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Passive higher-harmonic rf cavities with general settings and multibunch instabilities in electron storage rings

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We introduce a perturbation-theory, mode-analysis method for longitudinal multibunch instabilities driven by the higher harmonic cavity (HHC) fundamental mode. The method, based on the exact solution of the unperturbed particle motion in the rf bucket and suitable for modeling the effect of cavities with general settings, is applied to study the feasibility of reutilizing the existing Advanced Light Source (ALS) HHCs in the ALS Upgrade (ALS-U). We find that with ALS cavities the ALS-U would be susceptible to a fast $\ell = 1$ mode instability. Interestingly, the instability is driven by the imaginary rather than the real part of the cavity fundamental-mode impedance.

I. INTRODUCTION

The ALS-U is the Advanced Light Source (ALS) upgrade to a multibend achromat lattice, diffraction-limited light source [1]. While the upgrade entails the replacement of most components, for obvious reasons it is desirable to recycle as much as possible of the existing infrastructure, including the rf systems and in particular the passive normal-conducting higher-harmonic cavities (HHCs). HHCs are widely employed in the new-generation light sources to lengthen the bunches and reduce intrabeam scattering.

In passive operation, the basic HHC physics parameters are the shunt impedance R_s and the fundamental-mode resonance frequency ω_r. Adopting common language, we say that these parameters are "optimal" [2] if first and second derivatives of the total rf voltage experienced by the synchronous particle vanish (bunch profile maximally flat). For a given circulating average beam current, there is a unique pair of R_s and ω_r meeting the optimum condition.

The ALS currently operates with three 3rd-harmonic cavities, each with $R_s = 1.7$ MΩ. As a result of a lower main-cavity voltage requirement, in the ALS-U the optimum HHC shunt impedance is only 1.35 MΩ. In principle, a single ALS HHC, having shunt impedance close to optimum, would then be sufficient. Unfortunately, the resulting power loss would significantly exceed the cavity limit (about 5 kW).

The combined shunt impedance of two ALS cavities is farther from optimum but two cavities would still achieve the desired (∼4) bunch-lengthening factor and reduce

scattering effects as effectively, since the latter are not critically dependent on the details of the bunch longitudinal profile. A larger shunt impedance is accommodated by tuning the HHCs further away from the 3rd-harmonic of the rf generator frequency, and while this comes with some advantages (lower dissipated power and Robinson instability growth rate) it has the potential to drive the longitudinal $\ell = 1$ coupled-bunch instability mode. The study of this mode is the main topic of the paper. The problem is investigated by mode analysis with the primary goal of estimating the growth rates.

The framework for a perturbation-theory mode analysis applicable to our problem goes back at least to Sacherer's work in the 1970s [3] and later refinements by Wang and others [4–10], but to our knowledge it has always been applied in the form specialized to optimum HHC configuration, with more general cases handled by some heuristic adaptation of this theory [11,12]. Our approach is based on the exact numerical solution of the unperturbed particle motion at equilibrium, similar to the method successfully applied in the analysis of single-bunch broad-band impedance driven instabilities [13–15], permitting an accurate treatment of the more general HHC settings. Our main result is a mode $\ell = 1$ growth-rate estimate of about 5 ms^{-1}. In combination with the mode low oscillation frequency (less than 50 Hz), this appears to place the instability out of reach of existing longitudinal feed-back systems [16], thus undermining the feasibility of reusing two ALS HHCs as existing.

The content of the paper is as follows. In the next section we establish notation and sketch the derivation of the linearized Vlasov equation for mode analysis. In Sec. III we write and solve the dispersion-relation equation for the set-up with two ALS HHCs over a range of cavity tuning. In Sec. IV we study the dispersion equation for optimum HHCs in the approximate form found in the literature. Although the latter would be expected to apply strictly only

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to the optimum case, we attempt to apply it also to nonoptimum HHCs (tuned for comparable bunch lengthening) and find reasonable agreement with the results from Sec. III. We then work out asymptotic approximations to the solutions and use them to recognize that while the $\ell = 0$ mode (Robinson's) instability is driven by the real part of the impedance, in the case of interest the $\ell = 1$ mode instability is driven by the imaginary part. The Appendices report formulas for beam loading (A), bunch equilibrium and optimum HHC settings (B), details on the numerical method (C), effective impedance for the modes of interest (D), and useful formulas for motion in a purely quartic potential (E).

II. LINEARIZED VLASOV EQUATION

We write the equations of motions for synchrotron oscillations as

$$\frac{dz}{dt} = \alpha c \delta, \tag{1}$$

$$\frac{d\delta}{dt} = \frac{eV_{\text{rf}}(z) - U_0}{E_0 T_0}, \tag{2}$$

where $V_{\text{rf}}(z)$ is the total rf voltage, E_0 the design beam energy, T_0 the revolution time, U_0 the energy per turn lost to radiation, $\alpha > 0$ the momentum compaction, $\delta = (E - E_0)/E_0$ the particle relative energy, and z the longitudinal coordinate. We adopt the sign convention $z < 0$ for a particle in the bunch head and $eV_{\text{rf}} > 0$ for energy gain (elementary charge $e > 0$).

The total voltage $V_{\text{rf}}(z) = V_1(z) + V_3(z)$ results from main and passively operated 3rd higher-harmonic cavities. A cavity voltage has two contributions, one from the external rf generator and the other from beam loading. For simplicity, we model the main rf cavity voltage without distinguishing between the two and credit the rf feed-back system with maintaining the voltage amplitude V_{10} and phase ϕ_1 to their set values: $V_1(z) = V_{10} \sin(k_1 z + \phi_1)$, where $k_1 = \omega_1/c$ with $\omega_1 = h\omega_0$ being the rf generator frequency, h the (main cavity) harmonic number, and $\omega_0 = 2\pi/T_0$ the revolution frequency. Throughout this paper we assume a uniform beam filling with all the rf buckets occupied by bunches having particle population N and hence $I_{\text{avg}} = eN\omega_1/2\pi \equiv eN/T_1$ average circulating current.

The voltage of passive HHCs, $V_3(z) = V_{3,0}(z;\rho_0) + V_{3,1}(z;\rho_1)$, is entirely due to beam loading and can be distinguished into two components, one depending on the bunch profile $\rho_0(z)$ at equilibrium and the other on the time-dependent deviation $e^{-i\Omega t}\rho_1(z)$ from equilibrium occurring during an instability, where Ω is the mode complex-number frequency. The first has the form

$$V_{3,0}(z;\rho_0) = -2I_{\text{avg}}R_s F \cos\psi \cos(k_3 z + \psi - \Phi), \tag{3}$$

where F and Φ are the amplitude and phase of the Fourier integral of the bunch profile $\tilde{\rho}_0(k_3) = Fe^{i\Phi}$ evaluated at the third-harmonic $k_3 = \omega_3/c = 3\omega_1/c$, and ψ is the HHC tuning angle (see Appendix A). The second is

$$V_{3,1}(z;\rho_1) = -I_{\text{avg}}e^{-i\Omega t}\sum_{p=-\infty}^{\infty}\tilde{\rho}_1(\omega_{p,\ell})Z(\omega_{p,\ell}+\Omega)e^{-i\omega_{p,\ell}z/c}, \tag{4}$$

where $Z(\omega)$ is the HHC fundamental-mode impedance, $\tilde{\rho}_1$ is the Fourier integral of $\rho_1(z)$, and $\omega_{p,\ell} = (ph + \ell)\omega_0$, with $\ell = 0, 1, \ldots, h - 1$ being the instability coupled-bunch mode number of interest (for a justification of this expression, see [5,6,17–19]). For brevity we will write ω_p without the mode index and introduce the notation $\hat{\omega}_p = \omega_p + \Omega$. The sum in (4) extends to $\pm\infty$ but because Z is narrowband centered in a neighborhood of ω_3, to very good approximation it can be restricted to $p = \pm 3$. We then write the total rf potential as the sum of zero- and first-order terms $V_{\text{rf}}(z) = V_{\text{rf},0}(z;\rho_0) + V_{\text{rf},1}(z;\rho_1)$, with $V_{\text{rf},1}(z;\rho_1) = V_{3,1}(z;\rho_1)$.

The equations of motion are canonical with Hamiltonian $\mathcal{H} = \alpha c \delta^2/2 + \mathcal{U}(z)$ and potential $\mathcal{U}(z) = \mathcal{U}_0(z) + \mathcal{U}_1(z)$, with

$$\mathcal{U}_0(z) = -\int^z \frac{eV_{\text{rf},0}(z';\rho_0) - U_0}{E_0 T_0}dz', \tag{5}$$

$$\mathcal{U}_1(z) = -\int^z \frac{eV_{\text{rf},1}(z';\rho_1)}{E_0 T_0}dz'. \tag{6}$$

Similarly, we decompose the Hamiltonian as $\mathcal{H} = \mathcal{H}_0 + \mathcal{H}_1$, with $\mathcal{H}_0 = \alpha c \delta^2/2 + \mathcal{U}_0(z)$ and $\mathcal{H}_1 = \mathcal{U}_1(z)$.

Having introduced the action/angle variables (J, φ) for the unperturbed motion and used the corresponding canonical transformation to change the variables $(z, \delta) \to (J, \varphi)$ in the perturbed system (in the following $z = \zeta(J, \varphi)$ will denote the spacial coordinate part of this transformation), the Vlasov equation for the beam phase-space distribution reads

$$\frac{\partial\Psi}{\partial t} + \frac{\partial\Psi}{\partial\varphi}\frac{\partial\mathcal{H}}{\partial J} - \frac{\partial\Psi}{\partial J}\frac{\partial\mathcal{H}}{\partial\varphi} = 0. \tag{7}$$

Through first order

$$\frac{\partial\Psi_0}{\partial\varphi}\frac{\partial\mathcal{H}_0}{\partial J} - \frac{\partial\Psi_0}{\partial J}\frac{\partial\mathcal{H}_0}{\partial\varphi} = 0, \tag{8}$$

$$\frac{\partial\Psi_1}{\partial t} + \frac{\partial\Psi_1}{\partial\varphi}\frac{\partial\mathcal{H}_0}{\partial J} - \frac{\partial\Psi_0}{\partial J}\frac{\partial\mathcal{H}_1}{\partial\varphi} = 0. \tag{9}$$

Any function Ψ_0 of $\mathcal{H}_0$ solves (8) and is an equilibrium. The physical equilibrium in an electron storage ring has the particular form

$$\Psi_0 = Ae^{-\mathcal{H}_0/\beta}, \tag{10}$$

where A is a normalization constant and β is determined so as to yield the thermal distribution $\sim e^{-\delta^2/2\sigma_\delta^2}$ in energy deviation, with σ_δ being the natural rms energy spread. From inspection of the kinetic part of the Hamiltonian we infer $\beta = \alpha c \sigma_\delta^2$ and therefore $\Psi_0 = A e^{-\delta^2/2\sigma_\delta^2} e^{-\mathcal{U}_0(z)/\alpha c \sigma_\delta^2} = (\sqrt{2\pi}\sigma_\delta)^{-1} e^{-\delta^2/2\sigma_\delta^2} \rho_0(z)$ where

$$\rho_0(z) = \frac{e^{-\mathcal{U}_0(z)/\alpha c \sigma_\delta^2}}{\int e^{-\mathcal{U}_0(z')/\alpha c \sigma_\delta^2} dz'}, \qquad (11)$$

has normalization $\int \rho_0(z)dz = 1$. Note that (11) is a nontrivial equation since the HHC part of the potential $\mathcal{U}_0(z)$ depends on $\rho_0(z)$ through F and Φ [20], see Appendix B. Write $\Psi = \Psi_0 + e^{-i\Omega t}\Psi_1$ and the linearized equation (9) becomes

$$-i\Omega\Psi_1 + \omega_s \frac{\partial \Psi_1}{\partial \varphi} - \frac{\partial \Psi_0}{\partial J}\frac{\partial \mathcal{H}_1}{\partial \varphi} = 0, \qquad (12)$$

where $\omega_s = \omega_s(J) = \partial \mathcal{H}_0/\partial J$ is the synchrotron oscillation frequency. Representing the perturbation $\Psi_1(\varphi, J; \Omega) = \sum_{m'=-\infty}^{\infty} R_{m'}(J) e^{im'\varphi}$ as a series of azimuthal modes, we have

$$\frac{\partial \mathcal{H}_1}{\partial \varphi} = -\frac{eV_{\mathrm{rf},1}(\zeta;\rho_1)}{E_0 T_0}\frac{d\zeta}{d\varphi}$$
$$= \frac{eI_{\mathrm{avg}}}{E_0 T_0}\sum_{p=\pm 3}\tilde{\rho}_1(\omega_p)Z(\hat{\omega}_p)\frac{c}{-i\omega_p}\frac{d}{d\varphi}e^{-i\omega_p\zeta/c}, \qquad (13)$$

yielding

$$-i\sum_{m=l-\infty}^{\infty}(\Omega - m'\omega_s)R_{m'}e^{im'\varphi}$$
$$- \frac{eI_{\mathrm{avg}}}{E_0 T_0}\frac{\partial \Psi_0}{\partial J}\sum_{p=\pm 3}\tilde{\rho}_1(\omega_p)Z(\hat{\omega}_p)\frac{c}{-i\omega_p}\frac{d}{d\varphi}e^{-i\omega_p\zeta/c} = 0, \qquad (14)$$

with

$$\tilde{\rho}_1(\omega) = \int_{-\infty}^{\infty}dz e^{i(\omega/c)z}\rho_1(z) = \int_{-\infty}^{\infty}dz d\delta e^{i(\omega/c)z}\Psi_1(z,\delta)$$
$$= \sum_{m'=-\infty}^{\infty}\int_0^{\infty}dJ' R_{m'}(J')\int_0^{2\pi}d\varphi' e^{i\omega\zeta(J',\varphi')/c}e^{im'\varphi'}. \qquad (15)$$

Upon multiplying by $e^{-im\varphi}$, integrating over φ, and defining the following functions involving the canonical transformation ζ (see, e.g., Mosnier [14])

$$H_{m,p}(J) = \frac{1}{2\pi}\int_0^{2\pi} e^{im\varphi + i\omega_p\zeta(J,\varphi)/c}d\varphi, \qquad (16)$$

we finally write:

$$(\Omega - m\omega_s)R_m + 2\pi im\frac{eI_{\mathrm{avg}}}{E_0 T_0}\frac{\partial \Psi_0}{\partial J}\sum_{p'=\pm 3}\frac{cZ(\hat{\omega}_{p'})}{\omega_{p'}}H^*_{m,p'}(J)$$
$$\times \sum_{m'=-\infty}^{\infty}\int_0^{\infty}dJ' R_{m'}(J')H_{m',p'}(J') = 0. \qquad (17)$$

For later convenience, we have renamed the index $p \to p'$.

III. DISPERSION-RELATION EQUATION

In (17) multiply by $H_{m,p}(J)$, divide by $(\Omega - m\omega_s)$ and integrate over J to find

$$\int_0^{\infty}dJR_m(J)H_{m,p}(J) + 2\pi im\frac{eI_{\mathrm{avg}}}{E_0 T_0}\sum_{p'=\pm 3}\frac{cZ(\hat{\omega}_{p'})}{\omega_{p'}}G_{m;p,p'}(\Omega)$$
$$\times \sum_{m'=-\infty}^{\infty}\int_0^{\infty}dJ' R_{m'}(J')H_{m',p'}(J') = 0, \qquad (18)$$

where

$$G_{m;p,p'}(\Omega) = \int_0^{\infty}dJ\frac{H_{m,p}(J)H^*_{m,p'}(J)}{\Omega - m\omega_s(J)}\frac{\partial \Psi_0(J)}{\partial J}. \qquad (19)$$

In its form, Eq. (19) is strictly valid for Im $\Omega > 0$ (unstable modes); it can be extended to the whole complex plane by analytic continuation but for our purposes this will not be necessary.

Upon truncating the sum on m', Eq. (18) reduces to a $2(2m_{\mathrm{max}} + 1)$ system of linear equations in the form

$$\sum_{m=-m_{\mathrm{max}}}^{m_{\mathrm{max}}}\sum_{p'=\pm 3}B_{m,m';p,p'}(\Omega)X_{m',p'} = 0 \qquad (20)$$

with $X_{m,p} = \int_0^{\infty}dJR_m(J)H_{m,p}(J)$ and

$$B_{m,m';p,p'}(\Omega) = \delta_{m,m'}\delta_{p,p'} + 2\pi im\frac{eI_{\mathrm{avg}}}{E_0 T_0}\frac{cZ(\hat{\omega}_{p'})}{\omega_{p'}}G_{m;p,p'}(\Omega), \qquad (21)$$

being the entries of the $2(2m_{\mathrm{max}} + 1) \times 2(2m_{\mathrm{max}} + 1)$ dimensional square matrix B, leading to the dispersion-relation equation

$$\det \boldsymbol{B}(\Omega) = 0. \qquad (22)$$

An alternative approach, not adopted here but useful if we are interested in determining the form of the eigenfunctions, is to introduce $S_m(J) = [\Omega - m\omega_s(J)]R_m(J)[\frac{\partial \Psi_0}{\partial J}]^{-1}$ and rewrite

TABLE I.   ALS-U v20r lattice parameters.

Ring circumference	C	196.5 m
Revolution frequency	$\omega_0/2\pi$	1.526 MHz
Beam energy	E_0	2 GeV
Average current	I_{avg}	500 mA
Momentum compaction	α	2.11×10^{-4}
Natural energy spread	σ_δ	0.943×10^{-3}
Energy loss per turn	U_0	0.217 MeV
Synchronous phase (no HHCs)	ϕ_1	158.784 deg
Harmonic number	h	328
Main rf cavity generator frequency	$\omega_1/2\pi$	500.417 MHz
3rd-harmonic frequency	$\omega_3/2\pi$	1501.251 MHz
Main cavity voltage	V_{10}	0.6 MV
Natural rms bunch length (no HHCs)	σ_{z0}	3.54 mm
Synchrotron oscillation tune (no HHCs)	ν_{s0}	1.75×10^{-3}
Synchrotron oscillation frequency (no HHCs)	$\omega_{s0}/2\pi$	2.68 kHz
Longitudinal radiation damping time	τ_z	14 ms

$$S_m(J) + 2\pi i m \frac{e I_{\text{avg}}}{E_0 T_0} \sum_{p'=\pm 3} \frac{c Z(\hat{\omega}_{p'})}{\omega_{p'}} H_m^*(J, \omega_{p'})$$

$$\times \sum_{m'=-\infty}^{\infty} \int_0^\infty dJ' \frac{S_{m'}(J') H_{m'}(J', \omega_{p'})}{\Omega - m\omega_s(J')} \frac{\partial \Psi_0(J')}{\partial J'} = 0, \quad (23)$$

and then proceed with a discretization of $S(J)$ on a grid [15].

Equation (22) is solved numerically searching for roots with positive imaginary part for the $\ell = 0$ and $\ell = 1$ modes over a range of tuning angles ψ. Finding the numerical solution entails determining the equilibrium $\rho_0(z)$ and associated potential $\mathcal{U}_0(z)$ (Appendix B); and synchrotron frequency $\omega_s(J_i)$, Hamiltonian $\mathcal{H}_{0,i} = \int_0^{J_i} \omega_s(J') dJ'$, and canonical transformation $\zeta(J_i, \varphi)$ on a grid J_i, (see Appendix C). As a technical aside, the integral in (19) is best computed after a change of integration variable from J to $r \equiv z_R = \zeta(J, 0)$, where z_R is the

coordinate of the right turning point of the unperturbed orbit with action J.

The solutions, based on the ALS-U machine and HHC parameters of Tables I and II, are shown in Fig. 1 indicating a large $\ell = 1$ mode instability growth rate of about 5 ms^{-1}, for the design $\psi = 86.5^o$ working point yielding the desired bunch length. The dashed curve in the bottom right picture is the approximate asymptotic expression (49) derived later in Sec. IV B; the solid line is the expression (32), which applies to the limit where the HHCs are effectively turned off. In the bottom-left picture the solid line is Eq. (45), seen to track the numerical result very closely over the entire tuning angle range (we will get back to this point). For later consideration, notice that the ratio ImΩ/ReΩ is much smaller (larger) than unity for $\ell = 0$ ($\ell = 1$).

We expect coupled-bunch mode $\ell = h - 1$ (or equivalently $\ell = -1$) to have a similar growth rate as $\ell = 1$. As for the higher order modes $\ell > 1$ we expect them to lead to weaker (if any) instabilities since the beam-spectrum lines $\omega_3 \pm \ell \omega_0$ probe the impedance tails farther away from the resonance peak (see Fig. 6).

The bunch profiles for various HHC tuning are shown in Fig. 2, while Fig. 3 highlights the bunch profile for the nominal settings and related quantities of interest. The numerical calculation was done by retaining only the $|m| = 1$ dipole components; we verified that including the quadrupole components $|m| = 2$ changes the results only slightly.

In the next section we specialize the calculation to the dipole approximation and consider two limiting cases. One where the HHCs are absent (quadratic potential) and the other where they have optimum settings. We represent the rf potential in the second case as a pure quartic and use a simplified analytical expression for the canonical transformation to derive the approximate dispersion-relation equation in the form found in the literature. We solve this equation numerically and we work out asymptotic approximations to the solutions to gain insight into how the impedance relates to the instability.

TABLE II.   HHC design options and settings.

|		Two ALS HHCs	Optimal HHCs
HHC (total) shunt impedance (MΩ)	R_s	3.4	1.35
HHC Q-factor	Q	21,000	20,000
HHC tuning angle (rad/deg)	ψ	$1.5097/86.5^o$	$1.4188/81.29^o$
HHC resonance frequency (MHz)	$\omega_r/2\pi$	1501.835	1501.496
HHC tuning (kHz)	$(\omega_r - 3\omega_1)/2\pi$	584	245
HHC (total) power loss (kW)	P	5.1	12.6
Rms bunch length (mm)	σ_z	14.7	14.24
Average synchrotron oscillation freq. (kHz)	$\langle\omega_s\rangle/2\pi$	0.568	0.536
Average synchrotron oscillation tune	$\langle\nu_s\rangle$	3.7×10^{-4}	3.5×10^{-4}
Form factor amplitude	F	0.897	0.903
Form factor phase	Φ	-0.3	-4.5×10^{-3}
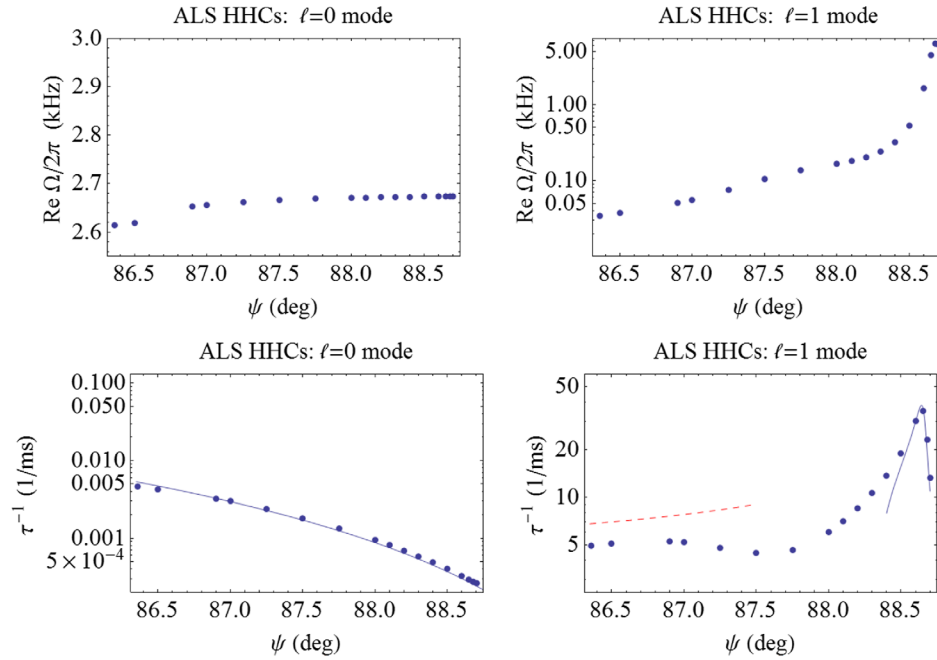
FIG. 1. The two pictures on the right capture the main result of this paper. Shown are the real (top) and imaginary $\text{Im}\,\Omega \equiv \tau^{-1}$ part (bottom) of the complex-number frequency for mode $\ell = 1$ if two of the existing ALS HHCs are to be used in ALS-U. The quantities are plotted vs. the tuning angle $\psi = 2Q(\omega_r - \omega_3)/\omega_3$. The lower end in the tuning angle $\psi = 86.5^o$, where the HHCs would be expected to operate, corresponds to about a factor 4 bunch lengthening. At that setting, the growth rate of the instability is about 5 ms^{-1} (or 0.2 ms growth time) while the oscillation frequency is less than 50 Hz (or 20 ms period); the large disparity between the two characteristic times places the instability out of reach of existing longitudinal feedback system. The pictures to the left are for the much more benign $\ell = 0$ (Robinson's) instability. Note that for this instability the oscillation frequency of the mode remains very close to the synchrotron oscillation frequency in the absence of HHCs (about 2.7 kHz, see Table I). See the text for the meaning of the curves in the bottom pictures.
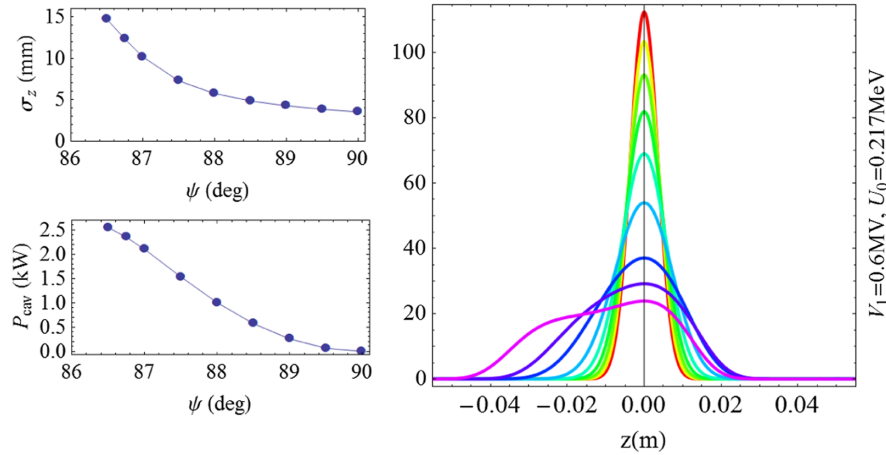

FIG. 2. Equilibrium bunch profiles in the presence of two ALS HHCs in ALS-U for various tuning (right), the corresponding rms bunch length (top left), and power dissipated by each cavity (bottom left).

IV. DIPOLE APPROXIMATION

Introduce the usual definition of effective impedance $Z_{\text{eff}}(\Omega) = \sum_{p=\pm 3} \frac{\omega_{p,\ell}}{\omega_1} Z(\omega_{p,\ell} + \Omega)$, see Appendix D. Noting $H_{m,p}^* \simeq H_{m,-p}$ and $H_{-m,p} = H_{m,-p}$ as $\zeta(\varphi)$ is an

even function, retaining only the dipole $|m| = 1$ terms, and as explained in Appendix D approximating $\omega_{\pm 3,\ell} \simeq \pm 3\omega_1$ unless $\omega_{\pm 3,\ell}$ appears in the argument of Z, it can be shown that the dispersion relation reads
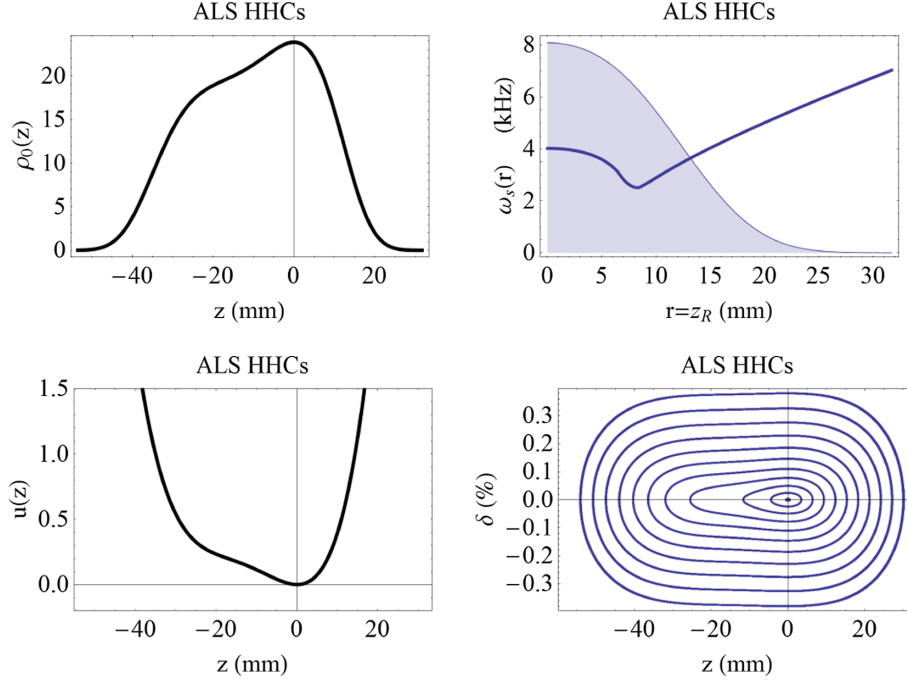
FIG. 3.   Two ALS HHCs at nominal setting ($\psi = 86.5$ deg). Bunch equilibrium profile (top left), scaled rf potential Eq. (B2) (bottom left), synchrotron oscillation frequency $\omega_s(r)$ with the bunch equilibrium profile $\Psi_0(r)$ in the background as a function of the amplitude variable r (top right), and phase space in the rf bucket for a few representative particle orbits (bottom right).

$$1+4\pi i\frac{eI_{\text{avg}}cZ_{\text{eff}}(\Omega)}{9E_0T_0\omega_1}\int_0^\infty dJ\frac{\partial\Psi_0(J)}{\partial J}\frac{|H_{1,3}(J)|^2\omega_s(J)}{\Omega^2-\omega_s(J)^2}=0. \tag{24}$$

In particular, for short bunches $\omega_3\zeta/c \ll 1$:

$$H_{1,3}(J)\simeq\frac{1}{2\pi}\int_0^{2\pi}e^{i\varphi}[1+i\omega_3\zeta/c]d\varphi\equiv\frac{i\omega_3}{c}\tilde{\zeta}_1(J), \tag{25}$$

where $\tilde{\zeta}_m(J)=(2\pi)^{-1}\int_0^{2\pi}e^{im\varphi}\zeta(J,\varphi)d\varphi$ is the Fourier integral of the canonical transformation. The dispersion-relation equation then reduces to

$$1+4\pi i\frac{eI_{\text{avg}}\omega_1Z_{\text{eff}}(\Omega)}{E_0C}\int_0^\infty dJ\frac{\partial\Psi_0(J)}{\partial J}\frac{\tilde{\zeta}_1^2(J)\omega_s(J)}{\Omega^2-\omega_s^2(J)}=0. \tag{26}$$

A. Quadratic potential

In the absence of harmonic cavities, the synchrotron frequency is amplitude-independent $\omega_s(J)=\omega_{s0}$, with the bunch equilibrium having the form of a gaussian. The relevant part of the canonical transformation to action/angle variable is $z=\zeta(J,\varphi)=\sqrt{Jac/\omega_{s0}}\cos\varphi$, yielding $\tilde{\zeta}_1(J)=\sqrt{Jac/\omega_{s0}}/4\pi$, and the dispersion equation (26) becomes

$$1+4\pi i\frac{eI_{\text{avg}}\omega_1Z_{\text{eff}}(\Omega)}{E_0C}\frac{\alpha c}{\Omega^2-\omega_{s0}^2}\int_0^\infty dJ\frac{\partial\Psi_0(J)}{\partial J}J=0, \tag{27}$$

or equivalently, since $\int_0^\infty dJ\Psi_0'(J)J=-\int_0^\infty dJ\Psi_0(J)=-1$,

$$\Omega^2=\omega_{s0}^2+i\hat{I}_GZ_{\text{eff}}(\Omega), \tag{28}$$

having defined the current parameter

$$\hat{I}_G=\frac{eI_{\text{avg}}\omega_1\alpha}{E_0T_0}. \tag{29}$$

Consider two limiting cases depending on whether the imaginary part Ω_i of the complex mode frequency $\Omega=\Omega_r+i\Omega_i$ is much larger or smaller than the real part Ω_r: (1) Case $\Omega_i\ll\Omega_r$. We have $\Omega_r^2+2i\Omega_i\Omega_r-\omega_{s0}^2\simeq\hat{I}_G(i\text{Re}Z_{\text{eff}}-\text{Im}Z_{\text{eff}})$ and therefore

$$\Omega_r^2=\omega_{s0}^2-\hat{I}_G\text{Im}Z_{\text{eff}}, \tag{30}$$

$$\Omega_i=\frac{\hat{I}_G}{2\Omega_r}\text{Re}Z_{\text{eff}}. \tag{31}$$

If the detuning is small, we recover Sacherer's equations in the short-bunch limit (see [9,21]), $\Omega_r\simeq\omega_{s0}$ and $\Omega_i\simeq\frac{\hat{I}_G}{2\omega_{s0}}\text{Re}Z_{\text{eff}}(\omega_{s0})$. (2) Case $\Omega_i\gg\Omega_r$. We have $2i\Omega_i\Omega_r-\Omega_i^2-\omega_{s0}^2\simeq\hat{I}_G(i\text{Re}Z_{\text{eff}}-\text{Im}Z_{\text{eff}})$ and therefore (assuming $\text{Im}Z_{\text{eff}}>0$)
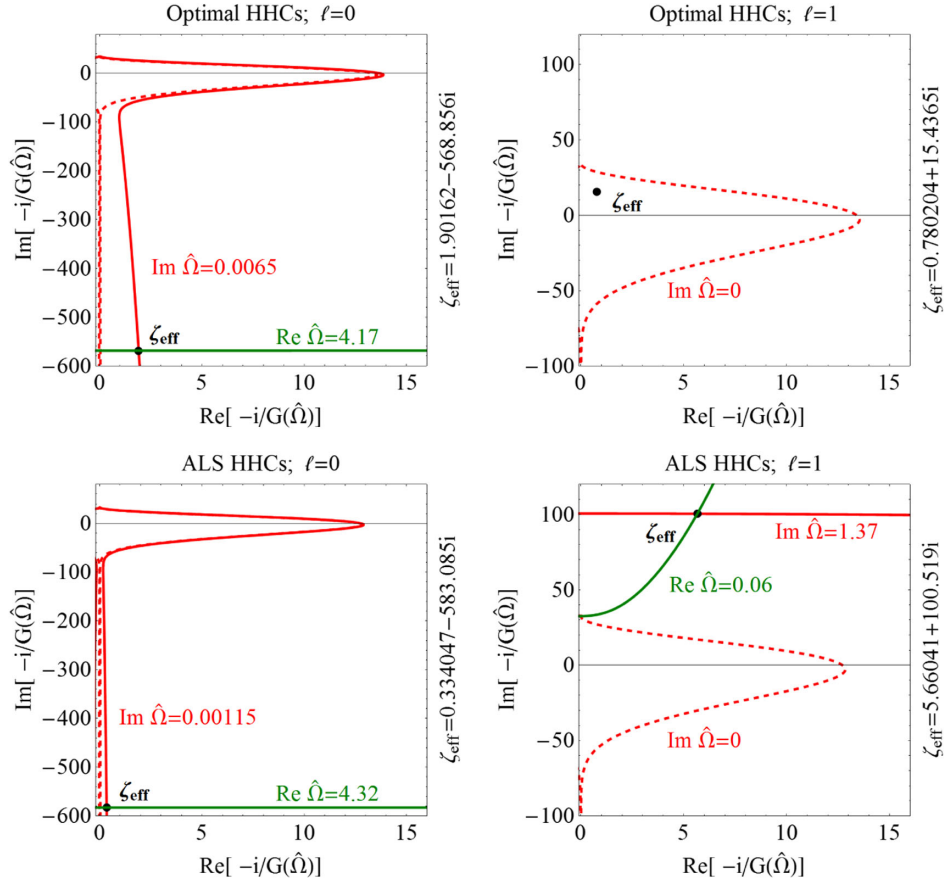
FIG. 4. Keil-Schnell diagrams representing the complex-number frequency solutions of the dispersion-relation equation Eq. (38) for mode $\ell = 0$ (left) and $\ell = 1$ (right) for optimum HHCs (top). Equation (38) is derived from a quartic potential model but we also try to apply it to the two ALS HHC case (bottom pictures) and find estimates that are within 10% of the more accurate results of Sec. III. A mode with impedance parameter ζ_{eff} defined in (37) is stable (Landau damping) if ζ_{eff} falls within the region delimited by the dashed curve containing the origin: this is the case for the $\ell = 1$ mode in the presence of optimum HHCs (top-right picture). The values appearing in the pictures are for the scaled frequency $\hat{\Omega}$ defined in Eq. (35); for the corresponding values in physical units see Table III.

$$\Omega_i^2 = \hat{I}_G \text{Im} Z_{\text{eff}} - \omega_{s0}^2, \qquad (32)$$

$$\Omega_r = \frac{\hat{I}_G}{2\Omega_i} \text{Re} Z_{\text{eff}}. \qquad (33)$$

B. Quartic potential (approximate canonical transformation)

1. Exact numerical solution to the approximate dispersion-relation equation

In a purely quartic potential the transformation from canonical to physical coordinates has the approximate form $z = r(J) \cos \varphi$ with $r(J)$ given by (E2) being a function of J only; the approximation (amounting to neglecting φ-harmonics of $\zeta(J, \varphi)$ of order higher than one), is accurate within 4–5% [6]. With this, the function $H_{1,3}(J) = iJ_1(k_3 r(J))$ reduces to a Bessel function of the first kind J_1. After a change of integration variable, the dispersion-relation equation reads

$$1 - i\frac{64\pi}{9\Gamma_{1/4}^3} \frac{eI_{\text{avg}}\alpha\omega_1}{E_0 T_0 \langle\omega_s\rangle^2 (\sigma_z k_1)^2} Z_{\text{eff}}(\Omega)$$

$$\times \int_0^\infty dx \frac{x^4 J_1^2(c_1 x)e^{-x^4}}{\hat{\Omega}^2 - x^2} = 0, \qquad (34)$$

where $c_1 = \frac{3\Gamma_{1/4}}{2^{1/4}\sqrt{\pi}} k_1\sigma_z \simeq 5.16 k_1\sigma_z$, we have made use of the expression (E5) for the equilibrium, introduced the dimensionless scaled mode frequency (Appendix E)

$$\hat{\Omega} = \frac{\Gamma_{1/4}}{2^{1/2}\pi} \frac{\Omega}{\langle\omega_s\rangle} \simeq 0.816 \times \frac{\Omega}{\langle\omega_s\rangle}, \qquad (35)$$

and used the notation $\Gamma_{1/4} \equiv \Gamma(1/4)$ for the Euler gamma function. This is the equation usually found in the literature in connection with HHCs, (in this form or with the additional short-bunch approximation $J_1(c_1 x) \simeq c_1 x/2$). Note that some authors present a version that differs from (34) in that only the $m = +1$ term is included in the derivation (with the result that the denominator in the

integrand is linear rather than quadratic in x); as pointed out in [5,6] both $m = \pm 1$ should be included. Define

$$G(\hat{\Omega}) = \int_0^\infty dx \frac{x^4 J_1^2(c_1 x) e^{-x^4}}{\hat{\Omega}^2 - x^2}, \qquad (36)$$

and introduce the dimensionless effective-impedance parameter

$$\zeta_{\rm eff}(\hat{\Omega}) = \frac{64\pi}{9\Gamma_{1/4}^3} \frac{e I_{\rm avg} \alpha \omega_1}{E_0 T_0 \langle \omega_s \rangle^2 (\sigma_z k_1)^2} Z_{\rm eff}\left(\frac{\langle \omega_s \rangle \hat{\Omega}}{0.816}\right), \qquad (37)$$

to write the dispersion-relation equation (34) in the form

$$\frac{-i}{G(\hat{\Omega})} = \zeta_{\rm eff}(\hat{\Omega}). \qquad (38)$$

We solve (38) numerically to study the $\ell = 0$, 1 modes for optimum HHCs and represent the solutions by Keil-Schnell diagrams, top pictures in Fig. 4.

In these plots, the solid red curves are drawn by letting Re $\hat{\Omega}$ vary in $[-\infty, \infty]$ while Im $\hat{\Omega}$ is set to the imaginary part of the numerical solution, as indicated. Similarly, the green curves are drawn by letting Im $\hat{\Omega}$ vary in $[0, \infty]$ while Re $\hat{\Omega}$ is set to the real part of the numerical solution as indicated, so that the solutions are at the intersection of the red and green curves. The red dashed curve, corresponding to Im $\hat{\Omega} = 0$ is the stability boundary: if $\zeta_{\rm eff}$ falls within the region containing the origin, as in the top-right picture, the mode is stable (Landau damping) [22].

We also make an attempt to apply (38) to the study of the two nonoptimum ALS HHCs (bottom figures in Fig. 4). In the calculation we used $\sigma_z = 14.7$ mm as determined from the exact equilibrium and then estimated $\langle \omega_s \rangle$ using Eq. (E6). We found results that are within 10% of the more accurate solution obtained in Sec. III, see summary in Table III. In the next section, we will then feel encouraged to employ (38) as a basis to work out analytical asymptotic expressions for studying the solutions in both the optimum and nonoptimum HHC cases.

From the table, also notice that the Robinson ($\ell = 0$) instability is considerably larger in the optimum HHC case, but still slow enough to be radiation damped (the radiation damping time being $\tau_z = 14$ ms).

TABLE III. Numerical solutions of the approximate dispersion-relation equation (38).

	Optimal HHCs		Two ALS HHCs	
	Re $\Omega/2\pi$ (kHz)	τ^{-1} (ms^{-1})	Re $\Omega/2\pi$ (kHz)	τ^{-1} (ms^{-1})
$\ell = 0$	2.7	0.027	2.7	0.0046
$\ell = 1$	$\cdots$	$\cdots$	0.038	5.5

2. Asymptotic analytical solution to the approximate dispersion-relation equation

Under the assumption $|\hat{\Omega}| \gg 1$, we approximate the denominator in the integrand of (36) as $\hat{\Omega}^2 - x^2 \simeq \hat{\Omega}^2$ and write

$$G(\hat{\Omega}) \simeq \frac{1}{\hat{\Omega}^2} \int_0^\infty dx\, x^4 J_1^2(c_1 x) e^{-x^4}$$
$$= \frac{1}{\hat{\Omega}^2} \frac{c_1^2}{16} \Gamma_{5/4}\left(1 - c_1^2 \frac{\Gamma_{7/4}}{\Gamma_{5/4}}\right), \qquad (39)$$

having expanded the square of the Bessel function through fourth order, in order to find the dispersion-relation equation for the asymptotic approximation to the solution. In terms of Ω, the mode frequency in physical units, Eq. (38) reads

$$\Omega^2 \simeq i\hat{I} Z_{\rm eff}(\Omega), \qquad (40)$$

with current parameter defined as

$$\hat{I} = \frac{\sqrt{2}\pi^2}{\Gamma_{1/4}^2} \frac{e I_{\rm avg} \alpha \omega_1}{E_0 T_0}\left(1 - \frac{27}{4} k_1^2 \sigma_z^2\right), \qquad (41)$$

where $\sqrt{2}\pi^2/\Gamma_{1/4}^2 \simeq 1.06$. Next, write $\Omega = \Omega_r + i\Omega_i$ and consider the following two subcases. (1) Case $\Omega_i \ll \Omega_r$. Relevant for mode $\ell = 0$. We have $\Omega_r^2 + 2i\Omega_r\Omega_i \simeq i\hat{I}{\rm Re}Z_{\rm eff} - \hat{I}{\rm Im}Z_{\rm eff}$, and therefore

$$\Omega_r^2 \simeq -\hat{I}{\rm Im}Z_{\rm eff}, \qquad (42)$$

$$\Omega_i \simeq \frac{\hat{I}}{2\Omega_r}{\rm Re}Z_{\rm eff}. \qquad (43)$$

Specifically, for $\ell = 0$ (see Appendix D)

$$\Omega_r^2 \simeq 3\hat{I}R_s \sin(2\psi), \qquad (44)$$

$$\Omega_i \simeq \frac{2\hat{I}}{\omega_1} R_s Q\cos^2\psi \sin(2\psi). \qquad (45)$$

It turns out that for $\ell = 0$ and optimum HHCs, it is always $|\hat{\Omega}| \gg 1$, thus making the asymptotic analytic expression (45) always valid. To show this, make use of (B8) with Φ set to zero to find $3 \sin 2\psi = V_1 |\cos \phi_1|/(I_{\rm agv} R_s F)$, insert in (44), and recall (35) to find

$$\hat{\Omega}_r^2 = \frac{3\Gamma_{1/4}^2}{2^{3/2}\pi^2} \frac{1}{F k_1^2 \sigma_z^2}\left(1 - \frac{27}{4} k_1^2 \sigma_z^2\right). \qquad (46)$$

Since F is on the order of unity and in electron machines $k_1 \sigma_z$ is naturally small, $\hat{\Omega}_r$ and hence $\hat{\Omega}$ are significantly larger than unity (for ALS-U, $k_1 \sigma_z \simeq 0.15$ and $\hat{\Omega}_r^2 \simeq 60$).
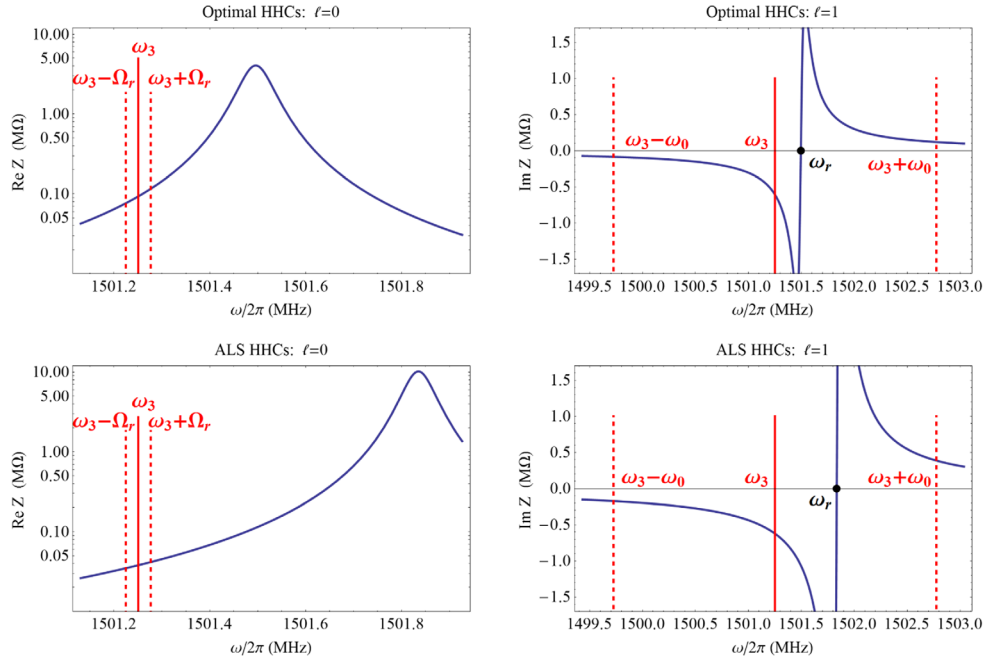
FIG. 5. Comparing the instability drivers for the $\ell = 0$ (left) and $\ell = 1$ (right) mode instability. For the $\ell = 0$ mode it is the real part of the HHC fundamental mode impedance to be relevant and the instability growth rate depends on the difference between the values of Re Z on the upper $\omega_3 + \Omega_r$ and lower $\omega_3 - \Omega_r$ sidebands, where Ω_r is the (real) mode oscillation frequency, divided by Ω_r or, effectively, the derivative of Re Z at $\omega = \omega_3$. The pictures indicate that the Re Z (positive) slope for the optimum HHCs (top) is larger than that for the ALS HHCs (bottom) and therefore the instability higher. (For better illustration, in the picture Ω_r is not to scale.) In contrast, for mode $\ell = 1$, in the regime where the asymptotic approximation (47), (49) applies, it is ImZ to be relevant: the growth rate is proportional to the square root of the algebraic sum of the two contributions $-(3/2)R_s \sin(2\psi_1)$ and $-(3/2)R_s \sin(2\psi_{-1})$ at $\omega_3 + \omega_0$ and $\omega_3 - \omega_0$ respectively, see Eq. (D5). When the resonance frequency ω_r is to the right of ω_3 (this is where HHCs are operated for bunch lengthening), the sum is always positive but it is much larger for the ALS HHCs (bottom-right picture) since these are tuned further away from ω_3. In fact, for optimum HHCs that sum is small enough for Landau damping to suppress the instability (see the top-right picture in Fig. 4).

Equation (45) is an improvement in accuracy (albeit small, about 10% for ALS-U size bunches) over, e.g., Eq. (8.115) in [18]. Also, notice that it tracks remarkably well the $\ell = 0$ mode growth rate for nonoptimum HHCs over the whole tuning range, (solid curve in the bottom-left picture of Fig. 1). (2) Case $\Omega_r \ll \Omega_i$. This is relevant for mode $\ell = 1$ when using two ALS HHCs. We have $-\Omega_i^2 + 2i\Omega_r\Omega_i, \simeq i\hat{I}\text{Re}Z_{\text{eff}} - \hat{I}\text{Im}Z_{\text{eff}}$, and therefore (for $\text{Im}Z_{\text{eff}} > 0$)

$$\Omega_i^2 \simeq \hat{I}\text{Im}Z_{\text{eff}}, \qquad (47)$$

$$\Omega_r \simeq \frac{\hat{I}}{2\Omega_i}\text{Re}Z_{\text{eff}}. \qquad (48)$$

Specifically, for $\ell = 1$, see (Appendix D)

$$\Omega_i^2 \simeq -\frac{3}{2}\hat{I}R_s[\sin(2\psi_1) + \sin(2\psi_{-1})]. \qquad (49)$$

From Eq. (47), note that in this regime it is the imaginary, not the real, part of the impedance that drives the instability, see also Figs. 5 and 6 for a graphical explanation.

The accuracy of (49) as judged from Fig. 1, dashed curve, is not as good as that of (45) as $|\hat{\Omega}| \simeq 1.4$ is only marginally greater than unity and the asymptotic approximation not fully valid.
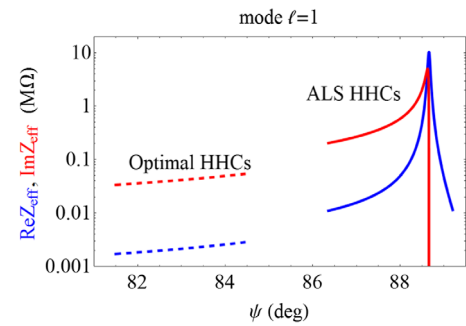

FIG. 6. Real (blue) and imaginary (red) part of the effective impedance for mode $\ell = 1$ for two ALS HHCs (solid) and optimum HHCs (dashed). The picture highlights how the ALS HHCs operating tuning range is at larger angles ψ (i.e., away from the resonance peak) compared to the optimum HHCs reflecting a larger shunt impedance. The left ends of the two ranges correspond to about a factor 4 lengthening in both cases. The larger ALS-HHC Im Z_{eff} is the reason for the higher sensitivity to the $\ell = 1$ mode instability.

We recognize that the asymptotic expressions derived here are very similar in form to those valid for a quadratic potential (previous section) with current parameter $\hat{I}_G$ replaced by $\hat{I}$. The two normalized current parameters are also very close

$$\hat{I} = \frac{\sqrt{2}\pi^2}{\Gamma_{1/4}^2}\left(1 - \frac{27}{4}k_1^2\sigma_z^2\right)\hat{I}_G$$

$$\simeq 1.06 \times \left(1 - \frac{27}{4}k_1^2\sigma_z^2\right)\hat{I}_G \simeq 0.9 \times \hat{I}_G, \quad (50)$$

having used $k_1\sigma_z \simeq 0.15$. In other terms, in the regime where the asymptotic approximation applies, the instability growth rates calculated using a Gaussian-profile approximation for the bunches are off by only 10%. We should note that this is the regime where Landau damping is absent.

This is a good place to pause and call attention to confusing statements on Landau damping occasionally found in the literature. Sometimes (e.g., [18], p. 333), a growth rate is first estimated invoking a quadratic form for the potential as in Sec. IV A, accompanied by the (correct) disclaimer that the naive derivation ignores Landau damping, with Landau then credited as yielding damping with a rate equal to some fraction of the system frequency spread, possibly restoring stability if the latter is large enough. Not always emphasized is the crucial qualification that in order for Landau damping to appear, the real part of the frequency of the mode of interest should overlap with the system natural frequency spread (here due to the rf bucket nonlinearities). In fact, this overlap does not occur for the HHC-induced Robinson instability since, as noticed in the comment made below Eq. (46), we always have $|\hat{\Omega}| \gg 1$.

In other words, (45) is an already accurate growth-rate estimate and Landau cannot be expected to come to the rescue (nor in this case would Landau's help be needed, since the combined main and higher-harmonic cavity system tends to be Robinson stable even before radiation damping is factored in). For instabilities other than Robinson's (e.g., due to HOMs) Landau damping from the HHC-induced synchrotron-oscillation frequency spread may or may not materialize, depending on the characteristics of the impedance and other relevant machine parameters. In fact, in many cases the presence of HHCs can aggravate the longitudinal instabilities, a known but not widely acknowledged fact [8,23,24]. On the other hand, the $\ell = 1$ mode damping found for optimal HHCs is an example where Landau damping is effective. Somewhat analogously, in the transverse plane HHCs help with damping instabilities in the presence of finite chromaticities [25] but may worsen the TMCI instability [26]. Further complicating the matter, we should add that there are other potential sources of Landau damping to multibunch longitudinal instabilities not considered here, like bunch-to-bunch synchrotron oscillation variations due to nonuniform beam filling [27,28].

V. SUMMARY AND CONCLUSIONS

In conclusion, we have shown that use of two of the existing ALS HHCs in the upgraded ALS can achieve the sought bunch lengthening but at the cost of driving a fast $\ell = 1$ longitudinal mode instability difficult to control. The reason is a shunt impedance of the two combined cavities significantly larger than the ALS-U optimum, forcing a large detuning that pushes the HHC fundamental mode to overlap with the $\omega_3 + \omega_0$ beam-spectrum line.

Short of installing a newly designed system, a conceivable solution to the problem is to add the third ALS HHC in the bunch-shortening mode (negative tuning angle $\psi < 0$) while the other two are retuned to maintain the desired bunch lengthening. This helps in two ways: it forces the resonance peak of the other two cavities closer to the 3rd-harmonic and creates a negative contribution to Im Z_{eff}, thus compensating the other two cavities' positive contribution. We have found a combination of tuning angles that would work in principle and result in complete (Landau) damping of the offensive mode. However, it remains to be determined if the solution is practical as the cavities power loss would be close to the limit. A more detailed discussion will be reported elsewhere.

While the relevance of the most immediate conclusion is somewhat restricted to the particular ALS/ALS-U circumstances, our study includes findings that are of more general interest. Summarizing, we have established: (i) a formula [Eq. (45)] that improves, albeit slightly, on the commonly found expression for the HHC-induced Robinson instability; (ii) that this instability is generally not Landau damped [Eq. (46)]; (iii) that the mode $\ell = 1$ may or may not be Landau damped depending on the HHC parameters and that in the case of interest the instability is driven by the imaginary rather than the real part of the impedance [Eq. (47)]; (iv) a consistent set of equations to frame the problem of determining the optimum HHC settings (Appendix B); (v) a simple formula for the power loss for optimum HHCs [Eq. (B14)].

We emphasize that the analysis of the $\ell = 1$ mode cannot be carried out using the familiar Sacherer's formulas (which relate the instability to the real part of the impedance [9,21]), and doing so would result in a large error.

Finally, our calculation was carried out under the assumption (not fulfilled by the ALS-U) of uniform beam filling. While we do not expect the presence of the eleven 10 ns gaps envisioned in the ALS-U beam for swap-out injection to alter the result substantially, it is possible that the presence of the gaps could have some stabilizing effect. This will be addressed in future studies. Also left to future work is the extension of mode analysis to include the relevant and desirable regime where the bunch is over-stretched (double-well rf potential), [29,30].

APPENDIX A: BEAM LOADING IN THE HHC

Coupling of the circulating beam with a passive cavity is modeled by the wake potential $W(t)$ and/or the corresponding impedance $Z(\omega)$:

$$W(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} d\omega e^{-i\omega t} Z(\omega). \qquad (A1)$$

Causality implies that $W(t) \neq 0$ only for $t \geq 0$. We assume the resonator model

$$Z(\omega) = \frac{R_s}{1 + iQ(\frac{\omega_r}{\omega} - \frac{\omega}{\omega_r})} \equiv R_s \cos\psi_\omega e^{-i\psi_\omega}, \qquad (A2)$$

with

$$\tan\psi_\omega = Q\left(\frac{\omega_r}{\omega} - \frac{\omega}{\omega_r}\right) \simeq 2Q\frac{\omega_r - \omega}{\omega_r}. \qquad (A3)$$

The effect of a passive HHC on beam dynamics is fully described by the shunt impedance R_s, quality factor Q, and resonant frequency ω_r. Notice our sign convention, where the tuning angle ψ_ω is positive for frequency ω below the cavity resonant frequency, $\omega < \omega_r$. To simplify notation in this section introduce $\tau = z/c$ in units of time to denote the longitudinal coordinate.

Assume the beam consists of a uniform train of bunches separated by $T_1 = T_0/h$ (all buckets are occupied), with identical profile $\rho(\tau)$ and N particles/bunch. The voltage experienced by a test particle with coordinate τ in one bunch is affected by the passage of that bunch and particles of other bunches that passed earlier:

$$V(\tau) = -eN \sum_{m=0}^{\infty} \int_{-\infty}^{\infty} d\tau' \rho(\tau') W(\tau - \tau' + mT_1), \quad (A4)$$

where the sign is consistent with $eV < 0$ indicating energy loss. Because of causality, the sum over m can be extended to $-\infty$ without changing the result. Using (A1) and

$$\rho(\tau) = \frac{1}{2\pi} \int_{-\infty}^{\infty} d\omega e^{-i\omega\tau} \tilde{\rho}(\omega) \qquad (A5)$$

into (A4) yields $V(\tau) = -eN(2\pi)^{-1} \sum_{m=-\infty}^{\infty} \int_{-\infty}^{\infty} d\omega \times \tilde{\rho}(\omega)e^{-i\omega(\tau+mT)}Z(\omega)$. Next, use the Poisson sum rule $\sum_{m=-\infty}^{\infty} e^{-im\omega T_1} = 2\pi \sum_{p=-\infty}^{\infty} \delta(\omega T_1 - 2\pi p)$ and obtain

$$V(\tau) = -I_{avg} \sum_{p=-\infty}^{\infty} \tilde{\rho}(\omega_1 p)Z(\omega_1 p)e^{-i\tau\omega_1 p} \quad (A6)$$

with $I_{avg} = eN/T_1$. Assuming the HHC resonance to be sufficiently narrow, only the terms $p = \pm 3$ (third-harmonic cavity) in the sum will contribute appreciably. Finally, making use of (A2) we conclude

$$\begin{aligned} V(\tau) &\simeq -I_{avg}[\tilde{\rho}(\omega_3)Z(\omega_3)e^{-i\omega_3\tau} + \text{c.c.}] \\ &= -2I_{avg}R_s F \cos\psi \cos(\omega_3\tau + \psi - \Phi), \quad (A7) \end{aligned}$$

having expressed the bunch form factor at the third harmonic frequency $\omega_3 = 3\omega_1$ in terms of amplitude and phase: $\tilde{\rho}(\omega_3) \equiv Fe^{i\Phi}$. In the above equation and throughout the paper $\psi \equiv \psi_{\omega_3}$ is the HHC tuning angle.

APPENDIX B: BEAM EQUILIBRIUM AND OPTIMUM HHC SETTINGS

At equilibrium the combined total rf voltage from main and higher-harmonic cavities is

$$\begin{aligned} V_{rf,0}(z; \rho_0) &= V_{10} \sin(k_1 z + \phi_1) \\ &\quad - 2I_{avg}R_s F \cos\psi \cos(k_3 z + \psi - \Phi). \quad (B1) \end{aligned}$$

Introduce the scaled potential $u(z; F, \Phi) = \mathcal{U}_0(z)/(\alpha c\sigma_\delta^2) = -\int^z [eV_{rf,0}(z'; \rho_0) - U_0]dz'/(\alpha c\sigma_\delta^2 E_0 T_0)$. In explicit form:

$$\begin{aligned} u(z; F, \Phi) &= u_1[\cos(k_1 z + \phi_1) - \cos\phi_1] \\ &\quad + u_3 \cos\psi[F \sin(k_3 z + \psi - \Phi) \\ &\quad - F \sin(\psi - \Phi)] + u_0 z, \quad (B2) \end{aligned}$$

with $\cos\phi_1 = -\sqrt{1 - \sin^2\phi_1}$, where $u_0 = U_0/(\alpha\sigma_\delta^2 E_0 C)$, $u_1 = eV_1/(\alpha\sigma_\delta^2 E_0 Ck_1)$, $u_3 = 2eI_{avg}R_s/(\alpha\sigma_\delta^2 E_0 Ck_3)$. The expression (11) for the bunch profile at equilibrium with normalization $\int \rho_0(z)dz = 1$ reads

$$\rho_0(z) = \frac{e^{-u(z;F,\Phi)}}{\int e^{-u(z';F,\Phi)}dz'}. \qquad (B3)$$

We choose the coordinate system so that $(z = 0, \delta = 0)$ corresponds to the synchronous particle at equilibrium. Energy balance for the synchronous particle requires $eV_{rf,0}(0; \rho_0) = U_0$, or from Eq. (B1)

$$V_{10} \sin\phi_1 = U_0 + 2I_{avg}R_s F \cos\psi \cos(\psi - \Phi). \quad (B4)$$

Equation (B3) can be regarded as a functional equation in the unknown $\rho_0(z)$, similar in form to a Haissinski equation or an algebraic equation in the two unknowns F and Φ. Adopting the latter interpretation we proceed to evaluate the FT of (B3) at $k = k_3$ and write

$$\tilde{\rho}_0(k_3) = \int e^{ik_3 z} \rho_0(z) dz = \frac{\int e^{ik_3 z} e^{-u(z;F,\Phi)} dz}{\int e^{-u(z;F,\Phi)} dz} \quad \text{(B5)}$$

or, after equating the real and imaginary parts of both sides,

$$F \cos \Phi = \frac{\int \cos(k_3 z) e^{-u(z;F,\Phi)} dz}{\int e^{-u(z;F,\Phi)} dz}, \quad \text{(B6)}$$

$$F \sin \Phi = \frac{\int \sin(k_3 z) e^{-u(z;F,\Phi)} dz}{\int e^{-u(z;F,\Phi)} dz}. \quad \text{(B7)}$$

For the given shunt impedance R_s and tuning angle ψ, Eq.'s (B6) and (B7) in combination with (B4) can be solved numerically for F, Φ, and ϕ_1. Optimally designed HHCs are defined as yielding an rf potential $V_{\rm rf,0}(z;\rho_0)$ with vanishing first and second derivative at $z = 0$, i.e.,

$$k_1 V_{10} \cos \phi_1 + 2I_{\rm avg} R_s F k_3 \cos \psi \sin(\psi - \Phi) = 0, \quad \text{(B8)}$$

$$-k_1^2 V_{10} \sin \phi_1 + 2I_{\rm avg} R_s F k_3^2 \cos \psi \cos(\psi - \Phi) = 0. \quad \text{(B9)}$$

The exact determination of the optimum settings entails the simultaneous numerical solution of the five equations (B4) and (B6)–(B9) for the five unknowns F, Φ, ϕ_1, R_s, and ψ. However, anticipating that the rf potential is accurately approximated by retaining only the quartic term (an even function, implying $\Phi = 0$), one can easily work out the following simple and fairly accurate analytical expressions. From (B6), expanding $\cos(k_3 z)$ through second order, $F \simeq \int [1 - (k_3 z)^2/2] \rho_0(z) dz = 1 - (k_3 \sigma_z)^2/2$, and from (B4), (B8), and (B9)

$$\sin \phi_1 = \frac{9}{8} \frac{U_0}{eV_{10}}, \quad \text{(B10)}$$

$$\tan \psi = \frac{3}{|\tan \phi_1|}, \quad \text{(B11)}$$

$$I_{\rm avg} R_s F = \frac{U_0/e}{16 \cos^2 \psi}, \quad \text{(B12)}$$

consistent with, e.g., [18]. For ALS-U parameters, with natural bunch length $\sigma_{z0} \simeq 3.5$ mm and bunch lengthening factor ~ 4 [see Eq. (E7) in Appendix E], we have $F \simeq 0.9$ and the optimum R_s can be quickly determined from (B12) once the tuning angle is derived from the two previous equations. To avoid confusion, note that (B12) is strictly valid only for ψ given by the optimal value (B11).

The beam power lost to the HHCs is calculated by averaging the voltage over a bunch and multiplying by the average circulating current

$$P_{\rm cav} = I_{\rm avg} \int V_{3,0}(z;\rho_0) \rho_0(z) dz$$
$$= 2I_{\rm avg}^2 R_s F^2 \cos^2 \psi, \quad \text{(B13)}$$

valid for arbitrary values of shunt impedance and tuning angle; the second equality follows from $\int dz \rho_0(z) \cos(k_3 z + \psi - \Phi) = F \cos \psi$. Interestingly, for optimum HHCs combining (B12) and (B13) yields the following handy formula exhibiting no explicit dependence on shunt impedance or tuning angle

$$P_{\rm cav} = I_{\rm avg} \frac{F(U_0/e)}{8} = \frac{F}{8} P_{\rm rad}, \quad \text{(B14)}$$

where $P_{\rm rad} = I_{\rm avg} U_0/e$ is the power lost to radiation. Observe that in the limit of vanishing radiation energy loss ($U_0 \to 0$), $P_{\rm cav}$ vanishes. In this limit, both the main and higher-harmonic cavities are operated at the zero-voltage crossing phase and in a bunch with symmetric profile as many particles lose as gain energy.

APPENDIX C: NUMERICAL DETERMINATION OF THE CANONICAL TRANSFORMATION

From the unperturbed Hamiltonian $\mathcal{H}_0 = \alpha c \delta^2/2 + u(z)\alpha c \sigma_\delta^2$ we derive the action variable:

$$J = \frac{1}{2\pi} \oint \delta(z) dz = \frac{1}{\pi} \int_{z_L}^{z_R} \left[\frac{2\mathcal{H}_0}{\alpha c} - 2u(z)\sigma_\delta^2 \right]^{-1/2} dz, \quad \text{(C1)}$$

where $z_L < z_R$ are the left/right turning points determined as the two z-roots of $2\mathcal{H}_0/(\alpha c) - 2u(z)\sigma_\delta^2 = 0$. (Our analysis is restricted to the case where there is only a single pair of turning points, excluding the double-well potential case). From the synchrotron oscillation period

$$T_s = 2 \int_0^{T_s/2} dt = 2 \int_{z_L}^{z_R} \frac{dz}{\alpha c \delta(z)}$$
$$= \frac{2}{\alpha c} \int_{z_L}^{z_R} \frac{dz}{[\frac{2\mathcal{H}_0}{\alpha c} - 2u(z)\sigma_\delta^2]^{1/2}} \quad \text{(C2)}$$

one deduces the synchrotron oscillation frequency $\omega_s(J) = 2\pi/T_s$. To determine the canonical transformation $z = \zeta(J, \varphi)$ we proceed as follows. (i) Establish $z_{\rm max} > 0$ such that $e^{-u(z_{\rm max})} < \varepsilon$, for ε sufficiently small. Set $\mathcal{H}_{0,\rm max} = u(z_{\rm max})\alpha c \sigma_\delta^2$ and find $z = z_{\rm min} < z_{\rm max}$ as the second root of $\mathcal{H}_{0,\rm max} = u(z)\alpha c \sigma_\delta^2$. Verify that $e^{-u(z_{\rm min})} < \varepsilon$; if not, choose a larger $z_{\rm max}$ and repeat. (ii) Determine z_e, the coordinate of the elliptical (stable) equilibrium point by solving $u'(z_e) = 0$. On a uniform grid, introduce the turning points to the right of z_e, $z_{R,i} = i\Delta z$, $i = 0, 1, \ldots n_z - 1$, with $\Delta z = (z_{\rm max} - z_{\rm min})/n_z$. Each $z_{R,i}$ identifies a distinct orbit, with left turning point $z_{L,i}$ obtained by finding the second root of $\mathcal{H}_{0,i} = u(z)\alpha c \sigma_\delta^2$,

where $\mathcal{H}_{0,i} = u(z_{R,i})\alpha c\sigma_\delta^2$. (iii) From (C1) and (C2) determine the action J_i and period $T_{s,i}$ corresponding to the orbit with turning point $z_{R,i}$. (iv) Solve the equations of motion for the unperturbed Hamiltonian numerically with initial conditions $z(t=0) = z_{R,i}$ and $\delta(t=0) = 0$, to find the orbit $(z(t_j;i), \delta(t_j;i))$ on a uniform grid t_j. Use $\varphi_j = \omega_s(J_i)t_j$, relating the angle coordinate φ to time, and thus determine the canonical transformation $\zeta(J_i, \varphi_j) = z(t_j;i)$ on a rectangular grid.

APPENDIX D: EFFECTIVE IMPEDANCE

Following established conventions, we define the effective impedance as

$$Z_{\text{eff},\ell}(\Omega) = \sum_{p=\pm 3} \frac{\omega_{p,\ell}}{\omega_1} Z(\omega_{p,\ell} + \Omega), \qquad \text{(D1)}$$

where $\omega_{p,\ell} = (ph + \ell)\omega_0$. We are specifically interested in the effective impedance associated with the fundamental mode of a third-harmonic cavity, to which only the terms $p = \pm 3$ contribute significantly. For vanishing or small mode number $\ell \ll h$ the coefficient in front of Z can be approximated as $\omega_{\pm 3,\ell}/\omega_1 \simeq \pm 3$ and therefore

$$Z_{\text{eff},\ell}(\Omega) \simeq 3Z(\omega_{3,\ell} + \Omega) - 3Z(\omega_{-3,\ell} + \Omega), \qquad \text{(D2)}$$

where $\omega_{\pm 3,\ell} = \pm\omega_3 + \ell\omega_0$. Expressions in the small Ω limit: (i) Effective impedance for $\ell = 0$ mode:

$$Z_{\text{eff},\ell=0}(\Omega) \simeq 4R_s Q\cos^2\psi \sin(2\psi)\frac{\Omega}{\omega_1}$$
$$- 3iR_s \sin(2\psi) + \mathcal{O}(\Omega^2). \qquad \text{(D3)}$$

(ii) Effective impedance for $\ell = 1$ mode. Define the tuning angles $\psi_{\pm 1}$:

$$\tan\psi_{\pm 1} = Q\left(\frac{\omega_r}{\omega_3 \pm \omega_0} - \frac{\omega_3 \pm \omega_0}{\omega_r}\right). \qquad \text{(D4)}$$

We have:

$$Z_{\text{eff},\ell=1}(\Omega) \simeq 3R_s(\cos^2\psi_1 - \cos^2\psi_{-1})$$
$$- i\frac{3R_s}{2}[\sin(2\psi_1) + \sin(2\psi_{-1})] + \mathcal{O}(\Omega). \qquad \text{(D5)}$$

For instability analysis the Ω dependence can effectively be ignored. Also, observe that mode $\ell = h - 1$ (equivalent to $\ell = -1$) has the same $\text{Im}Z_{\text{eff}}$ as $\ell = 1$ and therefore can be expected to exhibit similar growth rate.

APPENDIX E: USEFUL FORMULAS FOR MOTION IN A PURELY QUARTIC POTENTIAL

For the reader's convenience, here we report useful formulas for particle motion in a quartic potential $u(z)$, relevant when 3rd-harmonic cavities are operated with optimum settings, see, e.g., [6,26] for the details. The Hamiltonian is $\mathcal{H} = \alpha c\delta^2/2 + \alpha c\lambda z^4/4$, with

$$\lambda = \frac{4}{3}\frac{eV_{10}k_1^3}{\alpha cE_0T_0}|\cos\phi_1|. \qquad \text{(E1)}$$

The action depends on the turning point $r = z_R$ (because of the symmetry, the left turning point is $-r$) as

$$J = \frac{\Gamma_{1/4}^2}{6\pi^{3/2}}\sqrt{\lambda}r^3, \qquad \text{(E2)}$$

where $\Gamma_{1/4} \equiv \Gamma(1/4) \simeq 3.62$ is the Euler function with argument $1/4$. The synchrotron frequency ω_s and equilibrium bunch distribution Ψ_0 are more simply expressed in terms of the amplitude r rather than the action. We have

$$\omega_s(r) = \frac{2^{3/4}\pi^{3/2}}{\Gamma_{1/4}^2}\langle\omega_s\rangle\frac{r}{\sigma_z} \simeq 0.712 \times \langle\omega_s\rangle\frac{r}{\sigma_z}, \qquad \text{(E3)}$$

with $\langle\omega_s\rangle = \int d\varphi \int dJ\Psi_0(J)\omega_s(J)$ being the synchrotron-oscillation frequency averaged over the bunch population

$$\langle\omega_s\rangle = \frac{2 \times 2^{3/4}\pi}{\Gamma_{1/4}^2}\frac{\alpha c\sigma_\delta}{\sigma_z} \simeq 0.803 \times \frac{\alpha c\sigma_\delta}{\sigma_z}; \qquad \text{(E4)}$$

and

$$\Psi_0(r) = \frac{2^{3/4}}{\Gamma_{1/4}^2\sigma_z\sigma_\delta}\exp\left(-\frac{2\pi^2}{\Gamma_{1/4}^4}\frac{r^4}{\sigma_z^4}\right), \qquad \text{(E5)}$$

where σ_z is the bunch rms length

$$\sigma_z^2 = \sigma_\delta\frac{2}{\sqrt{\lambda}}\frac{\Gamma_{3/4}}{\Gamma_{1/4}}. \qquad \text{(E6)}$$

Finally, it is useful to derive an approximate estimate of the bunch lengthening factor σ_z/σ_{z0}. In the absence of HHCs, the synchrotron frequency is $\omega_{s0}^2 = \alpha ceV_1k_1|\cos\phi_1|/(E_0T_0)$, with synchronous phase ϕ_1 given by $\sin\phi_1 = U_0/eV_{10}$. With HHCs the phase is only slightly different, see Eq. (B10), and therefore we make a small error if upon recalling the equation $\sigma_{z0} = \sigma_\delta c\alpha/\omega_{s0}$ for the natural bunch length, we write $\lambda \simeq (4/3)\sigma_\delta^2k_1^2/\sigma_{z0}^2$ for the parameter (E1). In combination with (E6) this results into

$$\frac{\sigma_z}{\sigma_{z0}} = \left[\frac{\sqrt{3}\Gamma_{3/4}}{\Gamma_{1/4}}\right]^{1/2}\frac{1}{\sqrt{\sigma_{z0}k_1}} \simeq \frac{0.76}{\sqrt{\sigma_{z0}k_1}}. \qquad \text{(E7)}$$

For ALS-U parameters this ratio is very close to 4.

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