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Probing the high-pressure densification of amorphous silica nanomaterials using SBA-15:  
An investigation into the paradoxical nature of the first sharp diffraction peak

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1 **Probing the High-Pressure Densification of Amorphous Silica Nanomaterials**  
2 **using SBA-15: an Investigation into the Paradoxical Nature of the First Sharp**  
3 **Diffraction Peak**

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21

22 **Probing the High-Pressure Densification of Amorphous Silica Nanomaterials**  
23 **using SBA-15: an Investigation into the Paradoxical Nature of the First Sharp**  
24 **Diffraction Peak**

25 **Abstract**

26 The densification and X-ray scattering of mesoporous silica (SBA-15) were measured  
27 simultaneously under gigapascal (GPa) pressures. The results are compared to  
28 previous work on amorphous silica ( $a\text{SiO}_2$ ) and demonstrate the feasibility of measuring  
29 the densification of  $a\text{SiO}_2$  nanomaterials with small angle X-ray scattering (SAXS) in-situ  
30 in a diamond anvil cell. Compared to fused silica, the position of the SBA-15 first sharp  
31 diffraction peak (FSDP) is 7 times more sensitive to pressure and has a transition in its  
32 pressure dependence at a lower pressure ( $\sim 2$  GPa vs.  $\sim 13$  GPa). SBA-15 has two  
33 densification regimes, low-density amorphous and high-density amorphous, which have  
34 equations of state comparable to low-density amorphous and high-density amorphous  
35 fused silica. The transition between these two regimes occurs at a lower pressure than  
36 for fused silica ( $\sim 1.5$  GPa vs.  $\sim 13$  GPa). The results suggest that there is no direct  
37 relationship between the FSDP position and the  $a\text{SiO}_2$  density during compression.

38 **Keywords:** Amorphous Silica, Mesoporous Silica, Diamond Anvil Cell, First Sharp  
39 Diffraction Peak, Equation of State, Small Angle X-ray Scattering

40 **Highlights**

- 41 • SBA-15, a type of nanoscale  $a\text{SiO}_2$ , is hydrostatically compressed up to  $\sim 5$  GPa.
- 42 • Equation of state and microstructural changes are probed in-situ using SAXS and  
43 WAXS.
- 44 • SBA-15 transitions from a low-density amorphous to a high-density amorphous  
45 EOS at low pressure and density.
- 46 • SBA-15's First Sharp Diffraction Peak is more pressure sensitive than other  
47 amorphous silica polyamorphs.
- 48 •  $a\text{SiO}_2$  bulk modulus is shown to not be coupled with the FSDP pressure-  
49 sensitivity.

50 **Inspec Classification Codes**

51 A60, A90

52

53 **1.0 Introduction**

54 Amorphous silica ( $a\text{SiO}_2$ ) is the archetypal model material for high pressure glass  
55 studies due to its ubiquity, chemical simplicity, and relevance to both geological and  
56 industrial systems. Current high pressure ( $>1$  GPa) studies on  $a\text{SiO}_2$  focus on melt-  
57 derived polyamorphs, e.g. fused silica, densified fused silica, and vitreous silica.  
58 However,  $a\text{SiO}_2$  consists of a much wider family of polyamorphs. One important subset  
59 is mesoporous silicas, commonly used for catalysis and environmental adsorption due  
60 to their high surface area. This work studies the high-pressure behavior of the periodic  
61 mesoporous silica SBA-15 using a diamond anvil cell (DAC) and in-situ X-ray scattering.

62 The molecular structure of  $a\text{SiO}_2$  is a polymerized three-dimensional (3D) network of  
63  $\text{SiO}_4$  tetrahedra [1]. Short-range order, at length scales below  $\sim 2$  Å, comes from bonding  
64 within these tetrahedra. The tetrahedra interconnect through bridging oxygens, forming  
65 a continuous network characterized by ring structures of various sizes [2]. The rings,  
66 while not regularly shaped, are all of fairly similar structure [3,4]. This regularity gives  
67 rise to structural ordering at intermediate length scales ( $\sim 5 - 50$  Å), referred to as  
68 intermediate range order (IRO) [1]. The microstructures comprising the IRO include  
69 rings, network cages formed by multiple rings, and hypothesized structures such as  
70 pseudo-Bragg planes [5]. The IRO structures are reflected in diffraction features such as  
71 the first sharp diffraction peak (FSDP).

72 The FSDP is a common, but largely qualitative, measure of change in the IRO with  
73 spatial correlations between  $\sim 4 - 10$  Å [5]. Many theories have been proposed  
74 regarding its structural origins, and there is significant controversy over which (if any)  
75 are correct [4–9]. Its position, intensity, and width are all highly sensitive to pressure  
76 [10–12]. The main structural differences between  $a\text{SiO}_2$  polyamorphs lie in the IRO,  
77 making the FSDP a useful marker for comparisons between them [13–15].

78 Amorphous-amorphous microstructural transitions are common during compression of  
79 glasses. These transitions are typically denoted by changes in density, i.e. going from a  
80 low-density amorphous (LDA) regime to a high-density amorphous (HDA) regime. The  
81 LDA and HDA mechanical properties and atomic structure can differ significantly, just as  
82 for crystalline polymorphs. The compressive behavior of both regimes can be quantified  
83 using equations of state (EOS), which describe the relationship between pressure and  
84 volume. Although most amorphous-amorphous transitions involve changing atomic  
85 coordination numbers,  $a\text{SiO}_2$  is a special case that can have a stable HDA state at  
86 pressures below those required to increase the coordination number [16,17].

87 We investigate SBA-15 under hydrostatic compression at room temperature (cold  
88 compression) up to  $\sim 5$  GPa and under uniaxial (non-hydrostatic) compression up to  
89  $\sim 1.2$  GPa using a diamond anvil cell (DAC) and in-situ synchrotron X-ray scattering.

90 SBA-15 is one of the most studied mesoporous silicas and is synthesized by molding a  
91 TEOS-based silicate gel around a surfactant template [18–21]. The gel is then heated to  
92 perform a condensation reaction and to burn out any remaining surfactants. After  
93 heating almost all organic groups are eliminated (except for a large number of hydroxyl  
94 defects) [22]. The resulting material is a glass powder composed of few-micron sized,  
95 elongated particles (aka grains). Each particle is a highly porous form of  $a\text{SiO}_2$ . The  
96 pore structure is dominated by  $\sim 10$  nm diameter mesopores that form a two-dimensional  
97 (2D) hexagonal array ( $P6mm$  mesolattice), with nanoscale  $a\text{SiO}_2$  walls surrounding them  
98 (Fig. 1) [23]. Embedded within the  $a\text{SiO}_2$  walls is a significant volume of both  
99 complementary pores forming “holes” between the primary mesopores and of  
100 micropores surrounding the mesopores in a “corona” [24–27]. It was previously found  
101 that  $\sim 53\%$  of the porosity volume in SBA-15 comes from the primary, ordered  
102 mesopores, and the remaining  $\sim 47\%$  comes from the complementary pores and  
103 micropores [25]. Thus, SBA-15 has a high degree of interconnectivity between the  
104 mesopores via irregular nano-scale channels. Despite micron-scale particle diameters,  
105 SBA-15 is a nanoscale material due to its high surface area to volume ratio and few-  
106 nanometer thin walls.

107 [Insert Figure 1 here]

108 The  $a\text{SiO}_2$  in the walls of SBA-15 shares a similar microstructure with fused silica,  
109 largely because the IRO structure must be similar for glasses of the same chemistry due  
110 to similar intertetrahedral ring sizes/shapes, cation nearest neighbor distances, and  
111 intertetrahedral bond angles. Both SBA-15 and fused silica have a fully polymerized bulk  
112 intertetrahedral network (see SI Section 1.5), identical Si-O bond angles and distances,  
113 and similar O-O and Si-Si nearest neighbor distances [5,15,28]. However, SBA-15 also  
114 has several microstructural differences with fused silica due to its larger skeletal density,  
115 different synthesis route, and nanoscale dimensions. SBA-15 has a higher proportion of  
116 Q2 and Q3 species due to its large surface area (for further details, see SI Section 1.5),  
117 and of small 3- and 4-membered intertetrahedral rings [29]. The SBA-15 FSDP peak  
118 typically has a weaker intensity, a larger full width half maximum (FWHM), and a higher  
119 momentum transfer,  $q$ , position than fused silica [15,22,30,31]. Differences in their IROs  
120 are observed (via the pair distribution function) beyond a correlation length of  $\sim 3.5$  Å  
121 [28].

122 Previous studies of mesoporous silicas using DACs have reported significantly different  
123 bulk moduli (ranging from 5 – 47 GPa), likely attributable to disparities in pressure  
124 conditions (either hydrostatic or quasi-hydrostatic) [32–34]. These previous studies  
125 lacked the densification datapoint density and signal-to-noise ratio to rigorously model a  
126 pressure dependent EOS. In addition to mesoporous silicas, fused silica nanoparticles

127 have also been studied with DACs. Fumed silica is another  $\alpha\text{SiO}_2$  nanomaterial made  
128 from a reactive Si precursor and in many ways is similar to SBA-15: due to its high  
129 surface area fumed silica has a higher proportion of Q2 and Q3 species [35] and more  
130 3- and 4-membered rings [29,36,37] than fused silica. However, fumed silica's density,  
131 ambient pressure FSDP position, and IRO (via the pair distribution function) are all  
132 dissimilar to SBA-15 and more like that of fused silica [13,37]. Notably, the FSDP of  
133 fumed silica [13] exhibits greater sensitivity to pressure than that of fused silica or  
134 almost any other type of  $\alpha\text{SiO}_2$  [16,38].

135

## 136 **2.0 Materials and methods**

### 137 **2.1 Materials and material property measurements**

138 SBA-15 was purchased from ACS Materials (synthesized via the hydrothermal method  
139 with Pluronic 123 as the surfactant template and TEOS as the silicon source, then  
140 calcined in air at 550°C for 6 hours). The material properties at ambient pressure (1  
141 atm) and room temperature were studied using the following techniques:  $^{29}\text{Si}$  MAS NMR  
142 (Bruker 500 MHz AVANCE) was used to measure the Q species and degree of  
143 polymerization. A nitrogen gas adsorption analyzer (Micrometric 3Flex Adsorption  
144 Analyzer) was used to measure the specific surface area, pore volume, and mesopore  
145 diameter. Helium pycnometry (Anton Paar Ultrapyc 5000 Micro) was used to measure  
146 the SBA-15 skeletal density. The tapping method was used to measure bulk powder  
147 density. Further details on material property measurements and a table of results are  
148 given in SI Section 1.

### 149 **2.2 X-ray scattering measurements**

150 Small angle X-ray scattering (SAXS) and wide angle X-ray scattering (WAXS)  
151 measurements were carried out at Argonne National Laboratory's Advanced Photon  
152 Source (APS) at HP-CAT (beamline 16-ID-D) using 20 keV monochromatic X-rays  
153 ( $\lambda=0.6199 \text{ \AA}$ ). Pt and Rh KB mirrors removed higher energy harmonics and focused the  
154 x-ray beam to  $\sim 25 \times 25 \mu\text{m}$  (FWHM) at the sample position and  $\sim 500 \times 500 \mu\text{m}$  (FWHM)  
155 at the SAXS detector position. All WAXS and SAXS data were measured in-situ in the  
156 diamond anvil cell (DAC).

157 The DAC delivered hydrostatic and uniaxial pressures for sample compression [39]. The  
158 hydrostatic measurements used a pressure-transmitting medium (PTM) of 4:1 methanol  
159 ethanol (hydrostatic up to 10 GPa [40]) and the non-hydrostatic (uniaxial) measurements  
160 used ambient air. The DAC was a symmetric design using type II diamonds, 300  $\mu\text{m}$

161 diameter culets, and a stainless-steel gasket. The sample chamber was  $\sim 100 \mu\text{m}$  in  
162 diameter and  $\sim 100 - 250 \mu\text{m}$  thick (at ambient conditions).

163 WAXS data was collected on a Pilatus 100K detector, offset to let the SAXS beam pass,  
164 and located  $\sim 170 \text{ mm}$  from the sample to capture a momentum transfer of  $1.4 < q < 4.0$   
165  $\text{\AA}^{-1}$  with azimuthal coverage of  $\sim 40 - 120^\circ$ . WAXS data was calibrated using a gold  
166 standard and radially integrated to 1D WAXS patterns using DIOPTAS [41]. Reported  
167 WAXS and SAXS intensities are not on an absolute scale but are self-consistent across  
168 our measurements.

169 SAXS data was collected using a MAR345 detector (345 mm diameter active area)  
170 located  $\sim 3050 \text{ mm}$  from the sample. To minimize air scattering, the SAXS beam was  
171 passed through an He-filled container with X-ray transparent windows: a  $50 \mu\text{m}$  thick  
172 mica window upstream and a  $17 \mu\text{m}$  thick Kapton window downstream. A beam stop  
173 immediately upstream of the Kapton window shielded the detector from the direct beam  
174 and intense low- $q$  scattering. Due to limitations in the dynamic range of the MAR345  
175 detector, SAXS data was collected in two measurements with overlapping  $q$  ranges. The  
176 low- $q$  configuration used a 2 mm diameter tungsten rod for the beam stop and  
177 measured data between  $0.0025 < q < 0.05 \text{\AA}^{-1}$ . The high- $q$  configuration used the  
178 tungsten rod and a U.S. dime (17.91 mm diameter 91.7 wt% Cu, 8.3 wt% Ni) for the  
179 beam stop and measured data between  $0.03 < q < 0.5 \text{\AA}^{-1}$ . Artifacts from intense  
180 diamond scattering limited the useful low- $q$  range to  $q > 0.0045 \text{\AA}^{-1}$ . Background  
181 measurements through a fully assembled DAC without a sample or PTM were used to  
182 quantify instrument specific scattering signals. The background limited the useful high- $q$   
183 range to  $q < 0.15 \text{\AA}^{-1}$ . SAXS data was calibrated using diffraction from a silver behenate  
184 standard. 1D SAXS patterns, in arbitrary units of intensity, were calculated by applying a  
185 dark field correction and subtracting the instrument specific scattering from the detector  
186 images, radially integrating the corrected images, and scaling the high- and low- $q$   
187 measurements to each other in the overlap region.

188 For fitting SAXS and WAXS data, the systematic error  $\sigma_I$  in Poisson counting statistics  
189 (intensity  $I$ ) was estimated  $\sigma_I = \sqrt{I} + (0.05 * I)$  and factored into fits as  $weight = 1/\sigma_I^2$ .  
190 All fitting used least squares regression (trust-region method) in MATLAB with intensity  
191 weights factored into the fits. The error in fitted parameters was taken as half of the 95%  
192 confidence interval, equivalent to one standard deviation.

193

### 194 **3.0 Theory and modelling for hydrostatic compression**

### 195 3.1 SAXS modelling

196 Modelling the small angle scattering of SBA-15 is well-established and previous  
197 investigators have used models of varying degrees of complexity [25,42–44]. The  
198 hydrostatic SBA-15 SAXS data was fit using a simple model focused on capturing the  
199 behavior of the ordered peaks. Modelling used four separate contributions: diffraction  
200 peaks from the ordered mesopore lattice (mesolattice), a Guinier-Porod contribution, a  
201 low- $q$  power law, and an instrument background:

$$202 \quad I(q) = I_{ordered}(q) + I_{Guinier-Porod}(q) + I_{PowerLaw}(q) + I_{background} \quad (1)$$

203  $I_{ordered}(q)$  comes from the mesolattice structure of SBA-15, which consists of long,  
204 cylindrical pores arranged in a 2D hexagonal mesolattice [21]. This contribution is  
205 modeled by five pseudo-Voigt peaks (area-normalized so that the intensity equals the  
206 area under the peak) with locations in  $q$  determined by the five lowest order  $hk$   
207 reflections of a 2D hexagonal mesolattice ( $P6mm$ ) [43].  $I_{Guinier-Porod}(q)$  uses  
208 Hammouda's model to represent diffuse scattering from the nanometer-scale pore walls  
209 [45]. We used a cylindrical form factor for the Guinier-Porod contribution and fixed the  
210 Porod exponent at -4. The low- $q$  scattering was modeled using a power law,  
211  $I_{PowerLaw}(q) = C * q^\alpha$ , where  $C$  is a constant and  $\alpha$ , the scattering exponent, is fixed to -4.  
212 The low- $q$  scattering likely arises from the surfaces of the largest scattering structures in  
213 the sample, which in SBA-15 is the micron-sized particles [25,42]. The instrument  
214 background was modeled as constant.

215 SI Section 2.1 shows a representative SBA-15 SAXS fit broken out into its components.

### 216 3.2 WAXS Modelling

217 WAXS fitting used a simple model focused on capturing the behavior of the FSDP and  
218 gold diffraction peak. The model used five separate contributions as shown in Eq. (2): a  
219 power law scattering contribution for the low- $q$  scattering, a flat instrument background,  
220 a Gaussian peak representing the gold diffraction (111) reflection, and two Gaussian  
221 peaks making up the FSDP (representing the high- $q$  and low- $q$  components).

$$222 \quad I(q) = I_{PowerLaw}(q) + I_{Gold}(q) + I_{FSDP,High-q}(q) + I_{FSDP,Low-q}(q) + I_{background} \quad (2)$$

223 The power law low- $q$  scattering behavior is also found in previous WAXS measurements  
224 of mesoporous silica [15]. This contribution likely arises from density fluctuations in the  
225  $aSiO_2$  walls. The diffraction peak is from gold particles added to the SBA-15 powder as  
226 a hydrostatic pressure probe (see next section). The FSDP is modelled using two peaks  
227 based on the primary features of the data. Only the low- $q$  peak (the highest-intensity,



228 principal component) was used to monitor FSDP position, FWHM, and intensity (as is  
229 common to most  $a\text{SiO}_2$  studies).

230 SI Section 2.2 shows a representative SBA-15 WAXS fit broken out into its components.

### 231 **3.3 Hydrostatic Pressure**

232 The hydrostatic pressure exerted on the  $a\text{SiO}_2$  walls of SBA-15 was calculated from the  
233 gold unit cell volume, determined from the (111) diffraction reflection, using a third-order  
234 Birch-Murnaghan EOS [46,47] and the parameters given in Anderson et al [48]. The  
235 systematic error in pressure was estimated at  $\sim 0.1$  GPa, peak fitting errors were  
236 comparatively negligible ( $\sim 2$  orders of magnitude smaller).

237 This calculation assumes that the pressure exerted by the PTM on the  $a\text{SiO}_2$  pore walls  
238 is hydrostatic and equivalent to that on the gold particles. For this to be true, the PTM  
239 must fully penetrate the pores. A previous study, using contrast-matched small angle  
240 neutron scattering (CM-SANS), showed that iso-octane almost entirely penetrates the  
241 pore volume in SBA-15 ( $\sim 10^{-4}$   $\text{cm}^3/\text{g}$  void volume remaining) [25]. Smaller molecules like  
242 n-decane (cross-sectional diameter  $\sim 4.9$  Å [49]) completely fill all pores leaving no  
243 measurable void volume. n-decane is larger than methanol or ethanol (cross sectional  
244 diameters of  $\sim 3.8$  Å and  $\sim 4.4$  Å respectively), indicating our PTM should fully occupy the  
245 pore space in SBA-15.

246 During SBA-15 hydrostatic compression, we assume that a fully pore-penetrating  
247 hydrostatic PTM (1) remains hydrostatic and pressure-equilibrated to the external PTM  
248 when inside nanoscale-sized pores, (2) stabilizes the pores against collapse so that  
249 porosity does not significantly affect SBA-15's compressibility, and (3) does not itself  
250 have a significant effect on SBA-15's compressibility. This implies that the DAC  
251 compresses only the SBA-15 skeletal structure, so the measured compressibility of the  
252 mesolattice reflects that of  $a\text{SiO}_2$  alone without PTM or porosity contributions. See  
253 Appendix A for a detailed defense of these assumptions.

### 254 **3.4 Volumetric Compression and Densification**

255 Volumetric compression of the  $a\text{SiO}_2$  walls is calculated  $V_{norm} = a^3/a_0^3$ , where  
256  $V_{norm} = V/V_0$  is the volume normalized to its ambient pressure value,  $a$  is the  
257 compressed 2D hexagonal mesolattice parameter, and  $a_0$  is the ambient mesolattice  
258 parameter (see SI Section 2.3 for derivation). However, mesolattice diffraction does not  
259 directly measure  $a\text{SiO}_2$  wall width and the 2D mesolattice lacks c-direction data for  
260 volume calculations (Fig. 1b). We estimate  $a\text{SiO}_2$  volumetric compression by assuming:  
261 (1) the contraction, i.e. linear strain, of the  $a\text{SiO}_2$  wall thickness is the same as that of

262 the mesolattice parameter, and (2) linear strain is the same in all crystallographic  
263 directions (including the *c*-direction) at any given hydrostatic pressure.

264 Both assumptions hold if SBA-15 undergoes linear isotropic compression, where a  
265 hydrostatic PTM distributes pressure equally in all directions resulting in uniform strains  
266 in all directions for isotropic materials. Assuming linear isotropic compression is  
267 common for hydrostatic compression of bulk  $a\text{SiO}_2$  [50]. Given that all bulk polyamorphs  
268 of  $a\text{SiO}_2$  are isotropic, it is likely that SBA-15 – which is microstructurally similar to fused  
269 silica – is also isotropic. While isotropic compression is straightforward for the *a*- and *b*-  
270 directions, it is more complex for the *c*-direction due to mesopore vertical alignment (Fig.  
271 1). Nonetheless, we approximate linear isotropic compression for the *c*-direction  
272 because (a) the bulk material's isotropy is more relevant than particle shape anisotropy  
273 during hydrostatic compression, and (b) the hydrostatic environment for SBA-15 should  
274 be uniform due to long equilibration times and complete PTM pore penetration.

### 275 **3.5 EOS modelling**

276 SBA-15 densification during hydrostatic compression was modelled using an EOS  
277 transition between a low- and a high-pressure densification regime. Both regimes are  
278 modeled using third-order Birch-Murnaghan EOSs [46,47,51]. A third-order Birch-  
279 Murnaghan EOS describes the change in  $V_{\text{norm}}$  under compressive pressures using two  
280 parameters  $K_0$  and  $K'_0$ , the bulk modulus at ambient pressure and the first derivative of  
281 the bulk modulus at ambient pressure respectively. At a transition density, defined as the  
282 coordinate where the low- and high-pressure EOSs intersect, the model instantaneously  
283 transitions from following the low-pressure EOS to following the high-pressure EOS.  
284 This model was chosen for its simplicity and does not imply the order of the transition  
285 mechanism.

286 The simple EOS transition model has fitting parameters  $\rho_{0,Low-P}$ ,  $K_{0,Low-P}$  and  $K'_{0,Low-P}$  for  
287 describing the low-pressure regime, and  $\rho_{0,High-P}$ ,  $K_{0,High-P}$  and  $K'_{0,High-P}$  for describing the  
288 high-pressure regime. Errors for fitted parameters were defined the same as for SAXS  
289 and WAXS. Fits were weighted using  $\sigma_{V_{\text{norm}}}$ , propagated from the hexagonal mesolattice  
290 parameter fitting errors.

291 Models with transitions between multiple EOSs are commonly used to describe phase  
292 or microstructural transitions in oxide glasses [16,52]. A detailed description of the  
293 equations and calculations for the simple EOS transition model is given in SI Section  
294 2.4.

295

## 296 **4.0 Results for hydrostatic compression**

## 297 4.1 Small Angle X-ray Scattering

298 [Insert Figure 2 here]

299 Figure 2 shows SAXS data and corresponding fits for the hydrostatic compression of  
300 SBA-15 [53]. At ambient pressure, the ordered SBA-15 mesopores give rise to a series  
301 of diffraction peaks including higher order reflections. This signifies a high degree of  
302 order between the mesopores. The SAXS data at 0 GPa match a  $P6mm$  space group  
303 (2D hexagonal) with mesolattice parameter  $a_0 = 118.9 \text{ \AA}$ , in agreement with previous  
304 literature [21,24,25,42]. Under applied hydrostatic pressure, the peaks shift to higher  $q$ ,  
305 decrease in intensity, and become broader, indicating a shrinking mesolattice and  
306 increasing mesolattice disorder (Fig. 3). The mesolattice peaks match a  $P6mm$  space  
307 group across the full pressure range.

308 Figure 3 displays the integrated peak intensity and FWHM of the low- $q$  peak as a  
309 function of hydrostatic pressure. At  $\sim 3 - 4$  GPa there is an inflection in both the peak  
310 intensity and FWHM. Decreasing peak intensity and increasing FWHM signify more  
311 disorder.

312 The Guinier-Porod scattering contribution could be fit using a range of different inputs  
313 (i.e. no unique solution), thus necessitating simplifying approximations. The form factor  
314 was estimated as cylinders (dimensionality=2) based on goodness of fit and rough  
315 agreement with the shape of the  $a\text{SiO}_2$  skeletal structure. The Porod exponent was  
316 estimated as -4 corresponding to smooth surfaces. This fit  $R_{\text{cylinder}} \approx 9 \text{ \AA}$ , in general  
317 agreement with scattering structure sizes from previous studies [25,42]. Uncertainty in  
318  $R_{\text{cylinder}}$  precluded determination of its pressure sensitivity. Previous studies used  
319 spherical form factors, so a different source of density fluctuations may be dominating  
320 the diffuse scattering in our sample. The fitted scattering structures are too large to arise  
321 from microporosity but similar in scale to the SBA-15  $a\text{SiO}_2$  pore walls, suggesting that  
322 they themselves are the source of the diffuse scattering.

323 The low- $q$  power law region, which corresponds to the micron-sized SBA-15 particles, fit  
324 well across the full range of pressures with the estimated power law exponent  $\alpha = -4$ .  
325 This corresponds to smooth particle surfaces and agrees with previous studies [25,42].

326 [Insert Figure 3 here]

## 327 4.2 Wide Angle X-ray Scattering

328 [Insert Figure 4 here]

329 Figure 4 shows WAXS data and corresponding fits for SBA-15 under hydrostatic  
330 compression [53]. The main WAXS feature for SBA-15 is the FSDP. At ambient  
331 pressure, SBA-15's FSDP is at  $q = 1.69 \pm 0.01 \text{ \AA}^{-1}$ . This is much higher than for fused or  
332 vitreous silica ( $q = 1.52 \text{ \AA}^{-1}$ ) [16,38,54,55], consistent with previous studies showing that  
333 SBA-15's FSDP is higher in  $q$ , significantly broader, and lower-intensity [15,22]. Under  
334 increasing hydrostatic pressure, the FSDP position shifts to higher  $q$  values and  
335 transitions to a less pressure-sensitive regime (Fig. 5). This is consistent with the real-  
336 space structures in the IRO that give rise to the FSDP getting smaller and less  
337 compressible with increasing pressure. The behavior of the minor component of the  
338 FSDP is described in SI Section 6. Throughout the entire compression measurement  
339 there are no signs of any crystalline  $\text{SiO}_2$  contributions or pressure-induced  
340 crystallization, which would have caused diffraction signals in the measured  $q$  range.  
341 The vertical feature near  $q \approx 2.6 \text{ \AA}^{-1}$  is the gold (111) diffraction reflection, used to  
342 measure pressure inside the chamber.

343 The relationship between SBA-15's ambient pressure FSDP position and its skeletal  
344 density ( $\rho = 2.42 \pm 0.02 \text{ g/cm}^3$ ) aligns closely with the trends observed by Tan and Arndt  
345 [56] and Salmon et al [2] for bulk  $\alpha\text{SiO}_2$  polymorphs (see SI Section 4). These previous  
346 studies demonstrate a linear relationship between the ambient FSDP position and  
347 ambient density. Therefore, the high  $q$  FSDP position of SBA-15 at ambient pressure is  
348 likely due to its higher skeletal density (not its ring size distribution, as has been  
349 previously suggested [4,15]). This suggests that the FSDP of SBA-15 shares a common  
350 origin with that of fused silica and that the materials have closely related microstructures.

351 Figure 5 shows the integrated peak intensity and FWHM of the low- $q$  FSDP component  
352 as a function of hydrostatic pressure. The intensity initially increases, and then starts to  
353 decrease after an inflection point at  $\sim 3 \text{ GPa}$ . The brief period ( $< \sim 3 \text{ GPa}$ ) where the  
354 intensity of the low- $q$  component is increasing signals an increase in the number of  
355 FSDP scattering structures, which in turn suggests an increase in the amount of order in  
356 the  $\alpha\text{SiO}_2$  IRO. The inflection point occurs at approximately the same pressure as the  
357 changes in the SAXS peaks shown in Figure 3. The FWHM increases (largely  
358 monotonically) over the measured pressure range, indicating increasing disorder.

359 [Insert Figure 5 here]

360

## 361 **5.0 Discussion**

### 362 **5.1 Evidence for direct, hydrostatic compression of the $\alpha\text{SiO}_2$ skeletal structure**

363 [Insert Figure 6 here]

364 During hydrostatic compression of SBA-15, SAXS measurements of mesolattice  
365 contraction likely reflect the densification of the  $a\text{SiO}_2$  skeletal structure (i.e. walls)  
366 without contributions from porosity or the pressure transmitting medium (PTM). As  
367 evidence, we first compare the hydrostatic compression of SBA-15 against the  
368 hydrostatic compression of fused silica.

369 Figure 6 compares the densification of SBA-15 under hydrostatic compression against  
370 the hydrostatic densification of fused silica and the uniaxial (non-hydrostatic)  
371 densification of SBA-15. Methods for fitting the uniaxial SBA-15 data are detailed in SI  
372 Section 5, along with representative uniaxial WAXS and SAXS fits and a waterfall plot of  
373 the fitted uniaxial SAXS data.

374 Figure 6 shows that the compressibility of hydrostatic SBA-15 closely matches that of  
375 fused silica. A linear fit of the three lowest-pressure points gives an initial bulk modulus  
376 for SBA-15 of  $\sim 35$  GPa, aligning well with that of fused silica ( $\sim 37$  GPa) [50]. Because  
377 nanoscale materials in hydrostatic compression typically exhibit moduli within  $\sim 30\%$  of  
378 their bulk equivalents [57–60], this suggests the DAC directly compresses the  $a\text{SiO}_2$   
379 walls and that alternative densification contributions are not significant.

380 Comparing the hydrostatic versus uniaxial (non-hydrostatic) compression of SBA-15  
381 evidences the stabilization of pores against collapse by a penetrating PTM. The  
382 ambient-pressure mesolattice parameter of the uniaxial measurement (which was  
383 measured in air),  $a_0 = 119.1$  Å, matches that of the hydrostatic case. This suggests there  
384 was no crushing of the SBA-15 pores during the initial DAC setup or mesolattice strain  
385 caused by the pore-penetrating PTM. Figure 6 shows that uniaxially compressed SBA-  
386 15 is more compressible, with an initial pseudo bulk modulus of  $\sim 2.2 \pm 0.2$  GPa. This is  
387 more than an order of magnitude lower than hydrostatic SBA-15 and agrees with the  
388 expected reduced modulus,  $\sim 1$  GPa, from un-stabilized porosity (via the Mackenzie  
389 equation, see SI Section 5.5) [61]. The uniaxial compression experiment illustrates how  
390 our hydrostatic sample compressibility would change if the pores were not stabilized.

391 During uniaxial compression, both the SAXS peaks and the WAXS gold diffraction peak  
392 become asymmetric as soon as significant non-hydrostatic force was applied (SI Figure  
393 12). As the pores collapsed, uniaxial SAXS peaks lost their intensity, widened, and  
394 reduced to only two discernable peaks. During hydrostatic compression these problems  
395 are absent, suggesting hydrostatic conditions were maintained.

## 396 **5.2 First Sharp Diffraction Peak**

397 [Insert Figure 7 here]

398 Figure 7 shows the FSDP position as a function of hydrostatic pressure for SBA-15 and  
399 several other  $a\text{SiO}_2$  polymorphs. The behavior of the fused silica FSDP position with  
400 pressure is used as the main benchmark for our SBA-15 results. At low pressures, the  
401 fused silica FSDP position has a high rate of change with pressure ( $dq_{\text{FSDP}}/dP$ ) and an  
402 approximately linear relationship to pressure. This is followed by a transition at  $\sim 12 - 15$   
403 GPa to a high-pressure regime which is also approximately linear, has a smaller  
404  $dq_{\text{FSDP}}/dP$ , and extends to  $\sim 40$  GPa [10,38]. The low-pressure FSDP regime with large  
405  $dq_{\text{FSDP}}/dP$  coincides with a high rate of rearrangement for the intertetrahedral bonding  
406 (and thus changes to the IRO) and minor changes to Si-O intratetrahedral bonds  
407 [38,62]. The high-pressure FSDP regime with smaller  $dq_{\text{FSDP}}/dP$  coincides with less  
408 rearrangement of the intertetrahedral bonding indicating stiffer IRO structures and major  
409 changes to the intratetrahedral bonds [38] (because  $> \sim 16$  GPa the main compression  
410 mechanism is the Si coordination change [10,38,63]). SBA-15 has an FSDP transition  
411 from high  $dq_{\text{FSDP}}/dP$  to low  $dq_{\text{FSDP}}/dP$  like fused silica (from now on just referred to as an  
412 FSDP transition), but at a much lower pressure of  $\sim 0.5 - 3$  GPa (Fig. 5). Importantly, for  
413 both fused silica and SBA-15 the FSDP transition happens at approximately the same  
414 pressure as the LDA-to-HDA EOS transition (described in the next section), suggesting  
415 a shared mechanism.

416 Other polymorphs of  $a\text{SiO}_2$  in Figure 7, densified fused silica [16] and fused silica with  
417 dissolved helium [54], have only low  $dq_{\text{FSDP}}/dP$  regimes (and no FSDP transitions) likely  
418 due to their significantly reduced interstitial void space, which makes structures within  
419 the IRO less compressible.

420 Another  $a\text{SiO}_2$  polymorph in Figure 7, fumed silica, is notable for having a larger  
421  $dq_{\text{FSDP}}/dP$  than fused silica [13]. This highly pressure-sensitive fumed silica regime  
422 continues until  $\sim 6$  GPa, where it likely starts having an FSDP transition. Similar to the  
423 fused silica low-pressure, large  $dq_{\text{FSDP}}/dP$  regime, this fumed silica regime was shown to  
424 be concurrent with a high rate of decrease in Si-O-Si angles (i.e. rearrangement of IRO  
425 structures) and minimal change to Si-O bond lengths and angles [13].

426 Like for fused silica, SBA-15 has an FSDP transition from a low-pressure regime with  
427 large  $dq_{\text{FSDP}}/dP$  to a high-pressure regime with smaller  $dq_{\text{FSDP}}/dP$  (Fig. 5). However,  
428 Figure 7 shows that SBA-15's  $dq_{\text{FSDP}}/dP$  is exceptionally large compared to that of fused  
429 silica and all other  $a\text{SiO}_2$  polymorphs shown in Fig. 7. At low pressures (i.e., less than  
430  $\sim 0.75$  GPa) SBA-15's  $dq_{\text{FSDP}}/dP$ ,  $\sim 0.24 \text{ \AA}^{-1} \cdot \text{GPa}^{-1}$ , is seven times larger than that of fused  
431 silica's low-pressure regime,  $\sim 0.03 \text{ \AA}^{-1} \cdot \text{GPa}^{-1}$ , and three times that of fumed silica,  $\sim 0.07$   
432  $\text{ \AA}^{-1} \cdot \text{GPa}^{-1}$ . In this highly pressure-dependent FSDP regime, it is likely that the IRO is

433 rapidly rearranging while the short-range order remains largely unchanged, like for fused  
434 silica and fumed silica. After its FSDP transition, SBA-15's  $dq_{\text{FSDP}}/dP$  decreases by  
435 almost an order of magnitude to  $\sim 0.03 \text{ \AA}^{-1} \cdot \text{GPa}^{-1}$  (Fig. 5) which is close to the  $dq_{\text{FSDP}}/dP$   
436 of the fused silica low-pressure regime. This is larger than the  $dq_{\text{FSDP}}/dP$  of either the  
437 fused silica high-pressure regime or densified fused silica (both  $\sim 0.01 \text{ \AA}^{-1} \cdot \text{GPa}^{-1}$ ) and  
438 much larger than the  $dq_{\text{FSDP}}/dP$  of fused silica with dissolved helium ( $\sim 0.004 \text{ \AA}^{-1} \cdot \text{GPa}^{-1}$ ). It  
439 is likely that the IRO is rearranging more slowly in the SBA-15 high-pressure, small  
440  $dq_{\text{FSDP}}/dP$  regime and that the intertetrahedral network has become less compressible,  
441 like for after the FSDP transition in fused silica.

442 While both SBA-15 and fumed silica have FSDP positions that start out with larger  
443  $dq_{\text{FSDP}}/dP$  than fused silica, there are still significant differences in their FSDP behavior.  
444 The ambient pressure FSDP position for SBA-15 is higher than for fumed silica  
445 nanoparticles, so the real-space structures in the IRO which give rise to the FSDP are  
446 smaller in SBA-15 than in fumed silica. The fumed silica FSDP position versus pressure  
447 slope is linear, like fused silica, up to  $\sim 6 \text{ GPa}$ . The SBA-15 FSDP position pressure-  
448 dependence is not linear throughout most of the compression measurement.

### 449 **5.3 Volumetric Compression and Equation of State**

450 [Insert Figure 8 here]

451 The hydrostatic, volumetric compression of SBA-15 is compared to different  $a\text{SiO}_2$   
452 polymorphs in Figure 8. The behavior of fused silica is used to benchmark our SBA-15  
453 results. At moderate pressures up to  $\sim 15 \text{ GPa}$ , where fused silica is entirely tetrahedrally  
454 coordinated [10,17,38,63], the compression of fused silica can be mostly described  
455 using two EOSs: an LDA-type EOS and an HDA-type EOS. The LDA-type EOS  
456 corresponds to fused silica at pressures below  $\sim 7 \text{ GPa}$  [50,64], and the HDA-type EOS  
457 corresponds to densified fused silica [16]. During a continuous compression experiment  
458 (i.e. when the pressure is monotonically increased up to the maximum pressure) up to  
459  $\sim 15 \text{ GPa}$ , fused silica undergoes a transition at  $\sim 11\text{-}15 \text{ GPa}$  from an LDA EOS to an  
460 HDA EOS [16,64].

461 Fused silica exhibits an LDA-type EOS within the compression range shown in Figure 8,  
462 for which the dominant densification mechanism is the rearrangement of the IRO  
463 structures (bending and rotation of the bridging oxygen bonds) resulting in the reduction  
464 of interstitial voids [16,54]. Meanwhile the short range order, i.e. the  $\text{SiO}_4$  tetrahedra, is  
465 minimally affected [10,38]. During compression of fused silica in the HDA regime, the  
466 intertetrahedral bonds are already strained [3] and the interstitial void space greatly  
467 reduced [16], making the IRO structures and intertetrahedral network less compressible.

468 Densified fused silica [16] and fused silica with dissolved helium [54] do not have  
469 strongly pressure-dependent FSDP regimes or LDA-type EOS regimes (Fig. 8). These  
470 materials don't have an LDA-type EOS regime because they already have significantly  
471 reduced interstitial void space and, in the case of densified fused silica, strained  
472 intertetrahedral bonds.

473 Figure 8 shows the fit of the EOS transition model to the densification of SBA-15. The  
474 model accurately replicates the behavior of SBA-15. See Supporting Information for a  
475 detailed description of the fitting process (SI Sections 3.1 and 3.2) and comparisons of  
476 several fitting iterations with fitting errors (SI Section 3.3).

477 To constrain the EOS transition model fit shown in Figure 8,  $K'_0$  was fixed at 4 for both  
478 the low- and high-pressure EOSs and  $\rho_0$  was fixed to the measured value of  $2.42 \text{ g/cm}^3$   
479 for the low-pressure EOS (see SI section 1.3 for pycnometry measurement). Note that  
480 fixing  $K'_0 = 4$  is equivalent to a second-order Birch-Murnaghan EOS. Fitting obtained  
481 bulk moduli values of  $K_0 = 35.1 \pm 0.6 \text{ GPa}$  for the low-pressure EOS, and  $K_0 = 62.5 \pm 2.4$   
482  $\text{GPa}$  and  $\rho_0 = 2.459 \pm 0.004 \text{ g/cm}^3$  for the high-pressure EOS, corresponding to a  
483 transition point at  $P_{\text{Transition}} = 1.5 \pm 0.4 \text{ GPa}$  and  $\rho_{\text{Transition}} = 2.516 \pm 0.021 \text{ g/cm}^3$ . Note that  
484 the density error from model fits reflects the error for percent densification, not for the  
485 actual density values for  $\rho_0$  and  $\rho_{\text{Transition}}$ .

486 Good fits with the EOS transition model could also be attained by fixing the bulk moduli  
487 of the low- and high-pressure EOS regimes to literature values of LDA fused silica [65]  
488 and densified fused silica [16] (SI Section 3.3). In addition, we investigated a modified  
489 EOS transition model where the instantaneous EOS transition is replaced with a  
490 transition zone in which the bulk modulus gradually switches between the two regimes  
491 (see SI Section 2.5 for detailed description). The modified EOS transition model fit the  
492 data with very low error and suggests SBA-15 could have a graded EOS transition  
493 spanning a pressure range of  $\sim 0.4 - 2.6 \text{ GPa}$  (SI Section 3.3). This pressure range  
494 agrees with the error range of the transition pressure from the simple EOS- transition  
495 model.

496 Thus, all the variations of the EOS transition model fit the SBA-15 compression data  
497 with similar physically reasonable values. The EOS transition model fits all indicate that  
498 (1) the SBA-15 compression data is consistent with a transition between two separate  
499 EOSs, (2) the bulk modulus for the low-pressure EOS is close to that of LDA fused  
500 silica, (3) the bulk modulus for the high-pressure EOS is close to that of HDA fused  
501 silica, (4) the transition between the low- and high-pressure EOSs takes place at  $\sim 1 - 2$   
502  $\text{GPa}$ , and (5) the ambient pressure density of the high-pressure EOS is approximately  
503  $2.46 \pm 0.01 \text{ g/cm}^3$ .



504 Several alternative types of EOS models were also tested to fit SBA-15 densification: a  
505 third-order Birch-Murnaghan EOS [46,47], a fourth-order Birch-Murnaghan EOS [46,47],  
506 and a model approximating the elastic anomaly in fused silica (SI Section 2.6). However,  
507 none of the alternative models could fit the SBA-15 densification data when constrained  
508 to physically realistic values, showing that they do not reflect the underlying  
509 compression mechanisms (Appendix B).

510 The SBA-15 low-pressure EOS likely corresponds to an LDA regime and the high-  
511 pressure EOS to an HDA regime, with the transition indicating an amorphous-  
512 amorphous microstructural transition. The bulk moduli for the SBA-15 low- and high-  
513 pressure EOSs are very close to the LDA and HDA bulk moduli for fused silica, a closely  
514 related  $a\text{SiO}_2$  polyamorph. With regards to other possible explanations for a  
515 discontinuous EOS: There are no crystalline diffraction peaks, indicating no pressure-  
516 induced crystallization. There are no indications of pore collapse during hydrostatic  
517 compression (Section 5.1 and Appendix A). The poor fit of the model approximating the  
518 elastic anomaly to the data (Appendix B) and the higher proportion of small rings in  
519 SBA-15 (which reduces the proportion of six-membered rings supposedly responsible  
520 for the elastic anomaly [66]) suggest it is unlikely that the transition stems from a  
521 mechanism similar to the fused silica elastic anomaly. There is no WAXS peak  
522 appearing at  $\sim 3 \text{ \AA}^{-1}$  during compression which would indicate sixfold coordinated Si [10],  
523 nor does the oxygen packing factor get large enough to suggest an increase in Si  
524 coordination number would be favorable [17]. There is no significant adsorption strain  
525 caused by the PTM (Section 5.1). Lastly, there are no compressibility changes caused  
526 by penetration of the PTM into bulk  $a\text{SiO}_2$  interstitial voids. Methanol and ethanol have  
527 been shown to be insoluble into bulk  $a\text{SiO}_2$  up to 10 GPa [54], and even a smaller  
528 molecule like argon cannot penetrate into bulk  $a\text{SiO}_2$  or silica zeolites up to at least 8  
529 GPa [60,67]. Thus, it is assumed for the remainder of the paper that the SBA-15 EOS  
530 transition is an LDA-to-HDA transition.

531 The LDA-to-HDA EOS transition for SBA-15 takes place at much lower pressure than in  
532 fused silica ( $\sim 1.5$  versus  $\sim 13$  GPa). The only similar behavior previously observed was  
533 in fused silica nanoparticles, where the onset of permanent densification takes place at  
534 a much lower pressure than for fused silica [68]. Permanent densification is likely related  
535 to the fused silica LDA-to-HDA transition [16]. The SBA-15 LDA-to-HDA EOS transition  
536 also occurs at a smaller densification ratio than for fused silica ( $\sim 3.5\%$  versus  $\sim 41\%$ )  
537 and at a lower density ( $\sim 2.51$  versus  $\sim 3.12 \text{ g/cm}^3$ ) [16].

538

#### 539 **5.4 Relationship between FSDP and EOS**

540 For both SBA-15 and fused silica, the pressure ranges for the EOS transition and the  
541 FSDP transition coincide. This suggests that the transition mechanisms are linked.  
542 Previous studies on oxide glasses, like  $\text{GeO}_2$  and aluminosilicates, also found FSDP  
543 transitions co-located with EOS transitions and asserted a similar connection [52,69].  
544 Notably, the current study demonstrates that altering the structure of a glass system  
545 (e.g., using a different  $a\text{SiO}_2$  polyamorph) causes the pressure of both the FSDP and  
546 EOS transitions to shift in tandem.

547 Assuming the EOS transition pressures of SBA-15 ( $\sim 1 - 2$  GPa) and fused silica ( $\sim 12 -$   
548  $14$  GPa) indicate their LDA-to-HDA transitions, the transitions occur at similar FSDP  
549 position ranges ( $q \approx 1.90 - 1.98 \text{ \AA}^{-1}$  and  $q \approx 1.92 - 1.98 \text{ \AA}^{-1}$  respectively) [16]. This  
550 suggests that during cold compression the EOS transition may occur at a critical FSDP  
551 position for all  $a\text{SiO}_2$  polyamorphs, possibly because the IRO structures and FSDP are  
552 closely related among all  $a\text{SiO}_2$  polymorphs.

553 The correlation in transition pressures for FSDP and bulk  $a\text{SiO}_2$  compression are  
554 unsurprising. The rearrangement of the intertetrahedral network is the dominant  
555 compression mechanism for LDA fused silica, and a significant mechanism for HDA  
556 fused silica [16]. The rearrangement of the intertetrahedral network is also the primary  
557 driver of change in the IRO. Because change in the FSDP signifies change happening in  
558 the IRO, one would expect that  $a\text{SiO}_2$  compression is closely correlated with the FSDP  
559 behavior.

560 Despite this connection, comparison of Figures 7 and 8 reveals that the rate of change  
561 of the FSDP position with pressure,  $dq_{\text{FSDP}}/dP$ , is not indicative of the  $a\text{SiO}_2$  bulk  
562 modulus. Figure 7 shows that  $dq_{\text{FSDP}}/dP$  is much larger for SBA-15 than for fused silica.  
563 If we assume that the FSDP in both materials manifests from the same real-space  
564 structures in the IRO - as evidenced by both materials following the same ambient  
565 pressure FSDP position versus density trend - then the difference in  $dq_{\text{FSDP}}/dP$  must be  
566 due to the FSDP structures rearranging at a higher rate in SBA-15 than in fused silica.  
567 Figure 8 shows that SBA-15 and fused silica have approximately the same bulk  
568 modulus, especially for the LDA EOS. Thus, the FSDP structures rearrange at a higher  
569 rate in SBA-15 than in fused silica, but both materials densify at the same rate. This  
570 suggests that, during cold compression, the rearrangement of the FSDP structures does  
571 not significantly affect the density of  $a\text{SiO}_2$  and thus there is no direct correlation  
572 between the FSDP position and the bulk modulus in  $a\text{SiO}_2$ . This finding is consistent  
573 with recent research indicating that the collapse of intertetrahedral rings significantly  
574 contributes to  $a\text{SiO}_2$  densification, and the FSDP is uncorrelated to the size or collapse  
575 of these rings [2].

576 This finding has two important implications. First, if intertetrahedral ring collapse is  
577 indeed a major contributor to densification, then the discrepancy between the pressure  
578 dependence of the FSDP position and the bulk modulus is further evidence that the  
579 FSDP does not originate from these rings. This inference challenges ring size-based  
580 models for the origin of the FSDP [4,7] and supports alternative models based on IRO  
581 structures with minimal densification impact. Second, the densification of  $a\text{SiO}_2$  cannot  
582 be monitored using the FSDP position. Although  $d_{\text{FSDP}}$  (FSDP correlation length  
583  $d = 2\pi/q_{\text{FSDP}}$ ) decreases much faster than bulk  $a\text{SiO}_2$  densifies which indicates the  
584 FSDP position cannot directly measure densification [56], it has remained a common  
585 assumption that  $dq_{\text{FSDP}}/dP$  qualitatively reflects the glass densification rate. This is  
586 because both FSDP positional changes and densification of LDA  $a\text{SiO}_2$  are strongly  
587 correlated with the rearrangement of the IRO. This assumption is inconsistent with the  
588 current results.

589 The inflection region for the intensity and FWHM of the SBA-15 SAXS peaks and FSDP  
590 ( $\sim 3 - 4$  GPa, Fig. 3 and 5) may signify a change in the compression mechanism.  
591 Because the inflections occur at higher pressures than the FSDP or EOS transitions, the  
592 change in compression mechanism would be unrelated to those transitions. Regardless,  
593 inflection regions occurring at the same pressure for both SAXS and WAXS peaks is  
594 further evidence of a correlation between the FSDP and bulk material compression.

## 595 **5.5 Comparing the Equation of State and Density of SBA-15 with Fused Silica**

596 Previous literature has found that the ambient compressibility of  $a\text{SiO}_2$  is closely tied to  
597 its ambient density [70], so that fused silica and its partially densified counterparts all  
598 follow the same density versus bulk modulus trend. In the current work, SBA-15 is  
599 shown to significantly deviate from this trend. The SBA-15 LDA regime has an ambient  
600 density of  $2.42 \text{ g/cm}^3$ , which would correspond to a bulk modulus of  $K_0 \approx 42.5$  GPa  
601 according to previous literature [70]. However, this modulus is inconsistent with our SBA-  
602 15 LDA compression data, which has approximately the same bulk modulus as LDA  
603 fused silica ( $2.20 \text{ g/cm}^3$ ). Similarly, the SBA-15 HDA EOS has an effective ambient  
604 density of  $\sim 2.46 \text{ g/cm}^3$  and a bulk modulus close to a highly densified fused silica ( $2.67$   
605  $\text{g/cm}^3$ ) [16], which is inconsistent with the expected bulk modulus of  $K \approx 46.4$  GPa  
606 according to the previous literature [70]. Thus, it is likely that the compressibilities of  
607 different types of  $a\text{SiO}_2$  materials have different correlations with their ambient densities.

608 This is a somewhat surprising result in that SBA-15 and fused silica follow the same  
609 ambient-pressure FSDP vs density trend (SI Section 4) and have closely related  
610 microstructures. While it is possible that the differences in compressibility vs. density  
611 between SBA-15 and fused silica arise from minor changes in the ring size distribution

612 or other IRO features, the difference is most likely due to the nanoscale nature of SBA-  
613 15. Previously, it was found from FTIR that the Si-O-Si bonds in nanoscale fumed silica  
614 are more flexible than compared to fused silica, have a slightly shifted stretching band,  
615 and their bond angles change more under applied pressure [37,71]. This suggests that,  
616 in general, nanoscale  $a\text{SiO}_2$  particles may have a more flexible intertetrahedral network  
617 with different Si-O-Si bond responses to pressure and density.

## 618 **5.6 First Sharp Diffraction Peak pressure sensitivity and LDA-to-HDA transition at** 619 **low pressure**

620 It is challenging to determine the underlying cause of the extreme FSDP pressure-  
621 sensitivity (i.e. very high  $dq_{\text{FSDP}}/dP$ ) and the shift of the LDA-to-HDA EOS transition to  
622 lower pressures for SBA-15 compared to fused silica. Uchino et al attributed the lower  
623 LDA-to-HDA transition pressure of fumed silica to a smaller bulk modulus by using  
624  $dq_{\text{FSDP}}/dP$  as a proxy for the bulk modulus [13]. However, we showed that  $dq_{\text{FSDP}}/dP$  is  
625 not indicative of the bulk modulus, and that nanoscale LDA  $a\text{SiO}_2$  has a similar bulk  
626 modulus to fused silica. The FSDP pressure-sensitivity and EOS transition shift are also  
627 not likely due to differences in chemistry or the IRO between SBA-15 and fused silica.  
628 Uchino et al found that high-temperature calcined fumed silica nanoparticles - which has  
629 an IRO similar to fused silica and should have much fewer hydroxyl impurities [37] - also  
630 had higher FSDP pressure-sensitivity than fused silica [13]. In addition, the levels of  
631 hydroxyl impurities in SBA-15 are relatively small and almost totally segregated to the  
632 external and pore surfaces (see SI Section 1.5).

633 The FSDP pressure-sensitivity is most likely due to the few-nanometer thin walls of  
634 SBA-15. As discussed in the previous section, the flexibility of Si-O-Si bonds in  $a\text{SiO}_2$  is  
635 likely enhanced in nanoscale particles. The increased flexibility of these bonds could  
636 allow the intertetrahedral network to rearrange more under the same amount of  
637 pressure, which would also make the FSDP more sensitive to pressure. This hypothesis  
638 is evidenced by comparing the compressibility of bulk  $a\text{SiO}_2$  against the pseudo-  
639 compressibility of the FSDP for different  $a\text{SiO}_2$  polyamorphs (Appendix C). Polyamorphs  
640 which likely have stiffer intertetrahedral networks have smaller compressibility  
641 differences between the bulk and the FSDP.

642 The lower-pressure EOS transition is also most likely due to the nanoscale nature of  
643 SBA-15. Studies on crystalline nanoparticles commonly find that nanoparticle size  
644 changes the pressure at which a phase transition occurs [59,72–74]. The lower EOS  
645 transition pressure may be explained by the interfacial free energy penalty between an  
646 HDA nucleus and the LDA volumetric phase (analogous to crystalline nanoparticles  
647 [72]). The magnitude of this energy penalty is proportional to the interfacial area

648 between the original phase and the nucleated phase. In bulk materials the interfacial  
649 area is assumed to be the entire surface area of the spherical nucleus. However, in  
650 SBA-15 the thin walls (~2 – 3 nm) result in part of the nucleus bordering the pore  
651 surface and the reduced interfacial area between HDA and LDA phases decreases the  
652 free energy penalty. Additionally, enhanced Si-O-Si bond flexibility could reduce the  
653 misfit strain energy and the interfacial energy per unit area between the HDA and LDA  
654 phases [72]. Overall, the decreased interfacial energy lowers the nucleation energy  
655 barrier and facilitates a microstructural transition at lower pressure. The HDA  
656 microstructural transition would lead to a stiffer network and thus decrease the pressure  
657 sensitivity of the FSDP.

658 Further research on nanoscale  $a\text{SiO}_2$  polyamorphs is necessary to test these  
659 hypotheses for the increased FSDP pressure-sensitivity and the lower LDA-to-HDA  
660 transition pressure in SBA-15 and fumed silica.

661

## 662 **6.0 Conclusion**

663 The densification and FSDP of SBA-15 under GPa pressures was measured by SAXS  
664 and WAXS in-situ in a diamond anvil cell. The EOS of SBA-15 has an LDA-to-HDA  
665 transition like fused silica, but at much lower pressures. The pressure dependence of  
666 the FSDP position for SBA-15 was higher than for fused silica and similar to fumed silica  
667 nanoparticles.

668 This study indicates that (1) the FSDP transition in  $a\text{SiO}_2$  materials signals the onset of  
669 the LDA-to-HDA EOS transition, (2) there is no direct relationship between the rate of  
670 change of the FSDP position with pressure and the  $a\text{SiO}_2$  bulk modulus, (3) the  
671 compressibility of  $a\text{SiO}_2$  materials is not necessarily a function of their ambient density,  
672 and (4) at ambient pressure, the skeletal density and FSDP position of SBA-15 map  
673 onto the same linear relationship observed for other  $a\text{SiO}_2$  polyamorphs. Additionally, we  
674 hypothesize a critical range for  $d_{\text{FSDP}}$  common to all  $a\text{SiO}_2$  polyamorphs at which the  
675 EOS LDA-to-HDA transition occurs.

676

## 677 **Glossary**

678  $a\text{SiO}_2$ : amorphous silica dioxide.

679 SBA-15: a periodic mesoporous material where the bulk/wall material is  $a\text{SiO}_2$ .

680 TEOS: tetraethyl orthosilicate, an organic silicate that is used as a precursor for silicon  
681 dioxide.

682 IRO: Intermediate Range Order, encompassing the ordering arising from intertetrahedral  
683 bonding between the  $\text{SiO}_4$  units on length scales between  $\sim 5 - 50 \text{ \AA}$ .

684 FSDP: First Sharp Diffraction Peak, a common and important feature in the WAXS/XRD  
685 spectrum of oxide glasses (as well as other amorphous materials) which arises due to  
686 intermediate range ordering.

687 SAXS: Small Angle X-ray Scattering, a scattering technique used for detecting features  
688 in the size range of nanometers to tens of nanometers, typically covering a  $q$  range  
689 between  $\sim 0.01 - 0.5 \text{ \AA}^{-1}$ .

690 WAXS: Wide-Angle X-ray Scattering (WAXS), a scattering technique used to probe  
691 ordering on the atomic length scale. Very similar to X-ray Diffraction

692 EOS: Equation of State, describes the relationship between pressure and volume.

693 LDA/HDA: Low Density Amorphous and High Density Amorphous, commonly used to  
694 denote a microstructural change in an amorphous material.

695 DAC: Diamond Anvil Cell, a scientific apparatus used to create extreme hydrostatic  
696 pressures  $>1 \text{ GPa}$ .

697 PTM: Pressure Transmitting Medium, the fluid that surrounds the SBA-15 sample and  
698 fills the DAC sample chamber, and which can transmit the pressure from the DAC to the  
699 sample hydrostatically.

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#### 714 **Declaration of Interests**

715 The authors report there are no competing interests to declare.

#### 716 **Authorship Contribution Statement – Credit**

717 Michael R. Bull: Conceptualization, Formal Analysis, Investigation, Visualization, Writing  
718 – original draft, review and editing. Rachel C. Huber: Investigation. Ping Yu:  
719 Investigation. Tanner J Finney: Investigation, Writing – review and editing. Noah Felvey:  
720 Investigation. Paul Chow: Investigation. Yuming Xiao: Investigation. Tonya L. Kuhl:  
721 Writing – original draft, review and editing. Erik B. Watkins: Conceptualization, Formal  
722 Analysis, Investigation, Visualization, Writing – original draft, review and editing.

#### 723 **Data Availability Statement**

724 The data that support the findings of this study (“In-situ SAXS and XRD of SBA-15 in a  
725 Diamond Anvil Cell during high-pressure densification”) are openly available in  
726 Mendeley Data at <http://doi.org/10.17632/4sncvxbn6x.1>, reference number [53].

#### 727 **Declaration of generative AI and AI-assisted technologies in the writing process**

728 During the preparation of this work the authors used ChatGPT in order to improve the  
729 manuscript’s readability and conciseness. After using this tool/service, the authors  
730 reviewed and edited the content as needed and take full responsibility for the content of  
731 the published article.

#### 732 **Appendix A: Discussion of the Hydrostatic Pressure and Stabilizing Effects inside** 733 **Mesopores Filled by a Pore-Penetrating PTM**

734 During hydrostatic compression of SBA-15, we assume that the PTM (1) remains  
735 hydrostatic and pressure-equilibrated to the external PTM when inside nanoscale-sized  
736 pores, (2) stabilizes the pores against collapse, and (3) does not itself have any  
737 significant effect on the particles’ compressibility.

738 Regarding assumption (1), problems that could prevent this include pore blockages or  
739 nanoscale confinement effects that would cause major deviations from bulk liquid  
740 behavior. First, pore blockages could trap the PTM in pockets or prevent the PTM from  
741 flowing freely into, out of, and through the pores and thus equilibrating with the  
742 surrounding environment. However, the SBA-15 porosity is highly interconnected, the  
743 mesopores are relatively large, and the PTM likely fully permeates all available pore  
744 space. This suggests any pore blockages or constrictions in SBA-15 are likely negligible.

745 Second, interactions between the PTM molecules and the pore walls can, especially for  
746 nanoscale pores, cause a difference of pressure inside vs outside of the pores  
747 (“capillary pressure”). Prior studies on small-molecule hydrocarbons in nanoscale pores  
748 show capillary pressures of ~0.1 MPa for molecules similar to our PTM [75]. This is  
749 several orders of magnitude below our systematic error for pressure. Lastly, deviations  
750 from hydrostatic behavior may arise if the pore size alters the PTM liquid “structure”. But  
751 with ~95 Å mesopores and ~4 Å PTM molecules, adsorption layers should be minimal  
752 relative to pore volume [76]. Thus, the liquid “structure” inside the pores is likely almost  
753 the same as externally, especially considering the nearly ideal mixing behavior of  
754 methanol and ethanol.

755 Regarding assumption (2), if the porosity within the SBA-15 particles collapses then the  
756 compressibility of the mesolattice will greatly decrease [61]. However, if the PTM has  
757 fully penetrated the pores and is applying pressure hydrostatically, then the pores will  
758 not collapse and instead shrink at a rate proportional to the  $\alpha\text{SiO}_2$  walls (i.e. linear  
759 isotropic compression). Numerous high-pressure compression studies have confirmed  
760 this stabilization effect. For example, research on pressured-induced amorphization  
761 (PIA, a type of pore collapse occurring in nanoporous crystalline materials [77]) found  
762 for zeolites and MOFs that use of a pore-penetrating PTM eliminated (or greatly  
763 delayed) signs of PIA and pore collapse [60,78].

764 Regarding assumption (3), the only effect of the PTM on the compressibility of the SBA-  
765 15 mesolattice should be pore stabilization. The compressibility of the PTM itself should  
766 not affect our measurements. First, while trapped pockets of PTM could affect the  
767 mesolattice compressibility, as discussed above the PTM is unlikely to be trapped by  
768 pore blockages and can flow freely in and out of the SBA-15 structure. Second,  
769 pressure-induced pore emptying (squeeze-out) is ruled out because it causes a  
770 reduction in compressibility with pressure, opposite to our observations [79]. Third,  
771 external pressures can sometimes force significantly more liquid molecules into a pore  
772 space than at ambient pressure (“hyperfilling”), changing the porous material’s  
773 compressibility [80]. However, this requires dominant pore/constriction dimensions  
774 similar in size to the PTM molecules and is typically accompanied by increases in the  
775 mesolattice size. Almost the entirety of SBA-15 porosity is at least several nanometers  
776 in diameter - the large majority more than 8 nanometers in diameter [25] - and the SBA-  
777 15 mesolattice does not expand upon uptake of or compression in the PTM.

778 Previous experiments have directly shown that pore-penetrating PTMs have no effect on  
779 the compressibility of nanoporous solids (other than stabilizing pores against collapse).  
780 The hydrostatic compressibility of brewsterite - a zeolite highly resistant to pore collapse  
781 and PIA – was shown to be the same when compressed in either a non-penetrating



782 PTM or a pore-penetrating PTM [81]. Its compression was completely unaffected by the  
783 PTM inside its nanoscale pores. Similarly, previous work has shown that compressing  
784 the same zeolites in different pore-penetrating PTMs results in no compressibility  
785 differences [60]. The PTMs had significantly different sizes and intermolecular  
786 interactions, such that one would expect a difference between the two if nanoscale  
787 confinement effects were affecting the compression experiments.

## 788 **Appendix B: Fitting Alternative EOS Models to SBA-15 Densification**

789 Three alternative EOS models were tested: a third-order Birch-Murnaghan EOS, a  
790 fourth-order Birch-Murnaghan EOS, and a model approximating the elastic anomaly in  
791 fused silica. The authors note that models involving more than one EOS transition were  
792 ruled out due to their unnecessary complexity. Also, trying other generalized EOSs than  
793 Birch-Murnaghan would not significantly change the fits because under 5 GPa all the  
794 generalized EOS formalisms are very similar [51].

### 795 Third-order Birch-Murnaghan EOS:

796 Initially, the SBA-15 compression data was fit using a single third-order Birch-  
797 Murnaghan EOS [46,47] with  $K_0 = 28.9 \pm 1.3$  GPa and  $K'_0 = 19.8 \pm 2.3$ . However, such a  
798 large  $K'_0$  is unphysical. A survey of previous literature studying single-phase EOSs for a  
799 range of materials like SBA-15 including crystalline oxides, metal and oxide glasses,  
800 nanoparticles, and mesostructured materials, showed that  $K'_0$  is typically close to 4 and  
801 always less than 10 (SI Section 3.1). We found that the SBA-15 data simply cannot be fit  
802 with  $K'_0 \leq 10$  GPa. The unusually large  $K'_0$  in this fit is most likely due to a material  
803 transition happening during compression. For example, gold and PbS nanoparticles that  
804 fit to a similar  $K'_0$  were shown to be undergoing a phase transition, meaning the large  $K'_0$   
805 was compensating for an improper single-phase EOS model fit to multi-phase data  
806 [82,83].

### 807 Fourth-Order Birch-Murnaghan EOS:

808 The fourth-order Birch-Murnaghan EOS [46,47] adds the second derivative of  $K$  with  
809 respect to pressure at 0 GPa ( $K''_0$ ) as another fitting parameter. This gives it more  
810 freedom to fit unusual data. However, this model also cannot reproduce the SBA-15 data  
811 when  $K'_0$  and  $K''_0$  are constrained to physically reasonable values. A survey of previous  
812 literature found that  $K''_0$  is typically less than  $1 \text{ GPa}^{-1}$  and always less than  $\sim 3 \text{ GPa}^{-1}$  (SI  
813 Section 3.1). In the fourth-order Birch-Murnaghan fits that properly fit the SBA-15 data, if  
814  $K'_0$  was limited to physically reasonable values then  $K''_0$  fit to  $>10 \text{ GPa}^{-1}$ . Alternatively, if  
815  $K''_0$  was limited to physically reasonable values then  $K'_0$  fit to  $>10 \text{ GPa}^{-1}$ .

## 816 EOS Model Approximating the Fused Silica Elastic Anomaly:

817 Attempts to fit the model approximating the elastic anomaly in fused silica (SI Section  
818 2.6) tested whether a similar phenomenon was taking place in SBA-15. First, we  
819 attempted to replicate the SBA-15 data using this model with similar bulk modulus  
820 behavior as fused silica ( $K_0 = 37$  GPa,  $K'_{\text{Low-P}} = -5$ ,  $K'_{\text{High-P}} = 3.5$  [50,65]) but with the  
821 elastic anomaly transition  $P_{\text{Transition}}$  moved to lower or higher pressures. This method  
822 cannot replicate the SBA-15 behavior. Similarly, when all the fitting parameters for this  
823 model are allowed to vary it is unable to fit the SBA-15 compression data while  $K'_{\text{Low-P}}$   
824 and  $K'_{\text{High-P}}$  are constrained to physically realistic values. Furthermore, the behavior of  
825 the bulk modulus  $K(P)$  tries to converge with that from the unphysical third-order Birch-  
826 Murnaghan fit. This shows that a sudden change in  $K'$  is an especially bad explanation  
827 for the SBA-15 EOS data. Thus, the SBA-15 EOS transition is likely mechanistically  
828 dissimilar to the elastic anomaly in fused silica. This is further supported by the fact that  
829 the FSDP transition is correlated to the EOS transition, which is not seen for the elastic  
830 anomaly but commonly observed for LDA-to-HDA transitions.

## 831 **Appendix C**

832 The position of the FSDP can be converted to a length scale  $d$  using  $d = (2\pi)/q_{\text{FSDP}}$ ,  
833 and if we assume that this length scale corresponds to a spherical scattering structure  
834 then we can calculate an “FSDP cell” volume using  $V_{\text{FSDP}} \propto d^3$  and  
835  $V_{\text{FSDP}, \text{normalized}} = d^3/d_0^3$  where  $d_0$  is the FSDP length scale at ambient pressure [56]. The  
836 normalized FSDP cell volume can be compared against the normalized bulk  $a\text{SiO}_2$   
837 volume to compare the “densification” of the FSDP cell with the densification of the bulk.

838 Figure C.1 compares the volumetric compression of the bulk  $a\text{SiO}_2$  against the  
839 volumetric compression of the FSDP cell for several  $a\text{SiO}_2$  polyamorphs. The figure  
840 shows that polyamorphs with stiffer intertetrahedral networks have more similar bulk and  
841 FSDP cell compressibilities. Fused silica with dissolved helium [54], which likely has the  
842 stiffest intertetrahedral network due to the “pinning” effect of interstitial helium, has  
843 almost no compressibility difference between the bulk and the FSDP cell. Densified  
844 fused silica [16], which has a stiffened intertetrahedral network due to reduced interstitial  
845 void space, has a small compressibility difference between the bulk and the FSDP cell.  
846 Fused silica, which does not have any mechanism to stiffen its intertetrahedral network,  
847 has a large compressibility difference between the bulk and the FSDP cell. SBA-15,  
848 which likely has increased Si-O-Si bond flexibility due to its nanoscale walls (as  
849 discussed in Section 5.5), has the largest compressibility difference between the bulk  
850 and the FSDP cell.

851 [Insert Figure C.1 near here]

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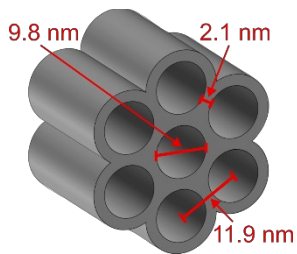
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1157 **Figures**

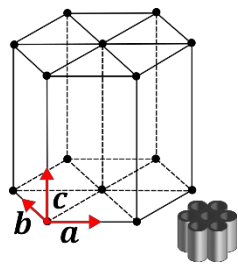
1158 Figure 1a



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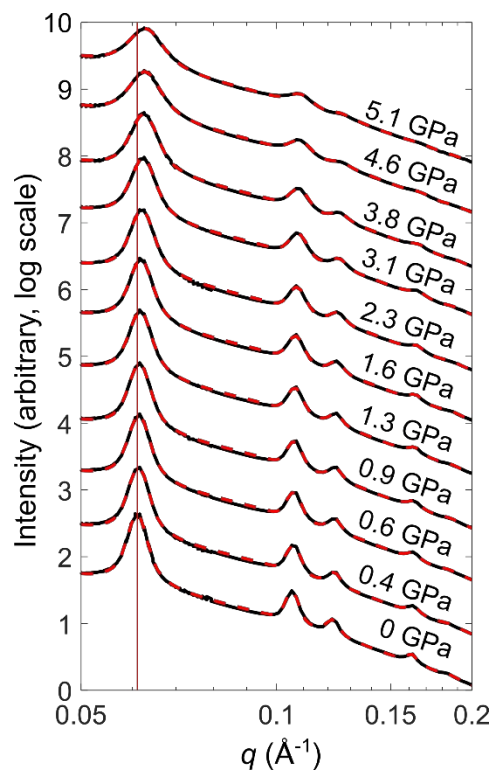
1161 Figure 1b



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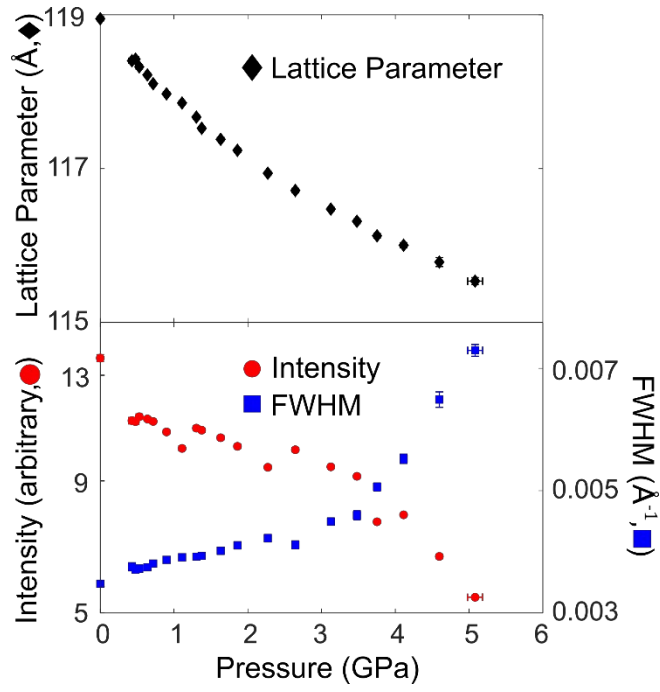
1164 Figure 2



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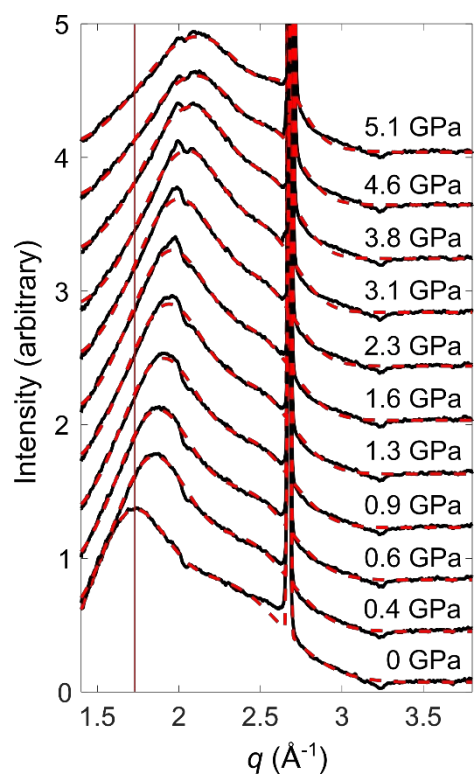
1167 Figure 3



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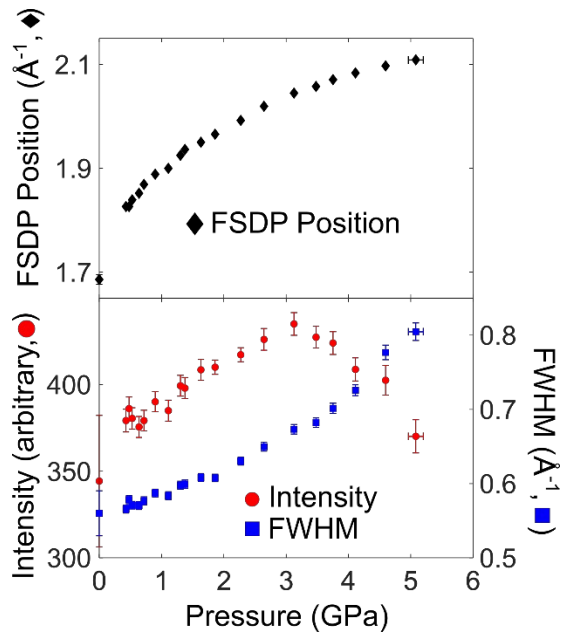
1170 Figure 4



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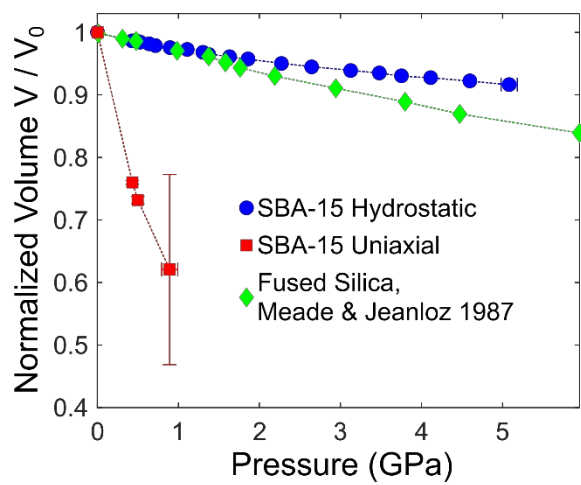
1173 Figure 5



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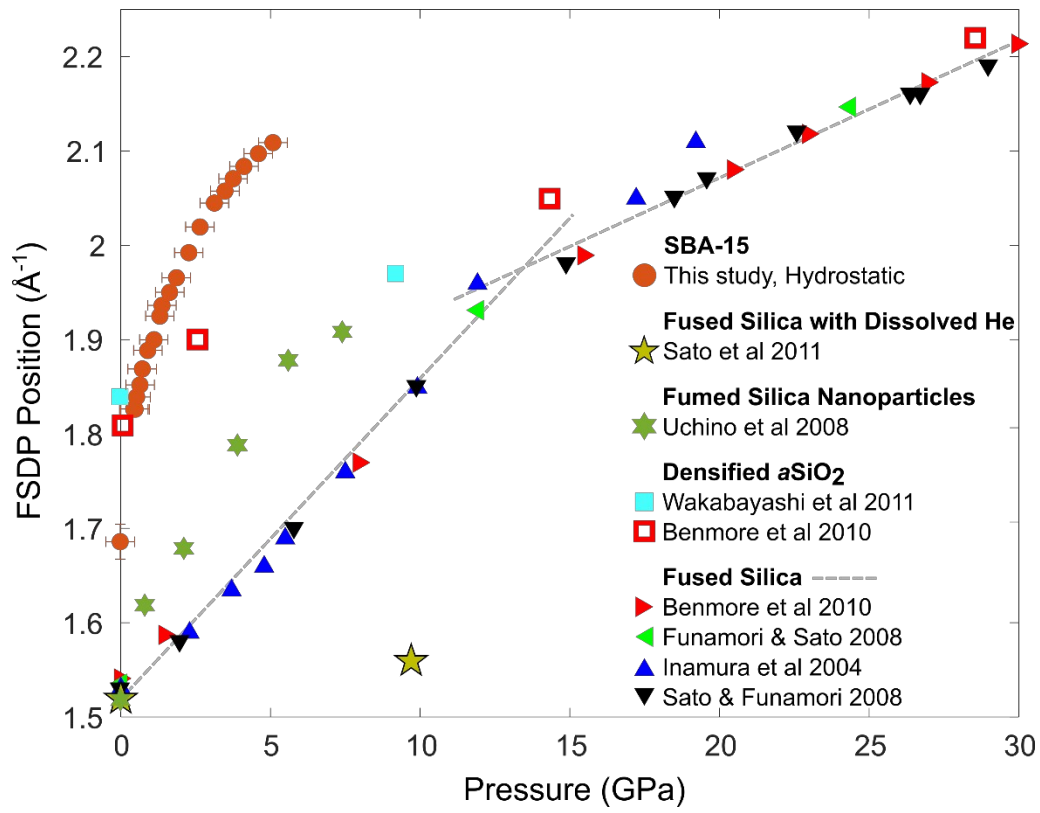
1176 Figure 6



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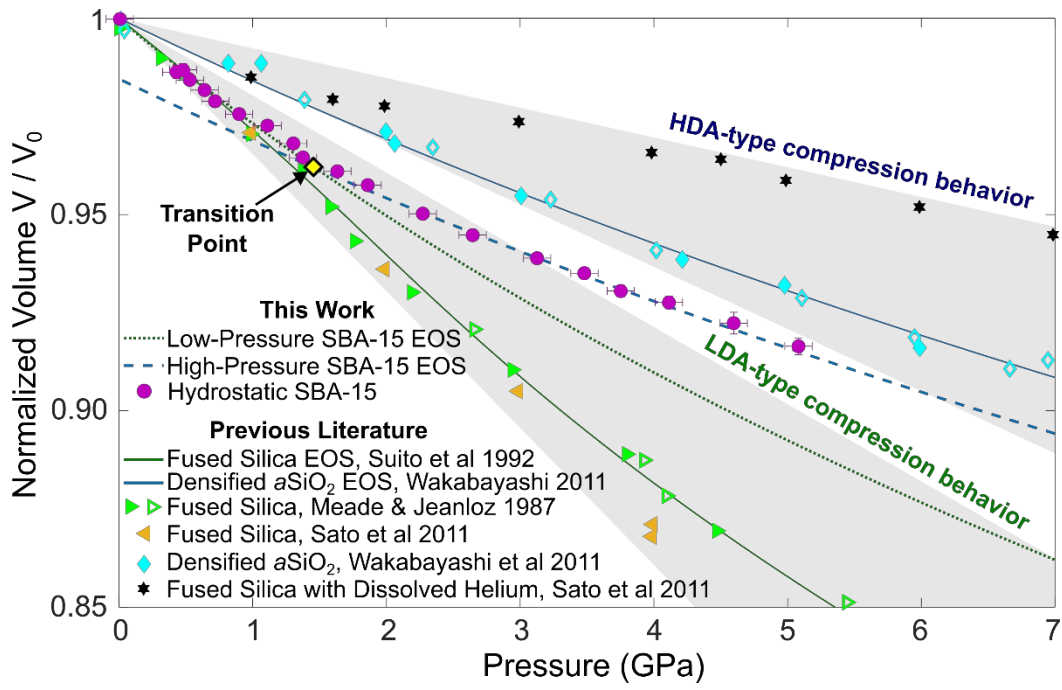
1179 Figure 7



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1182 Figure 8

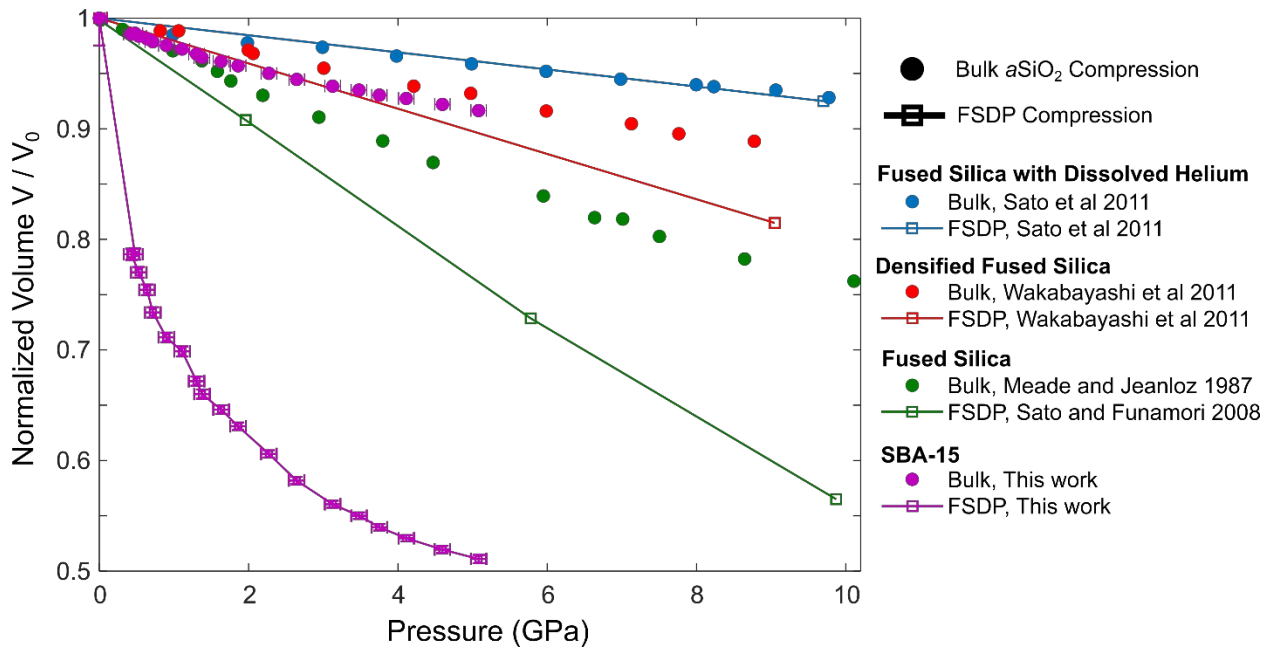


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1185 Figure C.1



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## 1188 Figure Captions

1189 Figure 1: (a) Schematic of SBA-15 honeycomb structure. Cylindrical mesopores are  
1190 arranged within an  $a\text{SiO}_2$  matrix which forms thin walls between the them. Although  
1191 schematically shown as smooth and solid, the  $a\text{SiO}_2$  walls are rough and have a high  
1192 intrawall void fraction [25]. The primary mesopores have diameters of 9.8 nm and the  
1193 minimum wall thickness is  $\sim 2.1$  nm. (b) The hexagonal  $P6mm$  mesolattice in SBA-15.  
1194 Each vertical line represents the center of a mesopore. Crystallographic directions are  
1195 shown as red vectors. Because the lattice is 2D, the lattice parameter in the  $c$ -direction  
1196 is essentially infinite. For a  $P6mm$  lattice, the parameters in the  $a$ - and  $b$ -crystallographic  
1197 directions are equivalent (11.9 nm).

1198 Figure 2: Hydrostatic compression of SBA-15 measured using SAXS. Black lines are  
1199 SAXS data, red dashed lines are model fits to the data. Data is offset for clarity. The  
1200 vertical light red line illustrates the shift in the low- $q$  peak with pressure.

1201 Figure 3: SBA-15 mesopore lattice parameter  $\alpha$  calculated from the  $q$  positions of the  
1202 SAXS diffraction peaks (black diamonds), and SAXS (10) reflection integrated peak  
1203 intensity (red circles) and FWHM (blue squares) for hydrostatically compressed SBA-15  
1204 as a function of pressure. At  $\sim 3 - 4$  GPa there is an inflection in the pressure  
1205 dependence of the intensity and FWHM, but not for the lattice parameter. Vertical error  
1206 bars are shown, but mostly smaller than the datapoints. Representative errors in  
1207 pressure are shown on the final symbol of each dataset.

1208 Figure 4: XRD data of SBA-15 under hydrostatic compression. Black lines are XRD  
1209 data, red dashed lines are model fits to the data. Porod and constant background  
1210 components have been subtracted and the data is shifted vertically for clarity. The  
1211 vertical feature near  $q \approx 2.6 \text{ \AA}^{-1}$  is the gold (111) reflection. The oscillation occurring in  
1212 all datasets around  $q \approx 2 \text{ \AA}^{-1}$  is a detector masking artifact. The vertical light red line  
1213 illustrates the shift in the FSDP with pressure.

1214 Figure 5: Position (black diamonds), Integrated peak intensity (red circles) and FWHM  
1215 (blue squares) of the low- $q$  component of the FSDP peak for SBA-15 during hydrostatic  
1216 compression. At  $\sim 3$  GPa there is an inflection point in the intensity. Vertical error bars  
1217 are shown, but mostly smaller than the symbols. Representative errors in pressure are  
1218 shown on the final symbol of each dataset.

1219 Figure 6: Comparison of the hydrostatic compression behaviors of SBA-15 with and  
1220 without a hydrostatic PTM. Fused silica [50] is shown as a benchmark for comparison.  
1221 Points without visible vertical error bars have errors smaller than their symbols.  
1222 Representative errors in pressure are shown on the final symbol of each SBA-15  
1223 dataset.

1224 Figure 7: Pressure dependence of the FSDP position for different types of amorphous  
1225 silica [13,16,38,54,55,84,85]. Dotted lines approximate the fused silica low- and high-  
1226 pressure FSDP regimes. Below ~4 GPa, SBA-15's FSDP position shows a stronger  
1227 pressure dependence than any previously studied  $a\text{SiO}_2$  polyamorph. Fused silica is  
1228 the only other polyamorph to have an FSDP position with a stronger pressure  
1229 dependence than fused silica. The SBA-15 FSDP undergoes a transition from strong-to-  
1230 weak pressure dependence by ~3 GPa, analogous to the FSDP behavior of fused silica  
1231 at ~13 GPa. After the transition, the FSDP pressure dependence is comparable to stiff  
1232  $a\text{SiO}_2$  polyamorphs like fully densified  $a\text{SiO}_2$ . All points represent compression data  
1233 except for the unfilled red squares which correspond to decompression of densified  
1234 fused silica. SBA-15 datapoints with FSDP position errorbars smaller than their symbols  
1235 have  $\sigma_{\text{FSDP}} \approx 0.002 \text{ \AA}^{-1}$ .

1236 Figure 8: The densification of different polyamorphs of amorphous silica, plotted as a  
1237 function of normalized volume [16,50,54]. Filled points represent compression, and  
1238 unfilled points represent decompression. The different compression behaviors can be  
1239 separated into two major groups: LDA-type behavior and HDA-type behavior. SBA-15 is  
1240 shown to transition from LDA- to HDA-type behavior at ~2 GPa. SBA-15 datapoints with  
1241 volume errorbars smaller than their symbols have  $\sigma_{V/V_0} \approx 0.0015$ .

1242 Figure C.1: Comparison between the volumetric compression of the bulk material and  
1243 the FSDP cell for fused silica with dissolved helium [54], densified fused silica [16],  
1244 fused silica [50,86], and SBA-15 (this work). Filled circles represent the compression of  
1245 bulk  $a\text{SiO}_2$ , lines with squares represent the compression of the FSDP cell.