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# Performance of a Hybrid ED-NF Membrane System for NOM Removal and Fouling Control

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### 1 Abstract

2 Natural organic matter (NOM) complicates water treatment and causes formation of 3 disinfection byproducts (DBPs). NOM is removed well by nanofiltration (NF) but causes 4 extensive membrane fouling, especially in the presence of divalent cations. This research 5 investigated a hybrid electrodialysis-nanofiltration (ED-NF) system to treat freshwaters 6 containing hardness and NOM. ED removes most ions but little to no NOM, and the ED diluate 7 is then treated with NF to remove NOM with reduced fouling. Subsequently, some or all of the 8 ED concentrate can be mixed with the NF permeate to increase water recovery, limit NOM 9 concentration (and thereby reduce DBPs), and control the ion content. Compared to NF alone, 10 ED-NF increases product water yield. NF fouling was reduced by the removal of divalent cations 11 in ED. Spectroscopic and resonant scattering measurements of fouled membranes near the 12 calcium K-edge reveal a significant contribution to NF fouling by calcium bridging between 13 carboxyl groups in NOM and on the membrane surface. This novel ED-NF system allows 14 several control "knobs" to increase water recovery and reduce DBP formation potential by 15 adjusting ED water recovery, ED diluate (and concentrate) ionic composition, and the fraction of 16 concentrate re-mixed with NF permeate to form the product water.

17 Keywords: Water treatment; Disinfection byproducts; Fouling mechanisms; X-ray spectroscopy;
18 Resonant X-ray scattering

### 19 Graphical Abstract



22 1 Introduction

23 Natural organic matter (NOM) is present in virtually all surface waters and includes 24 humic and non-humic fractions with a wide range of molecular weights and reactivities based on sources and the presence of specific functional groups.<sup>1,2</sup> NOM represents a major challenge in 25 26 water treatment; not only does it cause color and taste problems directly, but it reacts with 27 chlorine, the most commonly used disinfectant, to form potentially carcinogenic disinfection byproducts (DBPs) such as trihalomethanes (THMs) and haloacetic acids (HAAs).<sup>3,4</sup> The 28 29 reduction of DBPs in drinking water can be achieved by substituting other disinfection methods 30 for chlorination, removing DBPs precursors (e.g., NOM), and/or eliminating DBPs after formation.<sup>5,6</sup> These strategies to reduce DBPs in drinking water are reviewed briefly below, but 31 32 this research focused on systems that use nanofiltration (NF) for removal of the DBP precursor, 33 NOM. More specifically, since NOM often limits the productivity of NF membranes by fouling, 34 the objective of the research was to increase the water recovery in NF systems for drinking 35 water.

36 Water treatment processes for NOM removal include enhanced coagulation, advanced oxidation, adsorption, and membrane technologies.<sup>5,7</sup> Enhanced coagulation is a regulatory 37 38 requirement for conventional water treatment plants in the United States, but the targeted 39 dissolved organic carbon (DOC) removals (which depend on the influent alkalinity and DOC) 40 are relatively low and the process drastically increases production of residuals that need to be managed.<sup>8,9,10</sup> Advanced oxidation processes (AOPs) can achieve between 40-90% NOM 41 removal efficiency,<sup>11</sup> but the efficiency depends on the type and amount of organic matter and 42 43 the process creates smaller organics that are often biodegradable. Thus, AOPs are usually coupled with other technologies such as membrane filtration, adsorption, and biodegradation.<sup>12</sup> 44

In the United States, adsorption has been used more commonly to target undesirable synthetic organic chemicals (SOCs) such as pesticides and herbicides rather that NOM removal; NOM removal by adsorption can vary widely over time and can reduce the efficiency for target SOCs either through competition for sites or pore-blocking by NOM.<sup>13</sup> Ultrafiltration (UF) membranes can effectively remove NOM with relatively high molecular weights but the pores sizes (typically 30 to 1000 Å) allow most of the humic substances to pass through.

51 Nanofiltration (NF) can be an excellent solution for the removal of DBPs precursors 52 including the lower molecular weight fraction.<sup>5</sup> NOM removal efficiencies achieved by NF can exceed 80% and NF can be applied to various types of water.<sup>14–17</sup> However, membrane fouling 53 54 decreases permeate flux and limits the utility of NF for NOM removal because of the loss of productivity and added capital and operational costs;<sup>18,19</sup> productivity here includes both 55 56 permeate flux and volume throughput (or water recovery) between chemical cleanings. NF 57 membrane fouling increases in the presence of cations, as NOM molecules and membrane 58 surfaces are often negatively charged due to specific functional groups (e.g., carboxylic acids) 59 and reduced electrostatic repulsion of the negatively charged macromolecules can lead to the formation of dense/compact NOM fouling layers.<sup>15,20-22</sup> Additionally, divalent cations such as 60 Ca<sup>2+</sup> and Mg<sup>2+</sup> can bridge negatively charged functional groups to significantly increase 61 fouling.<sup>15,21,23</sup> Therefore, a pretreatment process to remove inorganic ions, particularly cations, 62 63 could considerably reduce NF membrane fouling and increase productivity during water 64 treatment. Precipitative softening to remove divalent cations prior to NF requires chemicals, such 65 as lime, and space for both coagulation/flocculation and sedimentation processes. Ion exchange is simpler than lime softening, but increases Na<sup>+</sup> concentration in the finished water and 66 produces high salinity regeneration waste streams.<sup>24,25</sup>. Since NF membranes are currently used 67

not only for NOM removal but also water softening (i.e., removal of multivalent cations),<sup>7,26,27</sup>
softening pretreatment via NF holds some attraction because membrane systems are modular,
scalable, energy efficient, and minimize chemical use,<sup>28,29</sup> but fouling, as indicated above, is
problematic.

72 Another possible (and heretofore unexplored) pretreatment strategy for NOM removal by 73 NF is electrodialysis (ED). ED is a technically verified water treatment technology with more 74 than a half-century of field-scale success at producing high quality water from brackish water.<sup>30,31</sup> ED separates charged molecules from feed waters using ion exchange membranes 75 (IEMs) but does not provide appreciable separation of NOM.<sup>32</sup> Although acidic fractions of 76 77 NOM are negatively charged, NOM molecules exhibit low diffusivity due to their large size<sup>33</sup> and cannot pass through the low molecular weight cut-off IEMs used in ED.<sup>34</sup> A coupled RO/ED 78 system has been used to isolate/extract NOM from freshwater and seawater<sup>35,36</sup>, but the studies 79 80 focused on NOM harvesting rather than drinkable water production and RO membrane fouling 81 mitigation. ED has been studied as a pretreatment to remove divalent cations in the presence of 82 NOM or neutral solutes, and the researchers of those studies also found that ED has a potential to separate divalent ions without separation of NOM or neutral solutes.<sup>32,37</sup> However, a complete 83 84 hybrid ED-NF process for NOM removal and NF fouling mitigation to improve productivity has 85 not been thoroughly investigated previously to our knowledge.

This research focuses on the development of a hybrid ED-NF membrane system to remove NOM and increase the productivity of NF systems while providing appropriate ion concentrations (for drinking water) in the final product water (Figure 1). With the proper choice of the ion-exchange membranes, ED can remove most inorganic ions while achieving minimal removal of NOM; subsequently, the ED diluate, containing few inorganic ions but NOM at 91 nearly the original concentration, can be treated by NF to remove NOM. In NF membrane
92 systems for drinking water production, remineralization after NF treatment is often required
93 because high removal of monovalent and/or divalent ions can produce unsavory and corrosive
94 water.<sup>38,39</sup> In this hybrid ED-NF system, some or all of the small volume of ED concentrate and
95 the large volume of NF permeate can be combined to yield water with dramatically lower NOM
96 concentration and ion concentrations appropriate for drinking water.

97 The total water recovery includes (some or all of) the ED concentrate and the NF 98 permeate, so varying the ratio of ED concentrate to NF permeate mixed in the final step can be 99 used to impact the recovery and tailor the resulting NOM and inorganic ion concentrations to 100 desired values. With low resulting NOM concentration, disinfection of the resulting water by 101 chlorination would result in acceptably low DBP concentrations.



Figure 1. The proposed hybrid electrodialysis-nanofiltration (ED-NF) system for drinking water
 treatment of freshwaters containing natural organic matter (NOM) and hardness.

In a previous study for the ED part of this hybrid process, we found that NOM can be sorbed onto the IEM surface but ED can effectively separate alkaline earth metal ions without separation of NOM and without significant NOM sorption with proper IEMs.<sup>32</sup> Here, we focus on the combination of ED and NF. To achieve the overall objective, tasks in this research were to

109 determine whether ED pretreatment is effective in reducing NF membrane fouling, to use 110 spectroscopic techniques to ascertain the causes of fouling, and to assess the DBP formation 111 potential of the hybrid ED-NF system product water. Fouling of the IEMs at the ED stage of the 112 hybrid ED-NF system was not investigated in this study, as it was considered in the previous 113 work.<sup>32</sup> Technical evaluation metrics of the hybrid ED-NF system include the fractional water 114 yield, product water quality, and fouling characteristics of the NF membrane in the absence and 115 presence of ED pretreatment. The performance of the hybrid ED-NF system was evaluated for 116 three synthetic feedwaters containing NOM and one natural feedwater. DBP formation potential, 117 particularly trihalomethane formation potential, of the product water was evaluated using two 118 natural feedwaters to real treatment plants and compared to the formation potential of product 119 waters from the NOM removal processes currently employed at those plants. The fractional 120 recovery of the natural waters treated with the hybrid system to achieve a trihalomethane 121 formation potential (THMFP) below the US standard for THMs was estimated.

122 2 Materials and methods

123

### 2.1 Experimental solutions

124 Table 1 shows feedwater compositions for the experiments performed in this research; additional 125 details are in Sections 1 and 2 of the Supporting Information. This research employed five 126 different NOM sources: Lake Austin NOM (LAN), Suwannee River NOM (SNOM), Leonardite 127 Humic Acid (LHA), Texas Water NOM (TWN), and Florida Water NOM (FWN). SNOM and 128 LHA were purchased from the International Humic Substances Society (IHSS, St. Paul, MN). 129 LAN was extracted from Lake Austin in Austin, TX. Three synthetic feedwaters were prepared 130 using filtered (1.5 µm) stock solutions of LHA, SNOM, and LAN. NOM stock solutions were 131 diluted to 5 mg/L dissolved organic carbon (DOC) using Milli-Q water (Millipore, Bedford, MA,

132 USA) and the target amounts of ACS grade NaCl, CaCl<sub>2</sub>·2H<sub>2</sub>O (both from Fisher, Pittsburgh, 133 PA), and MgCl<sub>2</sub>·4H<sub>2</sub>O (AMResco, Solon, OH) were added to each synthetic feedwater. Since 134 membrane fouling is known to be exacerbated by divalent cations, all synthetic feedwaters 135 utilized the same background anion, chloride. Although we focus on cations in this study, ED 136 pretreatment can also combat membrane fouling/scaling caused by anions (carbonate, sulfate, 137 phosphate). 138 Florida Water (FWN) and Texas Water (TWN) were filtered (1.5 µm) and used with their 139 natural concentrations of all ions and NOM. FWN contains approximately 16.5 mg/L DOC, and 140 TWN contains approximately 4.5 mg/L DOC (Table 1). SNOM, LHA, LAN, and FWN were

141 used for the hybrid ED-NF system technical performance evaluation, and FWN and TWN were

142 used for DBP formation potential experiments.

Type of feed	Feed Water <sup>a</sup>	Type of NOM	SUVA <sub>254</sub> <sup>b</sup> (L/mg·m)	Conductivity (µS/cm)	Ca mg/L	Mg (mg/L)	Na mg/L	DOC mg/L	Ca/DOC (mM/mM)	Note <sup>c</sup>
	LAN	Lake Austin NOM (LAN)	2.17±0.11 <sup>d</sup>	1224±2	68.2±0.4	7.3±0.8	112±10	5.1±0.4	4.02±0.20	
	LAN W/ ED		2.13±0.17	245±0.4	7.3±0.1	0.7±0.1	25.1±1.6	5.2±0.3	0.42±0.02	Ι
Synthetic	SNOM	Suwannee River NOM (SNOM)	3.77±0.19	937±1	28.0±0.6	7.2±0.6	154±7	5.0±0.4	1.69±0.11	Ι
freshwater	SNOM W/ ED		3.71±0.15	187±0.2	2.8±1.4	1.2±0.1	26.3±1.3	5.0±0.2	0.16±0.01	
	LHA	Leonardite	9.09±0.36	945±2	28.1±1.1	7.2±0.5	154±8	5.1±0.4	$1.66 \pm 0.07$	
	LHA W/ ED	Humic Acid (LHA)	9.05±0.41	189±0.4	2.7±0.3	1.4±0.1	20.6±9.6	5.0±0.3	0.16±0.10	Ι
	FWN	Florida Water	$3.74 \pm 0.05$	720±9	84.4±0.6	13.3±0.5	36.8±2.7	16.5±0.5	$1.54 \pm 0.04$	
Natural	FWN W/ ED	NOM (FWN)	3.64±0.38	144±4	7.3±1.6	1.6±1.2	9.7±0.6	16.7±0.5	0.13±0.03	I, II
freshwater	TWN	Texas Water	2.89±0.08	449±7	61.0±2.7	10.5±1.1	22.1±6.8	4.5±0.1	4.07±0.10	
	TWN W/ ED	NOM (TWN)	2.85±0.18	90±1	7.6±1.5	1.8±0.3	8.7±0.5	4.5±0.1	0.51±0.10	II

Table 1. Feedwater compositions for hybrid ED-NF system technical performance evaluation and disinfection by-product potential
 experiments.

a. W/ED feeds are the ED pretreatment product waters (ED diluate) that were subjected to NF treatment; feeds without that designation were the influent to NF in the NF alone experiments and the influent to ED in the hybrid ED-NF system

b. Specific Ultra Violet Absorbance (SUVA<sub>254</sub>) (L/mg·m) is an indicator of the relative fraction of aromatic NOM components and the hydrophobicity of NOM; a SUVA value greater than 4 suggests that the NOM contains high molar mass compounds and exhibits high hydrophobicity, whereas SUVA less than 2 suggests lower molar mass compounds and low hydrophobicity<sup>17</sup>.

c. Note specifies the experiments in which each feedwater was used: (I) technical performance evaluation tests; (II) DBP formation potential tests d. ± indicates 95% confidence intervals

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#### 2.2 Bench-scale Electrodialysis and Nanofiltration experiments

147 ED experiments were conducted using a batch-recycle ED experimental apparatus (Figure S2), as described in our previous study.<sup>32</sup> This apparatus consists of an electrodialyzer 148 149 and three streams: diluate (D), concentrate (C), and electrode rinse (E). ED pretreatment used 8 L 150 of diluate and 2 L of concentrate (i.e., 80% water recovery) with an 80% conductivity removal 151 goal. Details of the system are explained in Section 4 of the Supporting Information and are essentially identical to those reported by Kum et al.<sup>32</sup> The details of the specific energy 152 153 calculation (SEC) of the ED process are in Section 5 of the Supporting Information. In our 154 previous work we evaluated several different AEM/CEM pairs to identify a set that yielded the 155 lowest NOM adsorption; CMX/AMX IEM pair (Tokuyama Soda Co. Ltd. Japan) was chosen in this study based on its good separation of inorganic ions with minimal organic matter 156 157 separation/sorption.<sup>32,40</sup> 158 NF experiments were conducted using a laboratory-scale crossflow membrane system 159 (Figure S3); details of the system and its operation are in Section 6 of the Supporting Information. The NF270 membrane (DuPont FilmTec<sup>TM</sup>, Edina, MN) was chosen based on its 160 high permeate flux and NOM removal reported in previous research.<sup>41</sup> All NF experiments were 161 162 performed at a constant applied pressure of 4.8 bar (70 psig), the pressure that was applied by the manufacturer to identify the typical properties of NF270 membranes.<sup>42</sup> Performance of the 163

- 164 hybrid ED-NF system was compared to the NF system without any pretreatment.
- 165

#### 2.3 Water Sampling and Qualitative Analyses of Samples

Liquid samples were collected from the diluate/permeate and concentrate/feed of the
 ED/NF systems during experiments. In ED experiments, 10 mL samples were pipetted from each
 reservoir after each 10% reduction in conductivity from 10% to 80% to measure concentrations

169 of major cations (sodium, calcium, and magnesium) and the ultraviolet (UV) absorbance (254 170 nm), and 40 mL samples were withdrawn at the beginning and end to measure DOC 171 concentrations. In NF experiments, 50 mL of feedwater were withdrawn by pipette from the feed 172 reservoir and 50 mL of permeate were taken directly from the permeate stream at the beginning 173 of each experiment and every 24 hours for the duration of the NF experiments. Concentrations of 174 major cations and DOC, and the UV absorbance (254 nm), were measured for NF experimental 175 samples. NF experiments were run for six days with SNOM, LAN, and FWN, but the LHA 176 waters were run for only 24 hours due to higher fouling by this hydrophobic NOM. 177 Because cations significantly impact NOM fouling on membrane surfaces, our attention 178 was on cation removal rather than anion removal, as noted earlier. Concentrations of major 179 cations were measured via inductively coupled plasma-optical emission spectroscopy (ICP-OES, 180 Varian 710-ES, Varian, Inc, Palo Alto, CA). DOC concentrations were analyzed using a total 181 organic carbon analyzer (TOC-L CPH/CPN, Shimadzu, Japan). The ultraviolet absorbance at a 182 wavelength of 254 nm was measured using a diode array UV-Vis system (Agilent 8453, Agilent 183 Technologies, Santa Clara, CA) with a 1 cm path length quartz cell; specific ultraviolet 184 absorbance (SUVA254) values were calculated as the ratio of UV absorbance and DOC.

185

### 2.4 Membrane Surface Analysis

Fouled and virgin NF membranes were dried and stored in a desiccator at atmospheric
pressure. Sections of each NF membrane were cut for *ex situ* investigation via scanning electron
microscopy (SEM), attenuated total reflectance Fourier transform infrared spectroscopy (ATRFTIR), and X-ray photoelectron spectroscopy (XPS). SEM (FEI Quanta FEG 650, Thermo
Fisher Scientific, Waltham, MA) was employed to identify foulants on the surface of the NF
membranes. Membrane samples were platinum-coated by a benchtop sputter coater (Cressington

208, Cressington Scientific Instruments, UK) before SEM analysis. ATR-FTIR measurements
provided detailed information on the functional groups present in the membranes and fouling
layers with a sampling depth of approximately 0.7 μm,<sup>43</sup> while surface-sensitive XPS provided
chemical information for the top-most portion of the fouling layer (i.e., sampling depth less than
10 nm).<sup>44</sup> Detailed information on ATR-FTIR and XPS measurements is in Sections 11 and 12 of
the Supporting Information, respectively.

198 Furthermore, *ex situ* membrane samples were analyzed using near edge X-ray absorption 199 fine structure (NEXAFS) spectroscopy and tender resonant X-ray scattering (TReXS) near the 200 calcium K-edge on beamline 12-ID-C at the National Synchrotron Light Source II (Brookhaven, 201 NY, USA); as explained subsequently, similar measurements for magnesium would require a 202 different beamline and separate preparation and were not performed. NEXAFS spectroscopy is 203 sensitive to specific chemical bonds and functional groups, so investigation near the Ca K-edge provides insight into the chemical environment of calcium in the fouling layers.<sup>45</sup> Meanwhile, X-204 205 ray scattering probes spatial periodicities to distinguish the structural arrangements and material 206 morphology. By tuning the X-ray energy near the absorption edge of core-level electronic 207 transitions in calcium atoms using tender X-rays, TReXS can provide added contrast to help probe the distribution of calcium in the membrane samples.<sup>46</sup> Samples were prepared by 208 209 carefully removing the fabric backing of the membranes and mounting the resulting thin films 210 comprised of a fouling layer, a polyamide/piperazine active layer, and a polysulfone support 211 layer (~50-60 µm total thickness, Table S4) on 10 mm washers. Fluorescence-yield NEXAFS spectra and transmission TReXS data were collected at energies near the calcium K-edge (4030-212 213 4075 eV) using a Pilatus 300KW detector (Dectris, Philadelphia, PA, USA). Attenuation lengths 214 of tender X-rays through representative membrane/foulant materials (Table S6) are between 20

and 50 µm on-resonance and between 95 and 120 µm off-resonance,<sup>47</sup> indicating that the fouling
layers (<10 µm thick, Table S4) were fully probed during NEXAFS and TReXS measurements.</li>
Additional information on these measurements is in Section 13 of the Supporting Information.

218

### 2.5 Disinfection by-products formation potential experiments

219 Trihalomethane formation potential (THMFP) experiments were conducted using the two 220 natural feedwaters (TWN and FWN) to evaluate the water recovery possible when the ED-NF 221 system is used to limit DBPs in the final product water. The THMFP of product waters from the 222 hybrid ED-NF system was compared to that obtained by the existing NOM removal processes 223 employed at the treatment plants. The plant with TWN as its source water uses enhanced 224 coagulation to reduce NOM concentrations; poly-aluminum chloride coagulant was acquired from the plant and used for this research. The plant with FWN as its source water applies NF to 225 226 reduce hardness and NOM concentration, so we compared the hybrid ED-NF treated water to 227 water treated by NF alone. Since FWN has a very high NOM concentration, only 50% of the ED 228 concentrate was mixed with the NF permeate in the hybrid ED-NF system. THMFP tests were conducted based on Standard Method 5710B<sup>48</sup> and THM analyses were performed following US 229 Environmental Protection Agency (US EPA) Method 551.1.<sup>49</sup> Briefly, samples were spiked with 230 231 free chlorine (to yield residuals of 2 - 5 mg/L at day 7) and reacted for 7 days in the dark at 25 232 °C, followed by extraction of THMs into pentane and determination of THM concentrations via 233 gas chromatography with an electron capture detector.

#### **3 Results and Discussion**

235

#### **3.1** ED pretreatment provides selective removal of cations

236 Using four NOM sources, the ED pretreatment performance as a function of NOM source 237 characteristics could be examined (Figure 2). In Figure 2, the abscissa is the specific energy 238 consumption (SEC, a normalized measure of the energy use to accomplish gen amounts of separation), the left ordinate is the normalized concentration of Na<sup>+</sup>, Ca<sup>2+</sup>, and Mg<sup>2+</sup>, and the 239 240 right ordinate is the normalized UV absorbance (taken as a measure of NOM content). In ED 241 experiments with all four NOM sources, the CMX membrane provided greater relative separation of Ca<sup>2+</sup> and Mg<sup>2+</sup> compared to Na<sup>+</sup>, at least in the early stages of the experiments. This 242 243 cation separation trend is more obvious in the concentrate stream, which could reach at most five times the initial feed concentration of cations (the volumes of concentrate and diluate are 2 L and 244 8 L, respectively). This result is consistent with previous studies<sup>32,50,51</sup> and is attributed to the 245 246 selectivity of sulfonic acid groups in the CMX membrane for multivalent cations over monovalent cations.<sup>52</sup> (Note, however, that for all but FWN, the molar concentration of Na<sup>+</sup>--and 247 248 therefore the molar flux through the CEM--was substantially higher than that of the divalent 249 cations.)

For both LAN (Figure 2a) and SNOM (Figure 2b), the relative UV absorbance ratio in the diluate and concentrate streams stayed near one throughout the entire ED experiment, and DOC concentrations and SUVA<sub>254</sub> values in the diluate before and after ED pretreatment were similar (Table 1). Each of these trends indicates that little NOM separation and little NOM sorption to the IEMs occurred; total NOM mass loss during ED pretreatment was less than 1% for both LAN and SNOM. Generally, if a NOM contains a large number of hydrophobic components, the NOM likely has a SUVA<sub>254</sub> value over 4 and contains substantial fraction of

NOM with molecular weights over 10000 Da.<sup>16,17,53</sup> According to the SUVA<sub>254</sub> values (Table 1)
and NOM molecular weight distributions (Figure S4), both NOMs have the SUVA<sub>254</sub> value less
than 4, and the weight-averaged molecular weights (Table S3) of LAN and SNOM are 750 Da
and 1260 Da, respectively, indicating LAN and SNOM are less likely to contain hydrophobic
components; the results were consistent with this expectation in that the LAN and SNOM
sorption to the IEMs during ED pretreatment was minimal.





Figure 2. Electrodialysis pretreatment separates inorganic ions ( $Ca^{2+}$ ,  $Mg^{2+}$ ,  $Na^{+}$ ) but does not provide significant NOM separation at 80% water recovery and 80% conductivity separation.



267 Since the initial conductivity of FWN is the lowest among the four NOM solutions (Table 268 1), the total SEC of ED to achieve the separation goal for FWN was less than that of the others. 269 In FWN, the calcium removal was greater than sodium in the diluate stream, but the degree of 270 calcium separation in the concentrate stream at the end of the experiment was not as significant 271 as observed in LAN and SNOM experiments; these observations could be due to calcium 272 carbonate precipitation and/or the IEM fouling in the concentrate. FWN is a natural freshwater 273 containing alkalinity and a relatively high calcium concentration. As ED removes inorganic ions 274 in the diluate, both the calcium and carbonate concentration in the concentrate increases; 275 therefore, there is a chance for calcium carbonate precipitation since the pH of concentrate 276 stream is above 7.8 and the saturation index (the ratio of the ion activity product to the saturation 277 equilibrium constant) of calcite (CaCO<sub>3</sub>) rises to 55 ( $\log SI > 1$ , oversaturated) at the end of the 278 ED experiment. In experiments with FWN, we again observed that the UV absorbance and DOC 279 concentrations in the diluate (Figure 2c and Table 1) before and after ED pretreatment did not 280 change significantly, but there was a nearly 14% UV absorbance and 5% DOC decrease in the 281 concentrate after ED pretreatment. These losses suggest that some NOM from the concentrate 282 stream sorbed to the IEMs during ED pretreatment, but minimal sorption occurred to the diluate 283 side of the membranes. The greater reduction in UV compared to DOC suggests that the more 284 hydrophobic fraction of NOM sorbed preferentially. This IEM fouling in the concentrate could 285 be due to the relatively high initial divalent ion concentration in the FWN solution; the calcium 286 and magnesium concentrations in the concentrate stream rose to nearly 8.5 mM and 2.2 mM, 287 respectively at 80% water recovery. In addition to high hardness concentrations, the high DOC 288 of FWN (16.5 mg/L) could have contributed to the observed NOM mass loss in the concentrate.

289	The inorganic ion separation trends with LHA are similar to those for the other waters,
290	but the organic separation trends show differences. Since LHA is a soil NOM and more
291	hydrophobic than the other NOM sources, it has greater tendency to sorb to the IEMs during ED,
292	and our results show LHA separation during ED not because of actual organic compound
293	separation through the IEMs but due to sorption to the IEMs in the concentrate. <sup>32</sup> Meanwhile,
294	minimal changes in UV absorbances, DOC concentrations, and SUVA254 values in the diluate
295	stream (Figure 2d and Table 1) indicate that IEM fouling only occurred in the concentrate
296	stream. At the end of ED pretreatment, the losses of UV and DOC were similar to those for
297	FWN; UV absorbance and DOC decreased by 17% and 7% in the concentrate, respectively.
298	Moreover, the amount of NOM sorption increased as the inorganic ion concentration increased in
299	the concentrate stream (Figure 3d). As the ionic strength rises with the percent of water recovery,
300	NOM molecules become coiled and compact, <sup>15</sup> thereby increasing the likelihood of membrane
301	surface adsorption and bridging by the increased divalent cation concentrations in the
302	concentrate. Additionally, both the AEM and CEM can be fouled by NOM in the concentrate,
303	but AEMs tends to exhibit greater fouling by NOM than CEMs because AEMs attract negatively
304	charged NOM to the membrane surface; <sup>32</sup> therefore, if the feed solution for ED pretreatment is
305	similar to FWN (high NOM and calcium concentrations) or LHA (high SUVA254 values),
306	additional efforts such as controlling pH, adding antiscalants, or choosing AEMs with minimal
307	NOM interaction, might be required to prevent NOM adsorption to the IEMs from the
308	concentrate and allow ED pretreatment to realize its full potential.

309

### 3.2 Improvements in NF permeate flux and water recovery following ED

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### pretreatment

To evaluate the impact of ED pretreatment on NF performance, NF experiments without and with ED pretreatment were operated for 144 hours with LAN, SNOM, and FWN and for 24 hours with LHA due to increased fouling by this hydrophobic NOM. The normalized permeate flux decline as a function of the cumulative normalized volume throughput for the four NOM sources without and with ED pretreatment is shown in Figure 3.

316 In all cases, the normalized permeate fluxes with ED pretreatment are higher than without 317 ED pretreatment immediately after the experiment begins; that is, ED pretreatment delays NOM 318 fouling on the membrane surface and improves the water production rate at constant applied 319 pressure due to the lower ion concentrations in the NF feed solution following ED (Table 1). The 320 permeate fluxes without ED pretreatment decreased immediately at the beginning of system 321 operation, an indication that the presence of divalent cations (Figure S6) and relatively high ionic 322 strength of the untreated water led to rapid NOM fouling of the NF membrane. Indeed, a set of experiments with SNOM that isolated the effects of the three cations (Na<sup>+</sup>, Ca<sup>2+</sup>, and Mg<sup>2+</sup>) and 323 324 reported in Section 10 of the Supporting Information showed that the presence of calcium or 325 magnesium ions leads to approximately 20% more permeate flux decline and 7-8% less water 326 production after 144 hours relative to experiments with SNOM and sodium.

The results in Figure 3 indicate that the flux decline rate slowed at the end of NF operation in SNOM and LAN, but FWN and LHA had continuous flux decline throughout the experiments. The higher NOM concentration in FWN, the greater hydrophobicity of LHA, and the high molecular weight fractions of these two NOM sources (Figure S4) are the likely causes for this observed behavior. ED pretreatment improved the flux in all cases, but the impacts of the composition and concentration of the NOMs on NF fouling persisted. In this work, the ED
system targeted only 80% removal of conductivity; however, optimization of ion removal during
ED could yield greater improvement of NF flux.

335 Pressure membranes are often cleaned when the normalized permeate flux declines by 10

to 15% from the initial stabilized flux.<sup>54,55</sup> On Figure 3, the 10% and 15% permeate drop points

are marked on the trend lines and the associated cumulative normalized volume throughput

338 values are indicated. At the 10% flux decline, ED pretreatment improves the product water yield

by approximately 100% for LAN, 60% for SNOM and FWN, and 400% for LHA. ED

340 pretreatment increases the product water yield, extends the NF operating period, and thereby

341 reduces chemical use.



Figure 3. Normalized permeate flux decline as a function of cumulative normalized volume
throughput in the NOM feed solutions without and with ED pretreatment reveal an increase in
permeate flux and total volume throughput following ED pretreatment: a) Lake Austin NOM
(LAN), b) Suwannee River NOM (SNOM), c) Florida Water NOM (FWN), and Leonardite
Humic Acid (LHA). Smoothing lines are provided to highlight trends.

348

#### 3.3 Increased removal of NOM and cations by ED-NF relative to NF

349 The NF270 membrane is relatively hydrophilic and negatively charged, and has a molecular weight cut-off of 155 Da (Table S2);<sup>56,57</sup> therefore, it impedes some substances from 350 351 passing through the membrane by electrostatic repulsion and rejects substances larger than 155 352 Da by size exclusion. Table 2 presents inorganic ions and organic (i.e., DOC) removal 353 efficiencies achieved by NF without and with ED pretreatment. The removal efficiency of 354 inorganic cations increased after ED pretreatment as a result of fewer inorganic ions in the NF 355 feed solution after ED pretreatment and an increase in the permeate flux in NF experiments 356 following ED pretreatment. Although the differences in NOM removal efficiency between NF 357 experiments without and with ED pretreatment are quite small, these differences were found to 358 be statistically significant (P-value  $\leq 0.05$ ) for LAN, SNOM, and LHA. Moreover, as the NOM 359 fouling layer on the membrane surface continuously builds, the NOM removal efficiency 360 remained fairly consistent throughout NF experiments, suggesting that fouling has little impact 361 on NOM removal efficiency. Regardless, ED pretreatment improves the quality of the product 362 water due to the partial desalination of the NF feedwaters.

Type of NOM LAN **SNOM** FWN LHA Control<sup>\*\*</sup> None ED Pretreatment None ED ED None ED None None 42±2 73±2 47±1 71±4 34±5  $80\pm2$ 46±1  $76\pm4$ 45±2 Ca 70±1 74±2 77±3 45±3 80±3 51±2 74±1 76±2 Removal Mg 62±1 Efficiency\* Na 22±1 43±1  $32 \pm 0.3$  $48\pm2$  $18\pm4$ 56±3 32±1  $56\pm4$ 19±2 (%) 89.9 93.1 92.5 93.9 94.8 95.5 89.9 91.9 DOC N/A  $\pm 0.6$  $\pm 0.8$ ±0.9 ±0.6 ±0.4  $\pm 0.5$  $\pm 3.5$ ±3.3

363 Table 2. Rejection of inorganic cations and NOM by the NF270 membrane without and with ED

364 pretreatment. (Values in table represent % removal in NF treatment)

\*± indicates 95% confidence intervals

\*\*Control experiment were carried out with the synthetic feed water for SNOM and LHA without NOM

#### 365

### **3.4** Investigation of fouling-related benefits of the ED-NF system

### 366 3.4.1 Reduced visual fouling of NF membranes following ED pretreatment

367 Photographic and SEM images of NF membranes before and after fouling experiments 368 are presented in Figure 4. Recall that the NF operation duration was 24 hours for LHA and 144 369 hours for the other three NOMs. NOM fouling is evident for all four NOMs based on the color 370 change from the original white virgin membrane (Figure 4a), and SEM images of fouled 371 membranes confirm that the fouling of the membrane is mainly due to accumulation of NOM 372 rather than mineral scaling (e.g., calcite). The degree of NOM fouling depends on the type and 373 initial concentration of NOM, and the absence/presence of ED pretreatment. Optically, the 374 degree of NOM fouling by LAN is the least among the four NOMs, but NOM aggregates are 375 observed in SEM images (Figure 4, parts b and c). Both photographic and SEM images of 376 SNOM fouled membranes (Figure 4, parts d and e) are similar to LAN except for the notably 377 darker color due to the color of SNOM (Figure S1). Visible differences between the membrane 378 surfaces without and with ED pretreatment for LAN and SNOM are observed with careful 379 examination—more dark area in the membrane surface without ED pretreatment. Although flux decline results for LAN and SNOM (Figure 3, parts a and b) highlight differences in fouling
between the experiments without and with ED pretreatment, visible differences between the
membrane surfaces without and with ED pretreatment for LAN and SNOM are less significant,
suggesting that fouling mechanisms are similar in these experiments (Figure 4, parts b to e).



384

Figure 4. Photographic and SEM images of the virgin NF270 membrane (top) and membranes
fouled by the four NOM sources without (left) and with (right) ED pretreatment show a visual

387 decrease in NOM fouling following ED pretreatment.

388	Visible differences in the NF membrane surfaces between the experiments without and
389	with ED pretreatment are observed for FWN and LHA. The high NOM concentration in FWN
390	promotes additional NOM accumulation on the membrane surface (Figure 4, parts f and g), and
391	these solutions had the second most dramatic flux declines (Figure 3). Additionally,
392	colloids/particles in FWN (observed via nanoparticle tracking analyses, Figure S5) may
393	contribute to fouling via deposition/cake layer formation. Although the operation time for LHA
394	was only 1/6 of that for the other NOMs, the images in Figure 4, parts h and i, clearly
395	demonstrate that LHA caused significant NOM fouling. In fact, cracking of the LHA foulants
396	occurred upon drying due to excessive accumulation of NOM on these membranes. These results
397	explain the dramatic permeate flux declines of LHA (Figure 3d). The higher fouling potential of
398	LHA can be explained by its higher average molecular weight (Figure S4) and its greater
399	hydrophobicity, as it is a soil NOM. <sup>58</sup> The NF270 membrane is a very hydrophilic membrane
400	(i.e., its water contact angle is 27°, Table S2), but it is semi-aromatic polyamide thin-film
401	composite membrane, containing some hydrophobic structure in it, as a result, hydrophobic
402	fractions of the NOM likely sorbed to the membrane. Although high NOM concentration (FWN)
403	and high NOM hydrophobicity (LHA) enhance NOM fouling during NF, both FWN and LHA
404	visibly show significant fouling mitigation after ED pretreatment.
405	Another benefit of the ED pretreatment is the significant reduction in conductivity and
406	ionic strength that was evident in the NF feed waters (Table 1). Variation in ionic strength
407	influences NOM size/shape (e.g., coiling and aggregation), which likely impact the density and

408 compaction of the fouling layers. The lower ionic strengths associated with ED pretreatment may

409 have also contributed to reductions in flux and fouling.

410

### 3.4.2 Elucidation of fouling mechanisms using spectroscopy and scattering

411 To further unravel the important fouling mechanisms that influence the performance of 412 this hybrid ED-NF system, several conventional- and synchrotron-based characterization 413 techniques were employed. The goals of these analyses were to determine the contributions of 414 calcium to NF membrane fouling and to elucidate the mechanisms of NF membrane fouling in 415 the ED-NF system. While magnesium also contributes to NOM fouling of NF membranes 416 (Section 10 of the Supporting Information), calcium was chosen as the model inorganic species 417 for this investigation due to its presence in the feedwaters at higher concentrations than 418 magnesium (Table 1) and the absence of any magnesium signal during preliminary XPS survey 419 scans.

420 Figure 5 presents Ca K-edge TReXS (a) and NEXAFS (b) results of the NF membranes 421 fouled by waters without ED pretreatment; results were similar for the membranes fouled by ED 422 pretreated waters, as shown in Figure S11. TReXS results of the fouled membranes near the Ca K-edge reveal broad scattering features in the q-range 0.2-0.5 Å<sup>-1</sup> (Error! Reference source not 423 424 found.a) that are not present in the virgin NF270 membrane. The broad features in the q-range 0.2-0.5 Å<sup>-1</sup> are specific to the fouling layers and correspond to characteristic length scales, 425  $d=2\pi/q$ , in the range 1.7-2.8 nm. Meanwhile, the feature near 1.2 Å<sup>-1</sup> present in all samples is 426 427 attributed to the so-called amorphous halo that is typically seen for amorphous polymers and it is likely coming from the polysulfone support layer of the NF270 membrane.<sup>59</sup> Scattering at 428 429 energies near an elemental absorption edge enhances the contrast of the absorbed element due to 430 changes in the complex index of refraction such that the spatial distribution of the absorbed 431 element can be probed with greater sensitivity<sup>60</sup>, as highlighted in previous research that 432 employed TReXS near the sulfur K-edge to determine the phase segregation of perfluorinated





434 edge likely correspond to the average spacing between calcium atoms within the fouling layers.

436 Figure 5. (a) TReXS results of NF membranes fouled by the four NOM sources following ED 437 pretreatment and the virgin NF270 membrane near the Ca K-edge reveal distinct scattering 438 features in fouled membranes that represent the spacing of NOM-calcium-NOM and/or NOM-439 calcium-membrane complexes within the fouling layers. (b) Calcium K-edge NEXAFS spectra 440 of membranes fouled by the four NOM sources with ED pretreatment suggest calcium bridging 441 of carboxylate groups as a fouling mechanism, per their agreement with the spectra of calcite and 442 calcium acetate (taken from Guo et al.<sup>62</sup>). The results are similar regardless of ED pretreatment, 443 see Section 13 of the Supporting Information.

The characteristic length scales of calcium in the fouling layers obtained from Ca K-edge TReXS (1.7-2.8 nm) are similar to the estimated NOM molecule sizes per size exclusion chromatography results (1.2–2.6 nm, Table S3). Although the distribution of interacting functional groups varies as a function of NOM source/composition, the general agreement

448 between length scales obtained from the two techniques suggests that interactions between 449 calcium and NOM contribute to fouling of the NF membranes. The FWN-fouled membranes 450 exhibit a more intense scattering peak centered at lower q compared to the other samples, 451 suggesting a greater number of scatterers (i.e., more calcium atoms) and a larger characteristic 452 length (i.e., more spacing between calcium atoms) in FWN fouling layers relative to other 453 samples. The increased amount of calcium in the FWN fouling layers may be due in part to the 454 higher NOM and calcium concentrations in the FWN feedwater, which led to increased 455 incorporation of calcium in FWN fouling layers relative to the other samples. The larger 456 characteristic length in FWN fouling layers is attributed to the high molecular weight fraction of 457 FWN observed in size exclusion chromatography (Figure S4), which likely consists of 458 macromolecules and/or polysaccharides with larger spacing of interacting functional groups 459 relative to low molecular weight NOM fractions.

460 The Ca K-edge TReXS results indicate contributions of interactions between calcium, 461 NOM, and membrane surfaces to NF fouling, so further spectroscopic investigation aimed to 462 determine the mechanisms by which fouling occurs during NF. Ca K-edge NEXAFS spectra of 463 the fouled membranes reveal a similar local chemical bonding environment around calcium 464 among the samples (i.e., all NOM sources, with and without ED pretreatment) that is consistent 465 with the spectrum of calcium acetate, a surrogate compound to represent calcium bridging of two carboxylate groups (Error! Reference source not found.b).<sup>63,64</sup> The agreement in these spectra 466 467 to that of calcium acetate indicates that calcium bridging of carboxylate groups is the primary 468 mechanism by which calcium interacted with NOM and the membrane surface during NF 469 fouling experiments. ATR-FTIR spectra (Figure S7) and C 1s XPS spectra (Figure S8) of fouled 470 membranes confirm the presence of carboxyl groups in the fouling layers, in agreement with

previous studies on NOM fouling of NF membranes.<sup>19</sup> SEM images (Figure 4) and Ca K-edge
NEXAFS (Figure 5b) show no signs of calcite scaling, ruling out this fouling mechanism in the
current study.

474 Surface-sensitive Ca 2p XPS results (Figure S9) suggest a decrease in the amount of 475 calcium in the top-most surface region of fouling layers formed during experiments with ED 476 pretreatment relative to experiments without ED pretreatment for all four NOM sources. The 477 XPS spectra predominantly captured NOM-Ca-NOM interactions due to the low penetration 478 depth (<10 nm) of XPS measurements. Meanwhile, Ca K-edge jump ratios based on NEXAFS 479 spectroscopy (Section 13 of the Supporting Information), which have been proposed by Osawa<sup>65</sup> 480 to represent the relative amount of an element in a homogeneous material, are similar between 481 NF experiments without and with ED pretreatment; differences range from 1.0 percent for 482 SNOM to 6.8 percent for FWN. Given that the thickness of the fouling layers without and with 483 ED are similar for a given NOM (Table S4) and the NEXAFS measurements fully probed the 484 fouling layers, the similarity in the Ca K-edge jump ratios suggests that similar amounts of Ca 485 were present throughout the entire fouling layer thickness without and with ED pretreatment. 486 Perhaps, the increased depth penetration in NEXAFS compared to XPS captured both the NOM-487 Ca-membrane interactions as well as the NOM-Ca-NOM interactions. Taken together with the 488 XPS data, which shows a decrease in Ca in the top surface of the fouling layer with ED 489 pretreatment, it is possible that a gradient in calcium concentration developed in the fouling layer 490 with ED pretreatment. The gradient of calcium in the fouling layers could be due to 491 concentration polarization, among other factors. 492 The conventional ATR-FTIR and XPS and synchrotron TReXS and NEXAFS results all suggest 493 the importance of Ca-bridging as a major NF fouling mechanism associated with all of the

494 NOMs regardless of pretreatment. However, additional contributions to fouling from other 495 mechanisms (e.g., hydrophobic interactions, mineral scaling) also influence the performance of a 496 hybrid ED-NF system. For instance, LHA-fouled membranes exhibit peaks characteristic of soil 497 NOM fractions such as aromatic C=C stretching (Figure S7), suggesting that hydrophobic 498 interactions between LHA and the membrane surface significantly contributed to fouling by this 499 NOM. In this study, the inclusion of the Ca-specific synchrotron data highlighted the ability to 500 identify Ca-carboxylate length scales within the fouling layers. The NEXAFS results allowed 501 identification of Ca-bridging to carboxylate groups at greater depth penetration than XPS, 502 thereby providing additional insight into interactions, including those at the membrane-fouling 503 layer interface. While synchrotron techniques have previously been employed to study calcium bridging of organic matter and mineral surfaces,<sup>66</sup> this work is among the first to apply these 504 505 tools, especially resonant X-ray scattering, to describe membrane fouling, thus opening the door for future work in this space.<sup>67,68</sup> In particular, a complementary synchrotron investigation at the 506 507 Mg K-edge would be insightful regarding the specific interactions between divalent cations and 508 NOM that influence membrane fouling.

### 509

### 4 Engineering Applications for the ED-NF system

The two major advantages of the hybrid ED-NF system are the greater productivity of an NF system and the potential to reduce DBP formation. The two raw waters from actual treatment plants in Texas and Florida were put through the hybrid ED-NF system. For the TWN, ED was operated at 80% recovery and 80% conductivity reduction, and the diluate was then applied to the NF stage. The entire volume of the ED concentrate (20% of the original water) was then mixed with the NF permeate; the water recovery from this system is intrinsically greater than with NF alone because of the greater volume throughput prior to the need for membrane cleaning (as shown in Figure 3) and the use of the entire ED concentrate. The trihalomethane formation potential (THMFP) of TWN of this mixture was  $76\pm 3 \mu g/L$ , just below 80.0  $\mu g/L$ , the Maximum Contaminant Level (MCL) of total THMs regulated by US EPA.<sup>69</sup> The THMFP of TWN after treatment by the existing enhanced coagulation process was  $150\pm 3 \mu g/L$ , far

521 exceeding the MCL.

522 The Florida water, with its much higher concentrations of inorganic ions and NOM, is 523 more complicated. With 80% recovery and 80% conductivity reduction in ED, mixing the full 524 ED concentrate with the NF permeate would not yield sufficient NOM reduction because the ED 525 concentrate has the original NOM concentration. Even using only half of the concentrate yielded 526 a THMFP of  $112\pm10 \,\mu$ g/L, well in excess of the MCL; the results are shown as Case I (with 527 50% ED concentrate) in Error! Reference source not found.. However, a major advantage of 528 the proposed hybrid system is that it affords far greater flexibility in achieving treatment goals. A 529 lower DOC and resulting THMFP could be achieved in this hybrid ED-NF system in three 530 different ways, either singly or in combination: reducing the percent of ED concentrate in the 531 final blend, achieving higher ED recovery, or choosing a different NF membrane. The latter 532 would likely change removal efficiencies of all constituents as well as the NF water recovery. 533 Our experimentation did not include investigating all of these possibilities, but combining 534 results we did investigate with reasonable assumptions leads to the values shown in Case II in 535 Error! Reference source not found.. The primary difference from Case I is the higher recovery 536 from the ED process (90% rather than 80%). Using the measured DOC and TTHMFP values and 537 assuming that the TTHMFP is proportional to the DOC<sup>70</sup> resulted in the determination that the 538 final DOC after blending the NF permeate and a fraction of the ED concentrate needed to be  $\leq$ 539 1.7 mg/L to achieve a TTHMFP value below 80 µg/L. For Case I with 80% ED recovery, that

540	value could be achieved by blending 25% of the ED concentrate with the NF permeate, thereby
541	achieving an estimated 77% overall recovery; in Error! Reference source not found., these
542	results are shown in the far-right column for Case I. For Case II with 90% ED recovery, the
543	maximum DOC of 1.7 mg/L could be achieved by blending 55% of the ED concentrate with the
544	NF permeate, achieving an estimated 87% overall recovery; this result is shown on the far right
545	of Case II in Error! Reference source not found This recovery exceeds the estimated 80%
546	recovery if NF was used as the sole treatment; although the DOC and THM values would be
547	higher with the hybrid ED-NF process, the water would comply with DBP regulations, the
548	recovery would be greater, and the need for NF cleaning would be reduced. More generally, the
549	hybrid ED-NF system would need to be optimized for specific waters and applications, but this
550	example showcases its potential for achieving treatment goals with high water recovery for
551	challenging waters.



### 552

Figure 6. The product water quality control examples of FWN in the ED-NF system. Water quality calculations are based on ED experimental results in Figure 2 and NF experimental results in Figure 3 and Table 2. We assume that no DOC mass loss occurs at the ED concentrate stream in this calculation and that TTHMFP is proportional to DOC.

### 557 **5** Conclusions

558 This study evaluated a hybrid ED-NF membrane system to treat freshwater with

559 moderate to high hardness and NOM concentrations. Compared to NF alone, the hybrid ED-NF

- 560 system provides increased product water yield, increased removal of inorganic cations and NOM
- 561 by NF, and reduced NF membrane fouling. Furthermore, some or all of the ED concentrate,
- 562 which contains most of the original ions, can be added to the NF permeate as an efficient means
- 563 of remineralization. ED pretreatment shows excellent ion separation and minimal NOM

564 separation, but natural waters with hydrophobic NOM and high NOM and calcium 565 concentrations require additional efforts to prevent NOM adsorption to the IEMs in the ED 566 concentrate. A reduction of NOM fouling on the NF membrane after ED pretreatment was 567 observed in all tested NOM sources, and that reduction is primarily caused by the lowered ionic 568 strength and, particularly, the lowered divalent cation concentration. Spectroscopic and resonant 569 scattering measurements near the calcium K-edge confirm a significant contribution of calcium-570 carboxyl interactions to fouling during NF, and the fouling mechanisms were similar among 571 several NOM sources without and with ED pretreatment.

572 The water produced from the hybrid ED-NF system would offer greater protection 573 against health issues associated with DBP formation (resulting from the interaction of NOM and 574 chlorine-based disinfectants). But, the amount of ED concentrate for remineralization should be 575 carefully determined to avoid excessive DBP formation and, perhaps, minimize the presence of 576 other toxic components. The hybrid ED-NF system is a promising treatment option, with a niche 577 in the drinking water industry for treating waters with moderate to high hardness and NOM 578 concentrations in their supply. The hybrid system would be worthwhile if the increased water 579 production by NF, extended NF membrane lifetime, reduced chemical use for the membrane 580 cleaning, and substituted remineralization process by ED concentrate stream offset the cost of an 581 ED system. Moreover, the operational flexibility that allows the operator to control the final 582 water TDS and DOC concentration is a major advantage of the hybrid system. This hybrid ED-583 NF system with its operational flexibility could also be applied to other water sources with 584 charged inorganic ions and neutral charge constituents that synergistically impact fouling of NF 585 membranes.

### 586 Supporting Information

587 The Supporting Information is available free of charge at https://pubs.acs.org/doi/XXXX.

• Details on preparation of natural organic matter and synthetic feed waters (Section 1 and

- 589 2); two fresh water quality data (Section 3); ED and NF experimental methods (Section 4
- and 5); the Specific Energy Consumption Calculation at the ED process (Section 6);
- 591 properties of NF270 membrane (Section 7); normalized permeate water flux calculation
- 592 (Section 8); details on source water characterization using HP-SEC and nanoparticle
- 593 tracking analyses and results (Section 9); impact of different cations on NF membrane
- 594 NOM fouling (Section 10); and details on ATR-FTIR, XPS, Synchrotron techniques and
- 595 further discussion of results (Section 11 to 13) (PDF)

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