{AsF}_6^-$. The structure of the 1:1 complex was of interest to us because of an earlier finding⁴ that the structure of the 1:1 $\text{XeF}_2 - \text{RuF}_5$ complex was consistent with the $\text{XeF}^+\text{RuF}_6^-$ formulation and our expectation that the formulation of the 1:1 $\text{XeF}_2 - \text{AsF}_5$ complex would be similar. Moreover, a preliminary study of 1:1 $\text{XeF}_2 - \text{AsF}_5$ by others⁵ had failed to find evidence of AsF_6^- and the authors concluded that this indicated that the complex was a molecular, possibly fluorine-bridged, adduct.

We give here the preparative conditions for 1:1 $\text{XeF}_2 - \text{AsF}_5$ complex, and the structure determined by single crystal x-ray diffraction.

EXPERIMENTAL SECTION

Preparation of XeFAsF_6 . XeF_2 (0.684 g, 4.04 mmoles) prepared as described by Williamson,⁶ was transferred in the dry atmosphere of a Vacuum Atmospheres Corporation Drilab, to a weighed quartz bulb (~ 60 cc capacity) joined to a Brass Whitey valve (IKS4) with a Teflon-gasketed Swagelock fitting. Bromine pentafluoride (Matheson Co., East Rutherford) sufficient (~ 2 ml) to dissolve the XeF_2 was

transferred to the bulb under vacuum. The resultant, almost colorless solution of XeF_2 in BrF_5 was exposed to arsenic pentafluoride gas (Ozark Mahoning, Tulsa, Okla.) to maintain a pressure of ~ 900 torr. A small Teflon-coated stirrer bar driven by an external magnet kept the solution mixed. The solution rapidly became pale yellow-green but the system was left for ~ 1 hr. to ensure full take up of AsF_5 gas. The solution was cooled to -22.8° (CCl_4 slush) and the bulk of the BrF_5 was removed in a dynamic vacuum. (At the beginning of this evaporation the valve was opened slowly to ensure smooth boiling and to avoid frothing). The crystalline solid so obtained was dried by intermittent opening and closing of the valve, for a few minutes, with the sample at room temperature. The solid remaining in the trap was almost white, with a pale yellow-green tint. It amounted to 1.372 g, indicating an AsF_5 uptake of 0.688 g (4.05 mmoles) which corresponds to a $\text{XeF}_2:\text{AsF}_5$ molar ratio of 1:1.002.

X-ray powder photographs were obtained by rapidly transferring the solid to a 0.5 mm quartz X-ray capillary in the Drilab. The capillary was sealed with a small flame. The data given in Table I were indexed using the single crystal information.

Single crystals of XeFAsF_6 were grown by sublimation of small samples of the powder sealed, as in the X-ray powder sample case, in thin-walled quartz X-ray capillaries. These capillaries were placed in an electrically heated tube which provided for a temperature gradient along the capillary of 1 or 2° at a temperature of $\sim 70^\circ$. The capillaries were left in this heater overnight and were then inspected for single crystal development using a polarizing microscope.

Raman spectra were obtained from a sample packed as for the X-ray powder sample, but in a 1.5 mm diam. quartz capillary. The sample was cooled by a cold nitrogen stream shrouded by a dry room temperature stream and the temperature was thereby maintained at $\sim -100^\circ$. The spectrum of $\text{Xe}_2\text{F}_3\text{AsF}_6$ was obtained in the same way. The spectra are compared in Fig. 1.

X-ray Measurements. The crystal selected for diffraction measurements was $0.09 \times 0.11 \times 0.15$ mm in size. Precession photographs established the lattice to be monoclinic. Absent reflections $h0l$ ($h + 1 \neq 2n$) and $0k0$ ($k \neq 2n$) indicate space group $P2_1/n$. Setting angles for the Picker FACS-I diffractometer for 12 reflections above $2\theta = 45^\circ$ (λ 0.70926 Å for $\text{MoK}\alpha_1$) were used for least-squares adjustment of the cell dimensions. Intensities were measured with graphite-monochromatized $\text{MoK}\alpha$ radiation and θ - 2θ technique for all reflections in the half-sphere with k non-negative and $2\theta < 55^\circ$. After averaging equivalent pairs there were 1447 unique ones of which 783 had $I > 3\sigma$. Measurements were made with a scan rate of $1^\circ/\text{min}$, backgrounds counted for 10 sec each at an offset of 1° from each end of the scan, and a scan length of 1.5° in 2θ plus the $\alpha_1 - \alpha_2$ divergence. Three standard reflections showed slight changes during the experiment, and a compensating correction (ranging 1.00 to 1.10) was applied to the intensities. Correction for absorption⁷ ($\mu = 103.4 \text{ cm}^{-1}$) was made by analytical integration with the crystal shape described by eight faces. Effects of extinction were evident in the data, and an empirical isotropic correction was applied which increased the structure factors

by 84% and 36% for the strongest and seventh-strongest reflections, respectively. The six strongest reflections were assigned zero weight because they failed to give good agreement even with this correction. A term $(0.03I)^2$ was added to the variance of I derived from counting statistics. Zero weight was also assigned to reflections with $I < 3\sigma$. Atomic scattering factors of Doyle and Turner⁸ with anomalous scattering corrections of Cromer and Liberman⁹ were used for neutral Xe, As, and F.

Crystal Data. XeFAsF_6 , monoclinic, $P2_1/n$, $a = 6.308(3)$, $b = 6.275(3)$, $c = 16.023(5)$ Å, $\beta = 99.97(5)^\circ$, $V = 624.66$ Å³, $Z = 4$, $D_x = 3.61$ g cm⁻³, at 24°C.

Determination of Structure. Analysis of a Patterson map indicated two sets of heavy atoms in general positions, a result incompatible with the preconceived opinion of the composition of the material.¹⁰ For this reason the subsequent analysis was carried out using the diffraction data to establish the composition. The peaks for the heavy atoms were of appropriate relative height to correspond to Xe and As, and other peaks were found which corresponded to six F atoms around the As atom. Fourier maps phased with these eight atoms revealed the seventh fluorine atom. Another smaller peak was tested as a possible fluorine atom, but it was rejected by the least-squares refinement. A later electron density map, prior to the absorption correction and with $F = \Sigma |\Delta F| / \Sigma F_o = 0.10$, showed no extra peaks as high as one-third the lowest fluorine atom. The final refinement by full-matrix least-squares reduced $R_w = [\Sigma w(\Delta F)^2 / \Sigma w F_o^2]^{1/2}$, the quantity minimized, to

0.036. The final R was 0.033 for 777 reflections and 0.076 for 1447 reflections including those of zero weight. In the last cycle no parameter shifted more than 0.01σ . The goodness-of-fit was 1.13. Final parameters are listed in Table II.

DISCUSSION

The crystal structure, Fig. 2(a) consists of an ordered arrangement of discrete FXeFAsF_5 units (Fig. 3), the closest contact between units being $2.92 \text{ \AA}$, a contact between F(1) and F(7). Bond distances and angles of this unit are listed in Tables III and IV. The amplitudes of thermal motion are considerable, and distances corrected for this motion according to the riding model are also listed in Table III. Table V gives the angles between principal axes of thermal motion of fluorine atoms and their bond vectors. In each case except Xe-F(6) the minimum amplitude of motion is nearly parallel to the bond, and in every case the largest amplitude is nearly perpendicular to the bond. These results lend credibility to the physical reality of this model of the thermal motion and support the propriety of the riding model. It may be noted that the consistency of As-F bond lengths (omitting the bridging bond which is not expected to be the same) is improved by the thermal correction.

The FXeFAsF_5 unit is remarkably similar in shape to the analogous unit in FXeFRuF_5^4 with which it is compared in Fig. 4. In both cases the bridging fluorine is more equally shared between Xe and As(Ru) than in the corresponding $[\text{XeF}_5^+][\text{MF}_6^-]$ compounds.^{3,4}

In spite of the close similarity of molecular geometry and the fact that the arsenic and ruthenium compounds crystallize with the same space group symmetry, the unit cell shapes are dissimilar and, moreover, the molecular packing is quite different. In FXeFAsF_5 the long dimensions of the formula units are all nearly parallel to each other, while in FXFRuF_5 there are two orientations nearly perpendicular to each other. The molecular volumes differ by less than 3%, reflecting the slightly larger size of Ru compared with As, and there is little difference in the shortest intermolecular distances.

Inspection of Fig. 2(b) reveals that in FXeFRuF_5 each XeF species is surrounded by a roughly cubic arrangement of RuF_6 species; the Xe...Ru distances are: 3.82, 4.47, 4.54, 4.82, 4.88, 4.91, 4.99, 5.66 Å. In FXeFAsF_5 (Fig. 2(a)) each XeF species has six AsF_6 species at Xe...As distances of 3.72, 4.38, 4.44, 4.46, 4.52, and 4.80 Å. This arrangement can be viewed as a grossly distorted octahedral coordination of the cation. The next nearest arsenic neighbor of the Xe atom is at 5.84 Å. Thus to a first approximation we can represent the FXeFRuF_5 as developed from a CsCl (8:8 coordination) structure type whereas we can represent FXeFAsF_5 as derived from a NaCl type (6:6 coordination). Such representations conform with the common structure types for hexafluoroarsenates and hexafluororuthenates.¹¹ Thus $\text{NO}^+[\text{AsF}_6]^-$ is of NaCl type¹² whereas $\text{NO}^+[\text{RuF}_6]^-$ is of CsCl type.¹³ Moreover, although the XeF_5^+ species is essentially the same in $\text{XeF}_5^+\text{AsF}_6^-$ (ref 3) and $\text{XeF}_5^+\text{RuF}_6^-$ (ref 4) the coordination is different. The coordination number differences are not to be associated with the non-transition-element transition-element content however. Thus $\text{NO}^+[\text{SbF}_6]^-$ is of CsCl type¹³ like $\text{NO}^+[\text{RuF}_6]^-$, and $\text{XeF}_5^+\text{AsF}_6^-$ has the same

structure¹⁴ as $\text{XeF}_5^+ \text{AsF}_6^-$. Indeed X-ray powder photographs¹⁵ indicate that FXeFSbF_5 is probably isostructural with FXeFRuF_5 .

It is probable that the difference in coordinating capability of the anions is associated with differences in polarizability of the F ligands in the MF_6^- . In those hexafluorometallates which can be unambiguously described as salts $\text{A}^+ \text{MF}_6^-$, the small less polarizable (harder) cations such as Li^+ and Na^+ generally prefer a NaCl type lattice, whereas the more polarizable (softer) cation, e.g., Cs^+ , prefer the CsCl type. The data for selected AsF_6^- , AuF_6^- , RuF_6^- and SbF_6^- salts,^{11,14,16-20} Table VI, shows the pattern. The data indicates that the effective molecular volume of the anions increases in the sequence $\text{AsF}_6^- < \text{AuF}_6^- < \text{RuF}_6^- < \text{SbF}_6^-$. One also notes that even with a large cation such as IF_6^+ , the AsF_6^- and AuF_6^- salts adopt the NaCl type lattice - presumably because the F ligands of that cation are not very polarizable (i.e., are hard). However, even with this cation, one sees that the CsCl lattice becomes the preferred one with the larger (and hence more polarizable) SbF_6^- anion.

The similarity of the FXeFAsF_5 and FXeFRuF_5 units (Fig. 4) suggests that the bonding of the xenon is essentially the same for both. The bonding in XeF_2 , following Coulson,²¹ can be conveniently represented as a resonance hybrid of the canonical forms $(\text{F-Xe})^+ \text{F}^-$ and $\text{F}^- (\text{Xe-F})^+$. This kind of representation permits one to make rough thermodynamic stability estimates.²² In the FXeFMF_5 compounds one can represent the equivalent canonical forms as $[\text{F-Xe}]^+ [\text{F-MF}_5]^-$ and $\text{F}^- [\text{XeFMF}_5]^+$. The components F^- , $[\text{Xe-F}]^+$ and $[\text{F-AsF}_5]^-$ in the listed canonical forms can each be visualized as providing each atom with its 'ideal' complement of eight valence

electrons.²³ The component $[\text{XeFMF}_5]^+$ cannot provide for this, without writing non-bonded forms such as $[(\text{Xe-F})^+\text{AsF}_5]$ and the unrealistic $[\text{Xe}(\text{F-AsF}_5)^+]$. We therefore believe that the canonical form $\text{F}^-[\text{XeFMF}_5]^+$ is not important. As has been argued previously⁴ we prefer to represent the formula units simply as $[\text{FXe}]^+[\text{MF}_6]^-$ and allow that the short distance between the Xe of the cation and one of the F atoms of the anion is a consequence of the cation having its positive charge centered largely at the Xe atom. This positive charge location is a consequence of the electron density in the Xe-F bond of the cation having depleted the xenon valence shell electron density (in comparison with atomic Xe). Moreover the formation of the bond in the cation must create an electron-density hole on the far side of the Xe atom (i.e., trans to the bond). One therefore anticipates that the Xe-F^+ species should show its highest effective positive charge when viewed along the axis towards the Xe atom. Thus the cation ought to possess a unique axis in its polarizing effects, as observed in these structures. Representation of FXeFMF_6 as the salts $\text{XeF}^+\text{MF}_6^-$, as for the XeF_3^+ and XeF_5^+ salts^{24,4} (allowing for the polarizing effects of the cations) predicts the observed disposition of cation to anion. The model is simple, and sufficient.

Supplementary Material Available. A listing of structure factors (6 pages). Ordering information is given on any current masthead page.

ACKNOWLEDGEMENTS

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Table I X-ray powder data for $[\text{XeF}]^+[\text{AsF}_6]^-$ (from a sample in 0.3 mm diam. quartz capillary using Cu K_α radiation).

hkl	$1/d^2$		Rel. intensity
	calc.	obs.	
002	.0161	.0170	vw
$11\bar{1}$	.0518	.0515	s
111	.0588	.0586	s
004	.0642	.0648	s
?	----	.0706	vvw
112	.0744	.0774	m
$11\bar{3}$	.0768		
014	.0896	.0885	vw
113	.0980		
020	.1016	.0988	mw
200	.1036		
021	.1056		
$20\bar{2}$	.1056	.1080	m
$10\bar{5}$	.1086		
120	.1275	.1241	w
$12\bar{1}$	.1280		
$11\bar{5}$	.1340	.1347	w
121	.1350		
$20\bar{4}$	.1396		
006	.1445	.1396	w
105	.1440		
023	.1377		

CONTD.

Table I (CONTD.)

212	.1592	.1599	w
024	.1658	.1679	w
115	.1693		
204	.1961	.1970	w
10 $\bar{7}$	.1979		
220	.2052		
20 $\bar{6}$	.2058	.2059	w
124	.2059		
12 $\bar{5}$	.2102		
21 $\bar{6}$	.2312	.2349	w
22 $\bar{4}$	.2412	.2426	w
008	.2570		
31 $\bar{1}$	.2520	.2550	mw
13 $\bar{1}$	.2549		
131	.2620	.2635	mw
31 $\bar{3}$	.2629		
224	.2977	.3019	w
027	.2983		
31 $\bar{5}$	.3059		
20 $\bar{8}$	.3041	.3077	w
133	.3012		
11 $\bar{9}$	.3447	.3484	vw
119	.4083		
208	.4171		
400	.4145	.4090	w
040	.4062		
00, 10	.4015		

Table II Coordinates and Thermal Parameters for $[\text{XeF}^+][\text{AsF}_6^-]^a$

	x	y	z	B_{11}	B_{22}	B_{33}	B_{12}	B_{13}	B_{23}
Xe	.25918(9)	.21684(12)	.62266(3)	3.94(3)	4.32(3)	3.51(2)	-.46(3)	.67(2)	.07(2)
As	.23792(13)	.27638(18)	.39041(5)	3.32(4)	3.83(5)	3.56(3)	-.19(4)	.46(3)	-.21(3)
F(1)	.4950(8)	.2815(14)	.3763(4)	4.4(3)	9.4(5)	8.1(4)	-.6(3)	2.4(3)	.0(3)
F(2)	.2308(13)	.5447(14)	.3816(5)	8.6(5)	4.8(4)	11.8(6)	.5(4)	2.6(4)	1.1(3)
F(3)	.1413(12)	.2335(16)	.2889(4)	8.9(4)	15.2(8)	3.9(3)	-3.3(5)	.1(3)	-1.8(4)
F(4)	-.0092(9)	.2721(13)	.4177(5)	4.0(3)	8.7(5)	8.7(4)	-.2(3)	2.1(3)	-.2(3)
F(5)	.2512(14)	.0141(13)	.4127(6)	9.1(5)	4.1(4)	13.9(6)	.2(4)	1.6(4)	.9(4)
F(6)	.3466(12)	.3220(15)	.5013(3)	7.1(3)	13.1(6)	3.8(2)	-5.4(5)	.1(2)	.5(2)
F(7)	.1843(13)	.1334(19)	.7260(4)	11.2(6)	15.5(7)	4.8(3)	-5.2(5)	3.0(3)	1.3(4)

^aEstimated standard deviation of the least significant digit(s) is given in parentheses here and in the following tables. The form of the temperature factor is $\exp[-0.25(h^2 a^{*2} B_{11} + 2hka^* b^* B_{12} + \dots)]$.

For space group $P2_1/n$ (an alternate setting of $P2_1/c$) the general positions are: x, y, z ; $-x, -y, -z$; $1/2 + x, 1/2 - y, 1/2 + z$; $1/2 - x, 1/2 + y, 1/2 - z$.

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Table III Interatomic Distances in $[\text{XeF}^+][\text{AsF}_6^-]$, Å

Xe-F(6)	2.212(5)	[2.25] ^a	As-F(3)	1.657(6)	[1.72]
Xe-F(7)	1.873(6)	[1.94]	As-F(4)	1.690(5)	[1.73]
As-F(1)	1.676(5)	[1.72]	As-F(5)	1.683(8)	[1.74]
As-F(2)	1.690(8)	[1.74]	As-F(6)	1.813(6)	[1.86]

^aValues in square brackets are corrected for thermal motion accordingly to the riding model.

Table IV Bond Angles (deg)

F(6)-Xe	-F(7)	178.9(7)	F(2)-As	-F(5)	172.7(6)
Xe	-F(6)-As	134.8(2)		-F(6)	85.7(5)
F(1)-As	-F(2)	89.0(4)	F(3)-As	-F(4)	93.0(4)
	-F(3)	94.1(4)		-F(5)	92.7(5)
	-F(4)	172.9(5)		-F(6)	179.3(7)
	-F(5)	91.9(4)	F(4)-As	-F(5)	86.8(4)
	-F(6)	85.3(3)		-F(6)	87.6(4)
F(2)-As	-F(3)	94.6(5)	F(5)-As	-F(6)	87.1(5)
	-F(4)	91.4(5)			

Table V Angles (deg) between Bond Vectors and Principal Axes
of the Thermal Ellipsoids, and Root-Mean-Square
Displacements ($\text{\AA}$)

Atom	Vector	Angles			Rms Displacements		
		1	2	3	1	2	3
F(1)	F(1)-As	7	85	85	.215	.325	.346
F(2)	F(2)-As	5	87	86	.242	.323	.390
F(3)	F(3)-As	2	90	88	.209	.324	.458
F(4)	F(4)-As	8	84	85	.211	.329	.336
F(5)	F(5)-As	7	89	83	.225	.340	.423
F(6)	F(6)-As	18	73	85	.215	.230	.458
F(6)	F(6)-Xe	63	27	90	.215	.230	.458
F(7)	F(7)-Xe	4	86	89	.200	.332	.492

Table VI Selected Formula Unit Volumes ($\text{\AA}^3$) and Lattice Type (N = NaCl type and C = CsCl type) for Selected $A^+MF_6^-$ Salts

M	As	Au	Ru	Sb
A				
Na	116.0, (N _R) ^a	?	120.4, (N _R) ^b	137.0, (N) ^b
IF ₆	214, (N) ^c	219, (N) ^d	?	223, (C) ^{d,e}
Cs	138.4, (C _R) ^f	141.3(C _R) ^d	142.6(C _R) ^b	147.1, (C _R) ^g

? indicates that the structure type is not known. Subscript R indicates a rhombohedral cell, absence indicates cubic.

^aRef 16

^bRef 11

^cRef 17

^dRef 14

^eRef 18

^fRef 19

^gRef 20

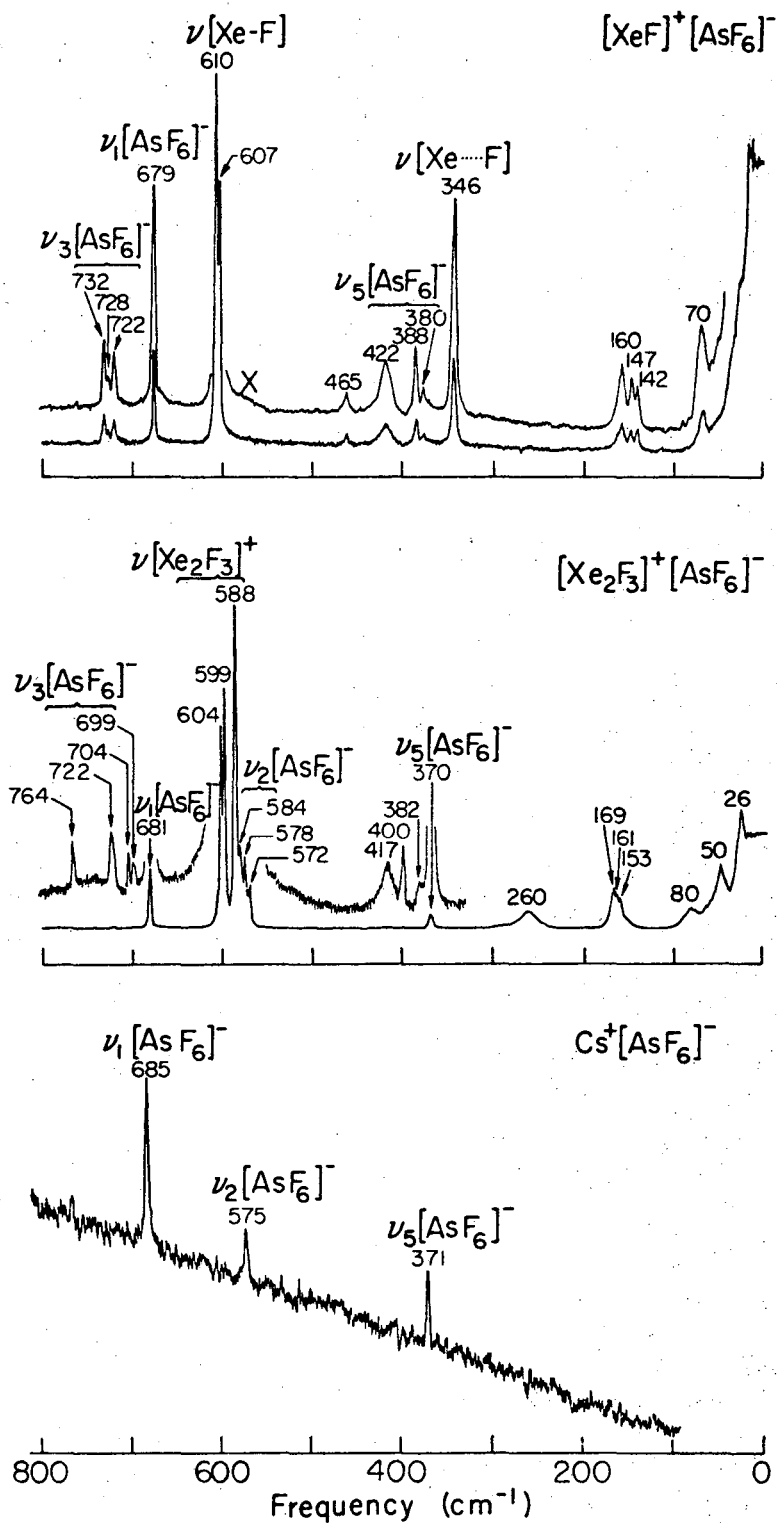
FIGURE CAPTIONS

Fig. 1. The spectra of XeFAsF_6 and $\text{Xe}_2\text{F}_3\text{AsF}_6$ are seen to be similar and the counterparts of the ν_1 and ν_5 modes are seen, from comparison with the CsAsF_6 spectrum to be present in both. $\text{Xe}_2\text{F}_3\text{AsF}_6$ consists of well separated ions Xe_2F_3^+ and AsF_6^- (Ref. 3) whereas in XeFAsF_6 there is a unique interaction of cation and anion. This interaction is probably responsible for the relatively intense band at 346 cm^{-1} in XeFAsF_6 . Similar assignments, but with a different bonding interpretation have been given by Gillespie and Landa (Inorg. Chem. 12, 1385 (1973)); our spectrum of XeFAsF_6 shows less $\text{Xe}_2\text{F}_3\text{AsF}_6$ impurity (X) than theirs and fine structure and weak bands previously unrecorded.

Fig. 2. Stereoviews of the crystal structure (a) of $[\text{XeF}^+][\text{AsF}_6^-]$ and (b) $[\text{XeF}^+][\text{RuF}_6^-]$, drawn with Johnson's ORTEP.

Fig. 3. Stereoview of the molecular unit with 50% probability ellipsoids.

Fig. 4. The formula units of XeFAsF_6 and XeFRuF_6 (Ref. 4), the former with 50% probability ellipsoids, the latter with 30%.



XBL 778-6003

Fig. 1

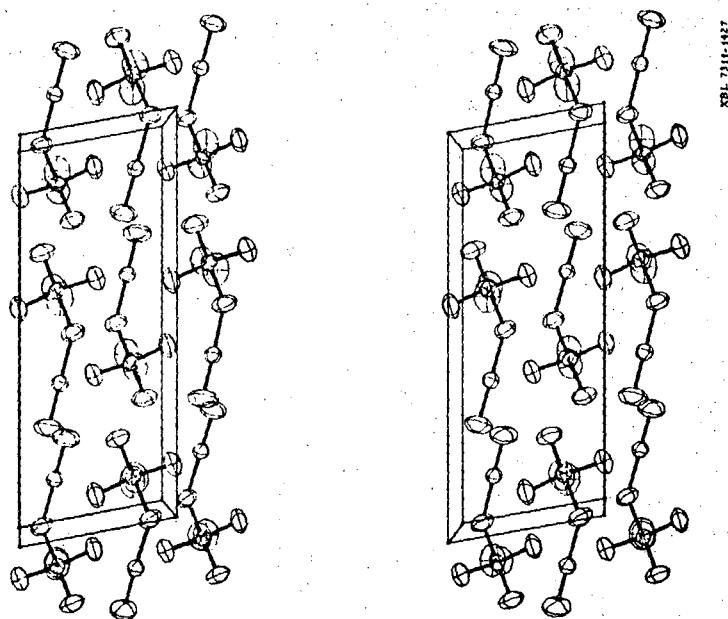


Fig. 2(a)

OBSERVED STRUCTURE FACTORS, STANDARD DEVIATIONS, AND DIFFERENCES (X 3.0) FOR
(XEF+)(ASF6-) F(0,0,0) = 1799

FOB AND FCA ARE THE OBSERVED AND CALCULATED STRUCTURE FACTORS.
SG = ESTIMATED STANDARD DEVIATION OF FOB. DEL = /FOB/ - /FCA/.
* INDICATES ZERO WEIGHTED DATA.

L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL	
H,K=	0,	0		H,K=	0,	3		14	41	3		15	29	9	-7*-12	85	6	5		
2	112	5	0	1	3	10	-6*	15	52	6		6	17	117	4	1	-11	44	11	-2*
4	999	32	117*	2	13	6	-3*	16	20	7		2*	19	48	5	6	-10	26	5	2*
6	312	6	12	3	136	3	1	H,K=	0,	6		H,K=	1,	1	-9	174	5	6		
8	698	15	64	4	55	2	1	0	77	9		-5	-20	0	26	-12*	-8	87	2	-1
10	298	5	2	5	30	5	9	1	121	2		-3	-19	22	26	10*	-7	202	10	2
12	307	5	7	6	96	2	3	2	20	8		14*-18		2118	-21*	-6	82	4	4	
14	89	5	-11	7	77	2	1	3	141	3		-1	-17	141	5	-5	-5	182	9	5
16	137	2	3	8	123	3	2	4	77	3		-1	-16	20168	-9*	-4	127	6	2	
18	99	2	1	9	31	3	-3	5	91	2		0	-15	31	4	-5	-3	208	9	8
20	55	2	3	10	74	2	-5	6	34	7		10*-14	15	44	-16*	-2	78	8	-1	
H,K=	0,	1		11	106	3	3	7	129	3		-0	-13	249	7	-0	-1	155	6	3
1	0	20	-3*	12	54	6	-7	8	52	4		-0	-12	0	22	-18*	0	161	5	-2
2	39	12	-8*	13	38	3	-5	9	45	7		-4	-11	97	4	-4	1	171	5	4
3	70	2	7	14	88	3	-3	10	19	12		-8*-10	125	5	-3	2	99	5	-6	
4	120	6	-2	15	43	3	-4	11	94	2		-1	-9	500	20	34	3	194	9	8
5	1	26	-6*	16	41	3	9	12	33	8		3*	-8	33	4	-3	4	105	3	1
6	194	4	6	17	30	5	7	13	31	10		14*	-7	237	7	8	5	173	6	0
7	63	2	0	18	63	3	-3	H,K=	0,	7		-6	124	6	-2	6	0	12	-4*	
8	159	3	-0	19	41	4	8	1	27	11		19*	-5	446	26	27	7	21	6	4*
9	6	11	-3*	H,K=	0,	4		2	22	10		6*	-4	0	38	-3*	8	44	5	-1
10	193	4	7	0	391	7	-20	3	28	16		2*	-3	443	23	7	9	178	5	3
11	43	2	-9	1	247	4	-8	4	8	18		0*	-2	176	9	3	10	41	4	5
12	96	2	-0	2	55	2	1	5	0	20		-3*	-1	632	40	-129*	11	30	12	12*
13	19	23	10*	3	292	8	0	6	18	7		7*	0	38	7	21	12	74	6	-5
14	129	3	-2	4	343	10	-1	7	37	3		-1	1	641	67	-24*	13	127	4	4
15	0	21	-14*	5	159	4	5	8	8	15		-5*	2	188	10	4	14	13	24	-10*
16	39	4	6	6	113	3	4	9	12	18		5*	3	517	58	5	15	33	9	-3*
17	0	16	-7*	7	237	6	0	10	20	16		17*	4	65	9	-6	16	22	30	-7*
18	106	2	-2	8	199	5	-1	H,K=	0,	8		5	513	35	18	17	101	4	5	
19	0	48	-16*	9	81	6	1	0	8	23		3*	6	146	5	-3	18	0	29	-10*
20	19	16	-1*	10	85	5	-9	1	60	3		-0	7	237	6	8	19	31	11	1*
H,K=	0,	2		11	145	3	-3	2	22	10		19*	8	37	14	-6*	H,K=	1,	3	
0	672	23	-156*	12	115	2	1	3	72	3		2	9	557	20	37	-19	10	19	2*
1	233	5	-7	13	32	6	4*	4	17	23		14*	10	103	4	4	-18	49	3	5
2	39	17	-5*	14	55	4	-5	H,K=	1,	0		11	115	2	1	-17	86	2	-0	
3	165	4	-2	15	90	3	2	-19	57	7		-6	12	0	17	-13*-16	52	7	1	
4	538	28	-17	16	46	4	-4	-17	95	2		-1	13	224	4	1	-15	33	10	14*
5	101	2	0	17	11	16	4*-15	78	5	-3		14	35	12	-7*-14	67	6	-3		
6	135	3	3	H,K=	0,	5	-13	152	3	-2		15	18	20	-11*-13	185	8	0		
7	205	5	4	1	48	4	2	-11	47	4		11	16	0	18	-24*-12	60	2	-2	
8	446	14	14	2	22	14	13*	-9	256	5		3	17	128	3	-1	-11	57	11	4*
9	71	2	-6	3	63	3	2	-7	243	4		20	18	11	23	-6*-10	152	9	-8	
10	193	3	6	4	46	13	11*	-5	176	4		5	19	12	16	5*	-9	275	14	5
11	114	3	-1	5	32	17	-7*	-3	105	2		8	H,K=	1,	2	-8	84	3	1	
12	231	4	-4	6	25	33	-12*	-1	65	2		-1	-20	31	9	-2*	-7	155	7	-2
13	21	33	-9*	7	57	5	-2	1	85	8		-8	-19	47	4	2	-6	214	10	4
14	97	2	1	8	37	6	-9	3	26	43		17*-18	4	20	-1*	-5	346	22	-0	
15	65	3	-2	9	23	10	-0*	5	181	4		-0	-17	95	4	8	-4	107	3	0
16	104	3	-3	10	37	6	1	7	120	2		-4	-16	37	3	0	-3	276	12	-5
17	6	17	6*	11	59	4	-2	9	249	4		2	-15	67	3	-1	-2	302	17	-15
18	69	3	-3	12	26	7	-4*	11	31	10		3*-14	0	27	-3*	-1	388	16	-31	
19	32	6	-7*	13	21	12	-6*	13	154	6		-2	-13	126	3	6	0	24	4	9

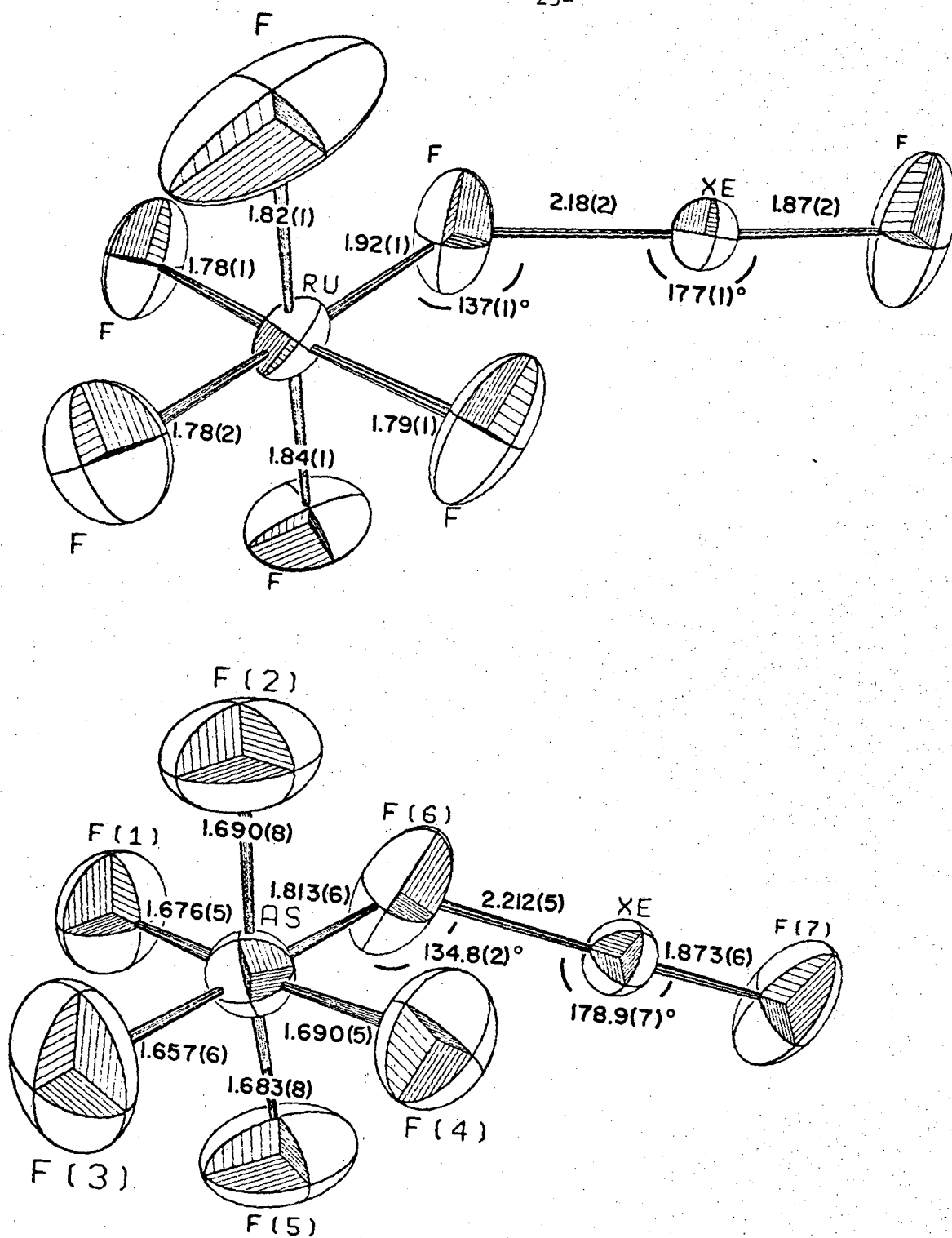
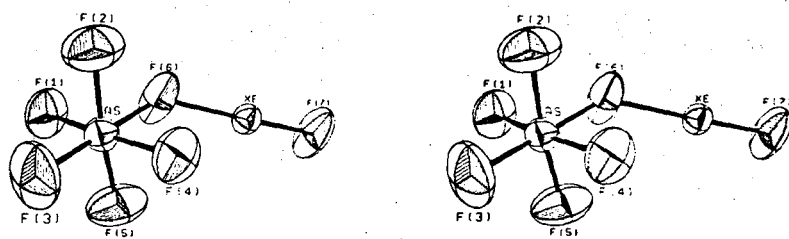


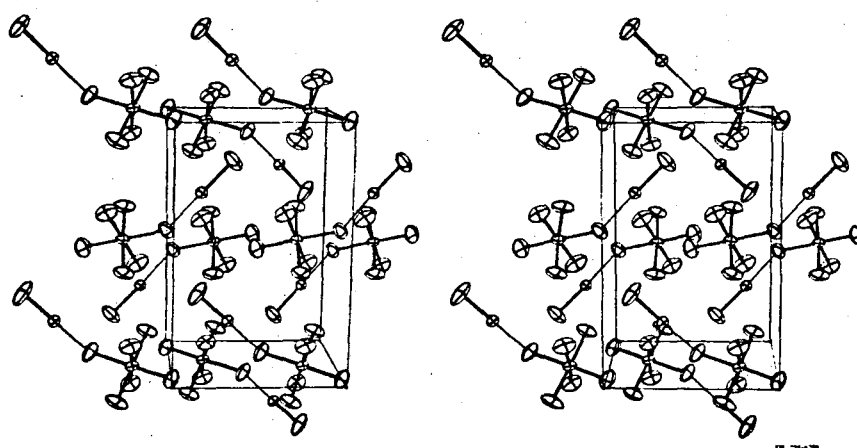
Fig. 4

XBL 7311-6807



XBL 7311-1428

Fig. 3



STRUCTURE FACTORS CONTINUED FOR
(XEF+)(ASF6-)

PAGE 2

L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL
1	326	8	-17	-15	0	18	-2*	11	26	8	17*-16	16	19	5*	1	125	5	5	
2	310	15	-12	-14	78	4	5	12	35	20	-6*-15	0	73	-10*	2	65	3	1	
3	306	16	-9	-13	60	7	-6	13	19	23	-2*-14	148	4	-0	3	77	1	1	
4	37	2	-3	-12	61	3	-1	H,K= 1, 7 -13				8	24	0*	4	373	35	-11	
5	369	25	-4	-11	22	14	6*-10	69	10	1	-12	112	3	-1	5	139	8	-11	
6	244	9	-2	-10	134	7	-2	-9	33	15	13*-11	32	4	-12	6	42	4	-5	
7	170	4	-0	-9	88	6	-5	-8	33	8	-8*-10	200	3	1	7	124	5	2	
8	92	3	3	-8	55	4	-1	-7	0	29	-10*-9	5	20	-13*	8	355	26	5	
9	293	12	1	-7	33	28	-6*	-6	107	5	3	-8	13	6	1*	9	49	5	-3
10	142	5	0	-6	202	6	5	-5	27	15	3*-7	17	5	-6*	10	87	8	7	
11	62	11	-4	-5	124	7	-1	-4	32	6	-2*-6	313	6	7	11	76	8	-2	
12	43	4	-4	-4	56	12	8*	-3	14	17	-6*-5	50	2	-1	12	192	7	-3	
13	163	6	3	-3	99	5	10	-2	131	5	-2	-4	9	21	-2*	13	36	10	-4*
14	80	3	0	-2	233	9	2	-1	36	12	12*-3	47	7	9	14	80	5	4	
15	18	31	5*	-1	128	4	-2	0	15	18	5*-2	180	4	1	15	57	3	-0	
16	42	5	-1	0	31	9	16*	1	19	26	-5*-1	15	36	-11*	16	82	2	-2	
17	79	3	-1	1	117	4	1	2	132	6	-2	0	0	35	-14*	17	10	20	3*
18	34	39	-4*	2	234	4	2	3	31	18	12*	1	72	8	4	18	53	8	1
H,K= 1, 4				3	100	5	5	4	27	32	8*	2	399	37	-20	H,K= 2, 3			
-18	0	22	-8*	4	23	29	11*	5	21	22	-5*	3	56	6	-4	-19	36	15	3*
-17	55	6	4	5	132	5	-2	6	107	4	1	4	48	3	2	-18	63	7	-7
-16	51	9	-4	6	213	5	5	7	12	25	5*	5	21	4	4	-17	32	13	-5*
-15	30	8	5*	7	40	10	-4*	8	29	29	-1*	6	119	4	-6	-16	28	11	0*
-14	13	24	4*	8	43	6	1	9	32	8	10*	7	23	12	-2*-15	46	12	4*	
-13	64	5	-7	9	94	4	-5	H,K= 1, 8				8	115	2	1	-14	96	3	-5
-12	81	7	4	10	130	4	-1	-3	22	26	8*	9	12	18	-3*-13	52	3	2	
-11	0	25	-14*	11	24	7	7*	-2	8	23	2*	10	136	3	-2	-12	56	4	-4
-10	20	38	-9*	12	46	4	0	-1	9	24	2*	11	38	14	3*-11	85	4	2	
-9	87	8	-3	13	59	4	-3	0	16	20	6*	12	54	11	-0*-10	93	4	-3	
-8	82	7	3	14	72	3	-0	1	0	35	-11*	13	0	21	-4*	-9	50	4	-6
-7	19	22	12*	15	7	17	6*	2	9	19	3*	14	101	3	-1	-8	65	3	5
-6	0	14	-18*	H,K= 1, 6				H,K= 2, 0				15	3	15	-15*	-7	82	2	-2
-5	87	3	-1	-14	20	22	8*-20	39	6	-2	16	68	5	6	-6	128	2	2	
-4	89	6	8	-13	25	7	0*-18	93	2	-2	17	2	23	-1*	-5	85	4	-1	
-3	8	17	-1*-12	47	5	-3	-16	128	2	2	18	79	3	3	-4	18	9	-0*	
-2	27	7	-2*-11	29	14	23*-14	165	4	-7	H,K= 2, 2				2	-3	86	3	-4	
-1	0	18	-5*-10	21	25	6*-12	248	4	6	-20	32	7	1*	-2	92	2	0		
0	40	16	-3*	-9	13	18	-11*-10	256	4	5	-19	25	29	-16*	-1	67	3	-0	
1	22	27	7*	-8	59	5	2	-8	522	10	33	-18	73	6	3	0	15	7	3*
2	46	4	2	-7	11	16	2*	-6	238	4	3	-17	12	24	10*	1	50	3	-0
3	12	14	-4*	-6	28	8	16*	-4	638	11	-4*-16	94	3	-4	2	123	7	1	
4	56	2	-2	-5	23	6	6*	-2	161	6	3	-15	59	7	-4	3	130	4	2
5	72	2	2	-4	64	2	-3	0	670	25	-187*-14	138	4	-1	4	15	19	-1*	
6	49	3	4	-3	12	22	8*	2	78	6	0	-13	0	35	-4*	5	29	3	6
7	44	5	12	-2	20	16	19*	4	548	15	-23	-12	200	4	-1	6	71	2	-2
8	56	15	-1*	-1	19	26	10*	6	100	2	-0	-11	112	3	-2	7	78	3	4
9	75	11	-8	0	70	7	5	8	486	12	16	-10	177	3	7	8	75	4	3
10	38	6	-8	1	0	17	-3*	10	125	2	2	-9	77	4	-6	9	35	17	5*
11	26	10	21*	2	16	19	6*	12	250	4	-0	-8	332	9	3	10	44	7	-15
12	63	5	-6	3	0	17	-4*	14	80	3	-1	-7	160	4	-2	11	73	4	-4
13	64	6	-2	4	49	3	-5	16	102	3	-2	-6	87	2	2	12	41	3	-5
14	31	19	5*	5	22	29	14*	18	67	4	0	-5	16	5	3*	13	25	29	6*
15	21	25	5*	6	19	25	-3*	H,K= 2, 1				-4	405	13	-25	14	65	7	-2
16	44	8	1	7	21	15	10*-20	18	16	4*	-3	134	4	-1	15	41	10	-3*	
17	55	3	6	8	49	7	4	-19	28	34	10*	-2	69	2	-3	16	41	6	3
H,K= 1, 5				9	10	34	-7*-18	113	2	-0	-1	145	2	-7	17	20	27	8*	
-16	40	14	-3*	10	26	6	-0*-17	8	25	-10*	0	380	12	-24	H,K= 2, 4				

STRUCTURE FACTORS CONTINUED FOR
(XEF+)(ASF6-)

PAGE 3

L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL
-18	30	18	-5*	5	21	25	-12*	H,K=	3,	0	16	20	30	10*	-2	231	7	-3	
-17	0	16	-1*	6	15	22	-13*	-19	58	10	-5	17	87	10	2	-1	315	8	-11
-16	46	10	2*	7	62	3	9	-17	88	3	-2	H,K=	3,	2	0	35	9	18*	
-15	90	3	4	8	24	9	-3*	-15	78	3	-7	-19	42	5	-6	1	198	10	6
-14	62	14	-8*	9	17	32	0*	-13	175	4	-4	-18	20	29	19*	2	219	6	4
-13	19	22	17*	10	26	31	4*	-11	18	6	9*	-17	82	4	2	3	233	11	0
-12	115	3	8	11	55	7	4	-9	233	4	-1	-16	43	5	-3	4	31	5	2
-11	147	3	-3	12	30	9	5*	-7	70	1	2	-15	63	2	-1	5	237	10	3
-10	91	4	-7	13	0	27	-11*	-5	143	3	2	-14	10	18	5*	6	174	8	-2
-9	55	15	-2*	14	34	11	8*	-3	158	3	4	-13	138	4	-1	7	146	5	-3
-8	159	6	-3	H,K=	2,	6	-1	57	3	1	-12	50	8	-1	8	17	36	-4*	
-7	208	4	0	-13	16	23	9*	1	125	2	1	-11	35	16	-1*	9	158	8	-1
-6	91	3	3	-12	33	38	5*	3	70	2	-2	-10	27	18	-2*	10	98	3	3
-5	85	2	1	-11	95	2	-0	5	126	3	-4	-9	158	8	2	11	73	3	1
-4	278	7	-1	-10	18	24	-6*	7	33	4	-3	-8	76	5	-9	12	14	20	-3*
-3	253	6	-1	-9	16	23	-15*	9	122	3	1	-7	73	4	5	13	107	2	0
-2	60	6	-4	-8	45	11	-2*	11	45	9	-6*	-6	11	22	-4*	14	61	6	-6
-1	162	4	-2	-7	121	4	0	13	100	3	-0	-5	124	3	0	15	23	9	8*
0	273	5	-4	-6	18	22	1*	15	0	31	-8*	-4	60	2	-3	16	29	14	9*
1	198	7	-1	-5	65	5	3	17	78	3	2	-3	51	2	2	H,K=	3,	4	
2	13	19	9*	-4	66	2	0	H,K=	3,	1	-2	0	20	-6*	-17	48	5	1	
3	176	6	4	-3	131	3	-1	-20	0	28	-13*	-1	93	2	-1	-16	54	3	-3
4	250	14	-1	-2	0	20	-5*	-19	6	21	-5*	0	91	3	-3	-15	29	30	8*
5	169	5	1	-1	88	2	2	-18	9	23	-11*	1	141	4	2	-14	16	20	10*
6	68	9	10	0	62	5	-4	-17	125	3	-2	2	27	6	1*	-13	68	4	-8
7	161	6	1	1	117	2	0	-16	26	7	-4*	3	111	3	6	-12	64	5	-0
8	171	9	-3	2	15	17	12*	-15	25	13	-1*	4	68	3	3	-11	20	11	2*
9	80	7	1	3	98	2	-0	-14	0	30	-18*	5	114	3	-2	-10	19	15	-4*
10	45	8	-5	4	55	6	-8	-13	254	5	1	6	28	8	8*	-9	84	2	-3
11	103	6	-1	5	97	3	3	-12	37	11	-5*	7	12	18	1*	-8	62	6	-11
12	94	8	-1	6	16	23	-2*	-11	15	17	10*	8	50	14	3*	-7	27	28	3*
13	37	5	-2	7	96	3	-1	-10	88	4	-2	9	89	7	-3	-6	40	30	4*
14	44	12	-3*	8	49	7	1	-9	407	10	16	10	16	27	0*	-5	67	8	1
15	66	7	-4	9	53	8	0	-8	48	6	1	11	14	20	-15*	-4	61	5	7
16	43	7	2	10	24	13	2*	-7	118	2	-1	12	43	7	5	-3	34	5	13
H,K=	2,	5	11	73	6	1	-6	93	2	-3	13	83	3	1	-2	13	21	11*	
-16	22	25	4*	12	31	7	6*	-5	564	12	-16	14	23	27	1*	-1	28	26	3*
-15	49	12	4*	H,K=	2,	7	-4	76	2	0	15	29	5	19	0	50	3	4	
-14	36	6	-3	-10	7	30	7*	-3	260	6	-2	16	25	16	5*	1	9	23	4*
-13	34	7	-1*	-9	31	5	18	-2	106	3	-5	17	65	13	4*	2	30	23	14*
-12	31	13	2*	-8	15	17	-2*	-1	481	34	-22	H,K=	3,	3	3	26	37	19*	
-11	50	6	-3	-7	35	7	-1*	0	12	15	9*	-18	30	11	-4*	4	35	37	-9*
-10	40	8	-3*	-6	10	17	2*	1	304	10	-7	-17	74	5	2	5	42	20	-4*
-9	32	7	-5*	-5	20	8	10*	2	108	3	1	-16	55	5	3	6	28	37	-6*
-8	31	4	-5	-4	16	22	4*	3	355	19	-13	-15	15	23	5*	7	3	18	-1*
-7	59	7	1	-3	21	25	-4*	4	63	3	-7	-14	40	6	-9	8	52	4	1
-6	24	30	-14*	-2	14	27	4*	5	320	13	-6	-13	175	6	2	9	39	8	-5*
-5	47	17	-11*	-1	12	22	-3*	6	97	2	-1	-12	91	3	-0	10	16	26	-12*
-4	23	36	-2*	0	7	28	-2*	7	223	6	0	-11	9	34	8*	11	16	20	13*
-3	57	16	0*	1	10	25	-1*	8	0	22	-5*	-10	114	7	-5	12	33	13	-5*
-2	33	38	-2*	2	5	24	-7*	9	242	5	3	-9	248	10	3	13	42	5	-3
-1	75	10	5	3	23	19	-0*	10	52	17	1*	-8	104	5	5	14	23	28	-1*
0	16	31	9*	4	19	23	18*	11	124	4	-3	-7	77	3	-3	H,K=	3,	5	
1	56	20	2*	5	0	25	-3*	12	0	16	-3*	-6	173	5	3	-15	10	24	7*
2	0	37	-25*	6	20	26	10*	13	155	4	-0	-5	350	13	-9	-14	54	6	-1
3	45	12	-13*	7	24	29	-6*	14	29	17	-6*	-4	143	3	-3	-13	58	5	0
4	18	34	-1*	8	6	20	1*	15	33	12	2*	-3	188	5	-2	-12	71	2	-4

STRUCTURE FACTORS CONTINUED FOR
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L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL	
-11	20	9	15*	-2	102	5	-0	9	0	14	-4*	-5	42	14	10*	-9	34	14	1*	
-10	106	4	3	-1	12	21	-6*	10	65	12	-3	-4	59	5	1	-8	32	15	-0*	
-9	88	4	1	0	18	24	-4*	11	4	22	-11*	-3	27	17	7*	-7	43	8	-2	
-8	80	5	1	1	21	25	-0*	12	59	4	6	-2	36	7	4*	-6	23	31	4*	
-7	30	4	3	2	108	3	7	13	0	27	-2*	-1	26	29	-9*	-5	28	33	1*	
-6	155	7	2	3	20	29	8*	14	50	4	-4	0	36	10	20*	-4	23	12	-6*	
-5	111	4	-3	4	27	9	27*	15	12	26	-1*	1	26	32	13*	-3	26	13	-3*	
-4	77	3	0	5	2	19	-20*	16	38	25	-3*	2	31	36	27*	-2	0	19	-15*	
-3	77	5	5	6	87	6	8	H,K= 4,				2	3	44	45	7*	-1	34	7	-2*
-2	179	3	-1	H,K= 4,				0	-18	51	6	-5	4	39	44	-1*	0	20	24	9*
-1	107	3	-1	-18	69	3	-2	-17	9	29	7*	5	4	35	-7*	1	19	23	-1*	
0	50	4	6	-16	91	3	2	-16	66	5	-2	6	21	26	-1*	2	6	25	3*	
1	82	5	-5	-14	154	3	-6	-15	47	10	-8*	7	52	4	-5	3	14	18	-12*	
2	177	5	5	-12	161	3	4	-14	117	3	-2	8	45	12	4*	4	25	26	9*	
3	73	3	1	-10	191	4	5	-13	25	9	8*	9	6	22	-1*	5	17	20	12*	
4	27	18	6*	-8	314	5	3	-12	134	2	-1	10	37	13	4*	6	15	22	5*	
5	98	3	5	-6	306	5	3	-11	84	3	-4	11	41	9	2*	7	34	7	-4*	
6	150	4	1	-4	524	13	6	-10	139	5	-2	12	35	4	-6	8	17	24	2*	
7	40	4	-2	-2	221	4	1	-9	42	13	10*	13	4	30	2*	9	0	25	-4*	
8	17	23	10*	0	477	8	-53	-8	221	4	-1	14	34	6	-1	10	12	18	0*	
9	61	11	-6	2	66	2	-0	-7	129	3	-1	H,K= 4,				4	11	34	12	2*
10	97	3	2	4	464	9	-20	-6	176	5	0	-16	28	10	-2*	H,K= 4,				6
11	19	25	1*	6	47	5	3	-5	21	24	16*-15	61	6	-7	-11	73	4	-0		
12	28	9	9*	8	274	5	-4	-4	360	7	-10	-14	52	3	-1	-10	35	8	17*	
13	45	16	1*	10	34	4	-4	-3	150	3	-4	-13	11	20	1*	-9	15	18	7*	
H,K= 3,				6	12	160	3	0	-2	138	2	1	-12	74	4	2	-8	40	6	4
-13	31	16	5*	14	56	3	3	-1	77	6	-4	-11	116	4	0	-7	98	4	0	
-12	47	9	2*	16	75	5	3	0	340	18	-7	-10	73	4	-8	-6	25	8	9*	
-11	24	24	19*	H,K= 4,				1	1	119	3	1	-9	28	28	17*	-5	25	18	-5*
-10	28	8	17*-19	14	17	3*	2	52	3	4	-8	111	4	-2	-4	47	4	-2		
-9	36	7	9	-18	83	3	-0	3	76	3	5	-7	163	3	1	-3	103	3	-5	
-8	46	8	-3	-17	0	15	-18*	4	341	22	-6	-6	91	2	-1	-2	14	29	6*	
-7	5	23	-9*-16	14	19	8*	5	115	8	-2	-5	30	13	-6*	-1	49	5	-0		
-6	16	27	4*-15	11	18	2*	6	28	37	-1*	-4	194	4	-0	0	61	3	6		
-5	14	18	-1*-14	123	2	-1	7	66	2	-4	-3	198	3	-3	1	101	3	1		
-4	46	6	-2	-13	0	25	-9*	8	218	9	-3	-2	71	8	-0	2	13	24	7*	
-3	24	33	14*-12	43	8	-0	9	46	13	4*	-1	84	8	-1	3	70	3	7		
-2	24	28	20*-11	0	31	-18*	10	27	6	-5*	0	206	5	0	4	45	5	-2		
-1	19	26	7*-10	142	3	1	11	44	7	-4	1	169	5	3	5	75	5	3		
0	56	9	9	-9	17	13	6*	12	124	2	-1	2	0	24	-12*	6	29	34	16*	
1	15	31	9*	-8	63	3	8	13	26	9	-5*	3	107	5	3	7	58	4	0	
2	0	22	-10*	-7	17	10	-3*	14	47	7	1	4	178	7	-1	H,K= 4,				7
3	0	19	-3*	-6	126	2	1	15	31	14	-2*	5	128	5	3	-5	21	25	13*	
4	38	7	3	-5	30	8	16*	H,K= 4,				3	6	40	18	13*	-4	19	16	4*
5	0	18	-4*	-4	83	3	1	-18	55	6	1	7	93	2	4	-3	21	25	4*	
6	26	7	7*	-3	14	25	13*-17	29	10	-6*	8	114	3	-1	-2	0	37	-6*		
7	15	21	11*	-2	11	17	-11*-16	32	13	13*	9	65	4	2	-1	19	23	10*		
8	33	35	1*	-1	0	24	-6*-15	41	13	8*	10	35	6	8	0	23	26	12*		
9	0	25	-8*	0	20	25	10*-14	76	3	-6	11	69	6	7	1	15	30	9*		
10	6	26	-14*	1	28	10	2*-13	36	14	-5*	12	57	4	-4	H,K= 5,				0	
H,K= 3,				7	2	60	4	-2	-12	40	7	11	13	39	5	6	-17	59	2	1
-8	53	6	6	3	9	21	3*-11	42	3	4	H,K= 4,				5	-15	66	5	-2	
-7	35	18	25*	4	75	4	-3	-10	84	4	-5	-14	35	20	4*-13	76	3	-1		
-6	85	2	3	5	0	17	-3*	-9	23	33	-18*-13	28	33	-4*-11	69	3	-3			
-5	32	38	12*	6	39	8	11*	-8	55	9	-4	-12	23	24	2*	-9	94	4	2	
-4	37	6	-4	7	21	36	10*	-7	64	15	-7*-11	36	5	2	-7	73	9	-4		
-3	15	18	-3*	8	71	10	-5	-6	55	10	3*-10	39	6	-1	-5	97	3	5		

STRUCTURE FACTORS CONTINUED FOR
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L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL		
-3	47	3	6	-3	72	14	2*	-6	6	19	-1*	-8	139	3	-1	2	48	7	2		
-1	59	8	3	-2	35	37	7*	-5	42	10	-1*	-6	136	3	0	3	26	7	3*		
1	48	10	4*	-1	64	14	3*	-4	39	6	-1	-4	193	7	2	4	146	4	-1		
3	19	34	11*	0	46	11	7*	-3	18	21	10*	-2	103	3	3	5	55	12	4*		
5	51	10	-4*	1	41	42	-5*	-2	20	24	5*	0	185	3	-3	6	21	25	6*		
7	31	14	7*	2	0	38	-5*	-1	30	7	-2*	2	63	7	-1	7	21	24	-3*		
9	66	5	0	3	5	37	1*	0	29	11	-2*	4	188	5	-4	8	108	2	1		
11	11	18	3*	4	11	22	-7*	1	0	17	-2*	6	24	12	3*	9	38	5	8		
13	64	7	2	5	49	14	2*	2	0	24	-9*	8	129	6	-0	10	18	30	9*		
H,K= 5,				1	6	32	10	5*	3	15	28	7*	10	12	19	5*	H,K= 6,				
-18	3	27	-8*	7	16	21	7*	4	27	28	11*	H,K= 6,				1	-14	50	7	-1	
-17	85	2	3	8	15	17	-8*	5	21	26	4*-16	0	18	-5*-13	26	6	-3*				
-16	16	21	-4*	9	46	6	-4	6	16	24	-11*-15	0	16	-8*-12	24	29	11*				
-15	4	15	-15*	10	22	27	6*	7	8	21	3*-14	83	2	3	-11	23	8	7*			
-14	17	19	2*	11	27	11	17*	8	12	29	-12*-13	23	6	13*-10	45	5	-12				
-13	154	4	0	12	12	18	1*	9	20	10	-3*-12	9	17	1*	-9	30	7	-2*			
-12	25	9	-4*	13	54	3	3	10	9	26	-12*-11	0	22	-6*	-8	16	31	-6*			
-11	12	19	-2*	H,K= 5,				3	H,K= 5,				5	-10	85	4	1	-7	25	29	-4*
-10	34	10	-5*-16	44	6	7	-12	52	3	1	-9	29	8	16*	-6	26	31	-15*			
-9	194	4	-3	-15	0	24	-8*-11	0	19	-5*	-8	23	18	6*	-5	20	9	-11*			
-8	24	28	-3*-14	13	18	-23*-10	58	10	2	-7	24	27	11*	-4	17	21	6*				
-7	57	9	4	-13	104	5	4	-9	58	4	3	-6	78	2	-0	-3	17	26	9*		
-6	51	14	3*-12	56	2	-4	-8	57	9	-4	-5	15	17	-1*	-2	44	8	-4*			
-5	301	5	5	-11	13	26	6*	-7	11	31	-5*	-4	10	21	4*	-1	32	5	-4		
-4	49	5	7	-10	63	6	2	-6	83	2	-2	-3	12	18	10*	0	28	12	23*		
-3	98	4	2	-9	140	5	1	-5	61	9	-3	-2	82	3	1	1	9	17	-3*		
-2	59	3	6	-8	61	3	-2	-4	52	9	-3	-1	17	28	-0*	2	17	27	-3*		
-1	260	6	-8	-7	33	5	-1	-3	27	28	-5*	0	5	28	-5*	3	27	19	5*		
0	32	33	11*	-6	95	4	1	-2	95	6	-5	1	9	33	-3*	4	5	24	-7*		
1	147	7	2	-5	183	4	-1	-1	63	7	-6	2	45	16	-2*	5	19	22	18*		
2	63	14	5*	-4	73	5	-4	0	49	9	2	3	24	25	17*	6	11	27	-7*		
3	244	6	-5	-3	69	4	-2	1	54	5	2	4	23	9	-1*	7	27	8	-2*		
4	10	35	-18*	-2	119	3	-0	2	107	5	3	5	20	8	19*	8	21	22	6*		
5	183	4	-6	-1	185	4	-3	3	49	7	-1	6	28	8	-5*	9	0	22	-1*		
6	45	9	-5*	0	44	12	-1*	4	12	33	-10*	7	16	19	4*	H,K= 6,					
7	144	2	-1	1	96	5	-5	5	52	6	0	8	33	15	5*-12	40	7	5			
8	11	17	9*	2	122	6	-3	6	84	5	-0	9	0	21	-1*-11	68	3	4			
9	127	2	-1	3	153	3	-1	7	33	14	1*	10	24	27	1*-10	57	3	6			
10	31	19	1*	4	35	13	9*	8	23	12	19*	11	0	22	-6*	-9	0	21	-10*		
11	63	7	-7	5	126	2	3	H,K= 5,				6	H,K= 6,				2	-8	68	8	4
12	0	33	-2*	6	98	4	1	-8	32	11	-1*-15	38	7	5*	-7	84	3	-1			
13	92	6	0	7	98	2	2	-7	21	24	15*-14	74	4	0	-6	45	8	-3			
H,K= 5,				2	8	14	18	13*	-6	15	21	13*-13	10	16	-3*	-5	13	25	2*		
-17	53	5	3	9	90	5	-1	-5	30	11	14*-12	67	5	0	-4	82	8	2			
-16	28	33	-6*	10	65	8	3	-4	33	5	3	-11	54	10	6	-3	94	7	3		
-15	47	4	-3	11	41	5	1	-3	34	9	27*-10	93	4	0	-2	34	16	-5*			
-14	9	22	-2*	12	3	22	-4*	-2	0	21	-5*	-9	9	30	6*	-1	22	15	2*		
-13	64	6	-2	H,K= 5,				4	-1	14	18	2*	-8	114	4	3	0	94	3	1	
-12	27	7	1*-15	15	22	-2*	0	23	27	-2*	-7	65	2	1	1	87	3	-1			
-11	64	3	-4	-14	17	26	13*	1	17	21	10*	-6	90	5	-1	2	27	29	12*		
-10	25	14	14*-13	45	6	0	2	0	36	-8*	-5	6	15	0*	3	34	5	-1			
-9	68	4	-1	-12	37	8	-4*	3	16	19	15*	-4	146	3	0	4	74	4	-5		
-8	47	3	-7	-11	26	10	-2*	H,K= 6,				0	-3	72	3	4	5	63	10	1	
-7	59	5	-2	-10	13	22	4*-16	39	18	4*	-2	68	6	-4	6	12	21	9*			
-6	6	45	-5*	-9	47	4	-3	-14	98	4	-1	-1	24	27	8*	7	25	29	-8*		
-5	71	12	-2	-8	52	3	1	-12	81	5	2	0	144	3	-4	H,K= 6,					
-4	45	8	7	-7	11	31	6*-10	115	2	-2	1	65	2	2	-8	30	20	13*			

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L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL	L	FOB	SG	DEL
-7	28	7	7*	-1	28	24	8*								
-6	0	28	-16*	0	11	17	-3*								
-5	22	8	-1*	1	0	17	-14*								
-4	28	13	14*	2	24	13	19*								
-3	23	8	8*	3	13	17	11*								
-2	24	8	10*	4	28	15	19*								
-1	31	7	7*	5	12	27	-9*								
0	13	27	5*	6	27	14	16*								
1	34	11	24*	H,K= 7,			3								
2	15	33	11*-10	20	24		-1*								
3	12	38	-6*	-9	86	5	1								
H,K= 7,			0	-8	52	3	3								
-13	61	5	9	-7	25	10	23*								
-11	32	4	-1	-6	42	7	-1								
-9	61	2	-3	-5	103	2	5								
-7	9	20	-0*	-4	42	10	-3*								
-5	43	11	-3*	-3	21	23	-2*								
-3	6	18	-8*	-2	54	4	4								
-1	23	23	2*	-1	102	2	5								
1	5	18	-12*	0	37	5	-0								
3	0	21	-2*	1	44	22	1*								
5	28	33	1*	2	52	3	-1								
7	19	30	16*	3	70	6	-1								
H,K= 7,			1	4	31	13	13*								
-13	83	4	3	H,K= 7,			4								
-12	9	16	-10*	-6	17	33	15*								
-11	26	6	-1*	-5	25	9	2*								
-10	12	26	1*	-4	19	22	-0*								
-9	125	4	-1	-3	25	9	23*								
-8	32	7	8*	-2	17	26	12*								
-7	9	16	3*	-1	18	38	6*								
-6	28	18	8*	0	22	26	9*								
-5	158	7	1	H,K= 8,			0								
-4	19	29	-4*	-8	60	3	7								
-3	34	20	5*	-6	82	2	5								
-2	20	27	-2*	-4	82	3	2								
-1	141	4	-2	-2	64	3	-1								
0	15	21	-4*	0	100	13	6								
1	59	7	5	H,K= 8,			1								
2	27	7	3*	-7	27	19	22*								
3	111	2	-2	-6	20	34	-10*								
4	0	17	-11*	-5	17	27	13*								
5	56	11	-3*	-4	29	30	16*								
6	26	31	8*	-3	12	20	10*								

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