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The tracking detector of the FASER experiment

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Abstract

FASER is a new experiment designed to search for new light weakly-interacting long-lived particles (LLPs) and study high-energy neutrino interactions in the very forward region of the LHC collisions at CERN. The experimental apparatus is situated 480 m downstream of the ATLAS interaction-point aligned with the beam collision axis. The FASER detector includes four identical tracker stations constructed from silicon microstrip detectors. Three of the tracker stations form a tracking spectrometer, and enable FASER to detect the decay products of LLPs decaying inside the apparatus, whereas the fourth station is used for the neutrino analysis. The spectrometer has been installed in the LHC complex since March 2021, while the fourth station is not yet installed. FASER will start physics data taking when the LHC resumes operation in early 2022. This paper describes the design, construction and testing of the tracking spectrometer, including the associated components such as the mechanics, readout electronics, power supplies and cooling system.

Keywords: Silicon microstrip detectors, Tracking detectors, FASER, LHC

1. Introduction

FASER (the ForwArd Seach ExpeRiment) was proposed in 2017 [1] to search for new particles at the LHC at CERN. The experiment is placed in the unused service tunnel, TI12, situated 480 m downstream from the ATLAS interaction point on the beam collision axis. TI12 was formerly used for connecting the Large Electron-Positron (LEP) collider to the Super Proton Synchrotron (SPS). Excavation of the floor of TI12 provides a 5.5 m-long and up to 1.5 m-wide trench centred on the beam collision axis, where the FASER detector is installed. This location enables FASER to search for new weakly-interacting long-lived particles (LLPs) with masses in the MeV to GeV range, produced from the copious inelastic pp scattering events at the LHC. The detector design utilized the benchmark physics process of a dark photon A' decaying into a pair of oppositely charged particles, *e.g.* $A' \rightarrow e^+e^-$. Along with this process, FASER is also sensitive to several other new physics models presented in [2] which predict LLPs that travel to and decay in the FASER detector into pairs of Standard Model particles including photons. In addition to the LLP searches, the FASER location allows to study neutrino interactions of all flavors in an uncharted energy region [3]¹. The experiment location greatly reduces background particles entering FASER from the LHC collisions, since such particles would have to traverse the LHC magnets, absorbers and 90 m of rock.

The FASER detector for LLP searches was installed in Spring 2021 and is currently being commissioned towards data taking during LHC operation in 2022-24 (Run 3). As a decay volume for LLP searches, the detector has a 1.5 m-long and 0.55 T dipole magnet with a 10 cm radius aperture to separate the pair of charged particles arising from the LLP decay. Due to the limited space and accessibility to TI12, a permanent magnet with a Halbach array design is used. A veto scintillator station and a timing scintillator station are placed upstream

¹Notably, a 29-kg pilot emulsion detector was temporarily installed in this location during LHC running in 2018, which has been used to observe the first neutrino interaction candidates at a collider [4].

and downstream of this to ensure that the LLPs decay inside the decay volume. Just behind the timing scintillator station, three tracker stations and two 1 m long magnets are alternately installed to form a tracking spectrometer allowing to measure the position and momentum of charged particles. These 1 m-long magnets have the same design as the 1.5 m-long decay volume magnet except for the length. Since the LLPs produced in the forward direction of the LHC collisions have energy at the TeV-scale, the pair of charged particles produced in their decay is highly collimated. In order to resolve these particles the tracker stations must have a position resolution of better than $\mathcal{O}(100\ \mu\text{m})$. For example, for an LLP with mass $m = 100\ \text{MeV}$ and energy $E = 2\ \text{TeV}$ decaying inside the decay volume, the separation between the decay products at the first tracker station can be $\mathcal{O}(200\ \mu\text{m})$. The tracker stations consist of silicon microstrip detectors with a pitch of $80\ \mu\text{m}$, which fully cover the aperture of the magnets; this paper will focus on details of these tracking detectors. The most downstream detector is a pre-shower scintillator station and an electromagnetic calorimeter with a depth of 2 and 25 radiation lengths (X_0), respectively, which will allow to discriminate electrons from muons and to measure the electromagnetic energy. A trigger signal for data taking is provided from the three types of scintillator stations and the calorimeter. Based on FLUKA [5, 6] simulations and *in situ* measurements [7, 8], a trigger rate of around 500 Hz is expected for a luminosity of $2 \times 10^{34}\ \text{cm}^{-2}\text{s}^{-1}$ ². This rate is dominated by high-energy muons penetrating through the 90 m of rock to get to FASER. Details of the trigger system are described in [9].

To allow neutrino measurements at FASER, the detector will be augmented with an additional veto scintillator station, a 1.1-ton tungsten/emulsion detector and an interface tracker. These elements will be installed in front of the FASER detector (described above) in late 2021. The interface tracker will enable tracks from a neutrino interaction in the emulsion detector to be matched to events in the tracker stations. This will enable FASER to measure separately the

²This is the expected peak luminosity during LHC Run 3.

muon neutrino and muon anti-neutrino interaction cross sections by using the charge of the muon reconstructed in the FASER spectrometer. The interface tracker will also improve the background rejection and energy reconstruction for the neutrino analysis. The interface tracker has an identical design to the tracker stations used in the FASER spectrometer. FASER will therefore have four tracker stations in total, but this paper focuses on the three tracker stations used in the FASER spectrometer and already installed in TI12.

The layout of this paper is as follows. Section 2 presents the mechanical design of the tracker stations including details of the silicon strip detectors and on-detector electronics. The power supply, cooling, and data acquisition systems are outlined in Section 3. The interlock and detector control systems are summarized in Section 4. All components are integrated and have been commissioned, as described in Section 5. Finally, conclusions and outlook are given in Section 6.

2. Tracker stations

The FASER tracker consists of 72 double-sided silicon microstrip modules arranged in three stations, each station being composed of three planes with eight modules per plane. Given the short timescale to build the entire tracker, spare modules of the ATLAS Semiconductor Tracker (SCT) have been used. The SCT is one of the three sub-systems composing the Inner Detector [10], the internal tracker of the ATLAS experiment at the LHC [11].

2.1. Silicon microstrip modules

The SCT barrel module [12] consists of four identical single-sided silicon microstrip detectors glued by pairs on the two sides of a central baseboard, and of a copper/polymide flex hybrid carrying the readout electronics. Each sensor has p^+ strip implants on a high-resistivity ($> 4 \text{ k}\Omega \cdot \text{cm}$) $285 \mu\text{m}$ -thick n -type substrate. The strip implants are AC-coupled to aluminum readout strips via a silicon dioxide layer. The High-Voltage (HV) is applied via a n -type

metalized implant covering the back-plane and the strip implants are biased through polysilicon resistors. Each sensor has a rectangular nominal geometry of $64 \times 63.6 \text{ mm}^2$, with 768 readout strips at a constant pitch of $80 \text{ }\mu\text{m}$. A guard-ring structure surrounding the sensor active area is used to prevent electrical breakdown at large bias voltages. The readout of 128 strip channels is done by means of the Atlas Binary ABCD3TA ASIC [13], which comprises the front-end (FE) electronics, a pipeline, buffer, readout and control logic. For each channel, the analog FE consists of a preamplifier, shaper and discriminator. The signal delivered by the preamplifier-shaper circuit has a peaking time of 25 ns , enough to ensure a discriminator timewalk of less than 16 ns and a double-pulse resolution below 50 ns as required for ATLAS operations. Since the discriminator threshold remains common to all channels within the chip, the effective threshold of a given channel corresponds to the offset of its discriminator with respect to the common threshold. A per-channel threshold correction 4-bit DAC allows to compensate for the spread of these threshold offsets. The pipeline, clocked at 40 MHz rate and with a depth of 132 cells, buffers the binary data of all channels for $3.3 \text{ }\mu\text{s}$. Upon reception of a trigger the data from the last three cells are transferred to a second-level derandomizing buffer where data compression is finally applied.

Figure 1 shows a SCT barrel module held inside an aluminum test-box. On each side of the module the sensors are bonded edge-to-edge to create $\sim 12.8 \text{ cm}$ -long readout strips. The total number of readout channels in the module is 1536 (768 per side). A 40 mrad stereo angle between the front and back pairs of sensors allows the module to provide a spatial resolution of $\sim 17 \text{ }\mu\text{m}$ in the precision coordinate (perpendicular to the strips) and $\sim 580 \text{ }\mu\text{m}$ in the non-precision coordinate (parallel to the strips) [12]. The flex hybrid, equipped with six ABCD3TA chips per side, is bridged over the sensors via a carbon-carbon substrate. Two NTC thermistors (one per hybrid side) allow to monitor the module temperature. The baseboard, made of Thermal Pyrolytic Graphite (TPG) with an excellent in-plane thermal conductivity and low radiation length, provides the mechanical support to the sensors and allows to dissipate the heat

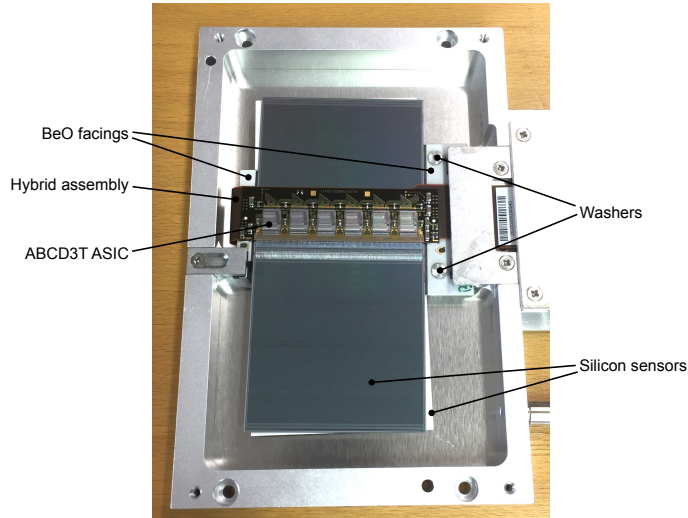


Figure 1: Photograph of a SCT barrel strip module.

generated by the FE electronics. The hybrid is attached to beryllia (BeO) facing plates located on the two ends of the TPG baseboard.

The strip modules used for the FASER tracker have been selected among the existing spares of the SCT barrel module production that was completed in 2004. Since then, the modules were stored at CERN in individual sealed bags within a controlled environment. Some of these spare modules failed the initial quality assurance by the SCT collaboration, typically because there were more than 1% defective channels, high leakage current (above $4 \mu\text{A}$) or early breakdown before 500 V (the maximum voltage expected after 10 years of operation in ATLAS). For FASER, modules with the lowest number of defective channels have been chosen. Given the much lower radiation levels expected in FASER compared to ATLAS³, the nominal operating voltage for the SCT modules is set to 150 V. This bias voltage is large enough to ensure full depletion of the sensors, and it

³with a total ionizing dose less than 5×10^{-3} Gy per year and a total fluence less than 5×10^7 1-MeV-neutrons equivalent $n_{\text{eq}}/\text{cm}^2$ per year as estimated from simulations with FLUKA and as confirmed with in-situ measurements in the TI12 tunnel [8]

is not expected to be increased during the lifetime of the experiment due to the lack of cumulated radiation damage. In all cases, IV curves have been taken at different stages of the tracker assembly and a good behaviour has been required at up to 150 V (more details are given in Section 5).

2.2. Tracker plane

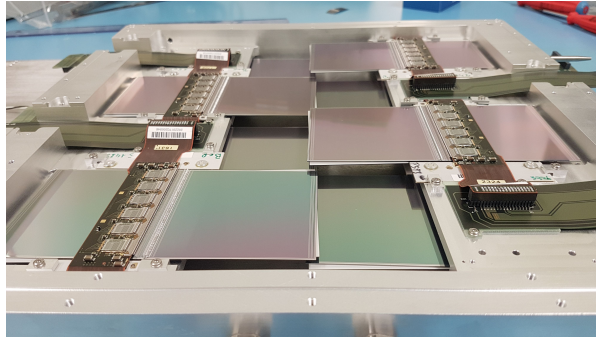


Figure 2: Photograph of a tracker plane with all eight SCT modules installed. The beam axis is perpendicular to the plane.

A tracker plane consists of an aluminum frame (AW-5083) holding eight SCT barrel modules as shown in Fig. 2. The modules are arranged by four on each side (front and back) of the frame to accommodate the flex pigtailed connectors (see Section 2.3). The distance between modules (closest sensors along the out-of-plane direction) is 2.4 mm, and the active area overlap (in-plane, along the strip-length) is 2 mm. The frame has a size of 320 mm \times 320 mm \times 31.5 mm. In order to minimize the material in front of the silicon detectors, the frame is cut-out for most of the active area within the acceptance of the magnet aperture, see Fig. 3. More details about the material distribution in the active area of a tracker station is given in Section 2.4.

The aluminium frames are CNC (Computer Numerical Control) machined (Fig. 4a) and then individually surveyed to check the quality and precision of the production process. The SCT modules are positioned in the frame by using two 1.8 mm-diameter PEEK 1000 pins (Fig. 4b). One locating pin provides the global precise positioning while a second pin (to be inserted into the slotted

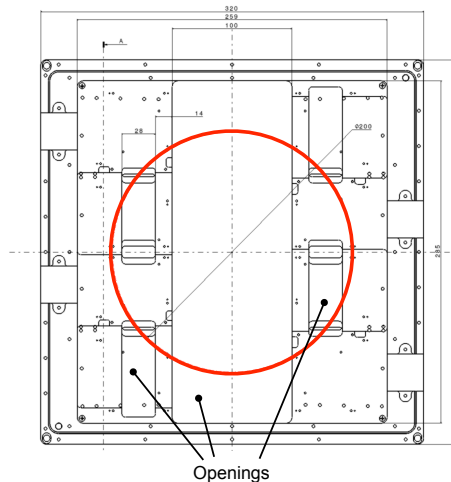


Figure 3: CAD view of a frame. The circle represents the 200 mm-diameter magnet aperture.

washer of the SCT module) is used for the module orientation. The PEEK material allows for a smooth and easy handling of the modules during insertion-removal operations. The modules are then pressed down to the frame by means of four small aluminum clamps fixed by four stainless steel M2 screws (Fig. 4c). A 5 mm-diameter inner cooling channel, integrated by design into the frame (Fig. 4d), provides the thermal path to extract by direct conduction through the water flow the heat generated by the FE electronics. A good thermal contact between the SCT modules and the aluminum frame is provided by the application of heat conducting thermal paste (Electrolube HTCP-20S) at the contact surface between the frame and the bottom side of the BeO facings. Finally, the frame also contains an inlet for dry air to be flushed, to keep a low relative humidity inside.

The metrology of each plane (Fig. 5) combines measurements performed with a mechanical touch-probe and an optical camera. Each frame is equipped with four stainless steel targets (one in each corner) used to define the plane reference coordinate system. The targets are visible from both sides, allowing to correlate measurements done on each side of the plane separately. The silicon sensors of the SCT modules include a set of fiducial marks used for the mechani-

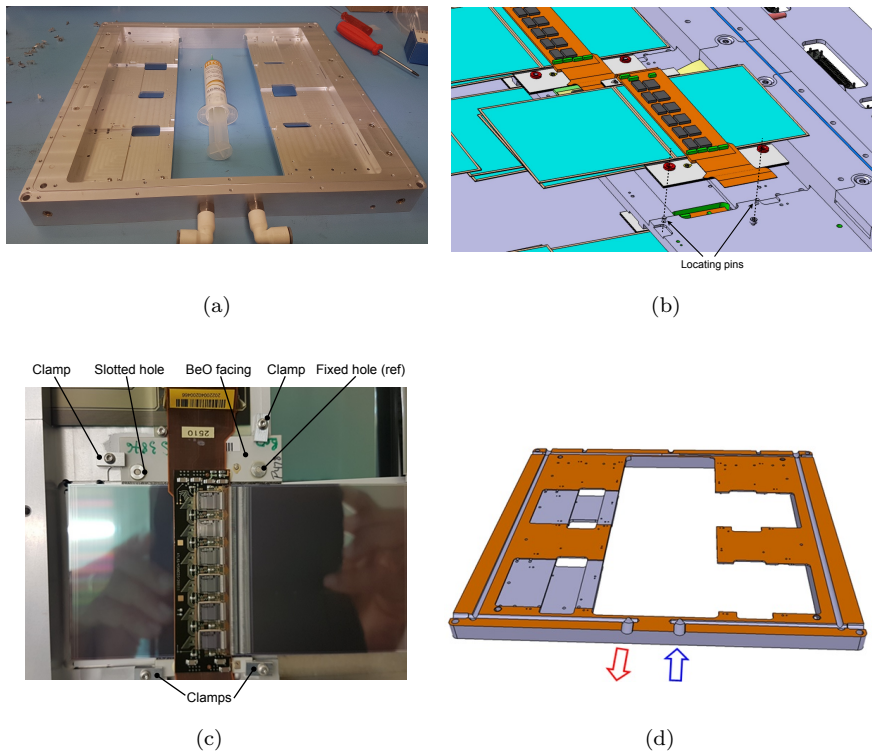


Figure 4: (a) Bare aluminum frame, (b) exploded CAD view of a SCT module while being positioned, (c) photograph of a module after its final fixation onto the frame using clamps and (d) mid-plane cross section showing the inner cooling channel. In (d), the arrows indicate the direction of the water flow.

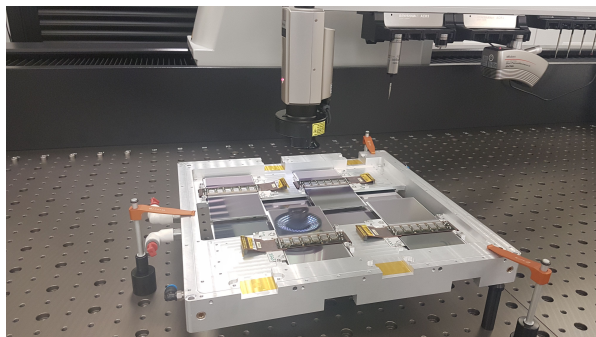


Figure 5: Metrology of a fully assembled tracker plane.

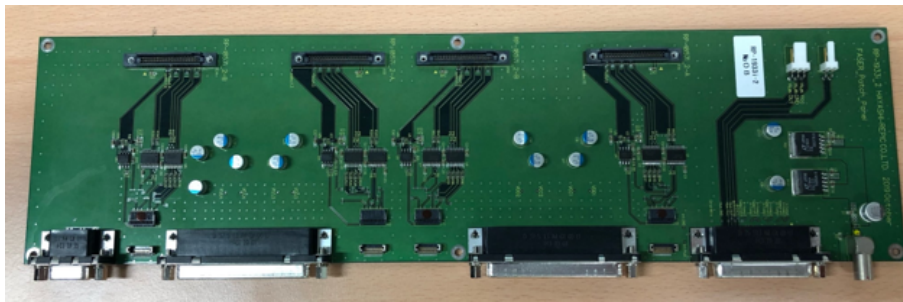
cal alignment during module assembly. Some of the fiducial marks are measured in 3D with respect to the plane reference system. All assembled planes were measured at the University of Geneva using a Mitutoyo CRYSTA-Apex S CNC coordinate measuring machine with automatic probe changer. The precision of the metrology machine for in-plane and out-of-plane measurements is $5\ \mu\text{m}$ and $10\text{-}15\ \mu\text{m}$, respectively. It is found that all frames are within the required tolerances ($\pm 20\ \mu\text{m}$) with respect to the CAD manufacturing drawings. A maximum deviation of $100\ \mu\text{m}$ is found for the positioning of the SCT modules with respect to the CAD model (corresponding to a perfect alignment). This maximum deviation accounts for the combined effect of machining tolerances, SCT modules positioning errors and assembly precisions.

2.3. On-detector electronics

A flexible printed circuit board (called the "pigtail") has been developed to route the electric lines of the SCT module to the outside (Fig. 6a). Four pigtails (one per module) at one side of the tracker plane are connected to a single patch-panel (Fig. 6b). The connectors on the patch-panel are mounted on the same side while the side of the module is arranged alternatively in the tracker plane as shown in 7. For that reason, two types of the pigtail were developed, arranging the lines in the opposite order. The size of the pigtail is



(a)



(b)

Figure 6: The pigtailed (a) and patch-panel (b).

6 cm \times 15 cm with 150 μ m thickness. The connector⁴ on the module side is oriented with 91.15 degrees on the pigtail to connect with the hybrids on the module as shown in Fig. 7.

The tracker is electrically connected to the Data Acquisition (DAQ) and powering systems. The patch-panel (Fig. 6b) was developed as the interface between them. A patch-panel is placed at each side of the tracker plane and fixed on the aluminum frame. The size of the patch-panel is 10 cm \times 30 cm with 1.6 mm thickness. The Tracker Readout Board (TRB, see Section 3.3) in the DAQ system is connected to two patch-panels via eight twinax Firefly cables⁵, *i.e.* one cable per SCT module. The cable provides all LVDS lines necessary for operation and readout of the ABCD3TA chips on the module.

⁴SFMC-120-L3-S-D manufactured by SAMTEC, Inc

⁵ECUE-08-300-T2-FF-01-1 manufactured by SAMTEC, Inc

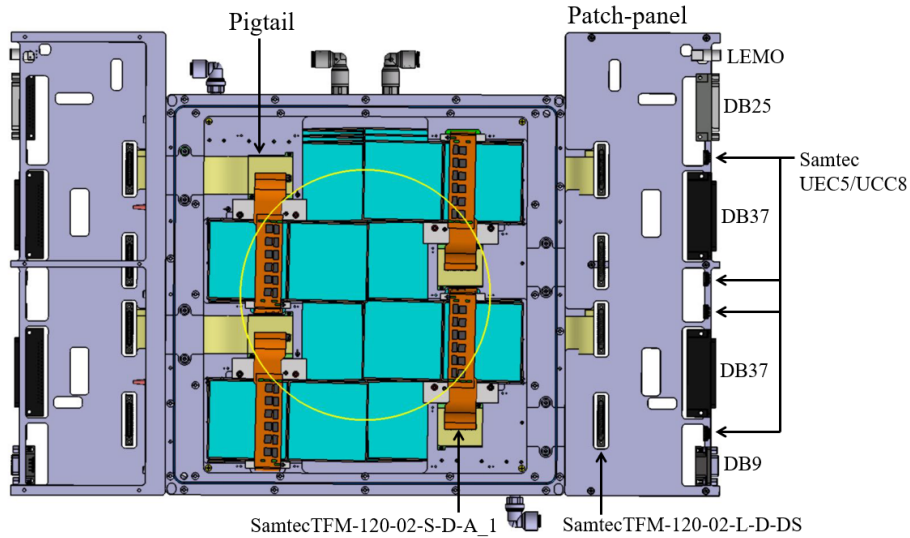


Figure 7: Schematic view of the tracker plane. One pigtail is connected to each hybrid on the SCT module. Note that adjacent SCT modules are mounted on opposite sides of the FASER module frame. The four pigtails in one side are connected to one patch-panel.

LVDS repeaters are mounted for all LVDS lines on the patch-panel to transmit signals along 3 m of the cable. In addition, LVDS receivers are placed to receive the operation signals for the ABCD3TA chips from the TRB. HV and Low-Voltage (LV) as well as their return lines are provided from a HV splitter board and a LV protection board to bias the sensors and power the ABCD3TA chips, respectively (see Section 3). Every patch-panel is connected with the HV splitter board, biasing the sensors on the four modules with one HV channel. LV for the analog and digital circuits in the ABCD3TA chips is provided to each module separately. The patch-panel works as the interface for the NTCs on the modules and temperature and humidity sensors on the plane frame with the Tracker Interlock and Monitoring Board (TIM, see Section 4.2) which is used for the environmental monitoring. In addition, there are 5 V power lines on the patch-panel for the LVDS repeaters and receivers as well as a line to transfer an interlock signal generated by the TIM to the LV power supply.

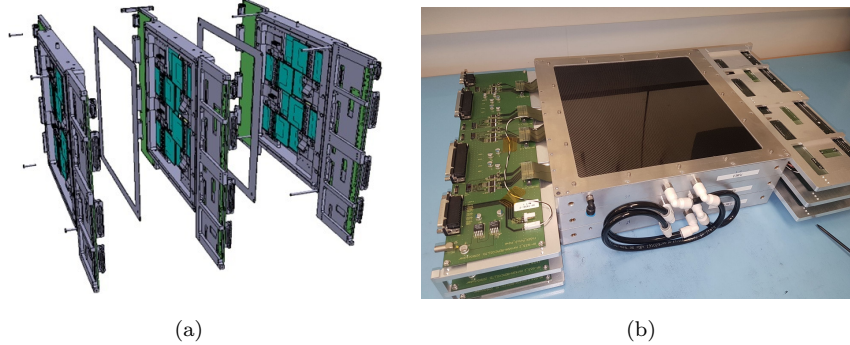


Figure 8: (a) Exploded CAD view of a tracker station and (b) photograph of a fully assembled station. The black cover on top of the station is a carbon-fibre plate. The cooling loops of each plane are connected together, so that per station there is only one inlet and one outlet for the cooling fluid.

2.4. Tracker stations

A tracker station is an assembly of three planes (including the patch-panels) as shown in Fig. 8. Within the station the three planes are staggered along the vertical direction, with a relative shift of the middle (last) plane of $+5$ mm (-5 mm) with respect to the first plane. This configuration ensures at least two 3D reconstructed space-points for a track crossing the station. Each station is flushed with dry air to reduce the relative humidity ensuring safe operating conditions against dew point. The patch-panels fit within the 32 mm thickness of one plane. All aluminium parts are post-treated with a trivalent chromium passivation⁶ to prevent any corrosion by the corona effect that may occur after putting the frames in contact during the station assembly. In addition, an O-ring sealing joint between frames provides a good tightness to keep the humidity inside the station as low as possible (typically about 5%). The station is connected only after the metrology and full commissioning of each individual plane is completed. The inter-plane alignment is done via two high-precision pins located in 5 mm-diameter H7 holes while the fixation between two adjacent

⁶SURTEC-650 coating

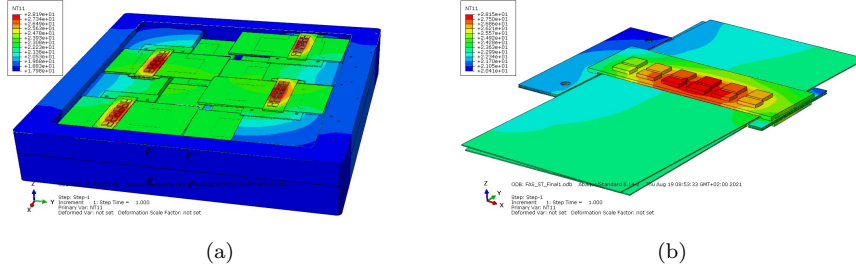


Figure 9: (a) FEA simulations on a complete station and (b) close up view on a single module. The maximum temperature estimated on the module is 28 °C (on the readout electronics). See text for additional details on the different simulation parameters.

planes is done via four M5 screws. The two end covers that close the station volume are made of 400 μm -thick carbon-fibre plates (standard T300 fibers). Without cables, the total weight of one station is about 15 kg.

Various Finite Element Analyses (FEA) simulations have been carried out to check the thermal performance of the system throughout the evolution of the frame design. Over-heating of the SCT modules can cause problems in the mechanical integrity and alignment of the SCT modules due to the glass-transition of glues. The glue ⁷ used for the SCT module assembly should have the lowest glass-transition temperature around 35 °C, which should be the absolute maximum temperature for the SCT modules. The safety scheme to ensure this is described in Section 4.

Figure 9 shows the FEA of a complete station. The different simulation parameters have been set to match the testing conditions during the plane and station commissioning at CERN. In particular, the coolant temperature has been fixed at 15 °C, the water flow at $31 \cdot \text{min}^{-1}$ (for a heat transfer coefficient of water of $500 \text{ W} \cdot \text{m}^{-2}$), and the outside air convection at 23 °C. The FEA gives a maximum temperature on the FE chips of $\sim 28 \text{ }^\circ\text{C}$, neglecting the temperature

⁷ARALDITE 2011 manufactured by Huntsman Corporation: https://samaro.fr/pdf/FT/Araldite_FT_2011_EN.pdf

rise within the water channel due to the heat load (estimated to be $+0.6\text{ }^{\circ}\text{C}$ for $31\cdot\text{min}^{-1}$). The FEA results are in good agreement (within $2\text{-}3\text{ }^{\circ}\text{C}$) with the measurements taken during the commissioning at CERN. Given the good modeling of data measurements by the FEA, the temperatures on the silicon sensors are estimated to be in a comfortable range between 21 and $23\text{ }^{\circ}\text{C}$.

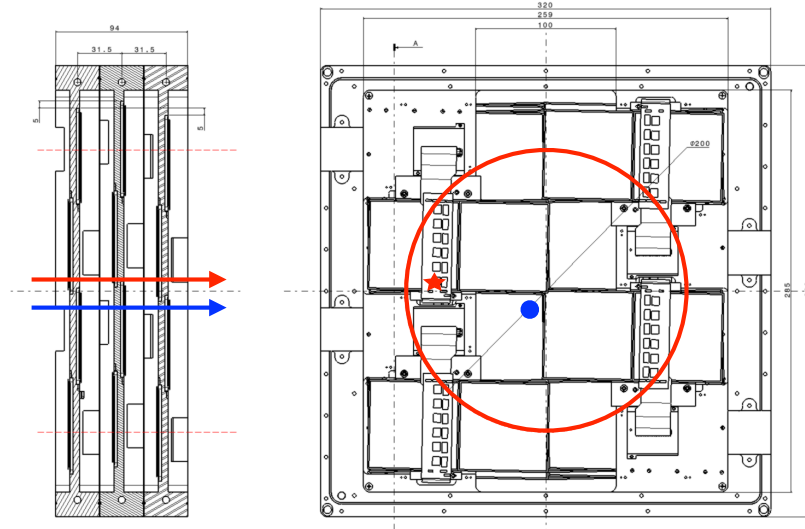


Figure 10: Side (left) and front (right) views of a tracker station. The circle represents the 200 mm-diameter magnet aperture. The dot and star markers respectively correspond to the reference positions for material calculation in the central and edge regions.

Figure 10 shows the front and side CAD views of a station. Two different reference positions have been considered to estimate the material distribution along the station depth (Z -axis, perpendicular to the station front-plane): a *central region*, close to the geometrical center of the plane, and an *edge region*. Table 1 summarizes the material budget in each case. The central region corresponds to a particle traversing the least amount of material inside the station, *i.e.* six silicon sensors and two carbon-fibre covers that account for a total of $2.1\% X_0$. The edge region is a worst-case position that corresponds to a particle traversing the six SCT modules (including sensors, TPG baseboard, flex hybrid with carbon-carbon bridge and readout ASICS), aluminum frames and station

covers, accounting for a total of 21.5% X_0 . For a benchmark dark photon model ($m_{A'}$ =100 MeV, $\epsilon = 10^{-5}$) for dark photons that decay in the FASER magnet aperture, 70% will be in the low material central region of the tracker. Given the range of particle momentum expected in the experiment the contribution of multiple scattering from the traversed material is expected to be negligible.

Component	Material	Number / station	X_0 (%)	
			Central region	Edge region
Silicon sensor	Si	6	1.8%	1.8%
Station Covers	CFRP	2	0.3%	0.3%
SCT module support	TPG	3	-	0.6%
C-C Hybrid	C (based)	3	-	2.2%
ABCD3TA chips	Si	3	-	6.5%
Layer frame	Al	3	-	10.1%
Total / station	-	-	2.1%	21.5%

Table 1: Amount of material in X_0 in the active area of a tracker station for two regions: i) the central region with only the silicon sensor material and ii) the edge region. Details of the material in the SCT module are given in Table 8 of Ref. [12]. The numbers are calculated directly from the CAD description of the tracker station.

The three tracker stations are mounted into the FASER detector with an aluminum structure (AW-5083) called the *backbone* as shown in Fig. 11a. Each station is fixed to the backbone via an aluminum support interface (Fig. 11b) with six M6 screws and two locating pins. The backbone has been CNC machined in one go for what concerns its key parts (stations interface areas, pin holes) to optimize the final precision. It has been assembled at the University of Geneva and surveyed by the CERN group to check its overall flatness, parallelism and straightness. The survey results show a 0.13 mm flatness over the three station interfaces, each one being 0.04 mm without load and 0.10 mm when loaded with the station weight.

The backbone is the primary global mechanical structure of the tracker as it

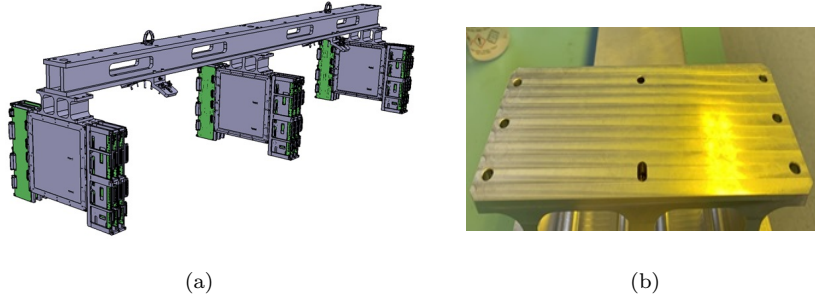


Figure 11: (a) CAD model of the backbone with three stations attached and (b) detail of the station interface.

links together the three stations. It allowed for an easy handling and transportation (Fig. 12a), and serves as a reference structure for the tracker alignment. The backbone is then supported by the first and second magnet cylinders via clamps (Figs. 12b and 12c).

3. Powering, cooling and readout system

Since access to the FASER location is guaranteed only every two or three months during technical stops of the LHC, it is important that the system is robust. The FASER tracker powering and cooling systems are based on commercial products, and the readout system is based on a custom general purpose I/O (GPIO) board with a dedicated interface card. Peripheral equipment is designed exclusively for the FASER tracking detector.

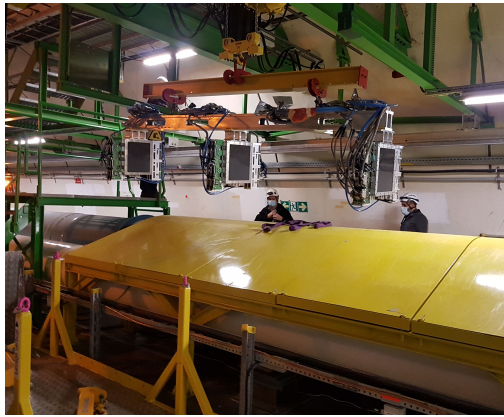
3.1. Power supply system

In order to provide HV and LV to the SCT modules described in Section 2.1, three 19-inch rack mountable crates called the MPOD LV/HV Power Supply System⁸ are installed in TI12, which host 3 HV modules⁹ and 18 LV modules¹⁰

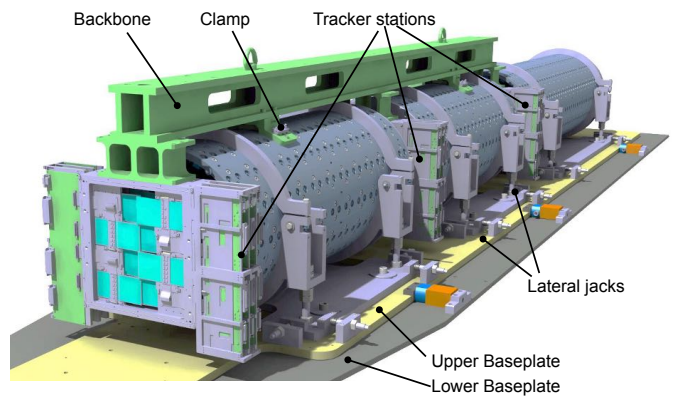
⁸MRAAH2500A2H manufactured by W-IE-NE-R Power Electronics GmbH.

⁹EHS 84 05p manufactured by Iseg Spezialelektronik GmbH.

¹⁰MPV 8008I manufactured by W-IE-NE-R Power Electronics GmbH.



(a)



(b)



(c)

Figure 12: (a) Transport of the backbone above the LHC, (b) CAD view of the FASER tracker and (c) photograph of the tracker after installation onto the detector in March 2021.

in total. For other electronics, one 19-inch rack mountable box (PSbox) is also installed, which holds fifteen 24V power supplies ¹¹.

Three types of printed circuit boards, the HV splitter board, the LV protection board and the 24V/6V board, were developed. These are mounted on the detector, directly above the tracker stations. The HV splitter board divides one HV channel into the four to supply the SCT modules connected to one patch-panel, corresponding to half a tracker plane. The LV protection board equips an integrated circuit¹² which protects against over-voltage possibly induced by radiation in TI12. The 24V/6V board is powered by the PSbox, and it is used to distribute 24V to the TIM, described in Section 4.2 and 6V to the patch-panel.

3.2. Cooling system

The cooling system was designed and built by the CERN cooling and ventilation group (EN-CV). It consists of two air-cooled water chillers¹³: one circulating chilled water through the tracker stations and the second acting as a hot spare.

As shown in Fig. 13, the cooling system is mounted on a single frame together with all instrumentation. An additional water reservoir is also installed, which makes it possible to refill the water tank inside the chiller in an automatic manner. The cooling capability of each chiller is about 1.8 kW at a 15°C water outlet temperature with $\Delta T = 3^\circ\text{C}$ between inlet and outlet temperature. Since one SCT module consumes 6 W, corresponding to an overall power consumption of 450 W for the full tracker, the cooling system is therefore sufficient to regulate the temperatures of the tracker stations.

In case of a failure of the chiller in use for the tracker stations, the cooling circuit is re-routed by controlling valves to the spare chiller to take over the cooling. Since in normal conditions both chillers are running in the normal state, one connected to the detector and the other in bypass mode, this swap

¹¹TXL 035-24S manufactured by Traco Power

¹²LTC4365 manufactured by ANALOGUE DEVICE

¹³HRS030-AF-20MT manufactured by SMC Corporation



Figure 13: Photograph of the cooling system.

can seamlessly take place without any impact on the operation of the tracker stations. If both chillers are not operating correctly, the power supply system is forced to be turned off without software intervention (Section 4.3).

A dry air system with a dew point of -40°C coming from compressed air supplied from LHC point 8 is used to flush the tracker stations to avoid condensation on the electronic due to the cooling. In case of lack of dry air an alarm is triggered and the cooling and detector will be stopped.

3.3. Data acquisition system

The Tracker Readout Board (TRB) is used for operation and readout of the SCT modules in the FASER tracker. It consists of a GPIO board and an adapter card as shown in Fig. 14. The GPIO board was developed as a general readout board centered around a CYCLONE V A7 FPGA (Field Programmable Gate Array). The FPGA is driven either by a 40 MHz oscillator on the GPIO board or by an external clock via LVDS input through dedicated two-pins LEMO connectors. The GPIO board is operated with an input voltage of 24 V and provides 5.0, 3.3 and 2.5 V to various active devices either on the GPIO board or

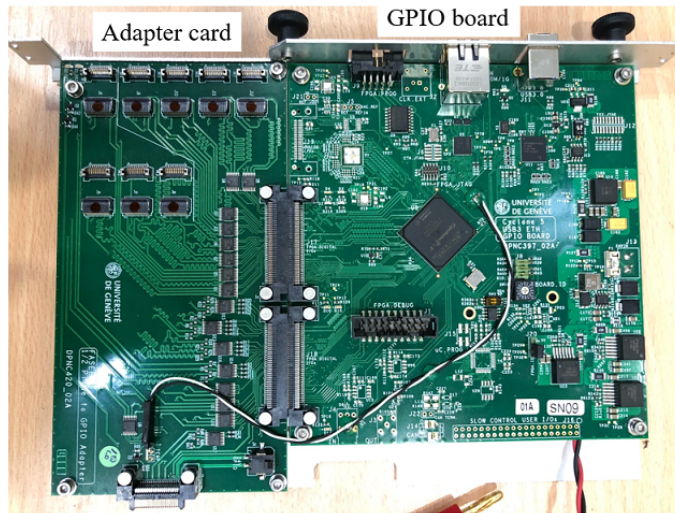


Figure 14: TRB consisting of GPIO board and adapter card.

to the adapter board. The adapter card is directly attached to the GPIO board and acts as an interface to the patch-panel and the Trigger Logic Board (TLB) [9]. The TLB, also a GPIO board, is the central trigger board of the FASER trigger and data acquisition system, which subsequently provides a global trigger accept signal (L1A).

For standalone operation during qualification of the tracker planes, the TRB can work independently without any external control and clock signals. On the other hand, in combined operation in the FASER detector, the TRB is controlled by the TLB which provides the 40 MHz clock used by the SCT modules, Level-1 trigger and bunch counter reset signals. A busy signal is also sent by the TRB to the TLB to hold the trigger during SCT data readout. The TRBs are housed on the detector in a custom-made minicrate, and the minicrate backplane provides 24 V power as well as the TLB signals for the GPIO boards. The TRB is connected to the TLB via RJ45 connector located on the rear side of the minicrate backplane.

One TRB reads out eight SCT modules corresponding to one tracker plane. Therefore, a total of nine TRBs (Fig. 15) are used for the three tracker stations

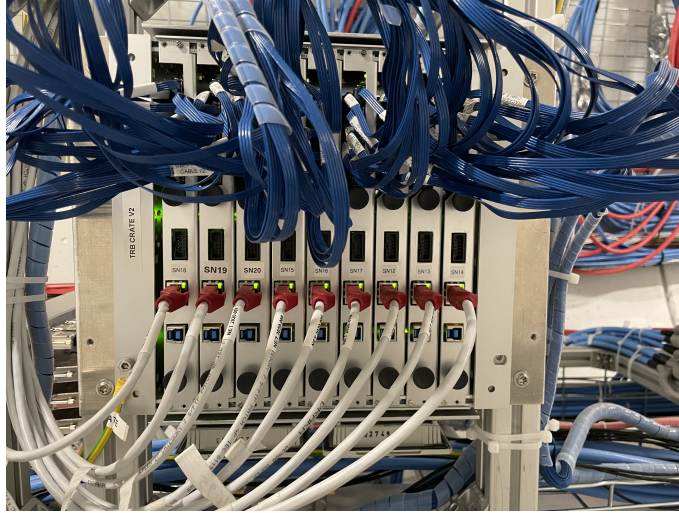


Figure 15: TRBs installed in the custom-made minicrate.

in the FASER spectrometer. In addition, three further TRBs are used in a separate minicrate for the interface tracker. The TRB adapter card is connected to the tracker plane patch-panels via eight Samtec twinax Firefly cables, one for every module. Each Firefly cable provides eight LVDS lines used for two clock, two command and two data signals as well as one reset and one select signal. The GPIO board communicates with a DAQ PC, situated at the surface, via a 1 Gbps Ethernet link.

The TRB FPGA logic is defined by the TRB firmware, and controlled by the DAQ software running on the surface PC. The software is written in C++ code and manages all operational procedures such as the calibration sequence as described Section 5.4 [9]. The firmware is designed to send low level protocol commands to the ABCD3TA chips on the SCT modules and read out data from them. The high level protocol commands are provided from the PC to the GPIO board, and then the corresponding operation signals are sent to the chips. The data from the chips are stored into First-In First-Out (FIFO) memories in the FPGA and sent to the PC. The software decodes the bit-stream of data from the SCT modules. The event and BCID (Beam Crossing Identifier) counters

are implemented in the firmware to ensure synchronization between all readout elements (the chips, different TRBs and TLB). The software in the central DAQ system can send a command to reset the chips as well as the counters and FIFOs in case desynchronization is detected. In addition, if an error is detected in the firmware, it provides error information to the DAQ PC, for example, in the case that the L1 trigger is received while hit data remain in the FIFOs.

The firmware contains four circuit blocks to set the readout timing. Two blocks are used to adjust the clock phase of the 40 MHz input clock with 390 ps steps and 25 ns range, with each four modules on the patch-panel connected to one of these blocks. The other two blocks are used for the circuits in the firmware to latch correctly the output data signals from the modules and compensate for the propagation delay of the cables and the latency in the modules.

The typical data size per plane is expected to be ~ 212 Bytes/event. At 500 Hz trigger rate in the FASER tracker, that corresponds to a required readout bandwidth of at least 106 kBytes/s (848 kbps), or an occupancy of just 0.04% of the 1 Gbps Ethernet link. On the other hand, the calibration scans lead to an occupancy of typically 25% of a module, corresponding to 8.5 kBytes of data per plane per L1A trigger.

4. Interlock and Detector control system

The aim of the safety system of the FASER tracker is to protect the delicate silicon tracker modules from damage under all circumstances. The FASER tracker follows hereby the common approach of a multi-level protections system consisting of high-level software-based detector monitoring (DCS: Detector Control System) and a low-level hardware-based interlock system. The software system is capable of triggering automatic actions that can turn off individual detector components in a controlled way while the hardware interlock system turns off power supplies immediately and acts therefore as the last level of safety.

4.1. Safety scheme

Generally, there are two sources of danger against which the detector has to be protected. One is electrical failures which can cause persistent damage on the detector electronics and silicon sensor due to over-voltage or over-current. Over-voltage and over-current are defined as $V_{\text{nominal}} + 200 \text{ mV}$ [13] and $I_{\text{nominal,max}} + 200 \text{ mA}$, respectively, where V_{nominal} is the nominal operation voltage and $I_{\text{nominal,max}}$ is the maximum current with V_{nominal} . The other is over-heating caused by a failure of the cooling system. As discussed in Section 2.4, the temperature of the SCT module is required to be less than $35 \text{ }^\circ\text{C}$.

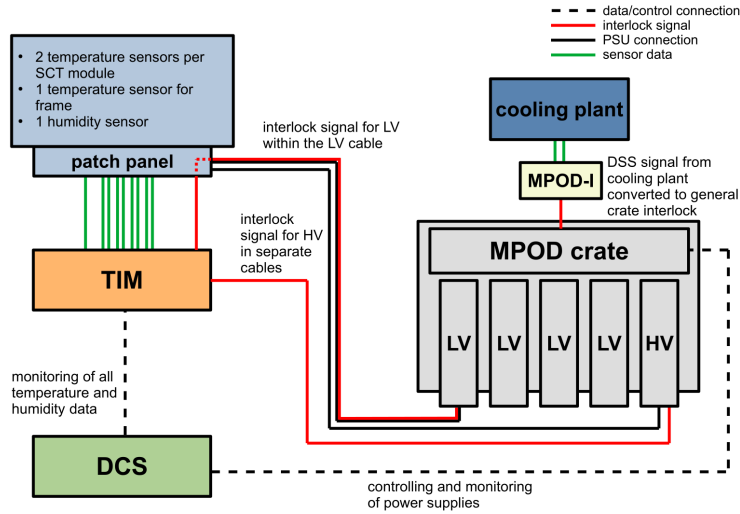


Figure 16: Schematic overview of the FASER safety and interlock system.

Figure 16 gives an overview of the protection system of the FASER tracker. In the upper left corner, one of the two patch-panels of a tracker plane is sketched. Each patch-panel serves four silicon strip modules and each module is equipped with two temperature sensors (NTC-10k thermistor) that are used for temperature monitoring close to the readout part of the tracker module. In addition, each patch-panel also connects to one temperature sensor (NTC-10k thermistor) that is thermally attached to the mechanical frame inside of the plane as the frame makes the thermal contact to the silicon strip modules

themselves. Finally, there is one sensor (HIH-4000) per plane which measures the humidity inside of the tracker plane.

All these sensors are read out by the TIM (Tracker Interlock and Monitoring Board). One TIM can receive the signals from a complete tracker station (three planes, six patch-panels). All sensor values are digitized and provided to the software DCS system via an Ethernet connection. Additionally, the frame temperatures of each plane are used as input to an analog comparator circuit which generates an interlock signal for the relevant LV and HV power supplies. The granularity of the temperature interlock can be changed from only a single tracker plane up to the full station by configuring six hardware switches on the TIM.

The interlock signal for HV is provided to the HV power supplies (one per station) in a separate cable, while the interlock signal for the LV power supplies (one per patch-panel) is propagated to the LV power supply through a dedicated signal line in the LV cable via the patch-panel.

In order to prevent the detector modules from electrical damage, each power supply has an independent supervision module that can turn off a channel as soon as it leaves the defined operation range. As an extra level of protection, an additional ASIC for over-voltage protection is placed in the LV power path.

The final component in the interlock system is the MPOD Interlock (MPOD-I) which receives the Detector Safety Signal (DSS) from the cooling plant and provides a crate-wide interlock to the MPOD crates in case of a cooling plant failure.

In the following sections the specific hardware components of the tracker safety system are described in more detail.

4.2. Tracker Interlock and Monitoring

Figure 17 shows a picture of TIM as well as its corresponding block diagram. The core of the TIM is the AM335X micro-controller as well as three independent comparator based interlock circuits.

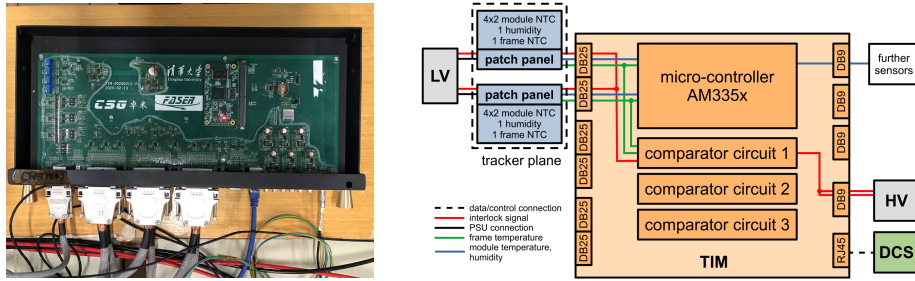


Figure 17: TIM board and corresponding block diagram (signal path shown for two patch-panels).

The TIM can connect to up to six tracker patch-panels via DB25 connectors each connector carrying the signal from one frame temperature sensor, 4×2 module temperature sensors, and one humidity sensor. There is one additional DB9 input that allows to connect up to 2 additional environmental temperature sensors. The latter is currently not used in the FASER trackers setup, but leaves flexibility for further monitoring in the future.

All the mentioned sensors are routed to the microprocessor for digitization and monitoring. In addition, the frame temperature sensors of patch-panels that belong to the same tracker plane enter into one of the three comparator-based circuits in which a hardware interlock signal is generated if the analog signal of those sensors lies outside of the valid range. The range itself can be adjusted with potentiometers. Eventually, two interlock signals are generated for the relevant power supply channels per comparator circuit: One for the LV power supplies and the other for the HV power supplies. The interlock is released at the power supply side in both cases when a logical high level is applied. In case of the LV interlock signal the logical high level amounts to 9 V while for the HV interlock signal 5 V is used. Additional hardware switches on the TIM allow to combine (or exclude) individual outputs of the three comparator circuits into a single interlock signal in case of the HV interlock signal.

Finally, the TIM features several interfaces for higher level communication: an Ethernet port for the communication with the DCS as well as several serial

interfaces for debugging and optional connection to other devices.

4.3. MPOD Interlock Board

The MPOD Interlock Board (MPOD-I) represents the interface between the DSS signal of the cooling plant and the FASER interlock system. The board and its corresponding block diagram are depicted in Fig. 18. The cooling plant PLC controls a loop which is physically interrupted in case of a cooling plant failure (DSS signal). The MPOD-I checks this loop constantly and translates the DSS signal into a voltage interlock signal which is distributed to up to four MPOD crates simultaneously. It is important to note that this interlock signal, in contrast to the interlock signals described earlier, is a crate-wide signal causing the shutdown of all the power supply modules which are part of the crate directly via the crate controller. A high logical signal (5 V) needs to be actively supplied in order to release the interlock at the controller side.

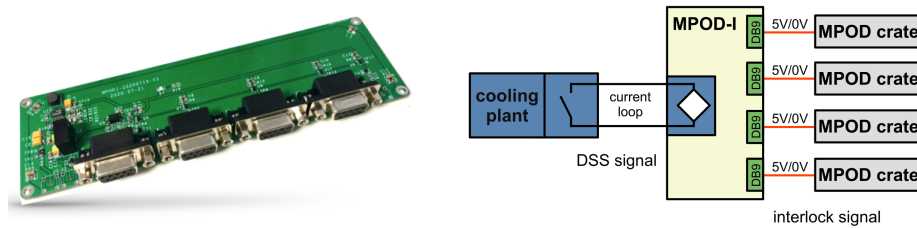


Figure 18: MPOD-I board and corresponding block diagram.

4.4. The DCS system

The DCS system is the central location where all monitoring data from the TIM boards as well as from the power supplies come together and is stored persistently into a database. Additionally, it provides high level controls of all the power supplies. The software is, therefore, capable of executing automatic actions in case the detector is leaving the operation parameter space indicated by one of the many available sensors. Due to the significantly larger number of sensor readings in the DCS system compared to the interlock system, a more

sophisticated warning and protection scheme can be implemented at the cost of the dependence on a software process. Details of the DCS system is described in [9].

4.5. Limits for DCS automatic actions and hardware interlock

Table 2 shows the thresholds values of temperature and humidity used for the operation of the tracker safety system. The thresholds for the automatic actions as well as the hardware interlock need to be chosen carefully such that the software-based automatic actions will step in before the actual hardware interlock in case of any abnormal temperature increase.

sensor	DCS warning	DCS automatic action	hardware interlock
module temperature	> 30.0 °C	> 31.0 °C	-
plane humidity	> 10%	-	-
frame temperature	> 23.0 °C	-	> 25.0 °C

Table 2: Thresholds of temperature and humidity to activate the different protection mechanism in the FASER tracker safety system.

In order to verify these limits, a potentially destructive test was performed on a prototype tracker plane. All protection mechanisms were disabled, the cooling was stopped, and the plane remained fully powered. Figure 19 shows the thermal evolution measured by a representative frame and module temperature sensor. The condition for the hardware interlock ($T_{\text{frame}} > 25.0\text{ °C}$) was reached after about 9 minutes. The corresponding module temperature at that moment was measured to be $T_{\text{module}} > 32.0\text{ °C}$ and was therefore well below the required 35.0 °C . The threshold for the automatic DCS actions are adjusted in such a way that they are sufficiently far away from the normal operation point, but low enough in order still trigger before the hardware interlock under normal circumstances.

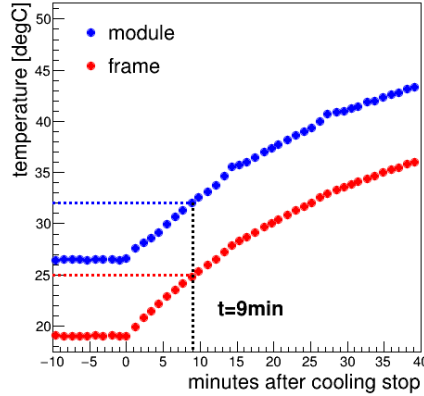


Figure 19: Thermal behaviour of frame and module in case of a cooling stop. A special single plane was used for this test and all protection mechanisms were deactivated.

5. Tests during construction and commissioning of the FASER tracker

The FASER tracker elements were tested at each stage of the construction. The electrical performance and behavior of the silicon sensors as a function of the applied bias voltage were investigated for the single SCT modules, individual tracker planes and full tracker stations on the surface before installation of the tracker stations into the FASER experimental site. In addition, metrology was performed for the layers and stations. After the installation, the performance was also tested using cosmic rays and random triggers deploying the central DAQ system of the FASER experiment. In this section, the test setup, procedure and results of the thermal and electrical tests are described.

5.1. Test setups during testing on surface

Three test setups were installed to perform the required measurements at the different stages, namely tests of a single module, plane and station.

The single module test was done with the readout system developed at Cambridge University [14]. It was used to evaluate the electrical performance of a single module. A chiller was used to cool down an environmental enclosed box to keep the module below 30°C. The number of functional strips, the noise value

and dependency on applied bias voltage (high-voltage behaviour) of the silicon sensors were verified and compared to the results in the module production of the ATLAS SCT detector [12].

The individual planes and stations were qualified on surface in test-stands which used equipment later used in the FASER experiment. Both the interlock and monitoring of the temperature, voltage and current were handled by the TIM unit (see Section 4.2). This allowed the DCS information to be monitored live and be archived into a database for evaluating the detector performance. The same powering and DAQ systems, cables and calibration software as used for the experiment were used during the testing on surface. This allows to compare the electrical performance at different stages of the assembly and installation as well as from different data taking periods in the tunnel. The surface commissioning with the components used in the real experiment made it possible to test their operation and investigate the long term behaviour early on. The operation of the different tracker planes and stations was conducted with specific finite state machines which took the modified detector mapping on the surface compared to the one in the tunnel into account. Figure 20 shows a picture of the test setup with its main components for station commissioning.

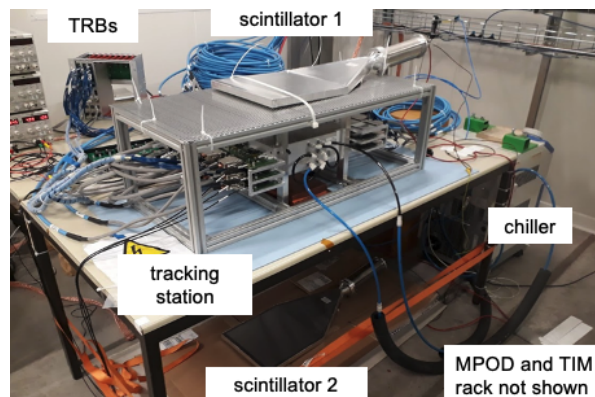


Figure 20: The test setup for the station commissioning on surface.

5.2. Test procedure

The procedures of the plane and station testing were consistent to allow for comparisons of the collected data. After installation of the plane or station under test into the test setup, the thermal and electrical measurements were conducted. The thermal measurements comprised of measurements of the frame NTC and SCT module NTCs without powering the SCT module, after powering and after configuring the ABCD3TA chips.

During the electrical characterization, the leakage current of the sensors was measured. The LV and its current consumed were also investigated after powering up and configuring the chips. Further important parameters measured in the electrical calibration sequence are the number of non-functional channels, so-called masked channels, the noise, the gain and the noise occupancy of each module after trimming the threshold offset of the ABCD3TA chips as explained in Section 5.4. The planes and stations were powered for at least 24 hours to investigate their long-term stability and behaviour of the leakage current in the silicon sensors.

The results were compared between those in the test of the individual modules, plane and station commissioning. The plane and station were signed-off, considering a list of the required parameters such as thermal stability, less than 0.5% masked strips, noise and gain values comparable to the single module testing. After installing all three stations into the FASER experiment in TI12, the same thermal and electrical tests were conducted and the test results were compared to the surface commissioning data. A general agreement was found as shown in more detail below.

5.3. Results of thermal tests

Figure 21 shows the temperature of the two NTC sensors on each module in one plane of one station, which was measured during surface commissioning of the first station. The temperature values are listed for power-off (green), after powering the modules (orange) and after powering and configuring the chips (blue). The values without powering correspond to the coolant temperature

of 15°C. The maximum values of around 27°C are reached after powering and configuring the modules. The module temperatures vary slightly in a pattern along the flow of the cooling loop. It leads to the behaviour that typically the modules in the corners of the plane (modules 0, 3, 4, and 7) are the coldest ones.

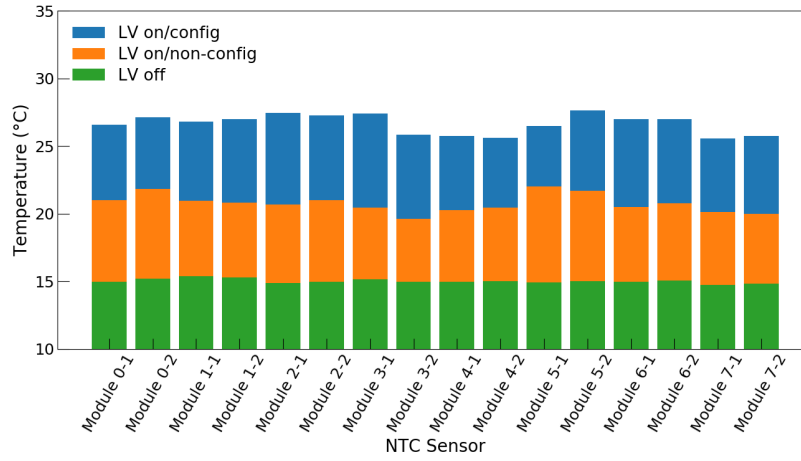


Figure 21: Thermal test results of one plane in the first station during surface commissioning. Temperature values of the SCT module NTCs for power-off (green), after powering the modules (orange) and after powering and configuring (blue).

All the temperature values are well below 35°C which is the required maximum temperature of the module. The difference was within 1°C, compared to the results in the plane commissioning. A similar thermal performance was obtained for the other two stations and after installation into TI12.

As an example of the temperature stability of the tracker planes, Figure 22 shows the temperature measured with one of two NTC sensors on each module (NTC1 and NTC2) in plane 5 during a period of 24 hours covering one calibration sequence. The analogue and digital currents consumed by the ABCD3TA chips fluctuate during the calibration, causing a slight variation of the module temperature, however this never exceeds 35°C. When the module is powered off, the temperature decreases to the coolant temperature of 15°C. It was confirmed

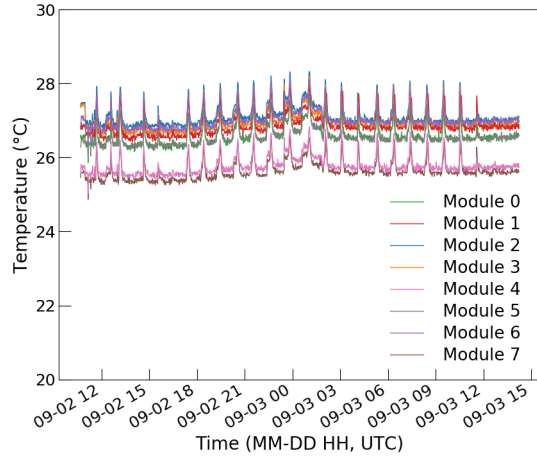


Figure 22: Temperature values of NTCs on SCT modules of plane 5 during a scan sequence for 24 hours in plane commissioning.

that the temperature was stable during the nominal operation. In addition, the dew point inside the planes was kept well below the coolant temperature during the commissioning.

5.4. Calibration procedure

The readout of the SCT barrel modules is binary, meaning there is only a hit or no-hit information depending on whether the current pulse generated by a charged particle passing through the silicon sensor is above or below the threshold set. Since the analog information of the signal pulse is not recorded, a good calibration of the ABCD3TA chips on the SCT module is essential. For this purpose, the chip contains an internal calibration circuit that enables to simulate a hit in a strip. Each channel of the readout ASIC has a 100 fC calibration capacitor connected to its input. An internal 8-bit DAC and chopper circuit are used to generate a voltage pulse that is sent to the calibration capacitor, thus by-passing the sensor strips. The amplitude of the calibration pulse can be set in the range from 0 to 160 mV (corresponding to input charges up to 16 fC), and its delay with respect to the clock phase can be adjusted in 64 steps within

50 ns. Every fourth channel can be tested simultaneously.

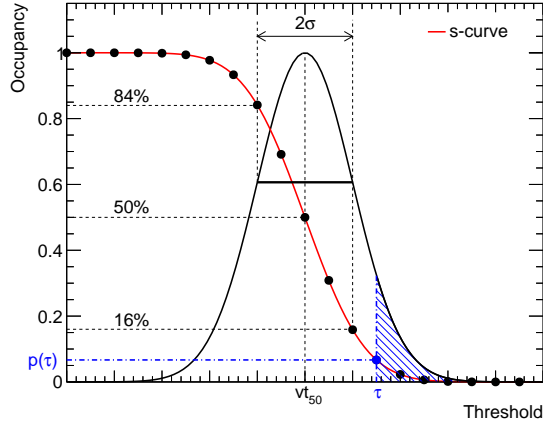


Figure 23: Illustration of a threshold scan, in which a certain number of calibration charges are injected at each threshold point. The input signal is convoluted with electronics noise, described by a Gaussian distribution function. For a given threshold τ , the hit occupancy is the fraction of signals above threshold (dashed area). The resulting s-curve, essentially a complementary error function, corresponds to the probability $p(\tau)$ that the signal is above the threshold τ .

The calibration of the chips mostly relies on so-called *threshold scans* (see Fig. 23), in which the discriminator threshold is varied in discrete steps and a set of well defined fixed-amplitude calibration charges is sent at each step. The hit occupancy, defined as the fraction of injected signals above threshold, is computed for each readout channel at each threshold point. Since the signal amplitude is convoluted with Gaussian electronics noise, the hit occupancy does not follow an ideal step function but is smeared out to give rise to the so-called *s-curve*. The threshold at which the occupancy is 50% is called the vt_{50} point and corresponds to the input charge amplitude. The width of the distribution is the noise at the discriminator output. The calibration procedure implemented for the FASER tracker largely follows that established by the ATLAS SCT collaboration [15], which has been extensively used during past years to perform the electrical characterization of the SCT modules. Typically, several tests / scans

are run in sequence, and the chip parameters are updated along the sequence. A typical calibration sequence is listed below.

1. *Mask-scan*. This test aims at determining two sorts of main defects, *i*) dead / non-responsive channels, and *ii*) very noisy channels. This is achieved by setting a very low (high) threshold, then sending a number of trigger signals (without charge injection) to read the data stored in the digital pipelines, and finally checking how many channels are below (above) threshold. The identified defective channels are disabled by tagging them in a dedicated in-chip mask register.
2. *StrobeDelay scan*. This scan is used to determine for each chip the optimum delay between the calibration charge and the clock. The calibration delay is varied in its full range and at each step the occupancy per channel is computed after charge injection. Then, the occupancies are projected to the calibration delay axis and a fit is carried out. The optimum delay is calculated to be in the plateau of maximum occupancy.
3. *Three-Point-Gain*. This test allows to estimate the gain and noise of the preamplification stage. Threshold scans are performed for three different input charges. A linear fit of the vt_{50} thresholds versus injected charge is carried out to obtain the gain (slope) and threshold offset (intercept). The input noise is calculated as the standard deviation of the s-curve fits (corresponding to the noise at the discriminator output) divided by the gain. This scan is also used to obtain a conversion for the measured thresholds in mV to fC or electrons, respectively.
4. *Trimming*. This scan aims at correcting for the threshold dispersion inside the chip. A 4-bit resolution DAC (TrimDac) allows to set individual channel threshold corrections. The TrimDac has four possible ranges, as the ABCD3TA chip was conceived to operate in the LHC environment in which the threshold spread increases with time due to accumulated radiation damage to the sensors and electronics. In the trimming procedure threshold scans are performed for various settings of the TrimDac (ranges

and step values). Given the excellent linearity of the DAC, four out of the sixteen possible steps per range are used. Using a linear fit to the vt_{50} as a function of trim value, a channel is flagged as “trimmable” if its offset can be corrected with respect to a given threshold target. The trimming settings are those that correspond to the minimum TrimDac range and the minimum threshold target (within that range) for which a maximum number of channels are trimmable. This is done on a module-by-module basis to achieve a good threshold uniformity across all channels of a given module.

5. *ResponseCurve*. With this test an accurate threshold-to-charge relation is obtained. Threshold scans are performed for ten input charges, from 0.5 fC to 8 fC. After the corresponding s-curve fits, the vt_{50} as a function of the input charge is fit to a first-degree polynomial with an exponential correction term to account for small non-linearities at very low and high injected charges, $\tau = p_2 + p_0/(1 + e^{-q/p_1})$, where p_0 , p_1 and p_2 are the fit parameters, and τ and q are the threshold in mV and fC, respectively. The average parameters for each individual ASIC are obtained to determine the mV to fC conversion.
6. *NoiseOccupancy*. Although this test is formally not part of the chip calibration (as no calibration parameters are derived from it), it is typically performed to assess the goodness of the above-mentioned procedure. The noise occupancy (NO) is defined as the probability for a strip to give rise to a hit only due to noise. This typically occurs when fluctuations at the discriminator input exceed its threshold. For the ATLAS SCT modules the noise occupancy per strip is specified to be less than 5×10^{-4} at 1 fC threshold and the nominal operating temperature. The NO is determined by performing a threshold scan without any input charge. The number of triggers sent is increased progressively as the threshold is raised.

5.5. Results of electrical and calibration tests

The calibration scans described in Section 5.4 were repeated during individual plane commissioning, station commissioning, and commissioning *in situ* after installation in TI12 as described in Section 5.1. The aim of the calibration is to achieve uniform threshold distribution, high hit efficiency ($> 99\%$) and low noise occupancy ($< 5 \times 10^{-4}$) at the nominal operating threshold of 1fC. In this sub-section, electrical calibration results are shown and compared between single module testing, plane testing and station testing - unless otherwise stated the station test results shown were obtained after the installation in TI12 during March/April 2021, however they are consistent with the station results obtained on the surface.

The leakage current of the silicon sensors was measured as a function of the applied bias voltage in the tests of a single module, plane and station. The curves are generally in fair agreement between the different stages. Figure 24 shows a comparison of the leakage current measured during single module commissioning and the plane commissioning. The individual module leakage currents are typically in the range 100–800 nA at 15°C. Since in the plane four modules are connected to one HV channel, the comparison is made by summing the individual module leakage current measurements for the four modules in a half a plane (either Module 0-3 or 4-7) (scaled to 15 °C) and comparing to the measurement in the plane itself (channel 0 or channel 1). Similar agreement was also found when comparing results of plane and station commissioning.

In order to achieve a high hit efficiency, the number of ‘bad’ strips – those identified as either dead or very noisy during the mask scan – in each module was carefully monitored during the tests for a single module and the plane and station commissioning. The modules with lower numbers of bad strips were selected to be mounted at one of the four inner module positions which are inside the central region of the magnet acceptance, as demonstrated in Figure 10. In addition, the station with the highest quality – that with lowest number of the bad strips in this region – was chosen to be placed at the front (upstream) of the spectrometer while the station with the lowest quality is located at the

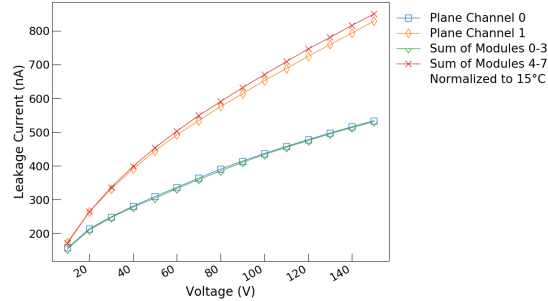


Figure 24: Comparison of leakage current measurements during single module testing (Sum of Modules 0-3/4-7 in green/red) and plane commissioning (Plane Channel 0/1 in blue/orange).

back (downstream). A pair of an electron and positron from the decay of a dark photon is most collimated at the upstream station, therefore, the station with the best performance was selected for that position. Table 3 shows the number of masked channels observed during the *in situ* commissioning after the installation. In the inner region of the magnet acceptance the number of masked channels is below 0.1%. Even in the region mostly outside the magnet acceptance, this is less than 0.5%.

Station	Inner region	Outer region
Station 1 (upstream)	0.02%	0.06%
Station 2 (middle)	0.03%	0.04%
Station 3 (downstream)	0.08%	0.31%

Table 3: Fraction of the masked channels in each tracker layer for the four modules in the inner (outer) region of the magnet acceptance.

The gain measured in the three-point-gain measurements are shown in Fig. 25a. The average over all the chips in all stations is 54 mV/fC, which is in good agreement with the ~ 55 mV/fC expected from the module specification [12]. The dependence of the gain over a larger range of injected charges is tested in the response curve scan. Figure 25b shows the typical result of the response curve scan for a single strip.

After the trim scan, an even response between different channels in a module is obtained, as shown in Fig. 26. The majority (99.9%) of the channels can be trimmed using the two lowest trim range settings, as expected for unirradiated modules, and an additional 0.05% of channels can be trimmed using one of the larger trim ranges. The remaining channels cannot be trimmed even at the largest trim range setting.

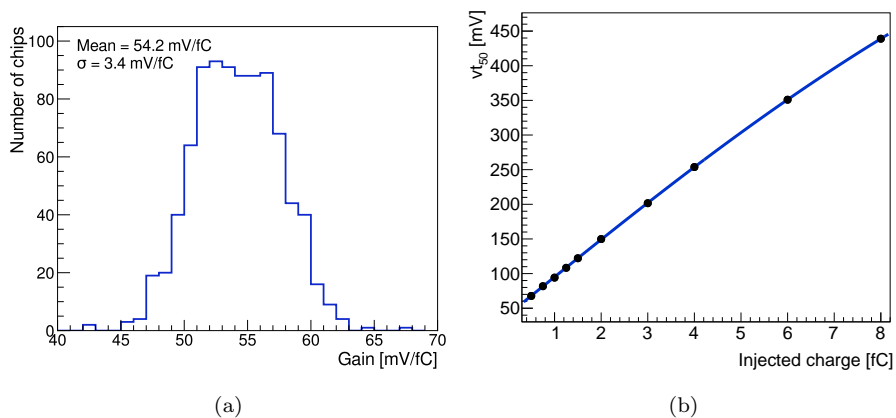


Figure 25: (a) Distributions of the gain per chip in each station. (b) Example response curve fit for a single strip.

It is important to keep the level of readout noise as low as possible to maintain low thresholds and accordingly realize high tracking efficiency. An estimate of the input Equivalent Noise Charge (ENC) is obtained, using the three-point-gain measurement during the routine calibration scans described in Section 5.4. This provides a measurement of the output noise value with an injection charge of 2 fC. The distribution of ENC for all the chips in the three stations are shown in Fig. 27a, whose mean value is 1515 electrons. This is in good agreement with the ~ 1500 electrons expected for unirradiated modules from the specifications [12].

The additional dedicated noise occupancy scans were also performed for a more direct measurement of the noise, where no charge is injected, as shown in Fig. 27b. Due to the large number of triggers required at high thresholds

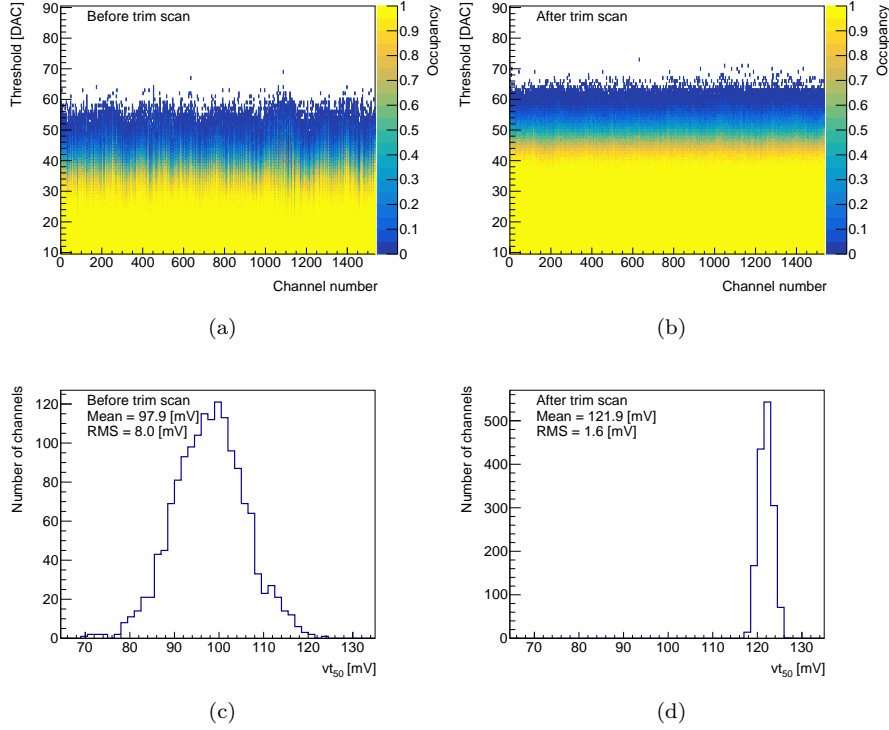


Figure 26: Threshold scan for an example module with 1.5 fC injected charge before (a), and after (b) optimal trim settings from the trim scan are applied. The distributions of the vt_{50} points for all strips are also shown before (c), and after (d) the trim scan.

these take a considerably longer time than the three-point-gain measurement. The noise occupancy scans are, however, more sensitive to the tails of the noise distribution and to external sources such as a commonly increased noise on several channels (common-mode noise). The ENC from the noise occupancy scans is extracted from a linear fit to $\log(\text{noise occupancy})$ vs threshold^2 in fC^2 .

The ENC evaluated from the noise occupancy scan and the three-point-gain measurement correlate well as shown in Fig. 28a, and are in good agreement with measurements of the ATLAS SCT modules [12]. Fig. 28b shows the noise occupancy at the nominal 1 fC thresholds using randomly triggered events dur-

ing combined system runs *in situ*, which provides a further cross-check of the measured noise. Over 99.7% of the the strips in the tracker satisfy the performance criteria that the noise occupancy per channel is less than 5×10^{-4} at the nominal 1 fC threshold. The main reason of noisy strips is a non-linear behavior in the response curve illustrated in Fig. 25b.

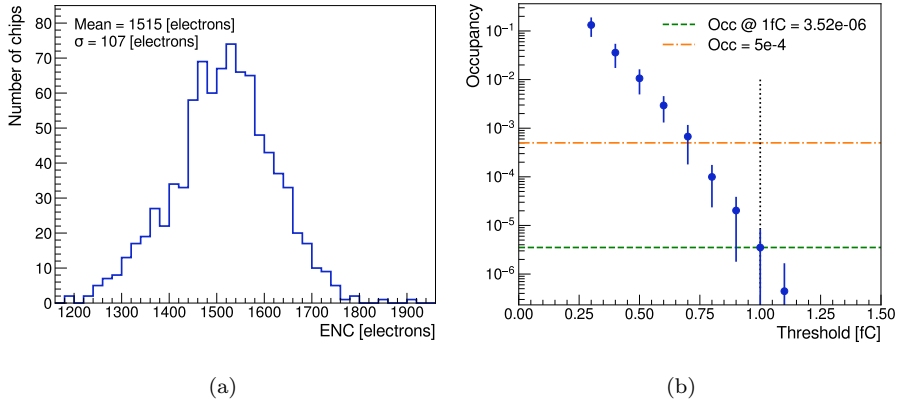


Figure 27: (a) ENC per chip in each tracker station, and (b) noise occupancy scan for a single chip.

There is the trend of a slight reduction in noise (for the same gain) in station commissioning compared to the plane commissioning step. This could be caused by an improved grounding scheme in the station.

5.6. Magnetic field test

One of the concerns for the installation of the FASER tracker in between the gaps of the permanent FASER magnets was the presence of the stray magnetic field during the lowering of the tracker planes. In order to exclude any negative impact on the performance or damage due to electromagnetic induction a test stand was set up that allowed to lower the FASER prototype tracker plane vertically in a controlled way at different distances to the aperture of one of the FASER magnets for testing purposes.

In a first step, the tracker plane was positioned 1 m away from the aperture (reference position) and a standard calibration and characterization sequence

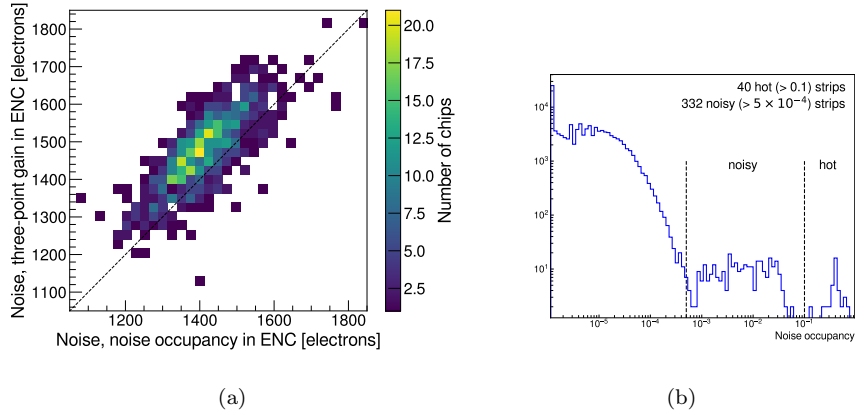


Figure 28: Correlation between (a) ENC measured in the three-point-gain and in the noise occupancy scans, and (b) strip-by-strip noise occupancy measured from random triggers during combined runs.

was run, i.e. the identification of noisy and non-responsive strips as well as the measurement of gain, threshold, electronics noise, and the sensor IV response. At the reference position the magnetic stray field is negligible. In a second stage, the mechanical mounting structure was placed in a distance of 65 mm from the magnet aperture which corresponds roughly to the distance of the first tracker plane in the final FASER assembly. At this location, the magnetic field strength of the stray field amounts to up to 60 mT. The plane was lowered at a very low speed of about 0.03 m/s until it was finally centered in front of the magnet aperture. During the lowering process all cables (data, power, DCS) remained attached to the patch-panel of the plane, but were disconnected at the off-detector end. A second set of performance measurements was taken at this position. In a final step, a further reference measurement was taken at the reference position after the plane has been extracted in the reverse order with respect to the installation.

The number of noisy and non-responsive strips was found to be very consistent between the different measurement positions. The same conclusion applies to the measured gain as well as thresholds. Only for the noise, changes in the

order of a few percent could be observed between the different measurement positions, but no correlation with respect to the presence of the magnetic field was observed. It is more likely that the observed changes can be attributed to small differences in the grounding after the mechanical movement of the setup.

In conclusion, no sign for any damage or performance degradation could be found in this installation tests.

5.7. Cosmic ray test

In order to test the FASER tracker station as a full detector system including trigger and DAQ, a cosmic ray test stand has was set up in the FASER surface laboratory. Figure 20 shows the setup in which the tracker station is placed horizontally in between two large trigger scintillators covering the full detector acceptance.

After successfully timing in the tracker with respect to the trigger, correlated hits could be reconstructed across all tracker layers. Figure 29 depicts an example event display of a cosmic ray candidate traversing all three tracker layers leaving a clear signature. The reconstructed space points from the crossing of two strips per layer are well compatible with a straight track through the detector.

Beyond the bare proof of the tracker functionality and its interplay with the larger FASER trigger/DAQ system, the collected cosmics data set is very valuable for the intra-station alignment due to the absence of any stray magnetic field which will not be the case once integrated in between the FASER permanent magnets. The successful cosmic ray test concluded the tracker station commissioning on the surface.

5.8. Summary of commissioning

Three stations consisting of nine planes were successfully assembled and commissioned on the surface and subsequently *in situ* after installation. Overall a very good performance was found, which is comparable between surface plane commissioning and station commissioning and in the tunnel. The long term

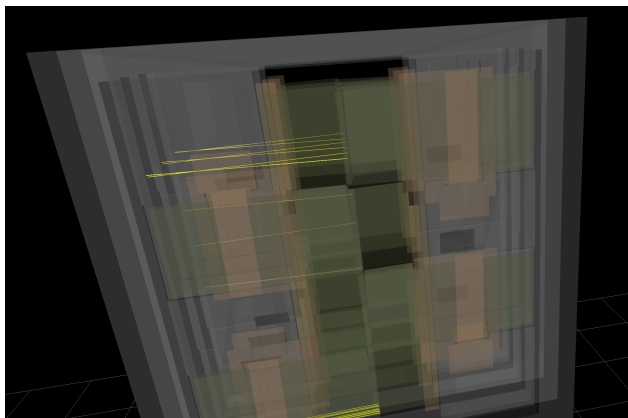


Figure 29: Event display of a cosmic ray candidate traversing all three layers of one FASER tracker station.

stability of full stations were additionally confirmed in long runs which lasted several weeks and was partially accompanied with data taking of cosmic ray events.

6. Conclusion and outlook

The FASER tracker was designed to fulfill the requirements needed to search for light new long-lived particles, produced in LHC collisions at the ATLAS interaction point, and decaying to two oppositely charged particles inside the FASER decay volume. The decay products would be high energy and extremely collimated, and the tracker must be able to resolve the two closely spaced charged particles down to $\mathcal{O}(100 \mu\text{m})$. Other constraints driving the tracker design were the need to minimize the required services, the need for a robust design, and to be able to construct and install the tracker in a short timescale (during LHC long shutdown 2) and at a low cost.

The FASER spectrometer was constructed with three tracker stations, comprising of nine planes of the silicon strip modules that were originally the spares for the ATLAS SCT barrel detector. All other parts of the tracker, including dedicated support frames, DCS and cooling system, readout electronics and

services were newly developed for FASER. After construction and assembly, metrology of the tracker, to ensure a precise alignment within the mechanical tolerances, was performed for each plane and station. The design of the system was carried out during 2018, prototype components were produced and tested during 2019, and the final system fabricated and commissioned on the surface during 2020. The installation of the tracker into the T112 tunnel was carried out in March 2021.

The installed detector is fully operational and shows excellent performance, well within the specifications. The number of dead channels is less than 0.5% (including the region outside the main magnet acceptance). The electrical performance of the detector was tested after calibration of the ABCD3TA readout chips at each stage of the construction. During the *in situ* commissioning of the final FASER setup, the average noise (ENC) was evaluated to be 1515 electrons, and the noise hit occupancy at 1 fC threshold was 2.3×10^{-5} which is within the requirement of $< 5 \times 10^{-4}$. Long-term operation as part of the commissioning showed that all the SCT modules can be kept below the required maximum temperature of 35 °C with coolant temperature of 15 °C. In addition to standalone tests, the tracking detector was tested as part of the full FASER detector commissioning using the final TDAQ system, for example for combined cosmic ray data taking.

A new tracker station, identical to the three already installed in FASER, and called the “Interface Tracker”, will be installed between the FASER ν emulsion detector and the main FASER detector. This Interface Tracker will allow matching tracks between the emulsion detector and the FASER tracker, and enable to distinguish ν_μ and $\bar{\nu}_\mu$ interactions by measuring the charge of the produced muon in the FASER spectrometer. The Interface Tracker construction and surface commissioning started in June in 2021, and the installation is planned for late-2021.

The FASER experiment will start physics data-taking in proton-proton collisions from the start of LHC Run 3 operations in 2022. The tracker will act as one of the crucial detectors to allow to search for new light long-lived neutral

particles in FASER.

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