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The data associated with this publication are available upon request.

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1	The Effect of Temporal Wave Averaging on the Performance of an
2	Empirical Shoreline Evolution Model
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4	M.A. Davidson, I.L. Turner and R.T. Guza
5	
6	Abstract
7	The effect of using time-averaged wave statistics in a simple empirical model for
8	shoreline change is investigated. The model was first calibrated with a six-year time
9	series of hourly wave conditions and weekly shoreline position at the Gold Coast,
10	Australia. The model was then recalibrated with the hourly waves averaged over
11	intervals up to 1 year. With wave averaging up to 2 days, model performance was
12	approximately constant (squared correlation $r^2 \sim 0.61$ -0.62), with only small changes in
13	the values of empirical model parameters (e.g. the beach response coefficient c varied
14	by less than 4%). With between 2 and 40 day averaging, individual storms are not
15	resolved; model skill decreased only modestly ($r^2 \sim 0.55$), but c varied erratically by
16	up to 40% of the original value. That is, optimal model coefficients depend on wave
17	averaging, an undesirable result. With increased averaging (>40 days) seasonal
18	variability in the wave field is not resolved well and model skill declined markedly.
19	Thus, temporal averaging of wave conditions increases numerical efficiency, but
20	over-averaging degrades model performance and distorts best-fit values of model free
21	parameters.
22	

1. Introduction

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24 Coastal management would benefit from realistic prediction of long-term (multi-year) 25 coastal variability and change. However, such predictions are beyond the capability 26 of processed-based, coastal evolution models [De Vriend et al., 1993; Van Rijn et al., 27 2003]. Process models based on detailed physics of hydrodynamic and sediment 28 transport processes (e.g., Mike21, Delft 3D and Telemac) are hindered at long time-29 scales by both excessive computation time and poor model accuracy. 30 To bypass these difficulties, empirical models with reduced computation loads have 31 been developed recently for shoreline position [e.g., Miller and Dean, 2004, Yates et 32 al., 2009], sandbar location [e.g., Plant et al. 2006, Pape et al 2010] and beach 33 gradient [e.g., Madsen and Plant, 2001]. Computational speed is obtained through 34 both drastic simplification of the underlying equations, and through larger model time 35 steps. 36 Accuracy is (hopefully) provided by extensive model calibration. However, the 37 impact of using time-averaged wave parameters on shoreline model skill is unclear. 38 Here, a six-year, highly temporally resolved (hourly waves and weekly shoreline 39 position) data set is used to investigate the impact of wave-averaging on the 40 performance of a simple empirical model for shoreline evolution [Davidson, Lewis 41 and Turner (2010), hereafter DLT10]. 42 Yates et al. (2009) developed a shoreline model similar to DLT10, based on wave 43 energy disequilibrium, and presented preliminary evidence that excessive wave 44 averaging degrades model performance by blurring the time history of storm waves. 45 For example, averaging wave parameters over the time period between sand level 46 surveys (weekly to monthly) vastly simplified the numerics of calculating optimal 47 values of model free parameter compared with hourly wave measurements, but model 48 performance was reduced substantially. Owing to the numerical complexity of 49 finding optimal free parameters of this model, the tipping points for model 50 degradation as functions of the degree of wave averaging were not established. This 51 illustrates the need to ascertain limits on wave averaging, even with simple empirical 52 models for coastal change. The DLT10 numerics for optimal free parameters are 53 much simpler, and therefore allow straightforward investigation of the impact of wave 54 averaging on model performance over a broad range of time-scales. DL10 is viewed 55 here as a generic, fast, empirical model for shoreline evolution. 56 The transfer functions for linear running average filters are well known. The cut-off 57 characteristics are notoriously broad and are described well using the Dirichlet 58 function. The (-3bB) cut-off frequency may be approximated by 0.433/Mdt, where dt 59 is the sampling interval and M in the number of points in the averaging window. 60 Thus, the impact of the filter stretches to frequencies that are considerably lower than 61 the reciprocal averaging window duration (1/Mdt). 62 The field site and observations are described in Section 2. Although the shoreline 63 model itself is not the topic of the present paper, the model is briefly reviewed in 64 section 3 for clarity, and the reader is referred to DLT10 for further information. The 65 effect on model performance of increased temporal averaging of the wave field is 66 presented in Section 4. Conclusions and implications for further model development 67 and application are summarised in Section 5. 68 69 2. Observations 70 A six-year record of wave and shoreline data from the Gold Coast, located on the SE 71 Australian coastline is used (see Davidson and Turner, 2009, for details.) Wave 72 parameters are reported hourly from a wave-rider buoy located approximately 2 km 73 offshore of the study site in 16 m of water. Mean sea level shoreline locations are 74 extracted weekly from a coastal video system. The shoreline data are averaged over 75 500 m of the coastline to remove small-scale variability. Waves are energetic with 76 significant offshore wave heights exceeding 7 m, and annual shoreline displacements 77 exceed 50 m. The comparative spectral distribution of variance in the shoreline and 78 hydrodynamic (dimensionless fall velocity) time-series are shown in Figure 1. Here 79 spectral estimates have been computed after de-trending the data and application of a 80 Hanning window. The spectral estimates have 19 degrees of freedom and a bandwidth 81 of 0.0028 Hz. Both the shoreline and hydrodynamic spectra are red in form, 82 dominated by a seasonal peak at 0.0028 cycles/d. Variance of the shoreline 83 displacement is roughly divided between seasonal/interannual, trend and storm as 84 55%, 35% and 10% respectively (DLT10). Note that the hydrodynamic spectrum of

dimensionless fall velocity has significantly more high frequency (0.01 cycles/d to 0.1

86 cycles/d) content than the shoreline series. There is a small diurnal peak in the fall

velocity spectrum at 1 cycle/d, but very little variance above this point.

The tidal range is microtidal with spring tidal ranges of 1.8 m. The beach sediments

have a median grain size and mean fall velocity of 0.25 mm and 0.03 m/s

90 respectively.

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3. Model

93 The 1-D scheme of DLT10 (building upon the earlier 2-D 'behavioural-template'

scheme of Davidson and Turner, 2009) was used to investigate the impact of temporal

95 wave-averaging on empirical shoreline evolution models. The cross-shore shoreline

96 position x at time t is:

97
$$\frac{dx}{dt} = b + c \left(\Omega_0 - \Omega\right)\Omega \tag{1}$$

where Ω is the time-varying dimensionless fall velocity $(=H/\omega T)$, ω is the sediment

fall velocity, T is the peak wave period and H is the significant offshore wave height.

 Ω_0 is the time-averaged, equilibrium dimensionless fall velocity that causes no net

shoreline change in equation 1, (DLT10). A linear shoreline trend (if present) is

given by b. The rate of shoreline change in response to time-varying wave forcing is

governed by the reciprocal response time coefficient (c), wave steepness (H/T), and

the disequilibrium magnitude $(\Omega_0 - \Omega)$. Although other empirical schemes (refer

Section 1) could have been chosen here, the model represented by Equation 1 is

simple and transparent, computationally efficient, stable over long (decadal) model

runs, and most importantly, skilfully hindcasts seasonal and multi-year shoreline

change at the test case site (DLT10).

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Temporal analytical integration of Equation 1 includes antecedent conditions and

enables an analytic solution for the least squares calibration of the three unknown

coefficients; a constant shoreline offset a (units of m), a linear trend b (ms⁻¹) and the

shoreline response parameter c (ms⁻¹) (DLT10).

115 To isolate the affect of using different wave averaging times, the model time-step (dt)116 was held constant at 1 hour. The averaging period (Δ) for the forcing wave data (T 117 and H) was progressively increased from hourly (as observed) up to 1 year. For each 118 Δ , the model was re-calibrated yielding values for model coefficients a, b and c, and a 119 hindcast of the 6-year shoreline position. Model performance relative to the observed 120 weekly shoreline measurements was quantified by the squared correlation (r^2) . The 121 transfer function for a 2 and 40 day moving average filter function is also included in 122 Figure 1, so that the influence of the filter on model forcing parameters may be fully 123 appreciated. Notice that the impact of the filter function encompasses much lower 124 frequencies than one might intuitively expect. The temporal integration of ordinary 125 differential equation (1) leads to downshifting of the frequency response, thus 126 propagating the impact of time-averaging forcing parameters to still lower 127 frequencies. Thus, it is unclear, without numerical experimentation such as this, what 128 the impacts of frequency averaging on predictions of shoreline response will be. 129 130 4. Results 131 Using hourly waves and optimal values for free parameters, the model captures both 132 the seasonal variability and the rapid shoreline retreat associated with energetic 133 storms at the start of 2001, 2004 and 2006 (Figure 2). However, the model fails to 134 reproduce all the high frequency variability in the observed shoreline location and the 135 squared model-data correlation $r^2 \sim 0.62$. 136 Model performance, and the value of optimal model free parameters, varies as wave 137 averaging is increased from 1 hour to 1 year (Figure 3). With wave averaging up to 2 138 days, model performance is approximately constant (squared correlation $r^2 \sim 0.6$), with 139 only small changes (< 4%) in the reciprocal response time, c. Thus, the time step can 140 be increased (from hourly) by a factor 50, without degrading model performance or 141 substantially distorting free parameter values. With between 2 and 10 day averaging 142 individual storms are not resolved; model skill decreased only modestly ($r^2 \sim 0.55$), 143 but c varies erratically by up to 45% of the hourly value. With further increases in 144 averaging (> 40 days), seasonal variability in the wave field is not resolved and model 145 skill declines markedly. Brier skill scores, using the linear trend as the base 146 prediction (not shown), are very similar to r^2 .

147 Pape et al (2010) showed that a model for sand bar location, with structure similar to 148 the present shoreline model (1), is sensitive to wave averaging that blurs storms. For 149 both shoreline and sandbar location models, temporal averaging of wave conditions 150 increases numerical efficiency, but over-averaging degrades model performance 151 and/or distorts best-fit values of model free parameters (e.g. response time). 152 153 5. Conclusion 154 Time-averaging of the waves forcing morphologic change models must be done 155 carefully. For the wave climate at the Gold Coast test site, model performance 156 deteriorates with averaging between 2-10 days, as short-duration storm events become 157 poorly resolved. The model skill again degrades with wave averaging greater than 158 about 40 days, as seasonal variations are progressively smoothed. 159 Declining model hindcast skill and variation in model optimal free parameter values 160 resulting from time-averaging of the seasonal wave component is more significant 161 than the impact of averaging over individual storms. This is consistent with the 162 distribution of shoreline variance in this dataset: seasonal/interannual band (55%) 163 with relatively small contributions at storm frequency (10%). 164 Another likely contributing factor was that, although the model when forced with 165 hourly wave parameters successfully predicts the larger shoreline recession events 166 associated with the major storms in this time-series (start of 2001, 2004 and 2006 -167 Figure 2), it does not reproduce all of the observed high frequency variability. With 168 an alternative model that better predicts high-frequency shoreline variability; the 169 impact of averaging over storm times-scales will be more significant. Similarly, 170 smoothing over storms may be more detrimental at other coastal sites where storm 171 frequency variance contributes a higher percentage of the total shoreline variance. 172 Storms and seasonality are the two most important drivers of wave-forced shoreline 173 change, so it is anticipated that the two key time-average thresholds (≥ 2 days and ≥ 40 174 days) corresponding to the initial and further degradation of model skill and 175 fluctuation in free parameter values, are likely more generically applicable to other 176 models and sites. This assertion warrants further investigation.

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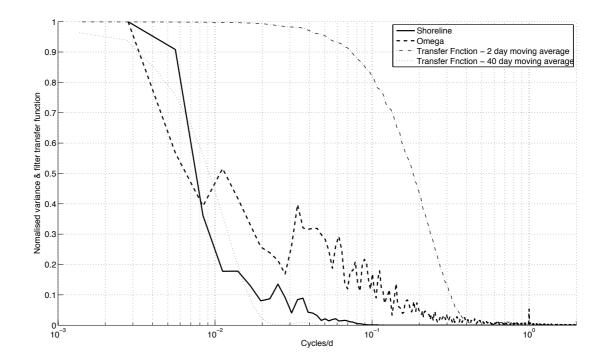


Figure 1. Spectral estimates of shoreline position and dimensionless fall velocity (omega) plotted together with moving average filter transfer functions with windows of 2 and 40 days.

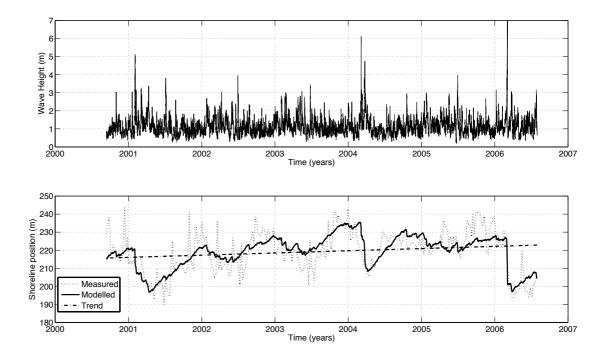
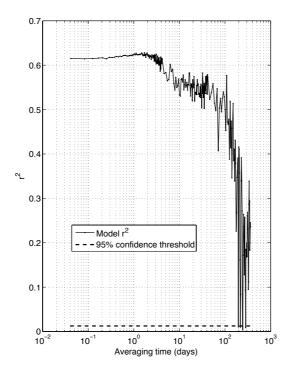


Figure 2. (top) Observed hourly significant offshore wave height, and (bottom) shoreline positions observed (dotted) and modelled (solid). The dashed broken line is a linear trend.



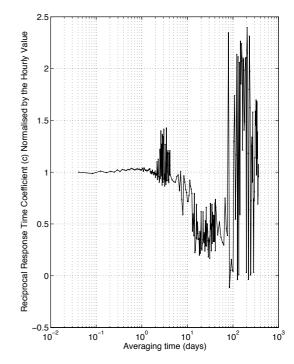


Figure 3. (left) Squared correlation (r^2) between model and observed shoreline position and 95% confidence threshold (dotted). (right) Reciprocal response coefficient c, normalised by the value for no wave averaging (hourly sampled wave parameters), versus wave averaging time (days) used in the model.