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**INITIAL RESULTS FROM THE SCOOP LIMITER EXPERIMENT IN PDX \***

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A particle scoop limiter with a graphite face backed by a 50 liter volume for collecting particles was used in PDX. Experiments were performed to test its particle control and power handling capabilities with up to 5 MW of D<sup>o</sup> power injected into D<sup>+</sup> plasmas. Line average plasma densities of up to  $8 \times 10^{13} \text{ cm}^{-3}$  and currents up to 450 kA were obtained. Plasma densities in the scoop channels greater than  $2 \times 10^{13} \text{ cm}^{-3}$  and neutral densities in the scoop volume greater than  $5 \times 10^{14} \text{ cm}^{-3}$  were observed. There is evidence that recycling may have occurred in the scoop channels for several discharges with large line-averaged plasma density. At beam powers up to 2.5 MW, energy confinement times above 40 ms were deduced from magnetics measurements and from transport analysis. Pressures in the vacuum vessel were in the  $10^{-5}$  Torr range, and recycling source neutral densities in the central plasma were low.

**1. Introduction**

Limiters equipped with various means for particle removal have been proposed for control of recycling, reduction of impurities, and ash removal in fusion reactors [1]. These "pump limiters" are typically designed with a volume for trapping particles behind the part of the limiter in contact with the plasma. Experiments in tokamaks [2–4] have shown that relatively large pressures (1–50 mTorr) can be obtained in such volumes. These results indicate that the fraction of the injected gas which gets trapped within the limiter volume can be large.

A specially designed pump limiter, called a scoop

limiter, was installed in PDX in 1982 (fig. 1). It consisted of a box with an internal volume of 50 ℓ rigidly mounted on the PDX vacuum vessel wall. The side facing the central plasma was made of four blades of uncoated (ATJ) graphite machined to approximate a saddle surface. The radius of curvature in the toroidal direction was 60 cm away from the plasma and the radius of curvature in the poloidal direction was 120 cm toward the plasma. The innermost part of the limiter blade was at a major radius of 193 cm.

Behind the graphite blades were two symmetrically placed crescent-shaped channel entrances (fig. 2a) facing the ion and electron drift directions. The two sides of the entrances approximated arcs with radii 60 and 40 cm separated by 2 cm at the midplane. Particles flowing into these entrances could continue in a short channel to a neutralizer made of copper and clad with 1/2 mm of vanadium (fig. 2b). The purpose of the vanadium was

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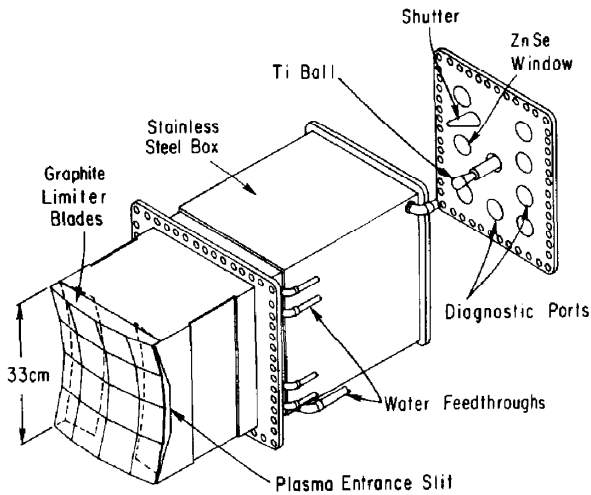


Fig. 1. Isometric view of the scoop.

to reduce sputtering. Neutrals leaving the neutralizer either could flow back into one of the channels and be ionized by the incoming plasma, or traverse the channel and exit back into the plasma edge, or remain in the box.

Calculations indicate that as the density or temperature of the plasma in the scoop channels increases, the probability of neutrals being ionized in the channels will

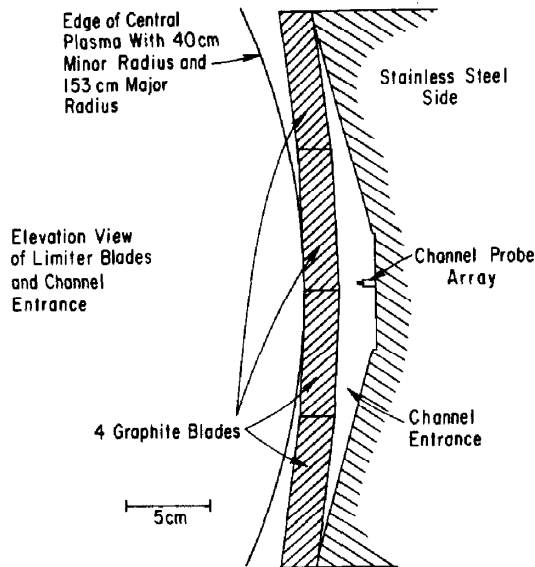


Fig. 2a. elevation view of limiter blades and the ion side channel entrance.

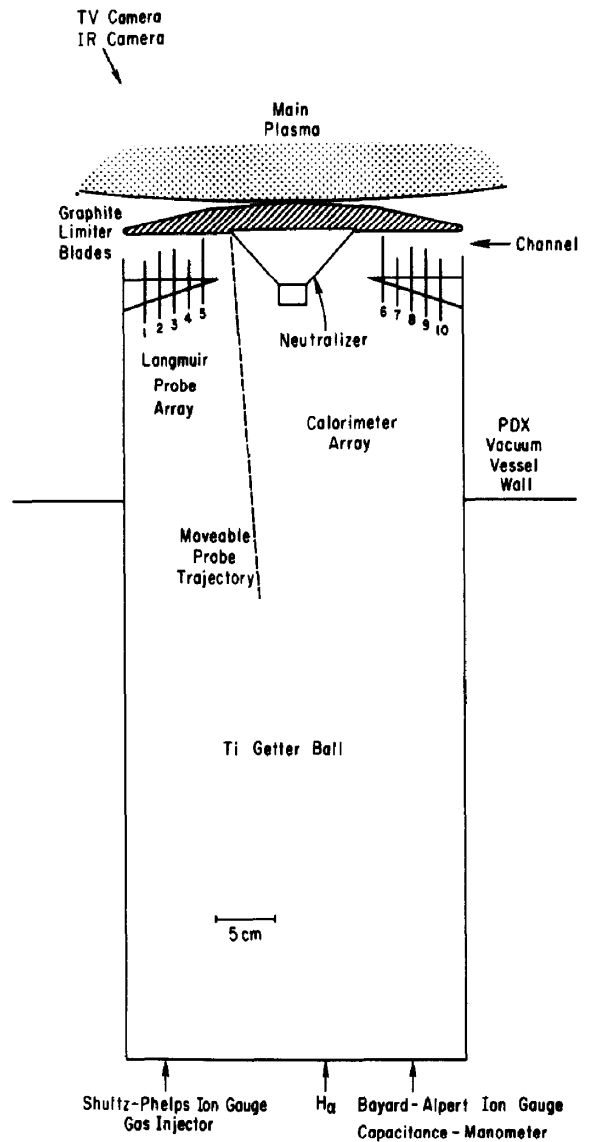


Fig. 2b. Plan view of the scoop showing the channels, neutralizer, and diagnostics.

increase [5]. When this probability is high, there is a hypothetical mode of operation where the neutral flow out of the volume is throttled, resulting in high steady-state scoop pressures [6]. One of the goals of the experiment was to investigate recycling in the channels and to look for such modes of "trapped" operation.

A TV camera and an IR camera viewed recycling and heat deposition on the limiter blades. Arrays of

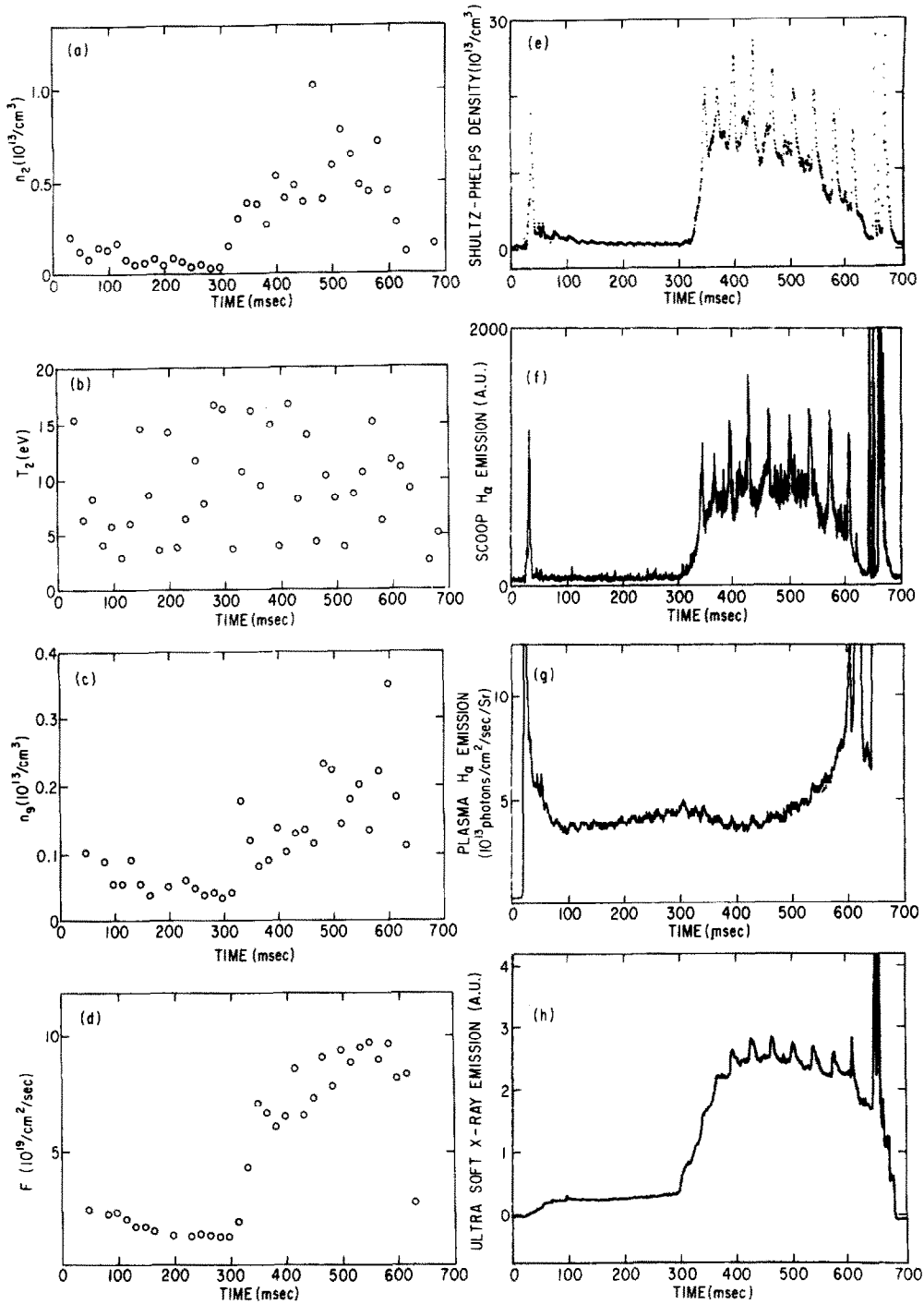


Fig. 3. Various measurements for a scoop discharge: (a) ion channel electron density, (b) electron temperature, (c) electron channel density, (d) sonic flow estimate, (e) neutral density measured by the Shultz-Phelps gauge, (f) scoop  $H_\alpha$  emission, (g) plasma  $H_\alpha$  emission, and (h) ultra-soft X-ray emission.

Langmuir probes sampled plasma conditions in the channels. Inside the scoop there were thermocouples to measure heating and calorimeters to detect the heat flux carried by neutrals. Pressure and density in the scoop were monitored using a capacitance manometer and ionization gauges. A ZnSe window on the back of the scoop allowed  $H_{\alpha}$  light from excited deuterium to be monitored. We discuss conditions in the scoop in section 2.

Plasma discharges limited only by the scoop were run on 13 days between December 1982 and June 1983. The plasmas were very disruptive during the first few (non-consecutive) days, most likely due to lack of conditioning of the graphite blades. Neutral beam heating was used during seven of the days. Characteristics of these beam-heated discharges are discussed in section 3.

### 2. Conditions in the scoop

Two arrays of fixed double Langmuir probes, which were located symmetrically to the left and right of the neutralizer, sampled plasma conditions in the two channels. Electron densities up to  $2 \times 10^{13} \text{ cm}^{-3}$  and electron temperatures of typically 5–20 eV were inferred from current–voltage characteristics.

Fig. 3 shows several measurements versus time for a discharge which had the line-averaged density  $\bar{n}_e$  rising to  $5 \times 10^{13} \text{ cm}^{-3}$  and 2 MW of neutral beam heating. The electron density  $n_2$ , measured by the second ion side array probe, is shown in fig. 3a. The density increased during the neutral beam phase between 300 and 600 ms. The electron temperature  $T_2$ , measured by this probe, shown in fig. 3b, fluctuated about 9 eV throughout the discharge. The density  $n_9$ , measured by the mirror image probe on the electron side, shown in fig. 3c, was considerably less than  $n_2$ . The electron temperature  $T_9$  was similar to  $T_2$ . Langmuir probe measurements in the edge plasma outside the scoop (about 1.9 m away) had comparable electron densities and temperatures for the magnetic flux surfaces intercepted by the channel probes [7].

An upper-bound for the particle flux toward the neutralizer is given by the local electron density times  $v_s \equiv \sqrt{k(T_e + T_i)/M_i}$ . This is proportional to the ion saturation current. The sum of these fluxes inferred from the 2nd, 3rd, etc. probes,

$$F \equiv F_2 + F_3 + F_5 + F_6 + F_8 + F_9,$$

is plotted in fig. 3d. The average,  $F/6$ , can be used to estimate the sonic flow to the neutralizer at the mid-plane.

Pressure in the back of the scoop was measured by a capacitance manometer (Baratron) with a slow response time ( $\sim 200$  ms), and densities were measured by two ion gauges (a Shultz–Phelps and a Bayard–Alpert) with fast response times ( $\sim 10$  and 50 ms). The density measured by the Shultz–Phelps ion gauge (fig. 3e) increased rapidly when the neutral beams started. The relative rise was larger than that of  $F$ . This may be partly due to plasma or beam ejection of neutrals near or in the scoop. It probably is not due to a decrease in particle confinement of the main plasma (outside the scoop) because the  $H_{\alpha}$  signal did not increase (cf. below).

Fig. 3f shows the  $H_{\alpha}$  signal observed through the ZnSe window in the back of the scoop. This signal is proportional to a volume average of the plasma density, times neutral density, times a rising function of the electron temperature. Fig. 3g shows the  $H_{\alpha}$  signal observed approximately  $110^\circ$  toroidally away from the scoop. The slight decrease during the neutral beam

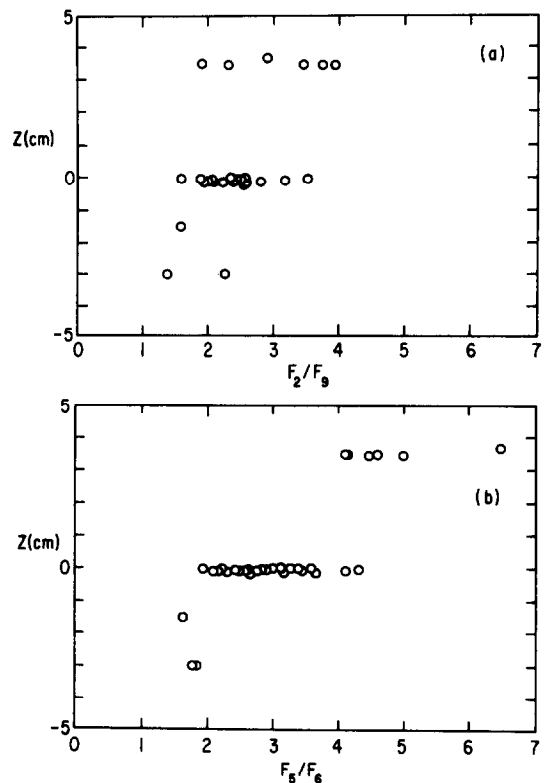


Fig. 4. Shot-to-shot variation of the ion side/electron side density ratio versus plasma vertical displacement measured by two sets of mirror-symmetric probes.

phase, when  $\bar{n}_e$  was increasing, suggests a decrease in recycling and an increase in the particle confinement time (unless impurities were fueling).

The ultra-soft X-ray signal emitted by the plasma outside the scoop is shown in fig. 3h. This emission is strongest from the plasma edge, so inverted sawteeth were observed when discharges were in the sawtooth mode. These sawteeth are correlated with spikes on the Shultz-Phelps and  $H_\alpha$  signals. They probably indicate real increases in density since pick-up would be different in these detectors. The plasma density in the channels may have spiked as well, but the probe measurements were too slow to detect this.

The ion saturation currents and inferred electron densities were usually asymmetric, being larger in the channel facing the ion side by about 50% during the ohmic heating phase, and by a factor of two to three during the neutral beam heating phase of the discharge. The magnitude of the asymmetry varied as the vertical position of the plasma was changed. Fig. 4 shows the ratio of densities measured during neutral beam heating by mirror image pairs of probes in the ion and electron channels (as labeled in fig. 2b) versus the vertical displacement of the plasma. During one neutral beam run, the toroidal field and plasma current were reversed to study counter injection, so that the ion drift direction was clockwise instead of counter-clockwise as viewed from above. The asymmetry reversed as well.

Part of the asymmetry could be explained by the pitch of the field lines. The probes were located near the midplane, so the flux tubes intercepted by one array would twist down at the channel entrance, and flux tubes intercepted by the other array would twist up at the opposite channel entrance. Since the tubes intercepted the neutralizer, plasma could not flow from both entrances to both arrays. As the plasma was displaced above or below the midplane, the location in the scoop channel entrances where the plasma density was largest would be displaced. Even when the plasma was centered (according to magnetics measurements) on the midplane, there was a left-right asymmetry. This could not be caused by the above mechanism.

This asymmetry might be caused by a toroidal rotation of the plasma in the flux surfaces flowing into the channels (at a minor radius between 42 and 45 cm). A rotation speed in the ion drift direction comparable to the sound speed at this surface,  $v_s \equiv \sqrt{k(T_e + T_i)}/M_i \sim 10^6$  cm/s would account for the observed asymmetry. Also, the precession of the banana orbiting beam ions in the direction of the plasma current would contribute to the asymmetry during the neutral beam heating phase.

To investigate recycling in the scoop channels, we

studied the ratio of the densities  $n_5/n_2$  measured by the fifth and second array probes. The fifth probe is 3.8 cm further down the channel than the second probe, and is approximately 3.8 cm from the neutralizer plate. Also, its major radius is 1 cm less, i.e., it is 1 cm closer to the back of the limiter blade. An increase in this ratio would indicate that the plasma density was increasing downstream towards the neutralizer, or alternatively, that the radial scrape-off length of the plasma density was becoming shorter. The former would indicate that neutrals were being ionized in the channels. The latter is not indicated by external probe measurements [7]. The ratio fluctuated considerably from fit to fit during each discharge, but most discharges did not exhibit a systematic variation with time. If these discharges did have channel recycling, it occurred only for brief periods lasting less than 50 ms, or else occurred only closer to the neutralizer than probes 5 and 6.

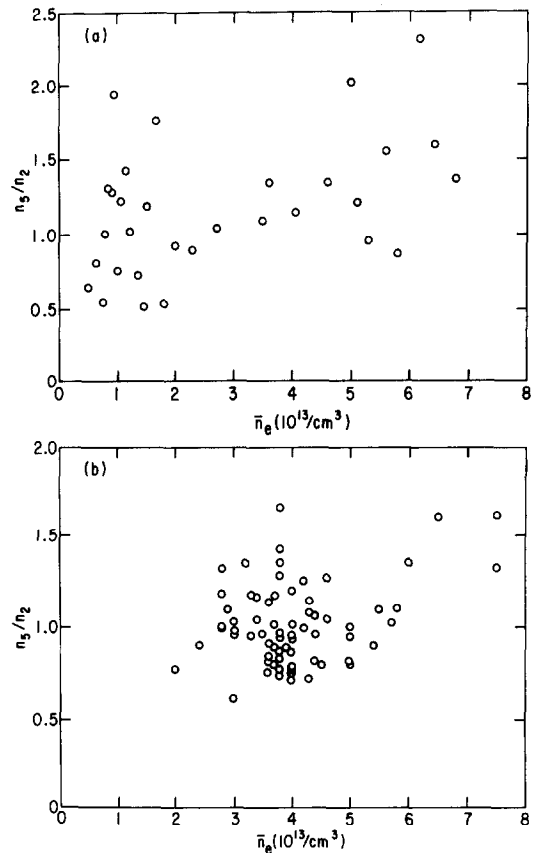


Fig. 5. Variation of the ratio of electron densities measured by probe 2 and probe 5 versus  $\bar{n}_e$  for (a) a single discharge, (b) many discharges at a single time.

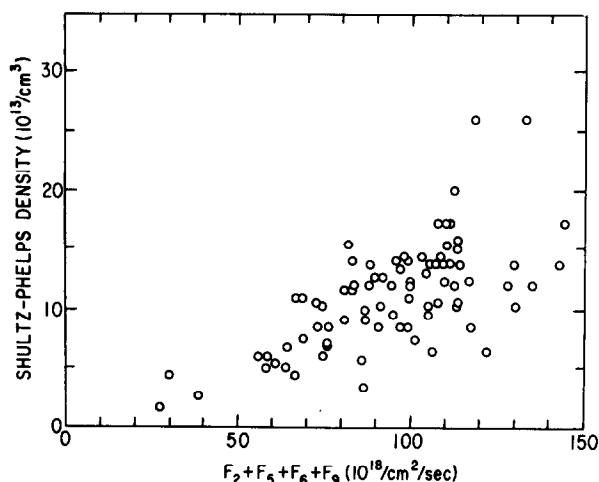


Fig. 6. Densities measured by the Shultz-Phelps gauge versus the sum of fluxes  $F_2 + F_5 + F_6 + F_9$ .

Several discharges did show a systematic variation in the ratio. These all had large  $\bar{n}_e$  and were displaced above the midplane. Fig. 5a shows the variation of  $n_5/n_2$  with  $\bar{n}_e$  for one such discharge. The ratio fluctuated considerably during the start-up, when  $\bar{n}_e$  was low, then it increased and decreased with  $\bar{n}_e$ . The shot-to-shot variation of  $n_5/n_2$  at one time near the end of the neutral beam phase (fig. 5b) also shows an increase with  $n_e$ . The ratio did not vary systematically with plasma current or with neutral beam power. Fig. 6 shows the shot-to-shot variation of the Shultz-Phelps density with  $F_2 + F_5 + F_6 + F_9$ . The density increased approximately linearly up to  $10^{20} \text{ cm}^{-2} \text{ s}^{-1}$ , then, in a few cases, appeared to rise faster than linearly. A change to a faster rise above some threshold would indicate neutral trapping.

We investigated particle balance by comparing the scoop neutral densities with estimates of the particle influx, the particle outflux from the main plasma, and the fueling rate. As shown in Fig. 3e, the number of neutrals in the scoop plenum was roughly constant during the neutral beam phase at  $N \sim 1.5 \times 10^{14} \text{ cm}^{-3} \times (5 \times 10^4 \text{ cm}^3) = 7.5 \times 10^{18}$ . This equals the rate for deuterium entering,  $R_{in}$ , times the exit time,  $\tau_{ex}$  for particles to leave the plenum, either by exiting the channels, or by being pumped by surfaces inside the scoop. The cross sectional area of each of the channel entrances (fig. 2a) was  $40 \text{ cm}^2$ . If the plasma flow into these was uniform poloidally and at one-half sonic speed, then the total rate for ions entering during the

neutral beam phase would be

$$R_{chan} = \frac{1}{2} \left( \frac{1}{6} F \right) \times 80 \text{ cm}^2 = 10^{21} / \text{s}.$$

Ions in the channels get accelerated by the sheath potential of the neutralizer, which increases their energy by about  $3 kT_e$ . After striking the neutralizer, about half get reflected, and lose about half their energy. The other half which gets imbedded is not reemitted in significant quantities during the discharge unless the pulse length is longer than the wall recycling time [8]. We do not know the surface condition or temperature of the neutralizer during discharges, but the recycling time probably was long. The volume of vanadium was sufficient to absorb all the imbedded deuterium used to fuel the scoop shots. Some fraction  $f$  of the reflected deuterium enters the plenum, so  $R_{in} \sim f R_{chan} / 2$ . Thus particle balance requires  $\tau_{ex} = N / R_{in} \sim (15/f) \text{ ms}$ .

If the plasma is not dense enough to alter  $f$ , then from the geometry of the neutralizer and channels,  $f \sim 1/3$  and thus  $\tau_{ex} \sim 50 \text{ ms}$ . The exhaust time for neutrals to exit out the channels, derived by estimating the conductance without plasma trapping in the channels, is

$$\tau_{ex} = \left\{ \frac{M}{M_{D_2} 40 T_{(eV)}} \right\}^{1/2} 50 \text{ ms}.$$

If the exiting deuterium is at room temperature,  $\tau_{ex}$  would be about 50 ms. If channel plasma trapped neutrals, then  $f$  would increase, requiring a smaller  $\tau_{ex}$ . Also, the decrease in conductance would increase the constant factor in the above expression for  $\tau_{ex}$ , so the exiting deuterium would have to be hotter, or pumping would be required to decrease  $\tau_{ex}$ . One piece of evidence for small  $\tau_{ex}$  is the rapid decrease of the Shultz-Phelps signal after sawteeth (fig. 4e), within several msec instead of 50 msec.

Monte Carlo calculations indicate that the average energy of atomic deuterium in the box was between 10 and 20 eV. A titanium getter ball has been used to deposit titanium inside the scoop during one afternoon 6 weeks before most of the neutral beam heated discharges occurred. Inside surfaces probably were coated with sufficient impurities such as oxygen to prevent the low energy deuterium from entering; however, they could have continued getting hot neutrals. 10 eV is probably sufficiently high to penetrate typical impurity layers. Also, there were stainless steel tubes and a large number of cables inside the box, so the internal surface area was extremely large. This may have increased the pumping speed.

If the global particle confinement time of the plasma were 100 ms (section 3) with  $\bar{n}_e = 5 \times 10^{13} \text{ cm}^{-3}$ , then

the number of particles leaving the plasma would be  $2.5 \times R_{\text{chan}}$ . The fueling rate for scoop discharges was typically less than  $R_{\text{chan}}$  by about an order of magnitude, which indicates that deuterium must have recycled through the scoop ten or more times.

### 3. Characteristics of neutral beam heated scoop discharges

Plasmas with major radius 153 cm and minor radius 40 cm were run on the scoop. Electron temperature and

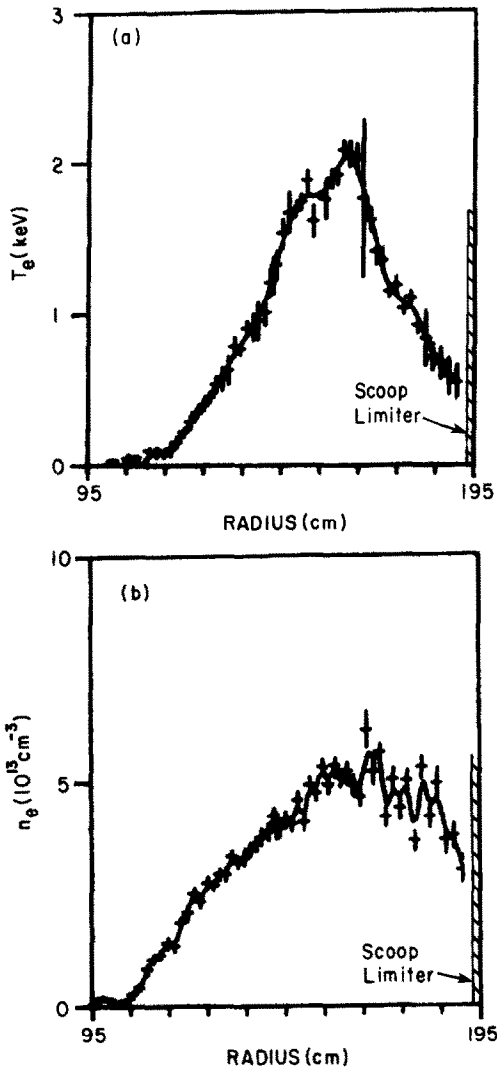


Fig. 7. Electron Temperature (a) and density profiles (b) for a discharge with  $I_p = 360$  kA and 2.3 MW of injected  $D^0$  power at 580 ms in the neutral beam phase.

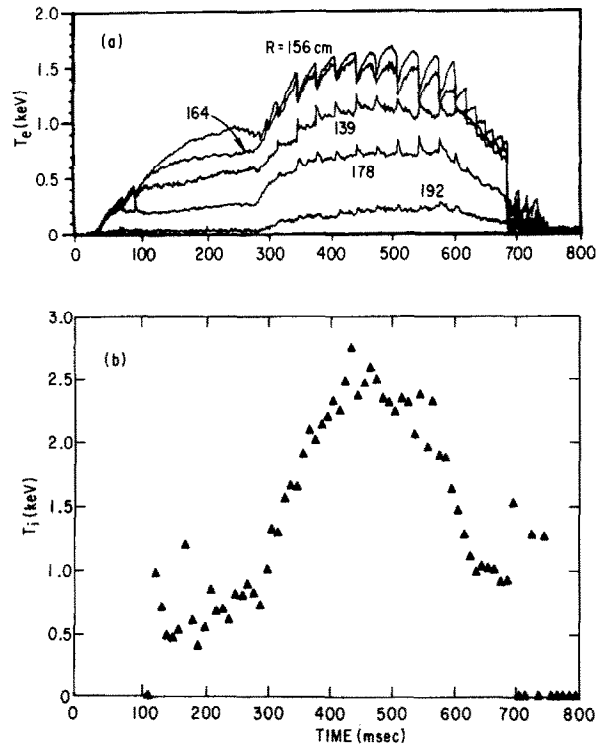


Fig. 8. Central electron (a) and ion temperature (b) measurements versus time averaged for several identical discharges, including the one used in fig. 7.

density profiles were measured by multi-point Thomson scattering, and by electron cyclotron emission. Thomson scattering profiles for a discharge heated with 2.3 MW of  $D^0$  power are shown in fig. 7. Electron temperatures were also measured by passive electron cyclotron emission, and central ion temperatures were measured by a passive charge exchange diagnostic using small amounts of hydrogen in the deuterium discharges. The variation with time measured during several identical discharges, including the one used in fig. 7, is shown in fig. 8.

The Thomson scattering profiles indicate surprisingly high electron densities and temperatures at major radii close to the limiter blades. However, the maximum temperature increase observed on the blades using an IR camera varied between 300 and 1500 °C from shot to shot, so the absorbed power must have been only 1–2.5 kW cm<sup>-2</sup>. Apparently a sharp gradient in power must have existed near the scoop.

The TV camera, which viewed the scoop from a port on the opposite side of PDX, observed very localized



visible light emission indicating that recycling on the scoop blades was very localized. Pressure measurements of the vacuum vessel indicated relatively low pressures ( $\sim 10^{-5}$  Torr). This contrasts with the high pressures ( $10^{-2}$  Torr) measured in the scoop (fig. 6).

Central chord bremsstrahlung emission yielded estimates of the line averaged  $Z_{\text{eff}} \approx 1.5$ –2.3. This range is comparable to that measured during H-mode divertor runs in PDX [9]. Vacuum ultraviolet spectroscopy indicates that the main impurity spectral lines were low-Z, such as carbon and oxygen.

Approximately 200 of the neutral beam heated discharges did not disrupt before the end of the beam pulse. Sufficient measurements were archived to permit magnetic analysis of most of these. For this analysis, the total stored plasma energy (thermal + beam ion)  $U$  was determined by constructing  $\beta_{\text{poloidal}} + I_p/2$  from the measured equilibrium vertical  $B$  field, and subtracting  $I_p/2$  using an estimate of the current profile. From  $U$  and the total heating power  $P_{\text{tot}}$ , which is the sum of the ohmic heating power  $I_p V$  and the neutral beam power absorbed by the plasma  $P_{\text{abs}}$ , the equilibrium energy confinement time is given by

$$\tau_E^{\text{eq}} = \frac{U}{P_{\text{tot}} - \partial U / \partial t}.$$

An example of this analysis for the discharge used in fig. 8 is given in fig. 9. From the figure, one can see the initial degradation of  $\tau_E^{\text{eq}}$  with the onset of neutral beam injection at 300 ms, followed by a continuing rise in  $I_p$  and  $\bar{n}_e$  and concomitant rise in  $\tau_E^{\text{eq}}$  to  $\approx 34$  ms at the end of the beam pulse.

Fig. 10 shows the variation of  $\tau_E^{\text{eq}}$  with  $P_{\text{abs}}$ . The  $\circ$  data, from shots with sawteeth, tended to have higher  $\tau_E^{\text{eq}}$  than the  $\bullet$  data from shots without sawteeth. Strong  $m = 2$  activity was identified in some of these  $\bullet$  discharges. We performed detailed transport analysis [10] of several high  $\tau_E^{\text{eq}}$  shots. This yielded thermal confinement times  $\tau_E^{\text{th}}$  which are determined from the stored energy and power losses from only the thermal plasma. The results, shown in fig. 10, agree reasonably well with the data given by the simpler magnetic analysis. Both methods show that  $\tau_E$  degrades as  $P_{\text{abs}}$  increased above 2.5 MW.

The variation of  $\tau_E^{\text{eq}}$  with the plasma current for shots with  $P_{\text{abs}}$  between 1.6 and 2.5 MW is shown in fig. 11a. For comparison, the line  $I_p/10$ , corresponding to average H-mode confinement times [9] is given. There was a tendency for  $\tau_E^{\text{eq}}$  to increase with  $I_p$ . Fig. 11b shows that  $\tau_E^{\text{eq}}$  scaled by  $I_p$  did not depend strongly on  $\bar{n}_e$ . No strong dependence of  $\tau_E^{\text{eq}}$  on internal scoop measurements was noticed.

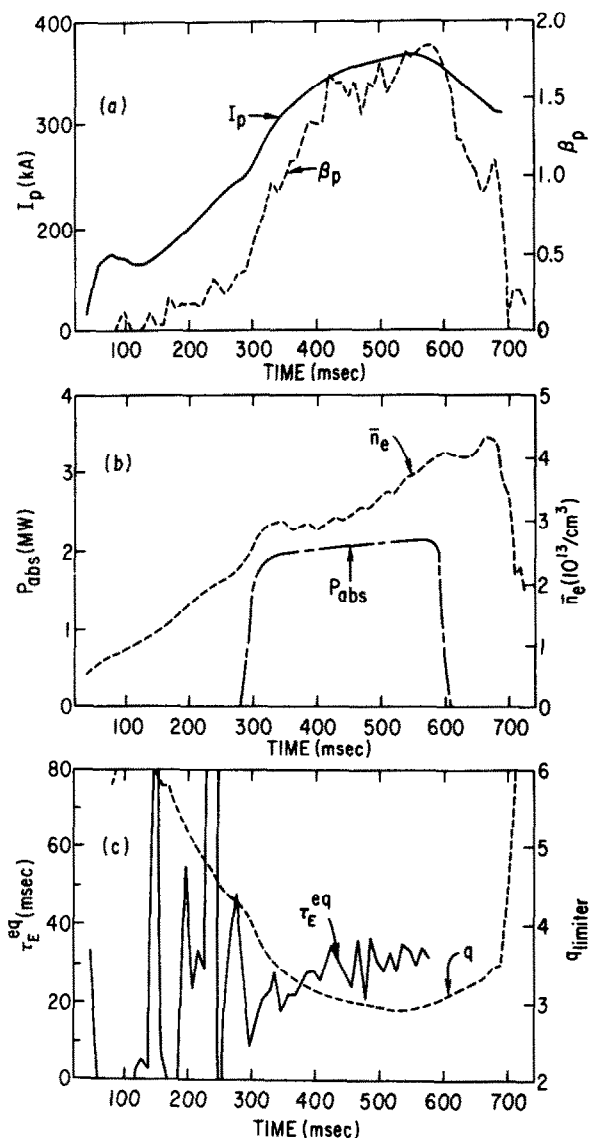


Fig. 9. Example of plasma conditions versus time and the magnetic analysis of a discharge (a) plasma current and beta toroidal, (b) line-averaged electron density and absorbed neutral beam power, (c)  $\tau_E^{\text{eq}}$  and the safety factor  $q$  at the limiter.

The horizontally scanning charge-exchange analyzer measured beam ion charge-exchange efflux from the plasma region close toroidally to the scoop. Absolute signal levels were about 1/3 of those measured with typical diverted plasmas. Comparison with the efflux calculated by the transport analysis code gives a coarse estimate of the deuterium confinement time and the neutral density distribution near the scoop. Long con-

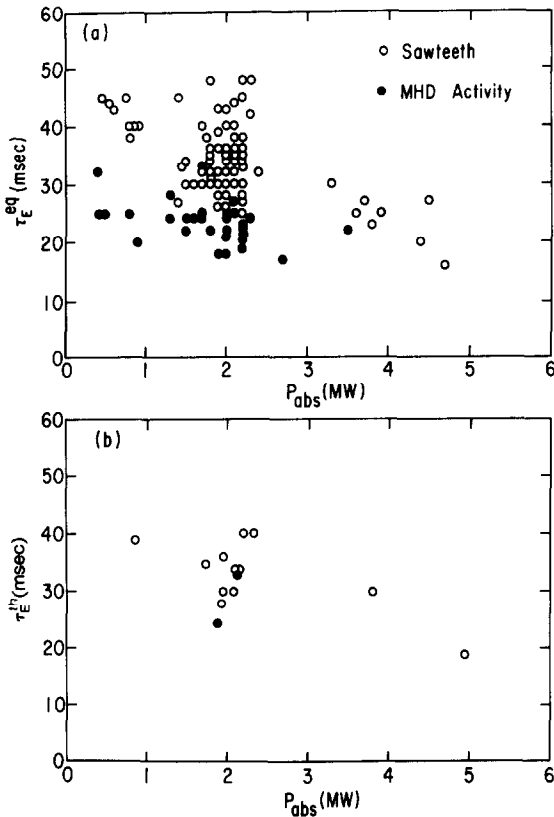


Fig. 10. Peak  $\tau_E$  during the neutral beam heated phases of discharges versus  $P_{abs}$ : (a)  $\tau_E^{eq}$  from magnetics analysis of shots with sawteeth  $\circ$ , and without  $\bullet$ , (b)  $\tau_E^{th}$  from transport analysis of shots with sawteeth.

finement times, greater than 100 ms, were inferred this way. The recycling source neutral density (as opposed to the beam halo source neutral density) was in the low to mid- $10^9 \text{ cm}^{-3}$  range at  $r = 40 \text{ cm}$ . This range is quite low, even compared with that deduced in the same manner for divertor discharges. One would have expected a high neutral density this close to a standard limiter.

We investigated power balance for shots with  $P_{tot} \sim 2 \text{ MW}$ . A 19 channel bolometer array measured energy flux along chords from the plasma, providing an estimate for the sum of the radiated and charge-exchange power loss. Less than 20–40% of  $P_{tot}$  was detected. Part of the rest was scraped onto the limiter blade or into the scoop channels. The IR camera measurements indicated that approximately 25–50% of the  $P_{tot}$  heated the limiter. A calorimeter measured heat flow in the limiter shadow region on the midplane about 2 m from the scoop. The

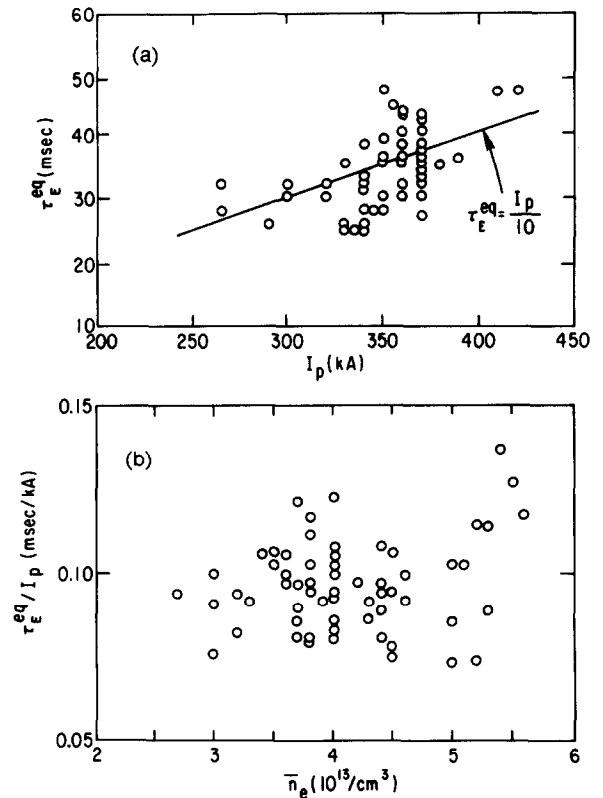


Fig. 11. Variation of peak  $\tau_E^{eq}$  for discharges with  $1.6 < P_{abs} < 2.5 \text{ MW}$ . (a) versus  $I_p$  and (b) scaled by  $I_p$  versus  $\bar{n}_e$ .

measured heat flux profile [7] indicates that approximately  $1 \text{ kW/cm}^2$  flowed into the ion side channel at the midplane during the neutral beam phase. If the heat flow was uniform poloidally across the channel entrance, and had the same left–right asymmetry as the ion current, then about 60 kW, or 3% of  $P_{tot}$  entered the scoop. About 5–50% of the power is thus unaccounted for. This is typical of limiter discharges in PDX. For these, it has been speculated that the cloud of neutrals around the limiter carried substantial amounts of the unobserved energy to the vacuum vessel wall. Since it appears that the scoop does not have as much of a cloud, this cannot explain the scoop observation.

Recycling and confinement of  $\text{He}^3$  were studied by puffing short bursts of  $\text{He}^3$  through the scoop or dome gas injection valves into the discharge and monitoring the protons from the  $\text{He}^3(d, p)\alpha$  reaction [11]. The rise time of the proton signal was about 50 ms and was probably determined by the gas conductance to the main chamber, thus the inward transport time for  $\text{He}^3$  was  $\leq 50 \text{ ms}$ . The exponential decay time of the proton

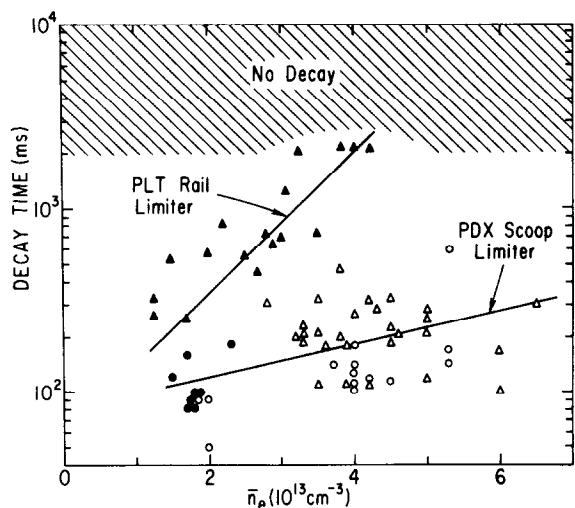


Fig. 12. Decay time of protons from  $D + \text{He}^3 \rightarrow p + \text{He}^4$  versus  $\bar{n}_e$  measured by  $\text{He}^3$  puffing in PDX and PLT. The  $\circ$  data are from PDX with scoop puffing and the  $\Delta$  data are from PDX with upper divertor dome puffing. The  $\bullet$  and  $\blacktriangle$  data are both from carbon rail limiter operation in PLT.

signal was longer (fig. 12) and was dominated primarily by the recycling and pumping of  $\text{He}^3$ . When the average plasma density was larger than  $3 \times 10^{13} \text{ cm}^{-3}$ , the  $\text{He}^3$  decay time was up to an order to magnitude shorter than for similar PLT experiments which used a carbon rail limiter. The enhanced pumping of  $\text{He}^3$  by the scoop might be explained by helium removal by the scoop, or by helium burial in the scoop limiter blades due to high edge temperature. The vacuum vessel of PDX is much larger than PLT, and this may have played a role in keeping the decay time short. Some calculations have indicated that a scoop will pump  $\text{He}^4$  preferentially [12]. Other calculations indicate the contrary [5].

#### 4. Conclusions

After several days of neutral beam conditioning, plasmas were run on the scoop with high scoop densities, low external neutral densities, and high energy confinement times. There are indications that scoop

channel recycling may have occurred for several shots with high line-averaged plasma densities. For most of the shots, including many with high energy confinement times and low neutral densities, scoop channel recycling was not observed. Apparently even without this recycling, neutrals from inside the scoop, and from the scoop limiter blades did not enter the plasma core in large quantities.

The use of the scoop limiter on PDX facilitated the production of plasmas with energy confinement and impurity concentrations comparable to the best PDX diverted plasmas. Further experimentation, especially with long pulse operation, would help to evaluate the potential of scoop limiters for fusion reactors.

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