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Ion-acoustic shocks with self-regulated ion reflection and acceleration

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An analytic solution describing an ion-acoustic collisionless shock, self-consistently with the evolution of shock-reflected ions, is obtained. The solution extends the classic soliton solution beyond a critical Mach number, where the soliton ceases to exist because of the upstream ion reflection. The reflection transforms the soliton into a shock with a trailing wave and a foot populated by the reflected ions. The solution relates parameters of the entire shock structure, such as the maximum and minimum of the potential in the trailing wave, the height of the foot, as well as the shock Mach number, to the number of reflected ions. This relation is resolvable for any given distribution of the upstream ions. In this paper, we have resolved it for a simple “box” distribution. Two separate models of electron interaction with the shock are considered. The first model corresponds to the standard Boltzmannian electron distribution in which case the critical shock Mach number only insignificantly increases from $M \approx 1.6$ (no ion reflection) to $M \approx 1.8$ (substantial reflection). The second model corresponds to adiabatically trapped electrons. They produce a stronger increase, from $M \approx 3.1$ to $M \approx 4.5$. The shock foot that is supported by the reflected ions also accelerates them somewhat further. A self-similar foot expansion into the upstream medium is described analytically. © 2016 AIP Publishing LLC. [<http://dx.doi.org/10.1063/1.4945649>]

I. INTRODUCTION

Collisionless shocks emerged in the 1950s and 1960s of the last century as an important branch of plasma physics (see Refs. 20, 36, 38, and 40 for review) and have remained ever since. Meanwhile, new applications have posed new challenges to our understanding of collisionless shock mechanisms. Particle acceleration in astrophysical settings, primarily studied to test the hypothesis of cosmic ray origin in supernova remnant shocks (see, e.g., Refs. 5, 6, and 29 for review), stands out, and the collisionless shock mechanism is the key here. Among recent laboratory applications, a laser-based tabletop proton accelerator is frequently highlighted as an affordable compact alternative to expensive synchrotron accelerators.^{7,12,18}

The goal of this article is twofold. First, we will obtain a self-consistent analytic solution for the electrostatic structure of an ion-acoustic collisionless shock with the Mach numbers beyond a critical value $M = M_* \approx 1.6$, for Boltzmannian electrons, and $M_* \approx 3.1$, for adiabatically trapped electrons. As these two models predict quantitatively different critical Mach numbers, a short digression into the choice between them is in order.¹⁶

First of all, one distinguishes between electrons freely passing the soliton (or shock structure) and those captured into its potential. The distribution of the first category of electrons is assumed to be Maxwellian in both Boltzmannian and adiabatic models, as these electrons originate from regions not related to the soliton (e.g., laser-heated plasma, acting as a piston that drives the soliton/shock). The distribution of the second category depends on whether or not they

intermix with the first category over the evolution time of the trapping potential, τ . The trapping region in velocity space has a width $\Delta V_{tr} \sim \sqrt{e\phi/m}$, where ϕ is the soliton or shock potential. On the other hand, electrons change their velocity due to collisions over time τ by $\Delta V_{col} \sim \sqrt{\nu\tau}V_{Te}$, where ν is the electron collision frequency, and V_{Te} is the thermal velocity. If $\Delta V_{col} > \Delta V_{tr}$, then the Maxwellian distribution spreads over the region of trapped particles in phase space. The Boltzmannian model applies to all electrons in this case. If the opposite is the case, $\Delta V_{col} < \Delta V_{tr}$, then the trapped particles, having closed orbits, sustain their distribution, generally depending on their trapping history. Therefore, they are more accurately described by the adiabatic trapping model, while the free electrons remain Maxwellian. Note that the collisions may be both binary or “effective,” i.e., associated with the instabilities of trapped electrons (e.g. Ref. 27).

The above models for electron distribution produce two different forms of electron density distribution in terms of the wave potential $n_e(\phi)$. One form is a Boltzmannian, $n_e = n_0 \exp(e\phi/T_e)$ which, as we pointed out, yields $M_* \approx 1.6$.³⁸ The other form corresponds to adiabatically trapped electrons with a flat distribution in the wave potential. In this case, $M_* \approx 3.1$.¹⁶ Depending on the practical situation, either model can be used. As discussed above, the Boltzmannian requires a Maxwellian distribution for electrons trapped in the potential wells (in analogy with barometric formula). One can expect such scenario in the case when a higher density plasma expands into a lower density (upstream) region. A suitable example found in the conventional gas dynamics is a shock tube, in which the shock is

generated by breaking up a diaphragm, which was separating the tube sections with different gas densities. By contrast, the adiabatic trapping can be expected in a piston tube, in which the piston moves into an initially uniform medium. Therefore, it models the shocks generated in the pulsed laser-plasmas more accurately. Under these circumstances, the production of reflected ions can be considered as the laser-driven acceleration. It becomes more energy-efficient at $M > M_*$, while producing almost monoenergetic ions over an extended time interval.

At $M \geq M_*$, the shock reflects some of the upstream ions. So the second goal of this paper is to study the dynamics of these ions, including their further acceleration. A self-similar simple wave solution for electrostatic potential in a foot region ahead of the shock will be obtained selfconsistently with the incident and reflected ion dynamics. We will show that an additional drop in the foot electrostatic potential critically affects the ion reflection from the main part of the shock. So, unlike most of the earlier analyzes treated the ion reflection using the test particle approximation, e.g., Refs. 12 and 32, we incorporate it into the global shock structure. This study is relevant to the electrostatic shock propagation in laser-produced plasmas, especially to the problem of generation of monoenergetic ion beams, ion injection into the diffusive shock acceleration (DSA) in astrophysical shocks, and other shock-related processes in astrophysical and space plasmas.

In studying collisionless shocks, it is crucial to identify the shock-supporting linear wave mode and to describe its nonlinear evolution, appropriate for the shock environment. In non-isothermal plasmas, with the electron temperature much higher than the ion temperature, $T_e \gg T_i$, a nonlinear Korteweg–de Vries (KdV) equation adequately describes the *ion-acoustic waves* as long as the nonlinearity remains *weak*. Of course, the KdV equation is famous for its soliton solution, one of the most remarkable mathematical construction widely used in physics. In plasmas, the solitons emerge when neither collisional nor Landau damping is present. The *ion-acoustic solitons*, in particular, are the building blocks of collisionless shock waves at $T_e \gg T_i$. Most lucidly, they emerge from a solution *pseudopotential*, for an arbitrarily *strong* nonlinearity, thus comprising the limiting case of a cnoidal wave solution with an infinite period.³⁸ This solution can also be interpreted as the uppermost “energy level” in a continuum of bound states in the pseudopotential, whereas the lower energy states correspond to the periodic (cnoidal) waves. The usage of pseudopotential also provides information about a soliton wave-train that forms when even a small “damping” leads to the particle energy change in the pseudopotential which in reality corresponds to the inner structure of the shock front.³³ The underlying mechanism here is the nonlinear Landau damping. Just a few ions upstream reflected by the electric potential of the first soliton will result in such damping. Then, by the “nonlinear saturation” effect, there are no more “resonant” ions to interact with the soliton train past the leading soliton.

In the absence of resonant ions upstream, the first soliton breaks down at $M > M_* \simeq 1.6$ (for cold upstream ions and Boltzmannian electrons). The solution ceases to exist beyond

this point, as there is no proper “energy level” in the pseudopotential. This solution disappearance was thought to be the point of “*overturning of the shock front*” and the end of the so-called “*laminar*” regime of ion-acoustic collisionless shocks. However, the results of this paper prove otherwise. Namely, by including the reflected ions into the shock structure, we have found the laminar solution to continue beyond $M = M_*$! More precisely, we found that when ions begin to reflect from the soliton tip at $M = M_1 \leq M_*$, the classical single soliton solution bifurcates into a more complex structure. It comprises (i) the first soliton, (ii) the infinite periodic wave train downstream of it, and (iii) the foot occupied by the reflected ions. The front edge of the foot undergoes self-similar spreading in a comoving reference frame of reflected ions. This solution continues up to $M = M_2 \geq M_*$.

At the second critical Mach number M_2 , almost all incident ions reflect, so the foot potential raises to increase the total shock Mach number significantly above M_* . For the cold upstream ions, $T_i \ll T_e$, M_1 approaches M_* , that is $M_1 = M_* - \mathcal{O}(\sqrt{T_i/T_e})$, while $M_2 \approx \sqrt{M_*^2 + (1 - 1/4M_*^2)^{-1} \ln(1 + \alpha)}$, where α is the fraction of reflected ions. Note that $M_2 \approx 1.8$ for $\alpha = 1$ and Boltzmannian electrons. The case of adiabatically trapped electrons, in which $M_* \approx 3.1$, gives a considerably higher Mach number, $M_2 \approx 4.5$. The same pseudopotential technique³⁸ also recovers the shock profile, although by introducing two separate pseudopotentials $\Phi^\pm(\phi) = 4\pi e \int (n_e - n_i^\pm) d\phi$, used for the plasma upstream and downstream of the leading soliton ($n_i^+ \neq n_i^-$ due to the ion reflection). Here, ϕ denotes the shock electrostatic potential.

Within the range between the two critical points $M_1 < M < M_2$, the only time-dependent part of the solution is near the leading edge of the reflected ion population. They support a pedestal upstream of the leading soliton on which it rests. The reflected ions escape upstream with double the shock speed in the pedestal reference frame, Fig. 1. Their further fate is determined by a relatively slow spreading of the initially sharp front edge. By even a small velocity dispersion, ions with higher initial velocity undergo additional electrostatic acceleration by passing through the shock pedestal. This process is described analytically as a self-similar solution, which also yields the maximum velocity of reflected ions.

The paper is organized as follows. In Sec. II, we discuss the shock model. Sec. III describes the main part of the shock transition that forms in place of the parent soliton after it has reflected a first few ions. Sec. IV presents a self-similar solution for the shock precursor supported by reflected ions. We conclude with a Discussion in Sec. V.

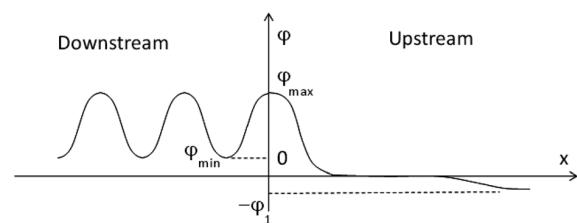


FIG. 1. Electrostatic potential of the shock structure consisting of a pedestal, leading soliton, and trailing wave.

II. THE SHOCK MODEL

The analytic solution for an ion-acoustic soliton was first obtained for the Boltzmannian electron distribution³⁸ and extended later to the case of adiabatically trapped electrons.¹⁶ Ions were assumed to be cold in both instances, which strictly limited the maximum Mach numbers to $M_* \simeq 1.6$ and $M_* \simeq 3.1$ for the Boltzmann and adiabatic electrons, respectively. When the Mach number reaches the maximum, the soliton begins to reflect some of the upstream ions and the shock model must include them. Unlike the soliton, the shock profile resulting from the ion reflection is asymmetric about the reflection point. As shown in Ref. 33, its downstream part oscillates. Upstream of the soliton, reflected ions will create a foot with an elevated electrostatic potential.

Seeking to extend the analytic solution beyond the ion reflection point, we need a manageable reflection model. At a minimum, the model should be able to relate the shock potential ϕ_{\max} and Mach number M to the number of reflected ions. Therefore, the model must be kinetic, so one obtains the shock potential given the shock speed and upstream ion distribution with a *finite* temperature. If the ion temperature upstream was zero ($V_{Ti} = 0$), the ions would reflect all at once when the shock Mach number crosses the point $M = \sqrt{2e\phi_{\max}/T_e}$. By contrast, if $V_{Ti} \neq 0$, then the reflection parameter $\alpha = n_{\text{refl}}/n_{\infty} < 1$, which is the ratio of reflected ion density to that of the incident ions far away from the soliton, will continuously depend on the shock parameters M and ϕ_{\max} . The region ahead of the shock filled with the reflected ions of constant density (foot of the shock) is mathematically regarded as “infinity” in the treatment of the main part of the shock transition. There all the relevant

quantities, such as the electrostatic potential ϕ , are considered asymptotically constant. The shock foot (precursor) will obviously expand linearly with time after the first ions are reflected. In considering the main part of the shock transition, we will count the plasma potential from its value in the foot, so that we set the potential at “infinity” to $\phi = 0$ in this section. Turning to the transition near the leading edge of reflected ions in Sec. IV, we will account for the foot potential ϕ_1 in the solution obtained in this section, Fig. 1.

To describe ion reflection, we use a simple generalization of a cold ion distribution upstream that provides an ion reflection model satisfying the above requirements. So we use a “box” ion distribution with the finite thermal velocity defined as $V_{Ti} = v_2 - v_1$:

$$f_i^{\infty}(v) = \frac{1}{v_2 - v_1} \begin{cases} 1, & -v_2 < v < -v_1 \\ 0, & v \notin (-v_2, -v_1). \end{cases} \quad (1)$$

The normalization of f_i^{∞} implies a unity density of incident ions far enough from the shock but not farther than the slowest particles in the leading group of reflected ions at a given time, as we discussed earlier. We use the shock frame throughout this section. It is convenient to introduce a dimensionless potential by replacing $e\phi/T_e \rightarrow \phi$ and measure the coordinate in units of $\lambda_D = \sqrt{T_e/4\pi e^2 n_{\infty}}$, while the ion velocity in units of the sound speed $C_s = \sqrt{T_e/m_i}$.

Suppose the soliton propagates in the positive x -direction with a nominal speed $U = \sqrt{2\phi_{\max}}$ (with respect to the foot), where $\phi_{\max} = \phi(0)$ is the maximum of its potential, and $v_1 \leq U \leq v_2$. The ion density upstream and downstream can then be written as follows, Fig. 2:

$$n_i(\phi) = \frac{1}{v_2 - v_1} \begin{cases} \sqrt{v_2^2 - 2\phi} - \sqrt{U^2 - 2\phi}, & x \leq 0 \\ \sqrt{v_2^2 - 2\phi} + \sqrt{U^2 - 2\phi} - 2\sqrt{v_1^2 - 2\phi}, & x > 0, \quad 0 < \phi < v_1^2/2 \\ \sqrt{v_2^2 - 2\phi} + \sqrt{U^2 - 2\phi}, & x > 0, \quad v_1^2/2 \leq \phi \leq U^2/2. \end{cases} \quad (2)$$

Again, we count the electrostatic potential from its value in the shock foot. We note that U is not precisely the soliton velocity but rather a convenient notation for $\sqrt{2\phi_{\max}}$, while the soliton velocity with respect to the foot plasma (Mach number in this reference frame) is $M = (v_1 + v_2)/2$. The soliton speed in the upstream plasma frame can only be determined when the foot potential ϕ_1 is obtained, Fig. 1. It is also important to note here that our choice of the simplest form of ion distribution, Eq. (1), resulting in the ion density including the reflected ions should lead to the same shock structure in the limit $V_{Ti} \rightarrow 0$ as in the case of, say, Maxwellian distribution. In the latter case, the ion density in Eq. (2) would be expressed through the error function. However, the limit $V_{Ti} \rightarrow 0$ can only be taken after the solution for the shock profile is obtained.

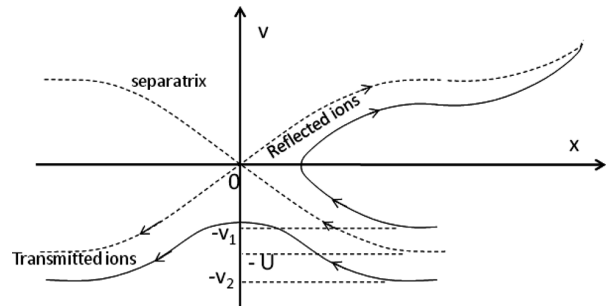


FIG. 2. Phase plane of ions at reflection point and propagation of reflected ion beam accompanied by its further acceleration into the upstream medium and narrowing its velocity distribution at large x .

From this point on, our treatment will depend on the particular electron model, Boltzmannian or adiabatically trapped electrons. In Subsections II A and II B, these two models are considered separately.

A. Boltzmannian electrons

Based on the above definitions, the Poisson equation for the shock electrostatic potential can be written as follows:

$$\frac{d^2\phi}{dx^2} = (1 + \alpha)e^{\phi} - n_i(\phi), \quad (3)$$

where

$$\alpha = \frac{U - v_1}{v_2 - v_1}, \quad (4)$$

is the fraction of ions reflected off the shock, so that the first term on the r.h.s of Eq. (3) corresponds to the electron contribution. We have chosen its normalization in such a way as to neutralize the sum of the incident and reflected ions in the foot, according to their normalization in Eq. (1). We may now integrate Eq. (3) once, also imposing the condition $\phi'(\phi_{\max}) = 0$. The resulting equation takes the following form:

$$\frac{1}{2} \left(\frac{d\phi}{dx} \right)^2 = \Phi(\phi) + \mathcal{F}^{\pm}(\phi) \equiv \Phi^{\pm}(\phi), \quad (5)$$

where “+” or “−” sign should be taken for $x \geq 0$ and $x < 0$, respectively. The functions Φ and \mathcal{F}^{\pm} are given by the following relations:

$$\Phi = (1 + \alpha) \left(e^{\phi} - e^{U^2/2} \right) + \frac{(v_2^2 - 2\phi)^{3/2} - (v_2^2 - U^2)^{3/2}}{3(v_2 - v_1)}, \quad (6)$$

$$\mathcal{F}^{\pm} = \frac{1}{3(v_2 - v_1)} \times \begin{cases} (U^2 - 2\phi)^{3/2} - 2(v_1^2 - 2\phi)^{3/2} \vartheta(v_1^2 - 2\phi), & x \geq 0 \\ -(U^2 - 2\phi)^{3/2}, & x < 0, \end{cases} \quad (7)$$

where ϑ is a Heaviside function. These relations are written for the case $U \geq v_1$, while the opposite case would correspond to the standard soliton solution with no ion reflection but with finite upstream ion temperature, which we do not

consider in this paper. It is convenient to refer to the functions $\Phi^{\pm}(\phi)$ as to pseudopotentials of anharmonic oscillators of unit masses, whose kinetic and potential energies correspond, respectively, to the l.h.s. and the r.h.s of Eq. (5). Here, ϕ represents the oscillator coordinate and x represents time.³⁸ The shock structure $\phi(x)$ is thus completely determined by Eq. (5) in a form of an inverse function $x(\phi)$ under an appropriate choice of its branches upstream and downstream. In Sec. III, we specify the critical parameters of the shock profile ϕ_{\max} and ϕ_{\min} , depending on the upstream ion temperature and Mach number. Again, by “upstream” we mean here the shock foot region where $\phi = 0$, Fig. 1.

B. Adiabatically trapped electrons

Boltzmann distribution for electrons near the shock that we considered above is not always the best choice. If they drive the shock by themselves, the shock may confine them, at least in part, to the downstream side by trapping in its potential. The trapped electrons acquire then a flat distribution, while the free ones maintain their Maxwellian distribution.¹⁶ Hence, the following electron density distribution replaces the Boltzmann distribution in the Poisson equation given by Eq. (3):

$$\frac{d^2\phi}{dx^2} = (1 + \alpha) \frac{F(\phi + \phi_1)}{F(\phi_1)} - n_i(\phi), \quad (8)$$

where

$$F(\phi) \equiv e^{\phi} \operatorname{erfc} \sqrt{\phi} + 2\sqrt{\phi/\pi},$$

while the ion distribution remains the same as in Eqs. (2) and (3). In deriving Eq. (8), we assumed electrons with negative energy $E_e = mv^2/2 - e\phi(x) \leq 0$ to remain on the downstream side of the shock structure, where their distribution f_0 is constant, while the rest of the electrons obey the standard Maxwell-Boltzmann distribution. Apart from the normalization factor that accounts for the ion reflection rate α and the finite shock foot potential ϕ_1 , this distribution is identical to that used by Gurevich in Ref. 16 for collisionless electrons trapped into a soliton. Similarly to Eq. (5), the first integral of the Poisson equation can be written as follows:

$$\frac{1}{2} \left(\frac{d\phi}{dx} \right)^2 = \Phi_a(\phi) + \mathcal{F}^{\pm}(\phi) \equiv \Phi_a^{\pm}(\phi),$$

where

$$\Phi_a(\phi) = (1 + \alpha) \frac{F(\phi + \phi_1) - F(\phi_{\max} + \phi_1) + \frac{4}{3\sqrt{\pi}} \left[(\phi + \phi_1)^{3/2} - (\phi_{\max} + \phi_1)^{3/2} \right]}{F(\phi_1)} \quad (9)$$

$$+ \frac{(v_2^2 - 2\phi)^{3/2} - (v_2^2 - U^2)^{3/2}}{3(v_2 - v_1)}, \quad (10)$$

and \mathcal{F}^{\pm} is given by Eq. (7). Again, we have added an integration constant to ensure that $d\phi/dx = 0$ at $\phi = \phi_{\max}$. Once the shock model is defined for the two types of electron distribution, we proceed with the solutions for the respective shock structures.

III. SOLUTION FOR THE MAIN PART OF THE SHOCK TRANSITION

A. Boltzmannian electrons

An implicit solution for the potential $\phi(x)$ in the regions $x \geq 0$ may be written using Eq. (5) by the following inverse relations for $x(\phi)$:

$$x(\phi) = \pm \frac{1}{\sqrt{2}} \int_{\phi}^{\phi_{\max}} \frac{d\phi'}{\sqrt{\Phi^{\pm}(\phi')}}. \quad (11)$$

At the point where ions are about to reflect off the soliton tip, that is when $U = v_1$ ($\alpha = 0$), two pseudopotentials are equal, $\Phi^+ = \Phi^-$. Therefore, the (soliton) solution remains symmetric, as it has to be in the case with no ion reflection. It is selected by imposing an additional constraint on the pseudopotential Φ^+ . Namely, $\Phi^+(\phi)$ must have a double root at $\phi = 0$: $\Phi^+(0) = 0$, $\Phi^{+'}(0) = 0$ regardless of α being zero or positive. Note that the second condition, $\Phi^{+'}(0) = 0$, is satisfied automatically via our choice of normalization of electron contribution, Eq. (3), that ensures charge neutrality at $+\infty$. The condition $d\phi/dx = 0$ at $x = \infty$, that amounts to $\Phi^+(\phi = 0) = 0$, yields the following nonlinear dispersion relation for the shock:

$$(1 + \alpha)(e^{U^2/2} - 1) = \frac{v_2^3 + U^3 - 2v_1^3 - (v_2^2 - U^2)^{3/2}}{3(v_2 - v_1)}. \quad (12)$$

Indeed, this is a relation between the shock amplitude $\phi_{\max} = U^2/2$ and its speed (Mach number with respect to shock foot) $M = (v_1 + v_2)/2$, just as in the case of conventional ion-acoustic soliton of Ref. 38. An important difference, however, is that this relation also includes the ion reflection coefficient $\alpha = (U - v_1)/(v_2 - v_1)$ and the upstream velocity dispersion $V_{Ti} = v_2 - v_1$, through which the upstream ion bounding velocities v_1 and v_2 in Eq. (12) may always be expressed. In particular, $M = U + (1/2 - \alpha)V_{Ti}$. Assuming that $V_{Ti} \ll U$, from Eq. (12), we obtain

$$e^{U^2/2} - 1 - U^2 = -\frac{1}{3}(2U)^{3/2} \frac{(1 - \alpha)^{3/2}}{1 + \alpha} V_{Ti}^{1/2}. \quad (13)$$

The l.h.s. of this relation is identical to the soliton dispersion relation (l.h.s. = 0) taken at the ion reflection potential ($\phi_{\max} = U^2/2$). Therefore, the ion reflection does not change the shock speed with respect to the shock precursor in a plasma with cold ions upstream, $V_{Ti} \rightarrow 0$. Comparing Eqs. (12) with (13), we see how this results from canceling out of the factor $1 + \alpha$. However, the shock speed does grow with the ion reflection rate α with respect to the upstream frame (since the precursor height ϕ_1 grows as well), which we discuss later. It is also interesting to observe that the thermal correction to the shock speed diminishes with an increase in ion reflection, $\alpha \rightarrow 1$.

Neglecting the r.h.s. of Eq. (13) (cold upstream ions, $V_{Ti} \rightarrow 0$, or $\alpha \rightarrow 1$) gives the solution for the critical Mach number $U = M_* \approx 1.6$.³⁸ For a finite $V_{Ti} \ll v_{1,2}$ and

arbitrary $\alpha < \alpha_c \approx 1$ (see below), we obtain the following dispersion relation:

$$U \approx M_* - \frac{2^{3/2}(1 - \alpha)^{3/2} M_*^{1/2} V_{Ti}^{1/2}}{3(1 + \alpha)(M_*^2 - 1)}. \quad (14)$$

Turning to the spatial profile of the potential downstream ($x < 0$), from Eq. (5) and Fig. 3, we see that it oscillates between its minimum value ϕ_{\min} and $\phi_{\max} = U^2/2$ that is given by Eq. (14). Similarly to the above equation for ϕ_{\max} , given by Eq. (13), from Eq. (5), we obtain the following equation for ϕ_{\min} :

$$\begin{aligned} e^{U^2/2} - e^{\phi_{\min}} &= \frac{(v_2^2 - 2\phi_{\min})^{3/2} - (U^2 - 2\phi_{\min})^{3/2} - (v_2^2 - U^2)^{3/2}}{3(1 + \alpha)(v_2 - v_1)}. \end{aligned} \quad (15)$$

The solution for ϕ_{\min} simplifies for the cases of weak and strong reflections. So, for $\alpha \ll 1$, using also Eq. (14), we find

$$\phi_{\min} \simeq \frac{2M_*^2 \sqrt{\alpha}}{\sqrt{M_*^2 - 1}}.$$

The opposite case of strong reflection, $1 - \alpha \ll 1$, should be treated with care when the small parameter $1 - \alpha$ approaches the thermal spread of incident ions, V_{Ti} . First, assuming that $V_{Ti} \ll 1 - \alpha \ll 1$, we obtain

$$\phi_{\min} \simeq \phi_{\max} - \frac{M_*^2(1 - \alpha)^2}{2(1 + M_*^2)^2}.$$

For smaller $1 - \alpha$, we may write

$$\phi_{\min} \simeq \phi_{\max} - \frac{9}{4}(1 - \alpha)V_{Ti}M_* \left[1 - \sqrt{\frac{2V_{Ti}}{(1 - \alpha)} \frac{(1 + M_*^2)}{\sqrt{M_*}}} \right]^2. \quad (16)$$

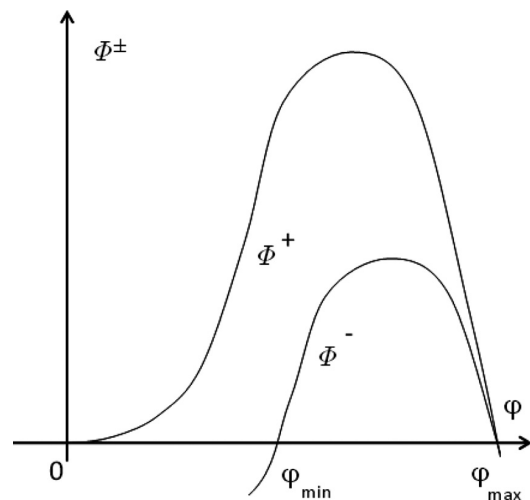


FIG. 3. Pseudopotentials of “oscillators” described by Eq. (5).

The last solution cannot be continued to $\alpha = 1$, as ϕ_{\min} reaches ϕ_{\max} at

$$\alpha = \alpha_c \simeq 1 - 2V_{Ti}(1 + M_*^2)^2/M_* < 1. \quad (17)$$

It is not difficult to understand why there is no solution corresponding to complete ion reflection as $\alpha_c \neq 1$. Indeed, a solution with all particles reflected from the shock would nevertheless require a finite density downstream (to neutralize electrons), which could be possible only if the incident ions had no velocity dispersion (that is why $1 - \alpha_c \sim V_{Ti}$ in Eq. (17)). Therefore, when α increases to $\alpha = \alpha_c$, a solution $\phi(x) \equiv \phi_{\max} = \text{const}$ establishes downstream (pure shock transition). Instead of using Eqs. (12) and (16), this special solution is easier to find directly by requiring charge neutrality condition fulfilled identically downstream, Eq. (3)

$$e^{U^2/2} = \frac{1 - \alpha}{1 + \alpha} \sqrt{\frac{2U}{V_{Ti}(1 - \alpha)}} + 1.$$

This result, in combination with Eq. (13), yields the critical value $\alpha = \alpha_c$ in Eq. (17). Under this condition, the maximum potential $\phi_{\max} = U^2/2$ is determined by

$$U = M_* - \frac{4V_{Ti}^2(M_*^2 + 1)^3}{3M_* M_*^2 - 1}. \quad (18)$$

Together with Eq. (14), the latter expression constrains the range of the shock Mach numbers for $0 < \alpha < \alpha_c \approx 1$. These values of the shock potential and Mach number ($\simeq U$) relate to the upstream region occupied by reflected ions (where $\phi = 0$). This region is located to the right from the leading soliton, but not farther than the slowest ions out of those that have been reflected first, Fig. 1. A more precise meaning of this condition will be given in Sec. IV. Now we turn to the calculation of the shock parameters for adiabatically trapped electrons.

B. Adiabatically trapped electrons

The calculation of shock characteristics for the adiabatically trapped electrons is similar to that for the Boltzmannian electrons, but with one significant difference: the foot potential ϕ_1 explicitly enters the Poisson equation also for the main part of the shock transition, cf. Eqs. (3) and (8). Therefore, unlike in the Boltzmannian case, where the ion reflection rate α explicitly enters the shock solution only in conjunction with the incident ion thermal spread (see, e.g., Eq. (14)), in the case of adiabatically trapped electrons the ion reflection effect is significantly stronger. The foot elevation ϕ_1 is the largest contributing factor to that. Although, the latter is also determined by α that we will discuss in Sec. IV.

Turning now to the shock solution, for its potential $\phi_{\max} \equiv U^2/2$, we obtain from Eq. (9) the following relation:

$$\frac{F(\phi_{\max} + \phi_1) + \frac{4}{3\sqrt{\pi}} \left[(\phi_{\max} + \phi_1)^{3/2} - \phi_1^{3/2} \right]}{F(\phi_1)} - 1 - 2\phi_{\max} = -\frac{2^{9/4}}{3} \phi_{\max}^{3/4} \frac{(1 - \alpha)^{3/2}}{1 + \alpha} V_{Ti}^{1/2}. \quad (19)$$

Unlike in the Boltzmann case, where the shock amplitude ϕ_{\max} was given by just a number $M_*^2/2$ in the limit $V_{Ti} \rightarrow 0$, now ϕ_{\max} depends directly on ϕ_1 . This dependence can be determined by solving Eq. (19) numerically for $V_{Ti} \rightarrow 0$, as the major contributing factor is ϕ_1 . Fig. 4 shows this solution in the form of the shock Mach number related to the far upstream medium and to the shock precursor, where $\phi = 0$. The latter is given by the relation $U(\phi_1) = \sqrt{2\phi_{\max}}$, shown with the dashed line. As expected, it starts from the value $U \approx 3.1$, which is the maximum speed of a non-reflecting soliton calculated by Gurevich.¹⁶ As the ion reflection rate α increases, so do $\phi_1(\alpha)$ and U .

To calculate the shock Mach number in the far upstream reference frame rather than the foot frame, one has to take into account the foot potential ϕ_1 . Indeed, the incident ions first slow down by passing through the potential ϕ_1 before they hit the leading soliton in the shock structure and specularly reflect off it. The total Mach number (i.e., the absolute shock speed, again, given for $V_{Ti} \rightarrow 0$) then amounts to

$$M = 2^{3/2} \sqrt{\phi_{\max} + \phi_1/4} - \sqrt{2\phi_{\max}} \approx \sqrt{2\phi_{\max} + \phi_1}, \quad (20)$$

where the last expression is an approximation for $\phi_1 \ll 2\phi_{\max}$ which holds up reasonably well for even a strong ion reflection. This dependence is shown in Fig. 4 with the solid line. We see from the last equation that the direct effect of the foot elevation ϕ_1 on the total Mach number is quite small, so that in the case of Boltzmannian electrons, where ϕ_{\max} does not depend on ϕ_1 explicitly (Eq. (12)) the maximum Mach number remains close to M_* . The dependence of the Mach number on α is considerably stronger for adiabatically trapped electrons, where ϕ_{\max} explicitly depends on $\phi_1(\alpha)$.

Now that we have obtained the shock structure up to the location of the first reflected ions, we turn to their dynamics. Obviously, they interact with the front end of the shock precursor, where the shock potential drops to its upstream value. Note that depending on the time elapsed from the first reflection, this potential barrier may have advanced far ahead of the main part of the main shock structure (first soliton, Fig. 1). Therefore, our assumption (Sec. II B) about the flat distribution of adiabatically trapped electrons in the soliton may

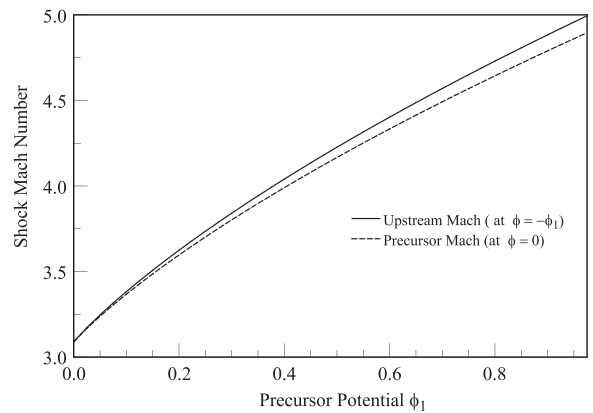


FIG. 4. Solution of Eq. (19) in the limit $V_{Ti} = 0$ shown in the form of the shock Mach number related to the upstream frame, M , and to the foot ion reference frames, $U = \sqrt{2\phi_{\max}}$ (see text).

become inconsistent with the Maxwellian distribution of free electrons. Indeed, part of the electrons passing the main shock transition is in fact reflected from the front of the shock precursor and may be significantly cooled in the expanding foot. Under these circumstances, we restrict our calculation of ϕ_1 to the case of Boltzmannian electrons, assuming that the condition $\Delta V_{\text{col}} > \Delta V_{\text{tr}}$ discussed in the Introduction applies throughout the entire shock transition. In fact, we will impose a stronger constraint on the time variation of the front part of the precursor in calculating the ion distribution in Sec. IV. In Sec. IV, we will relate the foot potential ϕ_1 to α . This relation provides the shock parameters depending only on the reflection parameter α , by using Eq. (20) and Fig. 4.

IV. SOLUTION FOR THE ION PRECURSOR

As we have seen, in the case of $\alpha > 0$, the shock propagates through a foot region with the electrostatic potential elevated to $\psi = \phi_1$ from its level $\psi = 0$ at $+\infty$. By entering this area, the incident ions slow down before they encounter the leading soliton. It is convenient to account for this change in the shock potential by shifting the variable ϕ used in Secs. I–III to ψ as follows: $\psi = \phi + \phi_1$. So we now focus on that part of the shock transition where ψ varies in the interval $0 < \psi < \phi_1$, Fig. 1. From the physics perspective, one may assume that after an initial propagation of the reflected beam upstream, a flow at a constant speed and potential $\psi = \phi_1$ establishes between the ion-reflecting soliton and the head of the beam. Our consideration of the beam dynamics below (see, in particular, Appendix) implies that this assumption is not justified if the beam reflection is not strictly stationary, so the beam may continue to evolve all the way through its extension. However, under a stationary reflection, most of the beam will also be stationary, and only its head will continue to spread via a self-induced electric field. In this region, the potential will gradually decrease from $\psi = \phi_1$ to $\psi = 0$, and the respective electric field will further accelerate the reflected particles.

There are at least two types of applications where the energy distribution of reflected ions is critical. The first type is when the reflected beam impinges on a dense target that completely absorbs the beam. Here, the spatially averaged energy distribution of reflected ions is more important than the local one. The deposited particle energy and, therefore, the particle penetration depth will decrease until the transient (more energetic) part of the beam coming from the region where $0 < \psi < \phi_1$ is absorbed. Then, the stationary part of the reflected beam, which carries the potential ϕ_1 , will maintain a constant energy deposition (fixed location of a particle stopping point). Note that the stopping point is associated with the so-called Bragg peak of particle energy losses, e.g., Ref. 34.

The second application of shock reflected ions is a long-standing problem of ion injection into the first order Fermi acceleration, e.g. Ref. 29. Here, more important than the dynamics of the front-running ions is the process of scattering of all reflected particles on *self-generated* waves. This process occurs in a magnetized shock environment and, for that matter, at significantly larger scales, such as the Larmor

radius of reflected ions and beyond. Numerically, this problem is usually treated using hybrid simulations.^{8,9,15} The hybrid simulations, however, do not resolve the sub-Debye-scale phenomena, crucial for the present investigation. We defer the injection aspect of the reflected ion beam to a future study.

In describing the pedestal part of the shock transition, it is natural to use the reference frame in which the stationary part of the reflected ion beam is at rest. It is also clear that this part of the shock profile can be described almost independently of the main part of the shock transition, presented earlier in the paper. Then, a matching condition in the region where $\phi = 0$ or, equivalently, $\psi = \phi_1$ applies. Here, all the relevant particle groups have a constant density. Using the plasma neutrality requirement for the Boltzmannian electrons and ions that enter this region at the speed $-w$ from $+\infty$, we obtain

$$e^{\phi_1} = \frac{1 + \alpha}{\sqrt{1 - 2\phi_1/w^2}}, \quad (21)$$

which, for $2\phi_1/w^2 \ll 1$, can be written also as $\exp[(1 - w^{-2})\phi_1] \approx 1 + \alpha$. Hence

$$\phi_1 \simeq \frac{\ln(1 + \alpha)}{1 - w^{-2}}, \quad (22)$$

for any $0 < \alpha < 1$. In the current reference frame, the velocity of the incoming upstream ions is $-w \simeq -2U$, so the requirement for Eq. (22) to be valid is $2\phi_1/w^2 \approx \phi_1/2\phi_{\text{max}} \ll 1$. This condition is warranted by Eq. (22), if $\alpha \ll 1$ but, because ϕ_1 is not large even for $\alpha \leq 1$, the approximate formula in Eq. (22) is accurate to within 1% for all $0 < \alpha < 1$. The thermal spread of ions is neglected here. To further simplify notations, we rescale the spatial variable x here as follows: $x' = (1 - 2\phi_1/w^2)^{1/4}x$. This change of variable is not significant for the sequel, though. Denoting the reflected ion density by ρ , we can write the Poisson equation in the following way:

$$\frac{d^2\psi}{dx'^2} = e^\psi - \frac{1}{\sqrt{1 - 2\psi/w^2}} - \rho. \quad (23)$$

The limiting values for ρ are $\rho(\psi = 0) = 0$ and

$$\rho(\psi = \phi_1) = \frac{\alpha}{\sqrt{1 - 2\phi_1/w^2}}. \quad (24)$$

As before, we assume that the front-running beam particles already escaped the main part of the shock and have spread to an area much larger than the Debye length. Hence, the following ‘‘quasi-neutral’’ version of Eq. (23) applies:

$$\rho = e^\psi - \frac{1}{\sqrt{1 - 2\psi/w^2}}. \quad (25)$$

The last relation can be used as an equation of state of the reflected ion gas. Furthermore, at this stage, the problem of subsequent spreading of the reflected beam lacks any characteristic length. Therefore, as in the case of its gasdynamics counterpart, the solution should depend only on the variable

$$\xi = x/t.$$

Placing the spreading front edge of the reflected ion beam at the origin, we obtain the following boundary conditions for the beam density, its velocity, and plasma potential: $\rho(\infty) = u(-\infty) = \psi(\infty) = 0$, $\psi(-\infty) = \phi_1$, and

$$\rho(-\infty) = \frac{\alpha}{\sqrt{1 - 2\phi_1/w^2}} \equiv \rho_1. \quad (26)$$

An additional limitation to this treatment, that uses the particle energy conservation in Eqs. (21)–(23), is that the potential ψ should not vary significantly during the crossing time of incident ions. The reason for such variation is, of course, the spreading of the reflected ions entering Eq. (23) through the term $\rho(x, t)$. Again, the above limitation is easily fulfilled as $\phi_1 \ll w^2/2$ even for $\alpha \sim 1$. By neglecting also the ion pressure, we arrive at the following hydrodynamic equations for the reflected ions:

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x} \rho u = 0, \quad (27)$$

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} = -\frac{\partial \psi}{\partial x}, \quad (28)$$

where u is the flow velocity of reflected ions in the comoving reference frame. As we use dimensionless variables introduced in Sec. II for x , u and ψ , time is now measured in the units of $\omega_{pi}^{-1} = \sqrt{m_i/4\pi e^2 n_\infty}$.

The problem, given by Eqs. (23), (27), and (28), has a close relation to the problem of expansion of one gas into another (or into vacuum).^{17,22} Indeed, as we assume the pedestal having already spread to a region larger than the Debye length, we use quasi-neutrality condition, Eq. (25), in place of the Poisson equation (23). This implies $\psi = \psi(\rho)$ (simple wave solution), and the r.h.s. of Eq. (28) corresponds to the specific enthalpy gradient of the gasdynamics analog of Eqs. (27) and (28). Looking for such solution, from Eqs. (27) and (28), we obtain (see also Appendix for a more general treatment of Eqs. (27) and (28))

$$\left[(u - \xi)^2 - \left(\frac{\partial \ln \rho}{\partial \psi} \right)^{-1} \right] \frac{\partial \psi}{\partial \xi} = 0, \quad (29)$$

where

$$u = \int_{\psi}^{\phi_1} d\psi \sqrt{\frac{\partial \ln \rho}{\partial \psi}}, \quad (30)$$

and $\rho(\psi)$, again, obeys the “equation of state” of the reflected ion gas given by Eq. (25). Eq. (29), in turn, is satisfied by the following piecewise continuous solution:

$$\psi = \begin{cases} \phi_1, & \xi \leq \xi_1 < 0 \\ 0, & \xi \geq \xi_2 > 0. \end{cases} \quad (31)$$

In the expanding wave region $\xi_1 < \xi < \xi_2$, the solution is given by

$$u = \xi + \left(\frac{\partial \ln \rho}{\partial \psi} \right)^{-1/2}. \quad (32)$$

Together with Eq. (30), the last equation determines the profile of the expanding wave in the form of $\xi(\psi)$

$$\xi(\psi) = \int_{\psi}^{\phi_1} d\psi \sqrt{\frac{\partial \ln \rho}{\partial \psi} - \left(\frac{\partial \ln \rho}{\partial \psi} \right)^{-1/2}}. \quad (33)$$

By applying the boundary conditions $\psi(\xi_1) = \phi_1$ and $\psi(\xi_2) = 0$, for the edges $\xi_{1,2}$ of the simple wave, given by Eqs. (31) and (32), we obtain

$$\xi_1 = - \left(\frac{\partial \ln \rho}{\partial \psi} \right)^{-1/2}_{\psi=\phi_1}, \quad (34)$$

$$\xi_2 = \int_0^{\phi_1} d\psi \sqrt{\frac{\partial \ln \rho}{\partial \psi}}. \quad (35)$$

These are the velocities with which the simple wave expands back into the beam and the upstream plasma, respectively.

From Eq. (30), for the maximum beam velocity (at $\psi = 0$), we obtain $u_{\max} \simeq 2\sqrt{\phi_1}$. The total speed of the shock is $M \simeq \sqrt{2\phi_{\max} + \phi_1}$ ($\phi_1 \ll 2\phi_{\max}$, Eq. (20)). Neglecting the upstream ion temperature in Eqs. (14)–(18) and using Eq. (22), this Mach number can be written as $M \approx \sqrt{M_*^2 + (1 - 1/4M_*^2)^{-1} \ln(1 + \alpha)}$, which yields $M = M_{\max} \approx 1.8$ for $\alpha \approx 1$ for a Boltzmannian electron distribution. The maximum reflected beam speed with respect to the upstream rest frame is $V_b = M + M_* + u_{\max} \approx 2[M_* + \sqrt{\ln(1 + \alpha)}]$. For the adiabatically trapped electrons, the calculation of $M(\alpha)$ is somewhat more complicated, since the shock maximum potential ϕ_{\max} explicitly depends on ϕ_1 , as we discussed in Sec. III B.

A. Acceleration of reflected ions

It follows that, even when ions are bouncing off the shock front, the laminar shock structure persists for up to a maximum Mach number M_{\max} . This value is somewhat higher than the classical limit $M = M_* \approx 1.6$ for the Boltzmannian electrons ($M_{\max} \approx 1.8$) and considerably higher for the adiabatically trapped electrons, where $M_* \approx 3.1$, Fig. 4. In the meanwhile, the fraction of reflected particles may approach almost unity, Eq. (17). At $\psi = 0$ in Eq. (30), the reflected beam velocity reaches its maximum. By expanding Eq. (30) for small α , we obtain $u_{\max} \simeq 2\sqrt{\phi_1}$ which is a factor of $\sqrt{2}$ higher than what the front running particles would gain from the energy conservation after being accelerated from the shock foot of a height ϕ_1 . The difference is explained by the expansion of reflected particles.

An equally important aspect of the reflected beam dynamics is that the beam, while being accelerated by the self-generated electric field, substantially narrows its velocity distribution. Indeed, consider the beam temperature evolution during its expansion upstream. As before, we neglect the internal pressure of the beam in the hydrodynamic

equations (27) and (28) that describe the flow. But once we have described the ion beam flow, we may also calculate the evolution of its temperature in a test-particle regime. Assuming that the beam expands adiabatically, the equation for its temperature T_b takes the following form:

$$\frac{\partial T_b}{\partial t} + u \frac{\partial T_b}{\partial x} + (\gamma - 1) T_b \frac{\partial u}{\partial x} = 0, \quad (36)$$

where γ is the ion adiabatic index. By combining this equation with the continuity Eq. (27), we obtain

$$\frac{T_b(\psi)}{T_b(\phi_1)} = \left[\frac{\rho(\psi)}{\rho(\phi_1)} \right]^{\gamma-1}, \quad (37)$$

where $T_b(\phi_1)$ is the reflected beam temperature in the foot region where $\psi = \phi_1$, Fig. 1. For the simple “box” model, $T_b(\phi_1) = (v_2 - U)^2/24$. The result shown in Eq. (37) is, as expected, just a familiar adiabatic law. Asymptotically, the width of reflected ion beam distribution narrows down to zero far upstream where $\psi \rightarrow 0$. Note that the local beam density also vanishes ($\rho \rightarrow 0$) at this point, according to Eq. (25). We see from Eq. (37) that the most efficient energy collimation occurs in 1D motion ($\gamma = 3$), e.g., if there is a strong magnetic field present.

In reality, the beam energy changes in space (and time) while it accelerates through the pedestal region, where the potential ψ changes between 0 and ϕ_1 . Therefore, an integrated energy deposition at a given point (target) cannot be strictly monoenergetic, even if the bulk of the beam is. Indeed, the head of the beam (which is at $\psi = 0$) escapes the bulk of it with the speed $2\sqrt{\phi_1}$ (one may use Eq. (22) for ϕ_1). However, the density of these fast moving beam particles is nominally zero, while the bulk of the beam has the density ρ_1 , Eq. (26). Therefore, the net effect of this beam energy spreading needs to be investigated depending on the nature of the target. Such investigation is beyond the scope of the present paper. We merely mention here that from the perspective of the proton/carbon radiation therapy, for example, the beam energy deposition is largely a collective phenomenon (e.g., Ref. 37 and referenced therein). If so, then the beam energy density $\rho V_b^2/2$ is probably more relevant than the individual particle energy $m_i V_b^2/2$. Therefore, dumping the rarefied head will not necessarily result in a significant additional spreading of the “hot spot” produced by the bulk of the beam.

Notwithstanding the above remarks, it is worthwhile to calculate the velocity spread of the beam. For cold upstream ions, we may neglect this spread for the bulk of the beam that carries the potential $\psi = \phi_1$ and calculate the spread for its head, where $0 < \psi < \phi_1$, using the approximation $\phi_1 \ll w^2$. Defining the beam velocity spread as

$$\Delta u = \frac{\int u \rho du}{\int \rho du},$$

where $0 < u < u_{\max} \simeq 2\sqrt{\phi_1}$, using Eqs. (25) and (30), we obtain for Δu the following simple result:

$$\Delta u = u_{\max}/4 \ll V_b.$$

The beam density ρ is falling off with its velocity as follows:

$$\rho(u) = \frac{1}{4} (1 - w^{-2}) (u_{\max} - u)^2.$$

One sees that the beam velocity distribution remains relatively narrow despite the acceleration of particles from its front. Also, the relative contribution to the integrated energy deposition of the head of the beam can be reduced by increasing the length of the primary beam; that is the system length.

V. DISCUSSION AND CONCLUSIONS

A better understanding of ion-acoustic collisionless shocks, including ion reflection, is required for the operation of laser-based accelerators^{12,18,26,34,35} (and many other applications, mentioned in passing in the Introduction section). Turning to the astrophysical applications, by far the most demanded particle acceleration mechanism, the diffusive shock acceleration (DSA) is also likely to be fed in by the shock-reflected particles. Although the DSA operates in magnetized plasmas, typically at much larger than Debye scale, the particle reflection can hardly be understood without understanding the DSA microscopics, to which the results of the present paper are directly relevant. Identifying a seed population (“injected” particles) for the DSA in the background plasma and understanding their selection mechanisms^{28,30,43} present a genuine challenge for interpreting the new, unprecedentedly accurate observations of cosmic rays, e.g., Refs. 1 and 2. These observations point to the elemental discrimination of particle acceleration that almost certainly is a carry-over from the injection of thermal particles into the DSA.³¹ Operating at the outer shocks of the supernova remnants, the DSA is the basis of contemporary models for the origin of galactic cosmic rays.^{3,4,6,10,13,19}

The injection has been studied numerically mostly with hybrid simulations.^{8,9,15,21,39} An accurate calculation of injection efficiency using the results of the present paper would go far beyond its scope and focus. At a minimum, such calculation must include the magnetic shock structure. Conversely, the particle reflection analyzes for magnetized shocks presented in many publications, e.g., Refs. 14, 23, 41, and 42, as well as the above-cited hybrid simulations, do not include the electrostatic structure into the reflection process self-consistently with electron and ion kinetics. In this paper, we addressed the questions of how does the reflection affects the shock speed, its structure, and reflected ions themselves. We have determined their distribution, given that of the incident ions and the shock Mach number. These results will, therefore, be important for the comprehensive DSA injection models yet to be built. Note that in the case of magnetized quasi-parallel shocks, the injection seed particles other than reflected ones have also been considered (see, e.g., Ref. 15 for a recent discussion of the alternatives). In particular, the thermalized downstream particles have long been deemed to be a viable source for injection¹¹ (so-called thermal leakage). One may argue, however, that if such leakage occurs from

the downstream region within 1–2 Larmor radii off the shock ramp, the difference between them and reflected particles is rather semantic from the DSA perspective.³¹

We further highlight the following findings of this paper: (i) when the soliton number increases to the point of ion reflection, and the soliton transforms into a soliton train downstream, this structure persists with the increasing Mach number until most of the incident ions reflect off the first soliton.⁴⁴ The reflection coefficient approaches $\alpha = \alpha_c \simeq 1 - 3.9\sqrt{T_i/T_e}$, (ii) at this point, the downstream potential is equal to $\phi_{max} \simeq M_*^2/2 \simeq 1.26$. In addition, the foot rises to $\phi_1 \simeq \ln(1 + \alpha_c)/(1 - 1/8\phi_{max}) \simeq 0.77$ (for $\alpha_c \rightarrow 1$), so that the total shock Mach number approaches $M = M_2 \simeq 1.8$. This result is obtained for the Boltzmannian electrons, while in the case of adiabatically trapped electrons the maximum Mach number approaches $M = M_2 \simeq 4.5$, (iii) the laminar shock structure cannot continue beyond this point.

Based on the numerous PIC simulations, available in the literature (e.g., Refs. 12, 18, and 24), we may speculate that when the Mach number exceeds its critical value M_2 , obtained in this paper, the shock evolution becomes time dependent; ions reflect intermittently. One example of such dynamics, Fig. 5, we adopted from the recent particle-in-cell (PIC) simulations²⁴ (see also Appendix for a further brief discussion of this result). For yet higher Mach numbers, the upstream and downstream flows do not couple together, but rather penetrate through each other, not being perturbed significantly. In a piston driven flow, ions reflect only from the piston, so the shock does not form. As for the prospects for a laser-based accelerator, this is probably a favorable scenario for generating ion beams when the high energy is a priority. Indeed, the maximum Mach number for a laminar shock, with sustainable ion reflection from its front, is rather low. Therefore, ions reflected directly from the piston may be a better solution.

In this paper, the main part of the shock structure was resolved exactly, by adopting a simplified kinetic model for a finite-temperature “box” distribution of upstream ions, using the shock pseudopotential. Considering T_i/T_e as a small parameter, the number of reflected ions is calculated as a function of the shock Mach number self-consistently with

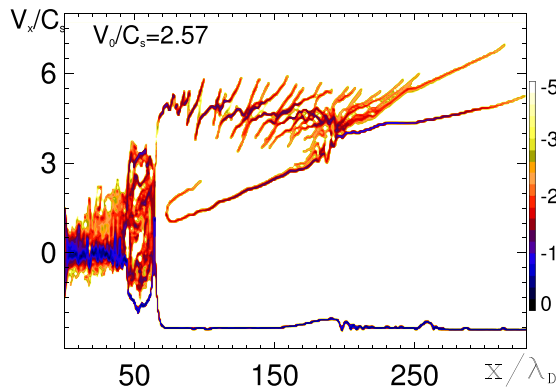


FIG. 5. PIC simulation result from Ref. 24. Shown is the ion phase plane at $t\omega_{pe} = 2800$, $M_0 = V_0/C_s = 2.57$; the resulting velocity of the shock is around 3.8. The color coding corresponds to the ion phase space density normalized to that of the upstream ions (logarithmic scale).

the shock foot potential. The dynamics of the reflected ion beam in the foot is investigated.

To recapitulate the relation of this and earlier studies, we note that many analyzes were limited to the case of monoenergetic upstream ions. For that reason, they could not resolve ion reflection as the incident ions should all reflect at once, when the peak of wave potential $e\phi_{max}$ becomes equal to the ion energy $m_i V_{shock}^2/2$. As we pointed out already, this happens when the Mach number $M = V_{shock}/C_s$ reaches $M = M_* \approx 1.6$ for Boltzmann electrons,³⁸ and $M = M_* \approx 3.1$, for adiabatically trapped electrons.¹⁶ Numerical treatments, however, included finite ion temperature and have been able to address the effect of ion reflection on the shock structure by using PIC simulations, e.g., Refs. 12 and 24. The ion reflection alters the shock amplitude and speed, thus impacting the reflection threshold itself. The most striking result of this feedback loop, we have studied in this paper, is a pedestal of the electrostatic potential, built upstream. It changes the speed of inflowing ions and thus, again, the condition for their subsequent reflection from the main shock. To our best knowledge, this important aspect of the collisionless shock physics has not yet been studied systematically in PIC simulations.

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APPENDIX: CHARACTERISTIC FORM OF REFLECTED ION DYNAMICS

By analogy with their gasdynamics counterparts, we rewrite Eqs. (27) and (28) in a form of two Riemann invariants conserved along two families of characteristics. To this end, we first change the dependent variable in Eq. (27) $\rho \rightarrow J$, so that this equation rewrites

$$\frac{\partial J}{\partial t} + u \frac{\partial J}{\partial x} + \sqrt{\rho \left(\frac{\partial \rho}{\partial \psi} \right)^{-1}} \frac{\partial u}{\partial x} = 0, \quad (\text{A1})$$

where

$$J = \int d\psi \sqrt{\frac{\partial \ln \rho}{\partial \psi}}. \quad (\text{A2})$$

By summing and negating Eqs. (28) and (A1), we arrive at the following characteristic form of them:

$$\frac{\partial R_{\pm}}{\partial t} + C_{\pm} \frac{\partial R_{\pm}}{\partial x} = 0, \quad (\text{A3})$$

with the Riemann's invariants R_{\pm} and the characteristics C_{\pm} , respectively, given by

$$R_{\pm} = u_{\pm} \int_{\phi_1}^{\psi} d\psi \sqrt{\frac{\partial \ln \rho}{\partial \psi}} \quad \text{and} \quad C_{\pm} = u_{\pm} \left(\frac{\partial \ln \rho}{\partial \psi} \right)^{-1/2}. \quad (\text{A4})$$

Therefore, the most general solution of the problem, described in Sec. IV by Eqs. (27) and (28), is determined by conservation of R_{\pm} along the characteristics C_{\pm} . From this perspective, the simple wave solution given by Eqs. (31)–(35) corresponds to a decaying discontinuity with $u(x < 0) = 0$ and $u(x \geq 0) = u_1 \equiv u(\psi = 0)$ (Eq. (30)). The initial beam density jump is defined in a similar way, $\rho(x \geq 0) = 0$ and $\rho(x < 0) = \rho_1$, Eq. (26). Under these initial conditions, the Riemann's invariant $R_{+} \equiv 0$ everywhere. Thus, the initial value problem given by Eq. (A3) significantly simplifies with only $R_{-} \neq 0$, and a single family of characteristics C_{-} involved in it. As C_{-} characteristics diverge from the origin, the simple wave solution described in Sec. IV emerges, and it is consistent with the initial conditions specified above.

It is important to emphasize that under more general initial conditions, the beam dynamics can be much more complicated. In particular, the flow characteristics generally intersect. As the beam “hydrodynamics” is truly collisionless, their intersection will result in a multi-flow state of the reflected beam. Such states copiously emerge in simulations, e.g., Refs. 12, 24, and 25, along with laminar reflected beam flows described in Sec. IV. An illustrative example, taken from recent PIC simulations,²⁴ is shown in Fig. 5. Even though the shock is super-critical, the quasi-laminar part of the reflected ion beam, described in this paper, can be easily identified in the area $x > 175$. Here, the flat part of the beam density distribution ($175 < x < 200$) transitions into an accelerating, rarefied part at $x > 200$. Other reflected ion components in this area stem from later, non-stationary, and highly intermittent reflection events. Being more energetic, these ions are catching up with the laminar part at the moment shown in the figure. Based on the color coding, however, they are considerably (about 10 times) lower in phase space density than the main reflected component is.

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