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CRYSTAL STRUCTURE OF THORIUM NITRATE PENTAHYDRATE  
BY X-RAY DIFFRACTION

Tatzuo Ueki, Allan Zalkin and David H. Templeton

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## Crystal Structure of Thorium Nitrate Pentahydrate by X-ray Diffraction\*

By Tatzuo Ueki, Allan Zalkin and David H. Templeton

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Crystals of  $\text{Th}(\text{NO}_3)_4 \cdot 5\text{H}_2\text{O}$  are orthorhombic, space group  $\text{Fdd}2$ ,  $a = 11.182$ ,  $b = 22.873$ ,  $c = 10.573 \text{ \AA}$ ,  $Z = 8$ . Thorium has three water molecules and 8 oxygen atoms from four nitrate ions as neighbors in a highly polar arrangement. All hydrogen atoms are in hydrogen bonds 2.71 to 2.96  $\text{\AA}$  in length. Average bond distances are: Th-O (water) = 2.46  $\text{\AA}$ , Th-O (nitrate) = 2.57  $\text{\AA}$ , N-O (next to Th) = 1.27  $\text{\AA}$ , N-O (terminal) = 1.22  $\text{\AA}$ . An error of about 0.05  $\text{\AA}$  is made in the position of the thorium atom if anomalous dispersion ( $\Delta f'' = 9$ ) is neglected.

Thorium nitrate crystallizes readily from aqueous nitric acid solutions as the pentahydrate,  $\text{Th}(\text{NO}_3)_4 \cdot 5\text{H}_2\text{O}$ . The earlier literature is confused and contradictory concerning its composition, and it is often found in chemical store rooms labeled as  $\text{Th}(\text{NO}_3)_4 \cdot 4\text{H}_2\text{O}$ . Ferraro, Katzin & Gibson (1954) made a definitive study of the phase diagram and showed that the tetrahydrate crystallizes only when the nitric acid concentration is very high.

\*Work done under the auspices of the U. S. Atomic Energy Commission.

An earlier X-ray study of the pentahydrate, then referred to as the hexahydrate, revealed the unit cell, space group, and thorium atom positions (Templeton & Dauben, 1950). No attempt was made at that time to determine the rest of the structure. With the advantage of electronic computers and better methods for X-ray intensity measurement, we recently solved the structure as reported in the present paper. An independent analysis by neutron diffraction, with results in good agreement with ours, is described in the adjacent paper (Taylor, Mueller & Hitterman, 196x). These studies confirm the composition, show an interesting coordination geometry for the thorium ions, and reveal an intricate structure of hydrogen bonds.

#### Experimental

A bottle from Allied Chemical, General Chemical Division, New York, and labeled  $\text{Th}(\text{NO}_3)_4 \cdot 4\text{H}_2\text{O}$  contained large clear colorless crystals and white powder. Our X-ray diffraction data were obtained from a fragment with dimensions  $0.22 \times 0.08 \times 0.08$  mm which was cut from one of the clear crystals. It was sealed in a silica-glass capillary (wall thickness 0.01 mm) to prevent deliquescence. Cell dimensions and intensities were measured with the General Electric XRD-5 goniostat with scintillation counter and pulse-height discriminator, using molybdenum radiation. Cell dimensions are based on  $\lambda(\text{K}\alpha_1) = 0.70926$  Å. Intensities were measured of 1036 independent reflections (121 recorded as zero) with the stationary crystal technique and counting time of 10 sec. A search for violations of the space-group rules failed to detect any. The thorium atoms in the special positions 8(a) cause intensities to be weak if  $\underline{h} + \underline{k} + \underline{l} = 4\underline{n} + 2$ , especially at large diffraction angles. For fear that many weak or zero data would be undesirable in the least-squares calculations, we assigned zero weight to the 156 reflections

with  $2\theta$  greater than  $40^\circ$  and with counting rates of 2 counts/sec or less. No correction was made for absorption or extinction. We estimate the absorption parameter  $\mu_R$  as 1.3 for the smaller dimensions of the crystal, and this effect limits the accuracy of the thermal parameters.

Calculations were made with the IBM 7044 computer using an unpublished full-matrix least-squares program which minimized  $\sum w(|F_o| - |F_c|)^2 / \sum w|F_o|^2$ . The weights  $w$  were taken as unity or zero. Atomic scattering factors for  $\text{Th}^{4+}$  were obtained by extrapolation from the values for  $\text{Yb}^{4+}$  and  $\text{Hg}^{4+}$  (Thomas & Umeda, 1957) with corrections  $\Delta f' = -6$  and  $\Delta f'' = 9$  for anomalous dispersion. For nitrogen and oxygen we used form factors for neutral atoms as listed by Ibers (1962).

#### Unit cell and space group

$\text{Th}(\text{NO}_3)_4 \cdot 5\text{H}_2\text{O}$  crystals are orthorhombic, space group Fdd2, with 8 formula units in the cell:

$$\underline{a} = 11.182 \pm 0.003 \text{ \AA} (11.191 \pm 0.005 \text{ \AA}),$$

$$\underline{b} = 22.873 \pm 0.005 \text{ \AA} (22.889 \pm 0.010 \text{ \AA}),$$

$$\underline{c} = 10.573 \pm 0.003 \text{ \AA} (10.579 \pm 0.005 \text{ \AA}).$$

The dimensions found by Taylor, Mueller & Hitterman (196x) are given in parentheses. The discrepancy of 6 to 8 parts in 10,000 is only slightly more than one would expect from the estimated accuracies. The density calculated from our data,  $2.800 \pm 0.002 \text{ g cm}^{-3}$ , is between the density measured by flotation in this laboratory, 2.84, and that reported by Staritzky (1956), 2.787. Our measurements were made at about  $21^\circ\text{C}$ .

Crystal data for the isomorphous cerium and plutonium compounds are given by Staritzky (1956). These crystals are expected to have very nearly the same atomic arrangement.

## Determination of the structure

The thorium atoms are in the special position set 8(a):  $(0, 0, \underline{z}; 1/4, 1/4, 1/4 + \underline{z}) + \underline{F}$ , and for this first atom  $\underline{z}$  can be taken as zero. Refinement of the two parameters (scale factor and isotropic thermal parameter) reduced  $\underline{R} = \sum ||\underline{F}_o| - |\underline{F}_c|| / \sum |\underline{F}_o|$  to 0.147. This partial structure has symmetry  $\underline{Fddd}$ , and therefore a Fourier calculation phased by the thorium atom shows duplicate images of the rest of the structure. Furthermore, no phase information is obtained for reflections with  $\underline{h} + \underline{k} + \underline{l} = 4\underline{n} + 2$ , which constitute about one-fourth of the data. The structure was solved by selecting various peaks in the Fourier functions as trial atoms and testing the behavior of their thermal parameters in least-squares calculations. At the third round of this, the nitrate groups were recognized. After several more trials,  $\underline{R}$  was reduced to 0.077 (isotropic thermal parameters) or 0.062 (thorium atom anisotropic) with one water molecule not correctly placed. The correct structure gave  $\underline{R} = 0.043$ , with only the thorium atom anisotropic. Further refinement with anisotropic thermal parameters for all atoms (hydrogen excluded) reduced  $\underline{R}$  to 0.034.

We had proceeded with the assumption that the water content was in doubt. To check for additional water molecules, we calculated a Fourier synthesis of  $(\underline{F}_o - \underline{F}_c)$ , deleting reflections with zero intensity. The largest peaks in this function were about 0.28 electron  $\text{\AA}^{-3}$ , in the neighborhood of the thorium atom. No evidence was found of further water molecules. With the help of an assignment of hydrogen bonds five peaks about one-third to one-half as high as the largest were selected as hydrogen atoms (Table 1). No attempt was made to include hydrogen in any of the structure factor calculations, or to refine these positions.



Table 1. Approximate hydrogen coordinates

<u>x</u>	<u>y</u>	<u>z</u>
0.45	-0.04	-0.25
0.33	-0.14	-0.16
0.06	0.12	0.06
0.35	0.18	-0.26
0.30	-0.14	0.16

Table 2. Structure factor magnitudes, observed (FOB) and calculated (FCA)

An asterisk (\*) indicates zero weight.

(Table to be reproduced photographically)

H,K= 0, 0	H,K= 0,30	7 134 142	12 185 179	0 193 190	5 224 229	L FOB FCA	8 173 163	3 254 244
L FOB FCA	L FOB FCA	9 153 156	14 0 3*	2 0 28*	7 188 182	0 116 112		5 217 207
4 660 668	2 175 178	11 110 109		4 206 198	9 169 156	2 398 423	H,K= 4,26	7 161 154
8 263 256			H,K= 2, 8	6 0 17*	11 109 116	4 107 107	L FOB FCA	9 152 144
12 191 193	H,K= 0,32	H,K= 1,19	L FOB FCA	8 156 144		6 397 412	0 0 12*	11 106 100
	L FOB FCA	L FOB FCA	0 125 121		H,K= 3,17	8 71 57	2 213 200	
H,K= 0, 2	0 148 153	L FOB FCA	2 576 572	H,K= 2,28	L FOB FCA	10 215 215	4 0 15*	H,K= 5,17
L FOB FCA		1 269 264	4 67 63	L FOB FCA	1 264 254	12 0 4*	6 174 174	L FOB FCA
10 241 249	H,K= 1, 1	5 184 181	6 360 373	0 0 3*	3 273 265			1 214 216
14 134 124	L FOB FCA	7 161 176	8 46 52	2 168 164	5 228 221		H,K= 4,28	3 193 200
	L FOB FCA	9 128 122	10 234 233	4 0 4*	7 179 182		L FOB FCA	5 159 159
	1 471 461	11 101 99	12 0 2*	6 146 141	9 165 164	H,K= 4, 8	0 222 221	7 120 130
H,K= 0, 4	3 352 351		14 127 122		11 86 95	L FOB FCA	2 35 25*	9 116 123
L FOB FCA	5 427 441			H,K= 2,30		2 90 84	4 196 183	11 81 92
0 699 712	7 242 252	H,K= 1,21		L FOB FCA	H,K= 3,19	4 390 402	6 0 13*	
4 661 669	9 201 207	L FOB FCA	H,K= 2,10	0 182 175	L FOB FCA	6 42 50		H,K= 5,19
8 318 331	11 135 139	1 201 201	0 719 705	2 0 25*	1 255 249	8 254 259	H,K= 4,30	L FOB FCA
12 167 107	13 117 120	3 216 206	2 65 63	4 147 146	3 249 238	10 31 31*	L FOB FCA	1 228 231
		5 203 200	4 389 393		5 191 199	12 148 157	0, 0 25*	3 183 176
H,K= 0, 6	H,K= 1, 3	7 135 135	6 34 33	H,K= 3, 1	7 136 132		2 179 170	5 163 168
L FOB FCA	L FOB FCA	9 124 116	8 300 300	L FOB FCA	9 111 116	H,K= 4,10		7 125 138
2 800 806	L FOB FCA	11 98 92	10 0 17*	1 418 424	11 81 90	L FOB FCA	H,K= 5, 1	9 109 117
6 374 391	3 346 356		12 200 183	3 442 443		0 29 18	L FOB FCA	11 74 88
10 198 206	5 338 348	H,K= 1,23	14 0 7*	5 351 348	H,K= 3,21	2 405 400	1 539 539	
14 130 128	7 227 234	L FOB FCA		7 162 161	L FOB FCA	4 33 37	3 394 394	H,K= 5,21
	9 234 233	1 200 190	H,K= 2,12	9 182 179	1 199 188	6 322 319	5 268 271	L FOB FCA
H,K= 0, 8	11 174 171	3 186 185	L FOB FCA	11 127 121	3 167 181	8 0 30	7 209 207	L FOB FCA
L FOB FCA	13 102 111	5 141 145	0 20 26	13 109 102	5 159 153	10 179 177	9 193 190	1 219 225
0 522 510		7 133 136	2,438 421		7 134 131	12 0 4*	11 131 138	3 204 211
4 504 523	H,K= 1, 5	9 113 110	4 79 73	H,K= 3, 3	9 104 111		13 100 106	5 155 159
8 260 263	L FOB FCA		6 313 304	L FOB FCA		H,K= 4,12		7 121 117
12 140 146	1 415 403	H,K= 1,25	8 40 28	1 347 347		L FOB FCA	H,K= 5, 3	9 101 112
	3 353 341	L FOB FCA	10 245 239	3 336 341	H,K= 3,23	0 458 463	L FOB FCA	H,K= 5,23
H,K= 0,10	5 346 355	1 171 162	12 34 4*	5 326 333	L FOB FCA	2 32 28	1 373 372	L FOB FCA
L FOB FCA	7 307 314	3 149 141		7 245 252	1 159 162	4 347 352	3 414 411	1 153 149
2 586 581	9 198 201	5 159 159		9 187 181	3 171 168	6 46 41	5 325 318	3 146 144
6 317 327	11 159 155	7 135 125	H,K= 2,14	L FOB FCA	5 167 174	8 253 243	7 223 225	5 141 145
10 178 176	13 103 100	9 111 106	0 455 454	11 102 104	7 140 139	10 0 20*	9 218 210	7 110 122
14 98 103			2 60 47	13 98 91	9 95 97	12 132 135	11 157 153	9 117 114
	H,K= 1, 7	H,K= 1,27	4 412 417	H,K= 3, 5	H,K= 3,25		13 100 104	
H,K= 0,12	L FOB FCA	L FOB FCA	6 46 24	L FOB FCA	L FOB FCA	H,K= 4,14		H,K= 5,25
L FOB FCA	1 372 355	1 136 154	8 300 300	1 412 421	1 135 132	L FOB FCA	H,K= 5, 5	L FOB FCA
0 539 535	3 435 436	3 164 167	10 0 21*	3 310 316	3 134 155	0 115 120	L FOB FCA	1 174 172
4 415 416	5 199 213	5 115 110	12 141 150	5 310 313	5 143 138	2 285 289	1 403 407	3 142 138
8 280 274	7 271 280	7 89 104		7 267 270	7 100 110	4 72 57	3 301 316	5 138 134
12 128 122	9 220 225		H,K= 2,16	9 203 200		6 283 279	5 246 243	7 120 117
	11 139 140	H,K= 1,29	L FOB FCA	11 156 147	H,K= 3,27	8 0 14*	7 201 205	
H,K= 0,14	13 92 99	L FOB FCA	L FOB FCA	10 71 65	L FOB FCA	10 171 181	9 186 184	H,K= 5,27
L FOB FCA		1 130 142	2 314 312	13 98 98	1 130 133	12 0 12*	11 125 124	L FOB FCA
2 309 309	H,K= 1, 9	3 106 109	4 51 46		3 113 111		13 94 102	1 158 157
6 283 274	L FOB FCA	5 103 117	6 309 317	H,K= 3, 7	5 117 109	H,K= 4,16		3 140 138
10 165 169	1 344 334		8 43 44*	L FOB FCA	7 90 96	L FOB FCA	H,K= 5, 7	5 120 133
	3 415 408	H,K= 1,31	L FOB FCA	1 481 484		0 315 305	L FOB FCA	
H,K= 0,16	5 274 278	L FOB FCA	10 201 205	3 395 402	H,K= 3,29	2 26 9	1 264 276	H,K= 5,29
L FOB FCA	7 214 218	1 103 114	12 0 7*	5 268 266	L FOB FCA	4 337 330	3 232 227	L FOB FCA
0 447 430	9 193 196	3 111 111		7 207 207	1 153 153	6 57 66	5 308 304	1 108 108
4 386 387	11 126 120		H,K= 2,18	9 166 167	3 113 114	8 217 209	7 256 256	3 116 107
8 182 183	13 99 106	H,K= 2, 0	L FOB FCA	11 138 137	5 97 112	10 0 6*	9 179 172	
12 113 117		L FOB FCA	0 360 353	13 93 98		12 110 116	11 108 112	H,K= 6, 0
	H,K= 1,11	L FOB FCA	2 281 274		H,K= 3, 9		13 72 87	L FOB FCA
H,K= 0,18	L FOB FCA	6 373 375	4 327 325	H,K= 3, 9	L FOB FCA	H,K= 4,18		2 500 501
L FOB FCA	1 267 264	10 263 248	6 0 13*	L FOB FCA	1 517 510	L FOB FCA	H,K= 5, 9	6 285 283
2 355 343	3 371 375	14 119 118	8 196 197	1 322 326	1 104 104	0 38 26	L FOB FCA	10 201 201
6 285 285	5 256 267		10 0 3*	5 275 279		2 345 340	1 304 319	
10 159 147	7 196 196	H,K= 2, 2	12 133 130	7 219 212	H,K= 4, 0	4 28 21	3 282 288	H,K= 6, 2
	9 156 163	L FOB FCA		9 147 147	L FOB FCA	6 216 213	5 303 298	L FOB FCA
H,K= 0,20	11 107 110	0 604 593	H,K= 2,20	11 101 114	0 683 702	8 46 22*	7 180 177	0 448 456
L FOB FCA	13 101 103	2 91 88	L FOB FCA	13 87 107	4 533 536	10 144 148	9 147 149	2 42 43
0 418 424		4 480 492	0 38 30		8 337 321		11 133 124	4 383 386
4 261 259	H,K= 1,13	6 30 34	2 303 293	H,K= 3,11	12 155 159	H,K= 4,20	13 89 87	6 79 72
8 171 160	L FOB FCA	8 317 318	4 41 41	L FOB FCA		L FOB FCA		8 295 286
	1 260 264	10 0 22	6 250 246	1 400 400	H,K= 4, 2	0 321 309	H,K= 5,11	10 31 35*
H,K= 0,22	3 210 211	12 168 168	8 0 22*	3 358 352	L FOB FCA	2 64 63	L FOB FCA	12 161 163
L FOB FCA	5 314 317	14 0 11*	10 149 152	5 301 307	0 127 118	4 260 263	1 317 315	
2 317 327	7 176 179			7 211 213	2 540 558	6 31 21*	3 212 216	H,K= 6, 4
6 202 196	9 191 188	H,K= 2, 4	H,K= 2,22	9 175 177	4 144 133	8 174 174	5 214 218	L FOB FCA
10 145 143	11 114 121	L FOB FCA	L FOB FCA	11 131 134	6 340 339	10 0 17*	7 146 144	0 0 1
	13 73 91	0 165 147	0 227 229	13 63 98	8 84 82		9 119 115	2 335 333
H,K= 0,24		2 361 387	4 226 225		10 252 240	H,K= 4,22	11 101 107	4 73 65
L FOB FCA	H,K= 1,15	4 109 115	6 55 34	H,K= 3,13	12 0 11*	L FOB FCA	13 83 89	6 345 354
0 275 271	L FOB FCA	6 410 414	8 201 200	L FOB FCA	14 116 122	0 30 36*		8 0 29
4 240 246	1 264 255	8 0 25	10 0 2*	1 365 355		2 274 258	H,K= 5,13	10 232 228
8 192 195	3 189 189	10 246 246		3 313 318	H,K= 4, 4	4 44 37*	L FOB FCA	12 0 6*
	5 281 273	12 0 20*		5 289 277	0 460 480	6 196 193	1 161 161	
H,K= 0,26	7 217 222	14 125 130	H,K= 2,24	7 161 161	2 60 50	8 0 10*	3 204 205	H,K= 6, 6
L FOB FCA	9 160 152		L FOB FCA	9 164 162	4 494 504	10 134 133	5 241 235	L FOB FCA
2 228 240	11 117 119	H,K= 2, 6	0 31 4*	11 125 120	6 52 56		7 224 216	0 445 445
6 151 165	13 74 82	L FOB FCA	2 205 191	13 90 92	8 322 317	H,K= 4,24	9 161 152	2 110 107
		0 240 243	4 0 21*		10 0 20*	L FOB FCA	11 60 86	4 389 384
H,K= 0,28	H,K= 1,17	2 57 50	6 176 178	H,K= 3,15	12 166 162	0 268 258		6 118 105
L FOB FCA	L FOB FCA	4 488 497	8 0 15*	L FOB FCA	14 0 9*	2 0 15*	H,K= 5,15	8 278 269
0 213 233	1 288 285	6 45 43		1 332 327		4 221 216	L FOB FCA	10 0 17*
4 215 215	3 211 200	8 344 343	H,K= 2,26	L FOB FCA		6 0 14*	1 213 207	12 156 155
	5 216 209	10 0 19*	L FOB FCA	3 209 208				

H,K= 6, 8	0 0 33*	9 72 93	H,K= 8,14	3 186 185	6 31 21*	7 125 115	H,K=12, 8	5 104 110
L FOB FCA	2 166 168		L FOB FCA	5 211 209	8 213 215	9 112 105	L FOB FCA	0 284 289
0 94 98	4 0 21*	H,K= 7,21	0 40 38	2 333 331	10 0 5*		0 284 289	H,K=13,15
2 365 362	H,K= 7, 1	L FOB FCA	1 173 159	4 0 7*		H,K=11, 7	2 32 22*	L FOB FCA
4 42 43	L FOB FCA	3 116 110	6 246 244	8 0 13*	H,K=10, 8	L FOB FCA	4 224 216	1 119 123
6 296 290	1 277 281	5 160 154	10 143 142	10 143 142	L FOB FCA	1 214 204	6 0 9*	3 96 105
8 29 48*	3 251 246	9 98 97			H,K= 9,11	3 165 158	8 145 152	H,K=13,17
10 208 201	5 256 245				L FOB FCA	5 219 214	H,K=12,10	L FOB FCA
12 0 8*	7 217 200				1 182 176	7 147 133	L FOB FCA	1 97 108
	9 142 136	H,K= 7,23	H,K= 8,16	3 173 165	6 229 228	9 102 97	L FOB FCA	3 112 112
H,K= 6,10	11 121 118	L FOB FCA	L FOB FCA	5 160 158	8 0 17*		0 32 9*	
L FOB FCA	13 82 83	1 144 147	0 311 311	7 158 156	10 149 152	H,K=11, 9	2 231 225	H,K=14, 0
0 396 388		3 134 141	2 0 15*	9 124 127		L FOB FCA	4 0 3*	L FOB FCA
2 41 36	H,K= 7, 3	5 125 126	4 243 231	6 46 27*	H,K=10,10	3 179 176	6 185 192	2 201 209
4 379 373	L FOB FCA	7 109 107	8 191 185	10 0 10*	L FOB FCA	5 162 162	8 0 10*	6 172 183
6 0 15	1 264 266	H,K= 7,25			2 0 14*	7 123 121		
8 251 244	3 205 210	L FOB FCA	H,K= 8,18	3 163 153	4 264 264	9 89 95	H,K=12,12	H,K=14, 2
10 0 13*	5 205 209	L FOB FCA	L FOB FCA	5 139 130	6 0 17*		0 229 222	L FOB FCA
12 129 133	7 211 214	1 97 103	0 0 2*	7 136 138	8 160 160	H,K=11,11	2 0 13*	0 209 226
	9 146 138	3 105 119	2 263 264	9 111 120	10 0 3*	L FOB FCA	4 191 200	2 35 2*
H,K= 6,12	11 106 96	5 120 123	4 45 10*			L FOB FCA	6 0 9*	4 187 191
L FOB FCA	13 82 88		6 185 185	H,K= 9,15	H,K=10,12	3 177 167		6 0 12*
0 81 79		H,K= 7,27	8 0 13*	L FOB FCA	L FOB FCA	5 155 149	H,K=12,14	H,K=14, 4
2 328 318	H,K= 7, 5	L FOB FCA		0 67 71	L FOB FCA	7 98 110	L FOB FCA	L FOB FCA
4 37 44	L FOB FCA	1 102 114	H,K= 8,20	2 229 223	2 229 223	9 90 87	0 34 1*	0 34 23*
6 282 284	1 187 183	3 97 100	L FOB FCA	3 202 200	4 0 30*		2 205 213	2 181 190
8 0 25*	3 294 284		0 270 268	5 147 139	6 227 224	H,K=11,13	4 0 10*	4 50 21*
10 189 183	5 284 275	H,K= 8, 0	2 0 16*	7 151 145	8 0 24*	L FOB FCA	6 178 174	6 156 160
12 0 7*	7 190 190	L FOB FCA	4 226 231	9 108 115	10 123 127	1 172 166		
	9 200 186	0 374 381	6 0 4*	H,K= 9,17	H,K=10,14	3 146 160	H,K=12,16	H,K=14, 6
H,K= 6,14	11 117 104	4 370 370	8 136 135	L FOB FCA	L FOB FCA	5 162 153	L FOB FCA	L FOB FCA
L FOB FCA	13 83 80	8 210 207		1 156 152	L FOB FCA	7 128 139	0 194 190	0 184 190
0 304 299		12 119 125	H,K= 8,22	3 127 127	0 177 174		2 0 7*	4 168 177
2 90 82	H,K= 7, 7	L FOB FCA	L FOB FCA	5 169 155	2 31 11*	H,K=11,15	4 206 203	6 0 20*
4 306 304	L FOB FCA	H,K= 8, 2	0 47 23*	7 130 124	6 0 19*	L FOB FCA	1 161 157	1 161 157
6 29 24*	1 292 292	0 53 40	2 171 170	9 83 91	8 171 169	3 174 171	5 143 138	H,K=12,18
8 229 231	3 263 264	2 414 417	4 0 15*			7 115 109	7 115 109	L FOB FCA
10 0 6*	5 259 254	4 0 5	6 164 173	H,K= 9,19	H,K=10,16		0 36 14*	H,K=14, 8
12 128 134	7 166 162	6 313 301		L FOB FCA	L FOB FCA		2 173 177	L FOB FCA
	9 165 155	8 0 33*	H,K= 8,24	1 79 160	0 32 5*	H,K=11,17	4 0 7*	2 170 187
H,K= 6,16	11 119 120	10 147 140	L FOB FCA	3 74 144	2 214 215	L FOB FCA	1 155 161	4 0 9*
L FOB FCA		12 0 4*	0 169 182	5 76 117	4 0 29*	3 158 160	H,K=12,20	H,K=14,10
0 60 59	H,K= 7, 9	L FOB FCA	2 0 6*	7 62 108	6 176 170	5 123 122	L FOB FCA	L FOB FCA
2 288 285	L FOB FCA	H,K= 8, 4	4 178 177		8 0 9*	7 105 100	0 173 169	H,K=14,10
4 28 46	1 334 328	L FOB FCA	6 0 15*	H,K= 9,21	H,K=10,18		2 0 9*	0 178 173
6 260 253	3 242 226	0 469 466		L FOB FCA	L FOB FCA			2 0 6*
8 0 21*	5 231 229	2 49 51	H,K= 8,26	1 151 151	0 204 221	H,K=11,19	H,K=13, 1	4 151 161
10 164 158	7 140 148	4 354 340	L FOB FCA	3 128 120	2 0 14*	L FOB FCA	L FOB FCA	H,K=14,12
	9 159 153	6 0 20	0 0 17*	5 137 140	4 187 190	1 131 145	1 163 160	L FOB FCA
H,K= 6,18	11 115 110	8 219 215	2 154 163	7 104 98	6 0 21*	3 147 152	3 169 161	0 0 2*
L FOB FCA		10 0 2*	4 0 5*			5 103 118	5 119 124	2 164 166
0 296 294	H,K= 7,11	12 120 127		H,K= 9,23	H,K=10,20	H,K=11,21	7 119 116	4 0 4*
2 41 25	L FOB FCA		H,K= 9, 1	L FOB FCA	L FOB FCA	L FOB FCA		H,K=13, 3
4 269 258	1 297 298	H,K= 8, 6	L FOB FCA	1 121 126	0 0 8*	1 135 143	H,K=13, 3	H,K=14,14
6 31 17*	3 273 271	L FOB FCA	1 277 268	3 107 114			L FOB FCA	L FOB FCA
8 198 195	5 213 210	0 43 37	3 241 230	5 110 105	2 189 190	3 116 120	1 150 145	0 139 143
10 0 6*	7 181 186	2 343 343	5 181 180		4 35 6*	H,K=11,23	5 158 155	2 0 13*
	9 145 151	4 53 40	7 208 194	H,K= 9,25	6 137 136	L FOB FCA	7 125 122	
H,K= 6,20	11 112 112	6 271 263	9 142 143	L FOB FCA		L FOB FCA		H,K=15, 1
L FOB FCA		8 31 8*	11 118 114	1 109 111	H,K=10,22	1 124 116		L FOB FCA
0 0 22*	H,K= 7,13	10 186 179		3 98 102	L FOB FCA		H,K=13, 5	L FOB FCA
2 259 250	L FOB FCA	12 0 5*	H,K= 9, 3	0 191 198	0 191 198	H,K=12, 0	L FOB FCA	1 140 149
4 31 49*	1 276 264		L FOB FCA	H,K=10, 0	2 0 27*	L FOB FCA	1 136 142	3 110 111
6 190 187	3 249 250	H,K= 8, 8	1 252 237	L FOB FCA	4 167 176	0 176 177	3 138 147	
8 0 8*	5 204 200	L FOB FCA	3 235 222	2 392 401		4 230 226	5 143 141	H,K=15, 3
10 139 140	7 162 159	0 472 473	5 221 213	6 230 232	H,K=10,24	8 142 146	7 120 115	L FOB FCA
	9 152 146	2 51 42	7 196 190	10 169 164	L FOB FCA		1 135 129	L FOB FCA
H,K= 6,22	11 108 108	4 381 378	9 154 152		0 0 5*	H,K=12, 2	3 104 121	3 104 121
L FOB FCA		6 41 42*	11 133 122		2 143 150	L FOB FCA		
0 248 254	H,K= 7,15	8 214 201		H,K=10, 2		0 31 11*	L FOB FCA	H,K=15, 5
2 45 61*	L FOB FCA	10 34 10*	H,K= 9, 5	L FOB FCA	H,K=11, 1	2 237 232	1 149 151	L FOB FCA
4 211 213	1 192 198	12 122 113	L FOB FCA	0 300 301	L FOB FCA	4 32 17*	3 152 142	L FOB FCA
6 34 16*	3 225 224		1 152 145	2 39 57	1 256 250	6 193 187	5 131 142	1 115 119
8 156 154	5 171 168	H,K= 8,10	3 217 214	6 0 11*	3 236 229	8 0 9*	7 104 104	3 98 113
	7 185 184	L FOB FCA	5 253 247	8 224 218	5 139 140			
H,K= 6,24	9 140 138	0 26 10	7 178 173	10 0 12*	7 144 133	H,K=12, 4	H,K=13, 9	H,K=15, 7
L FOB FCA	11 82 88	2 423 417	9 175 169		9 111 108	L FOB FCA	L FOB FCA	L FOB FCA
0 0 14*		4 39 25	11 108 99	H,K=10, 4		0 219 217	3 138 146	3 118 119
2 169 172	H,K= 7,17	6 200 204		L FOB FCA	H,K=11, 3	2 31 9*	5 118 110	
4 0 5*	L FOB FCA	8 0 2*	H,K= 9, 7	0 39 14	L FOB FCA	4 223 211	7 98 105	H,K=15, 9
6 173 178	1 223 227	10 165 162	L FOB FCA	2 280 273	L FOB FCA	6 34 13*		L FOB FCA
8 0 7*	3 193 183		1 221 223	4 29 33*	3 209 198	8 182 180	H,K=13,11	1 98 106
	5 209 204	H,K= 8,12	3 182 175	6 255 249	5 162 161		L FOB FCA	
H,K= 6,26	7 150 155	L FOB FCA	5 200 200	8 0 12*	7 140 132	H,K=12, 6	L FOB FCA	
L FOB FCA	9 111 110	0 370 364	7 164 153	10 170 174	9 122 110	L FOB FCA	3 126 124	
0 182 186		2 39 21	9 138 133			0 44 35*	5 114 119	
2 35 10*	H,K= 7,19	4 310 308	11 109 103	H,K=10, 6	H,K=11, 5	2 197 195		
4 177 168	L FOB FCA	6 0 2*		L FOB FCA	L FOB FCA	4 0 9*	H,K=13,13	H,K=15, 9
6 0 18*	1 200 199	8 178 183	H,K= 9, 9	0 345 347	1 208 208	6 195 186	L FOB FCA	L FOB FCA
	3 179 183	10 0 6*	L FOB FCA	2 57 53	3 215 214	8 0 12*	1 131 135	1 110 115
H,K= 6,28	5 170 165		1 217 214	4 271 268	5 169 173		3 138 128	3 118 119
L FOB FCA	7 107 124							

The calculations to this point had neglected the out-of-phase component  $\Delta f''$  of thorium. Because of the polar nature of the space group  $Fdd2$ , two orientations of the structure must be considered, one of which is the reflection of the other in (001). Further calculations with  $\Delta f''$  included and the correct orientation reduced  $R$  to 0.033 (or 0.045 including reflections of zero weight). With the reverse structure  $R$  could not be reduced below 0.035, and the weighted sum of squares was 15 percent larger. In the final cycle of the correct structure, no coordinate shifted more than 0.000008 and no thermal parameter more than 0.001. Observed and calculated structure factor magnitudes are listed in Table 2. The final coordinates are given in Table 3. The anisotropic thermal parameters, Table 4, are listed in the units of the isotropic Debye  $B$ , Zalkin, Forrester & Templeton (1964), Cruickshank (1965).

#### Effect of anomalous dispersion

Inclusion of the thorium phase shift in the calculations gives enough change in some of the structure factor magnitudes to establish the polarity of the structure, but the change in  $R$  is hardly dramatic. However, it causes a significant change in the structure. With the origin defined by the thorium atom, all other atoms shifted about 0.05 Å in the positive  $z$  direction when the correction was included. A similar shift of the reverse structure causes the two structures, after refinement, to differ by about 0.10 Å. This behavior is explained by the fact that all the calculations were made with reflections with positive values of  $\ell$ . The effect of the phase shift (which is an advance of phase) is to make the thorium atom appear to be closer to the X-ray source and detector than it really is. The symmetry of the space group gives a cancellation of the effect on  $x$  and  $y$  coordinates, but there is a systematic

Table 3. Atomic coordinates and estimated standard deviations

All values have been multiplied by  $10^4$ .

Atom	<u>x</u>	<u>y</u>	<u>z</u>
Th	0	0	0
O(1)	0	0	2277(17)
O(2)	-0042(11)	1041(4)	0656(11)
O(3)	4543(11)	-0892(5)	-1066(12)
N(1)	2651(10)	0046(6)	0508(12)
O(11)	2094(9)	-0381(4)	0025(15)
O(12)	1970(10)	0453(5)	0915(13)
O(13)	3733(8)	0093(5)	0538(13)
N(2)	0471(12)	0772(5)	-2259(17)
O(21)	1318(9)	0551(5)	-1619(12)
O(22)	0579(9)	-0631(4)	-1924(12)
O(23)	0677(12)	1066(6)	-3213(12)

Table 4. Anisotropic thermal parameters

T.F. =  $\exp(-\beta_{11}h^2 - 2\beta_{12}hk - \dots)$ ;  $4\beta_{12} = B_{12}a^*b^*$ , etc. Standard deviations estimated by least squares are less than 0.05 for Th and from 0.3 to 0.8 for the other atoms.

Atom	$B_{11}$	$B_{22}$	$B_{33}$	$B_{12}$	$B_{13}$	$B_{23}$
Th	1.2	1.4	2.1	0.0	---	---
O(1)	4.5	2.0	3.7	0.9	---	---
O(2)	2.1	2.0	4.3	-0.3	0.0	-0.5
O(3)	2.4	2.6	3.3	0.1	-0.6	-0.2
N(1)	1.5	2.0	2.9	0.5	-0.5	-0.5
O(11)	2.2	1.4	3.8	0.8	-0.6	-0.7
O(12)	2.3	2.5	3.7	0.3	-0.2	-0.5
O(13)	1.0	2.8	5.2	-0.1	-0.5	0.0
N(2)	2.1	2.0	4.4	-0.9	0.3	0.2
O(21)	1.3	2.9	3.9	0.2	-0.3	0.9
O(22)	1.7	1.7	3.8	-0.2	0.4	-0.1
O(23)	3.5	3.6	3.0	-0.2	1.1	1.5

biasing of the z components of interatomic vectors between thorium and the rest of the structure.

This kind of shift will be a general feature of polar structures which are refined with such incomplete data, unless one of several obvious steps is taken to prevent it.

The two structures of opposite polarity are not different in the sense of right and left handedness, but only with respect to their orientation in a specimen. We have not made a correlation of the polarity with respect to morphology or other physical property.

#### Comparison with neutron diffraction results

The neutron diffraction study by Taylor, Mueller & Hitterman (196x) gives us a chance to check the accuracy of the X-ray method in a case where the heavy atom dominates the data. The agreement of the coordinates is excellent, and it confirms that the estimated standard deviations are of the correct magnitude. Of 31 independent coordinates, 17 are within one standard deviation and none is as much as three standard deviations from the corresponding neutron result. The atomic positions in the two structures differ by 0.026 Å on the average and by 0.045 Å in the most extreme case.

The structure obtained before correction for the thorium phase shift is in significantly poorer agreement with the neutron results; the average distance between atomic locations is 0.065 Å.

The neutron results show that each hydrogen location (Table 1) is in the correct neighborhood, but indicate errors of 0.2 to 0.5 Å from the correct position.

## Discussion of the structure

Some interatomic distances are listed in Table 5. The thorium atom has its 11 oxygen neighbors arranged in a highly unsymmetrical way with respect to the polar direction (Fig. 1). These oxygen atoms are two each from four nitrate groups and three from water molecules, with all the water on one side. This polar arrangement is probably related to the large pyroelectric effect which is observed when the crystals are dipped in liquid nitrogen. One expects about 8 oxygen neighbors for thorium if the oxygen atoms are not bonded to each other. Two oxygen atoms in nitrate are closer than normal for atoms from separate molecules, and thus the coordination can be as high as 12 if the atoms are from six nitrate groups as in  $\text{MgTh}(\text{NO}_3)_6 \cdot 8\text{H}_2\text{O}$  (Šćavničar & Prodić, 1965). Thus to have 11 neighbors is reasonable if 8 of them are from nitrate ions.

In each nitrate ion the non-coordinated oxygen atom is significantly closer to nitrogen than are the other two. A similar effect is observed in several other nitrate crystals as listed by Taylor, Mueller & Hitterman (196x), as well as in  $\text{Ce}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$  and  $\text{Ce}(\text{NH}_4)_2(\text{NO}_3)_6$  (Ueki, Zalkin & Templeton, unpublished). The terminal oxygen atom, in each case which we have studied, has higher thermal parameters than the other two. Thus a correction of bond distance for thermal motion removes some of the difference, but this correction seems to be inadequate to explain as much as half of the effect. In the present case, the thermal effect is estimated to account for about 0.01 Å of the difference.

We recognize five hydrogen bonds (Table 5) which are completely confirmed by the neutron diffraction results. Their distances and angles



Table 5. Bond lengths in Å, uncorrected for thermal motion  
 Values found by Taylor, Mueller & Hitterman are given in parentheses.

Th-O (nitrate)		
Th-O(11)	2.50 ± 0.01	(2.528)
Th-O(12)	2.62 ± 0.01	(2.618)
Th-O(21)	2.59 ± 0.01	(2.573)
Th-O(22)	2.58 ± 0.01	(2.554)
Th-O (water)		
Th-O(1)	2.41 ± 0.02	(2.438)
Th-O(2)	2.48 ± 0.01	(2.473)
Nitrate groups		
N(1)-O(11)	1.27 ± 0.02	(1.270)
N(1)-O(12)	1.28 ± 0.02	(1.250)
N(1)-O(13)	1.21 ± 0.01	(1.202)
N(2)-O(21)	1.27 ± 0.02	(1.264)
N(2)-O(22)	1.27 ± 0.02	(1.275)
N(2)-O(23)	1.24 ± 0.02	(1.206)
Hydrogen bonds		
O(1)-O(3)	2.74 ± 0.02	(2.698)
O(2)-O(3)	2.71 ± 0.02	(2.697)
O(2)-O(22)	2.90 ± 0.02	(2.953)
O(3)-O(23)	2.86 ± 0.02	(2.901)
O(3)-O(13)	2.96 ± 0.02	(2.946)

(Table 6) are normal. The hydrogen bonds to O(1), because of the two-fold axis, are exactly coplanar with the Th-O(1) bond and at equal angles to it. The hydrogen bonds to O(2) are very nearly coplanar with the Th-O(2) bond. This arrangement, with the water dipoles pointed almost directly away from the cation, is not surprising for such a highly charged ion. The water molecules in  $\text{Zr}(\text{SO}_4)_2 \cdot 4\text{H}_2\text{O}$  are similarly oriented (Templeton, 1960). The water molecules designated as O(3) are bonded to the rest of the structure by four hydrogen bonds in directions corresponding to a rather distorted tetrahedron.

We thank J. C. Taylor, M. H. Mueller and R. L. Hitterman for sending us their manuscript prior to submission for publication.

Table 6. Bond angles

Atoms	Angle
Th-O(1)-O(3)	$129.8 \pm 0.4^\circ$
O(3)-O(1)-O(3)	$100.4 \pm 0.8^{\text{oa}}$
Th-O(2)-O(3)	$124.0 \pm 0.5^\circ$
Th-O(2)-O(22)	$127.2 \pm 0.5^\circ$
O(3)-O(2)-O(22)	$108.7 \pm 0.5^{\text{oa}}$
O(1)-O(3)-O(2)	$108.4 \pm 0.5^\circ$
O(1)-O(3)-O(13)	$81.7 \pm 0.5^\circ$
O(1)-O(3)-O(23)	$103.9 \pm 0.5^\circ$
O(2)-O(3)-O(13)	$106.5 \pm 0.5^\circ$
O(2)-O(3)-O(23)	$124.6 \pm 0.6^\circ$
O(13)-O(3)-O(23)	$121.9 \pm 0.5^{\text{oa}}$

<sup>a</sup>O...H-O-H...O angles.

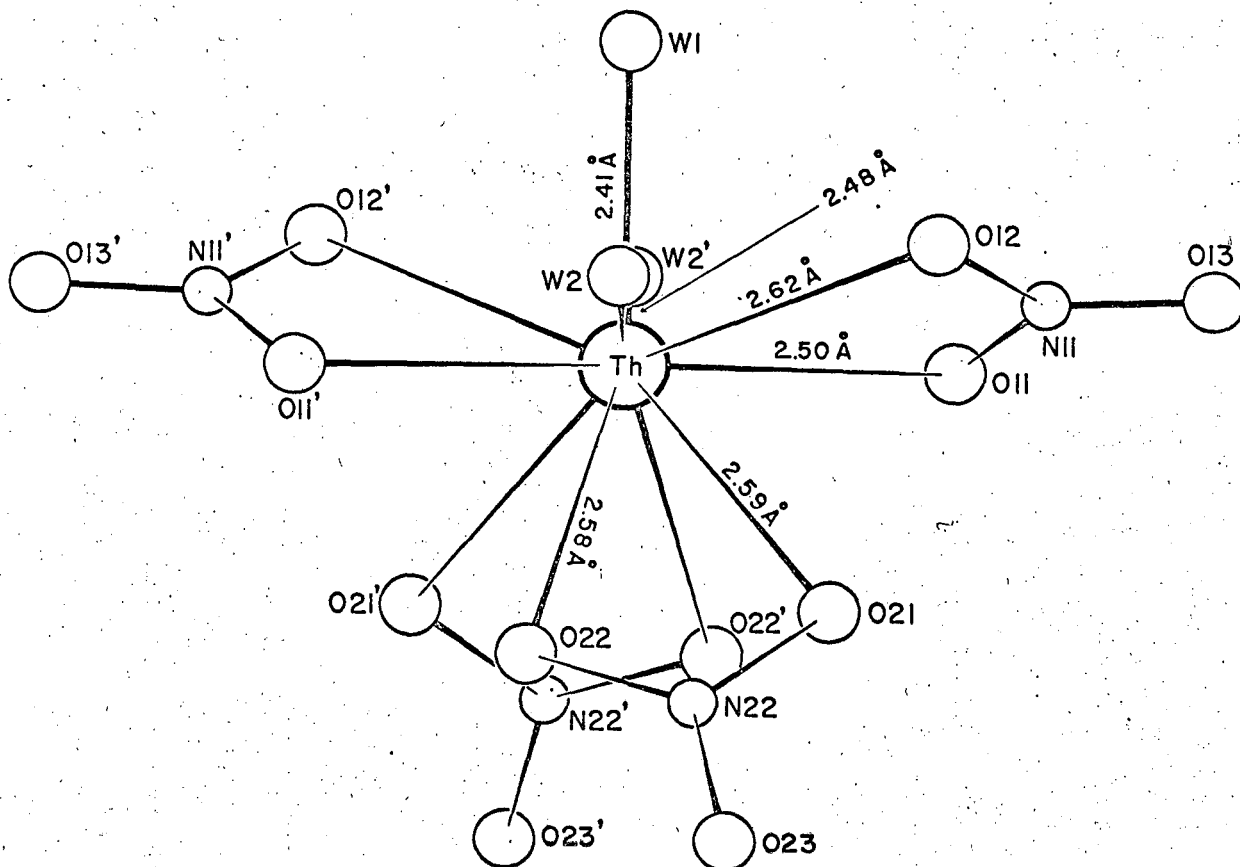
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Figure caption

Fig. 1. Neighbors of the thorium atom in  $\text{Th}(\text{NO}_3)_4 \cdot 5\text{H}_2\text{O}$ .

W1 and W2 indicate water molecules called O(1) and O(2) in the text.



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