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PROCESSING OF SODIUM-POTASSIUM
NIOBATE CERAMICS

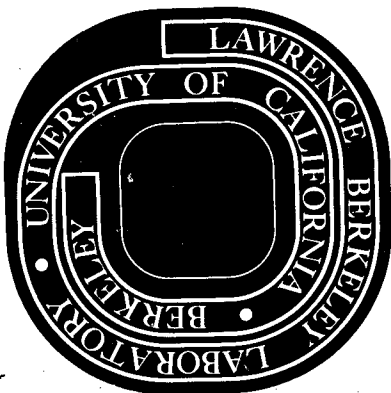
Bob R. Powell, Jr.
(M. S. Thesis)

December 2, 1971

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LBL-413

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	<u>Index</u>	<u>Page</u>
ABSTRACT		v
I. INTRODUCTION		1
II. EXPERIMENTAL		6
A. Preparation of Powders for Calcining		6
B. Calcining and the Reaction Studies		9
C. Sintering Studies		14
III. RESULTS AND DISCUSSION		17
A. Calcining Reactions		17
B. Sintering Phenomenon		24
IV. CONCLUSION		35
ACKNOWLEDGMENTS		36
REFERENCES		37

PROCESSING OF SODIUM-POTASSIUM NIOBATE CERAMICS

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Berkeley, California 94720

ABSTRACT

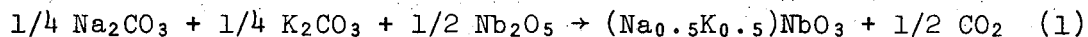
Sintering studies of undoped $(\text{Na}_{0.5}\text{K}_{0.5})\text{NbO}_3$ and the same material doped with 1/2, 1, 2, and 4 mole percent BaO and 2 mole % B_2O_3 were made. The persistence of a second phase after calcining to form the compound led to a study of reactions occurring during calcination.

The calcining of sodium-potassium niobates involves the formation of an intermediate compound (the second phase) and its subsequent reaction with sodium oxide and potassium oxide to form $(\text{Na}_{0.5}\text{K}_{0.5})\text{NbO}_3$. Sintering data show that up to 1/2 mole % BaO added to the system increases the initial densification. However, the sintered bodies then exhibit densification and form sharp cubic grains and large voids. Indications are that a liquid phase is the major contributor to densification of this system through the mechanism of particle rearrangement, and that the contribution of any sintering mechanism to densification is negligible.

I. INTRODUCTION

Sodium-potassium niobate (henceforth referred to as NKN) is a perovskite ferroelectric ceramic that has found extensive use in the production of ultrasonic delay lines.¹ NKN is the name given to the solid solution having equal mole percents of sodium niobate and potassium niobate. Sodium niobate and potassium niobate form a complete solid solution series having a low dielectric constant. At the equal mole percent composition the electromechanical coupling coefficient is a maximum, 0.34 to 0.39 at room temperature.² It is the low dielectric constant that makes NKN particularly useful in "high" frequency applications while it is the high coupling coefficient that is necessary for transducers.

Obtaining pure, high density NKN, is usually accomplished by hot-pressing.³ NKN is produced when raw materials are calcined to bring about the following reaction:



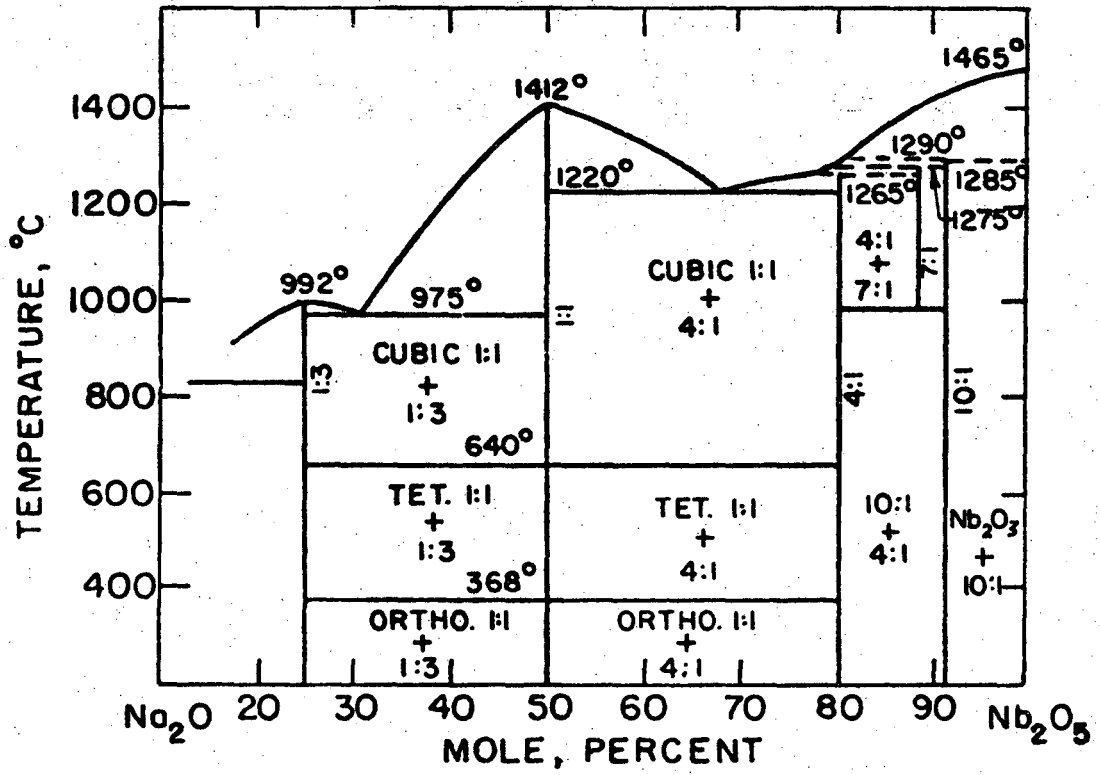
However, it is important to note that the common practice for preparing the above batch for calcining is to add small amounts (up to 2 mole %) excess of each carbonate. Egerton and Dillon² added 0.1 mole % excess while Stanek⁴ added 1.5 mole % excess of each carbonate. Stanek explained that this was done to eliminate the formation of a second phase, $(\text{NaK})\text{Nb}_9\text{O}_{21}$ which formed during calcination of the stoichiometrically mixed materials. Stanek also tried nitrates as starting materials and found that the second phase could be eliminated by adding 1.3 mole %

excess of each nitrate.

Nitrates have the advantage over carbonates of decomposing at lower temperatures, about 400°C for sodium nitrate and potassium nitrate as compared to about 870°C for the respective carbonates. In addition, the nitrates are very soluble in water and as a result, liquid-solid mixing can be used if an evaporation technique is used to remove the water. Also, the degree of mixing is less critical for the nitrates because they melt eutectically at 224°C⁵ to form a viscous liquid which should coat all the niobium pentoxide particles.

Calcining results in Stannek's work and this study for nitrate-prepared NKN showed a second phase. The concentration of the second phase increased toward the interior of a calcined compact of the mixed oxides. The reactions occurring during calcination are unknown, so a study was undertaken to determine them. Little is actually known of the structure of the sodium-potassium niobate compounds. Stannek⁴ indexed the pattern for pure NKN but X-ray patterns for other compounds in the sodium oxide-potassium oxide-niobium pentoxide phase diagrams have to be determined from the X-ray patterns of the single alkali oxide-niobium pentoxide compounds. Of these, the system Na₂O-Nb₂O₅ has been studied extensively^{6,7} and for this reason the calcining reactions in this system were studied. The effects of solid solution of potassium into the system should not change the reactions. The Na₂O-Nb₂O₅ phase diagram as determined by Shafer and Roy⁶ is shown in Fig. 1.

The complete (NaK)O-Nb₂O₅ phase diagram has not been determined, but from the data of Reisman and Banks,⁸ Shafer and Roy,⁶ and Reisman and Holtzberg,⁹ an approximate phase diagram for the system in the



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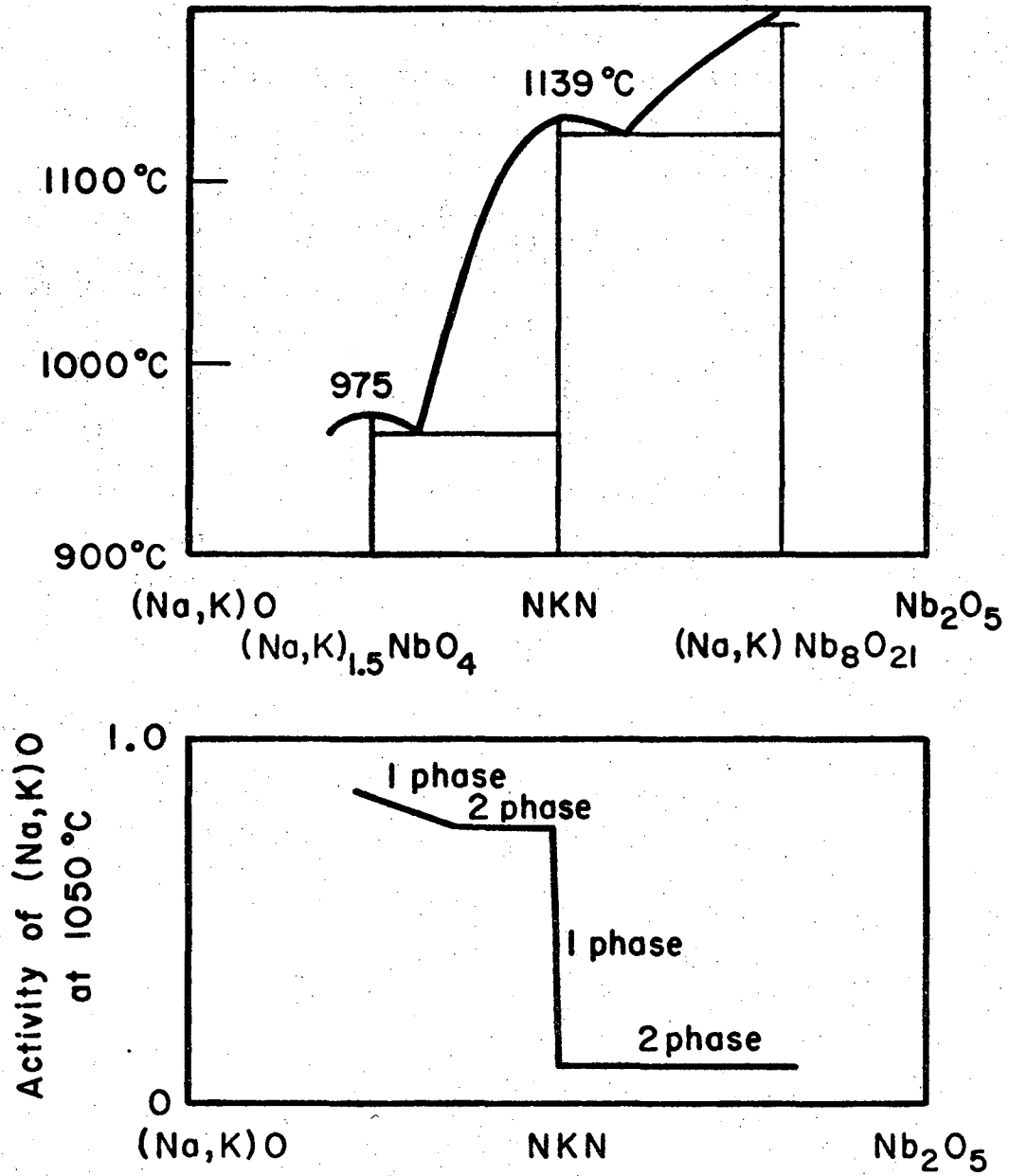
Fig. 1. Phase diagrams of the system Na₂O-Nb₂O₅ (Ref. 6).

region of interest was extrapolated, and is shown in Fig. 2. From the diagram it is clear that a small deviation from stoichiometry causes a large change in the alkali metal oxide activity. This is shown schematically in Fig. 2.

Sintering of NKN is difficult. To date, all industrially produced NKN is hot-pressed.^{10,11} Conventional sintering is the most economic method because it requires less elaborate equipment and is more applicable to producing large volumes of material. For NKN it has not been possible to obtain high density samples using conventional sintering. Stannek⁴ tried varying the parameters of sintering and was able to reach 94% of theoretical density. He varied atmosphere, time, temperature and tried doping NKN with varying amounts of BaO. In some cases de-densification was noted.

BaO was added as a dopant to reduce grain growth. The atmosphere also had a significant effect. Stannek's optimum sintering curves were obtained with 0.5 mole percent BaO at 1100°C in an oxygen atmosphere and a packing powder having excess Nb₂O₅ (low alkali activity). This was for material prepared from nitrates of sodium and potassium.

It was the purpose of this work to continue the study of the processing steps leading to pure nitrate prepared NKN and the sintering of it.



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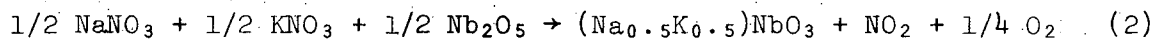
Fig. 2. Approximate phase diagram for the system (NaK)O-Nb₂O₅ with schematic of alkali activity.

II. EXPERIMENTAL

A. Preparation of Powders for Calcining

The nitrate compounds used were supplied by J. T. Baker Chemical Company while the niobium pentoxide came from Atomergic Chemetals Company. The impurity of each nitrate compound is shown in Table I.

The powder preparation method used was dry mixing. Before weighing, the materials were kept in a dryer for 50 hours. NKN was made in one mole batches according to the reaction:

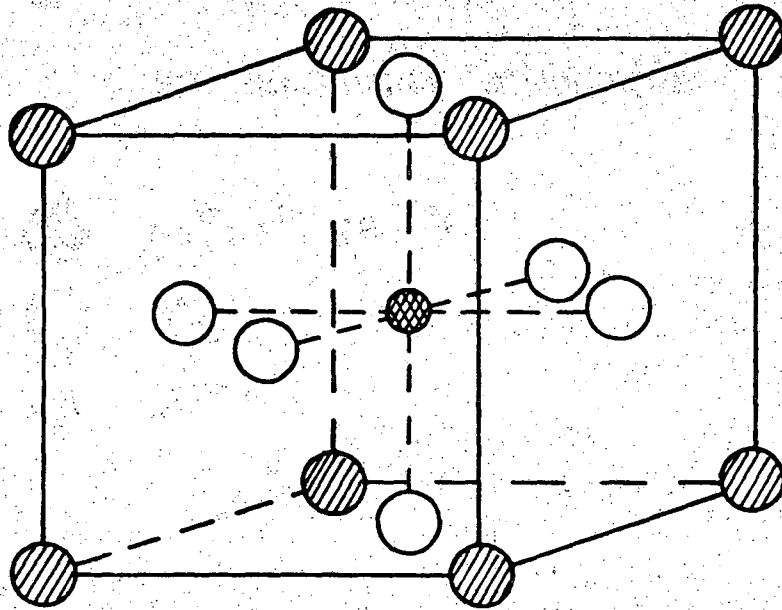


Mixing was done in a polyethylene container with teflon media. Mixing time was 24 hours. Next, the mixed powders were fired in air for 20 hours at 450°C to eliminate organic impurities picked up during processing. This created a liquid phase which caused the particles to agglomerate. Further grinding was not needed because the liquid phase reformed during calcining and intimate contact between nitrate and Nb₂O₅ particles was maintained.




To produce doped NKN for sintering, Ba(NO₃)₂ was used. From ionic radii data it is believed that Ba⁺² substitutes for either Na⁺ or K⁺ in the perovskite lattice, the A-sites (see Fig. 3). For each Ba⁺² ion that is substituted, a vacancy of either Na⁺ or K⁺ occurs. The reaction for producing 1.0 mole % BaO doped NKN is:

Table I. Impurity levels in nitrate compounds

	KNO ₃ Baker's reagent grade 99.9 wt%	NaNO ₃ Baker's reagent grade 99.6 wt%	Ba(NO ₃) ₂ Baker's reagent grade 99.9 wt%
Cl	0.002	0.001	0.001
IO ₃	<0.0005	<0.0005	-
NO ₂	<0.001	<0.001	-
PO ₄	0.0001	0.0002	-
SO ₄	0.0005	0.001	-
Ca, Mg	0.005	0.002	0.04
Heavy metals	0.0002	0.0002	0.0001
Fe	0.0001	0.0001	0.00005
Na	0.003	-	-
K	-	0.004	-
Sv	-	-	0.5

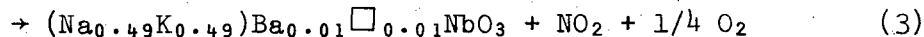
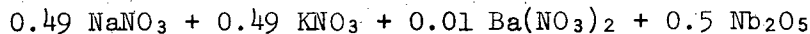


CUBIC PEROVSKITE STRUCTURE

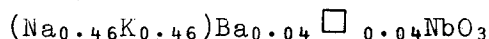
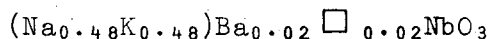
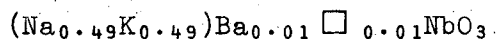
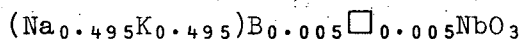
- A  Na⁺, K⁺, (Ba²⁺)
- O  O²⁻
- B  Nb⁵⁺

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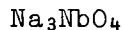
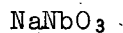
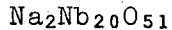
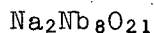
Fig. 3. Unit cell structure of perovskite (Na_{0.5}K_{0.5})NbO₃.



One-tenth mole doped batches of NKN were made for:



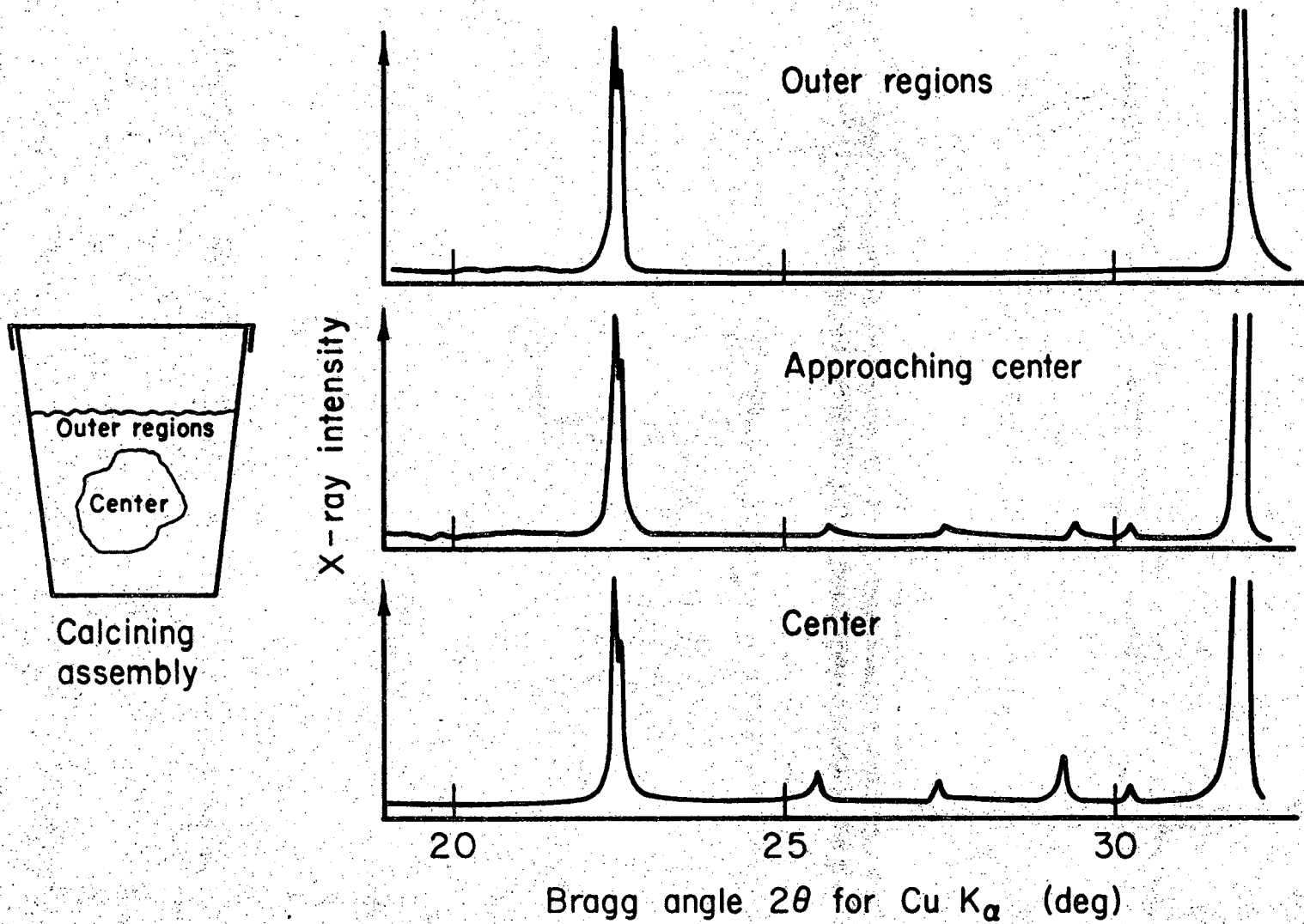
Mixtures of NaNO_3 and Nb_2O_5 were produced to yield compounds of:



B. Calcining and the Reaction Studies

Calcining was done in air and oxygen at 850°C for two hours. This time and temperature was selected because Stanek⁴ found it to be optimum for his carbonates. Crystal phases in the fired powder was checked using X-ray diffraction analysis.

For the first calcining runs, small amounts of NKN were loosely placed in the bottom of a covered platinum crucible. The results of X-ray analysis showed single phase NKN. Later larger quantities of powder and cold pressed one inch diameter, one inch high pellets were calcined. The results for the powder are shown in Fig. 4. The concentration of the second phase increased as the interior of the system was



-10-

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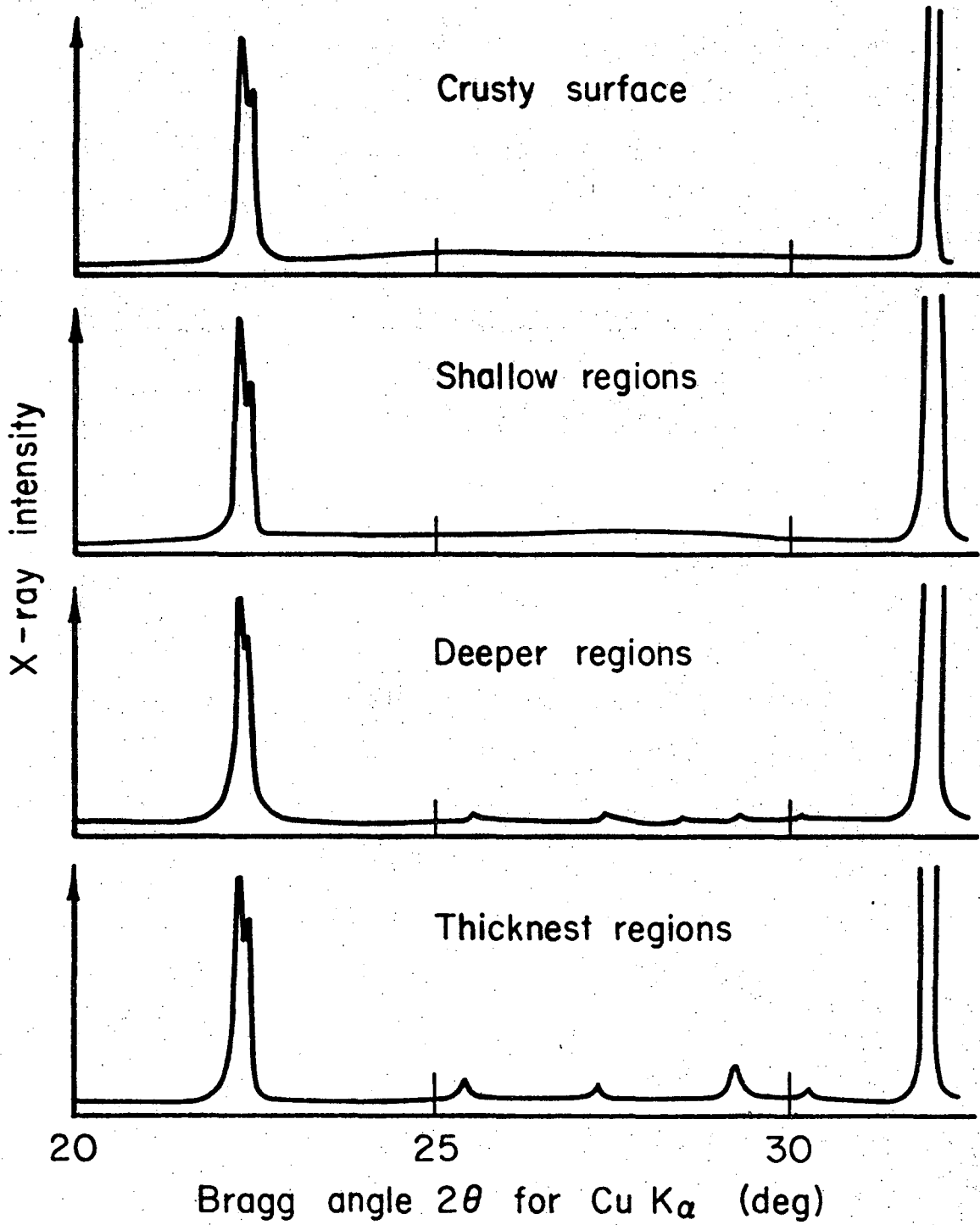
Fig. 4. X-ray patterns showing concentration gradient of second phase, $(\text{NaK})\text{Nb}_6\text{O}_{21}$, in NKN in calcining compact.

approached with the pressed pellet showing an even greater gradient. The X-ray patterns are included in the figure to show this gradient. To eliminate this second phase, mixtures with varying amounts (up to 2 mole %) of excess nitrates were calcined. The second phase was still present.

Because the interior of the calcining compact contained the second phase, calcining in thin sections to allow for gas escape was tried, assuming the gas reaction product inhibited the reaction. In order to obtain more material per firing, plates of fused silica were used. The plates were six inches square and were used to support platinum foil on which thin coatings of the mixed oxides were placed forming a shallow bed. The results of this method of calcining are shown in Fig. 5. Again, as the depth of the material increased, the second phase concentration increased. Also, the single phase material was crusty and hard and appeared to have formed from a melt, while the two-phase sections were unagglomerated and easily crushed.

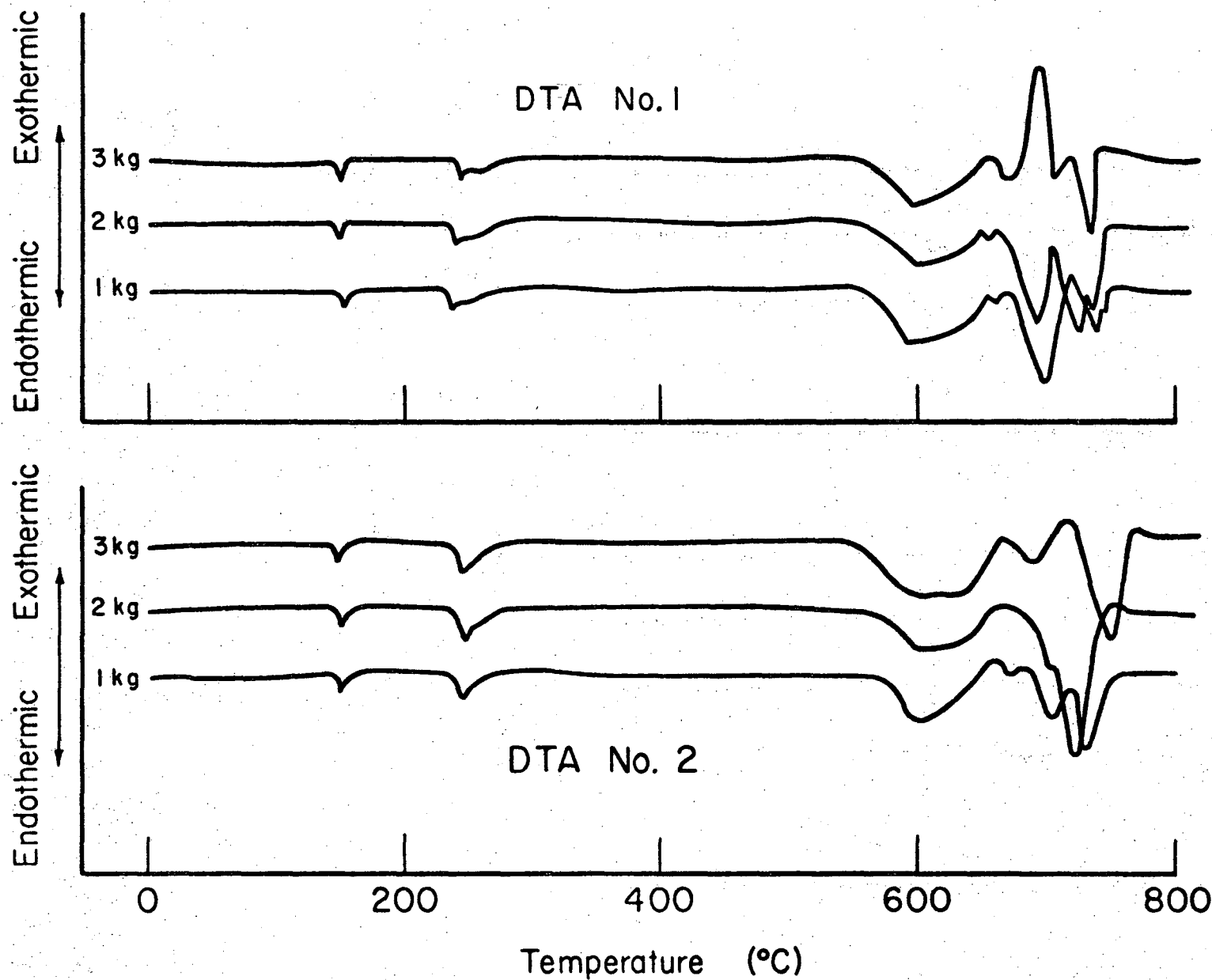
To better understand the calcining reactions, two thermogravimetric analyses were run on the dry mixed materials at heating rates of $2\ 1/2^{\circ}\text{C}$ and 12°C per minute. The results showed that only one major loss of weight occurred which coincided with the decomposition of the nitrates and was quantitatively predictable according to Eq. (2). The data also showed that at the slow heating rate, the decomposition was complete at about 700°C , compared to 830°C for the faster heating rate.

Differential thermal analyses of the mixed powders were also done. The results are shown in Fig. 6. It is evident from the data that the degree of packing of the powder before calcining has a marked effect on the reaction. At 690°C an endothermic and exothermic reaction take



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Fig. 5. X-ray patterns showing concentration gradient of second phase, $(\text{NaK})\text{Nb}_8\text{O}_{21}$ in NKN for tray firing assembly.



-13-

Fig. 6. Differential thermal analysis curves for reactions during calcination of mixed oxides with compacting pressure at the left for each sample.

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place. Loose packing favors the endothermic reaction while tight packing shows an exothermic reaction.

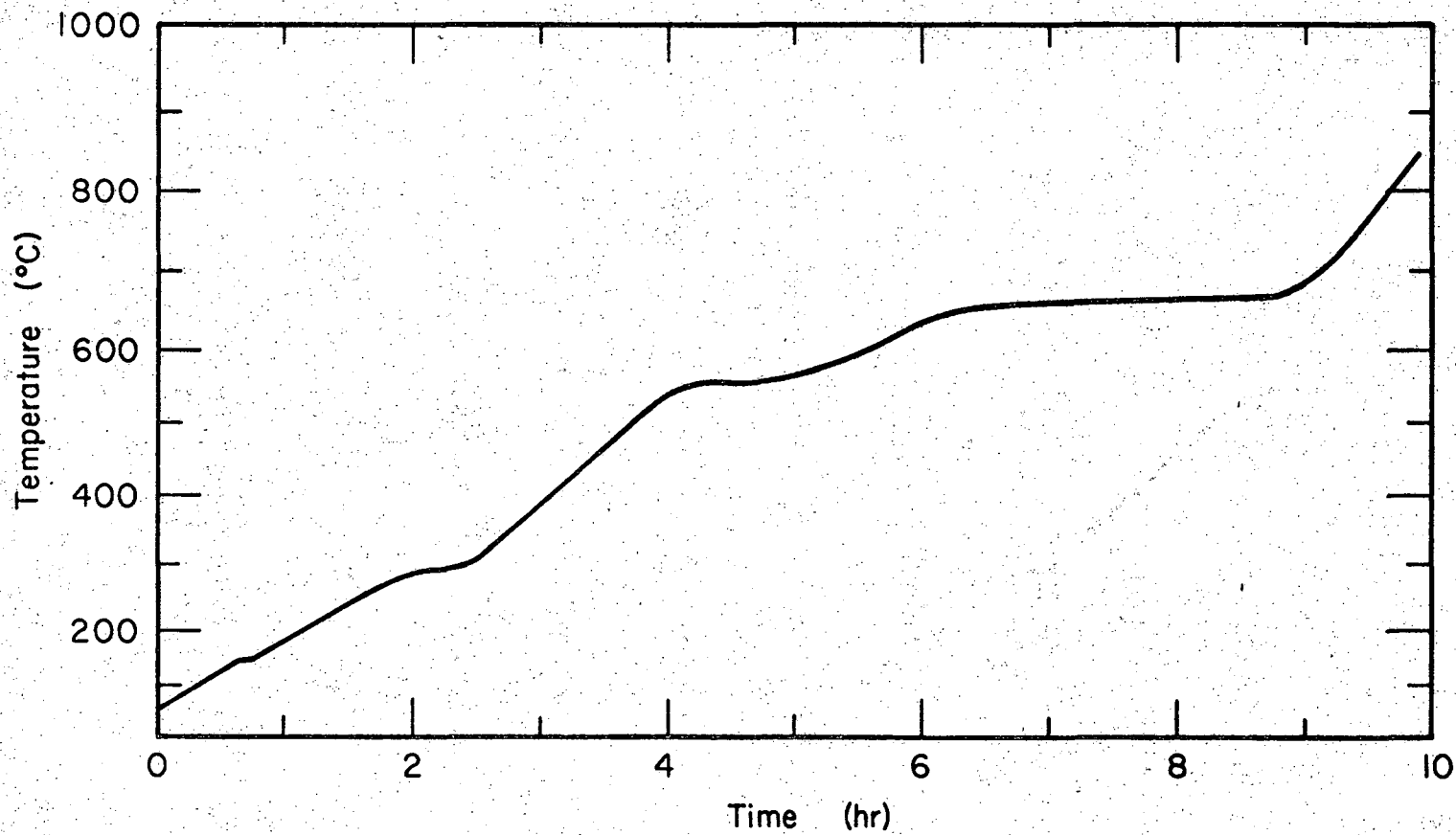
An additional experiment done was a gradient firing experiment.¹² The gradient firing experiment was done in a furnace designed to keep the temperature gradient between the center and exterior of the sample constant. For example, for an endothermic reaction, the heating rate is slowed down until the reaction is completed. The gradient firing data is shown in Fig. 7. When the decision to study the NaNbO_3 system was made, the calcining experiments, the DTA studies, and the thermogravimetric analyses had already been done on the NKN materials. The gradient firing experiment served to show that the reactions occurring in the NaNbO_3 and the NKN systems are analogous.

C. Sintering Studies

Each of the different batches of calcined single phase NKN, doped and undoped, was ground for 50 hours in a polyethylene container with teflon media to reduce particle size. This was followed by air firing at 450°C for 20 hours. Next the powder was passed through a 325 mesh screen and average particle size of 4.2 microns was determined using the "Fisher Sub Sieve Sizer."

The powder agglomerated easily so that no binding agent was needed in cold pressing. One-half inch diameter by one-eighth inch high pellets were cold pressed at 40,000 psi. Density determinations were made by two methods, mass volume measurements and mercury immersion. Green densities ranged from 63% to 72% of theoretical density.

The pellets were sintered in a covered platinum crucible with an oxygen pressure of one atmosphere. They were surrounded by packing



-15-

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Fig. 7. Thermal gradient analysis of mixed oxides during calcining to form NaNbO_3 .

powder containing 3 mole % excess Nb_2O_5 to keep the system on the high niobium side of the phase diagram.

Sintering was done in a kanthal wound furnace that was designed for loading and quenching from the hot zone in less than 10 seconds. Before insertion into the hot zone, the loaded crucible was evacuated in a dessicator and then filled with oxygen gas. After each insertion into the hot zone, 30 minutes were allowed for the specimens to reach the sintering temperature.

Fracture surfaces of pellets coated with a thin platinum-palladium layer to prevent charging were observed with the scanning electron microscope to study their microstructure.

Also, one sample of 44×37 micron sized NKN, undoped and in a hand pressed pellet was sintered in the hot-stage of the microscope. Photos were taken at 100° to 150° intervals up to 1100°C .

X-ray diffraction patterns were determined for the sintered pellets showing that they were still single phase NKN.

III. RESULTS AND DISCUSSION

A. Calcining Reactions

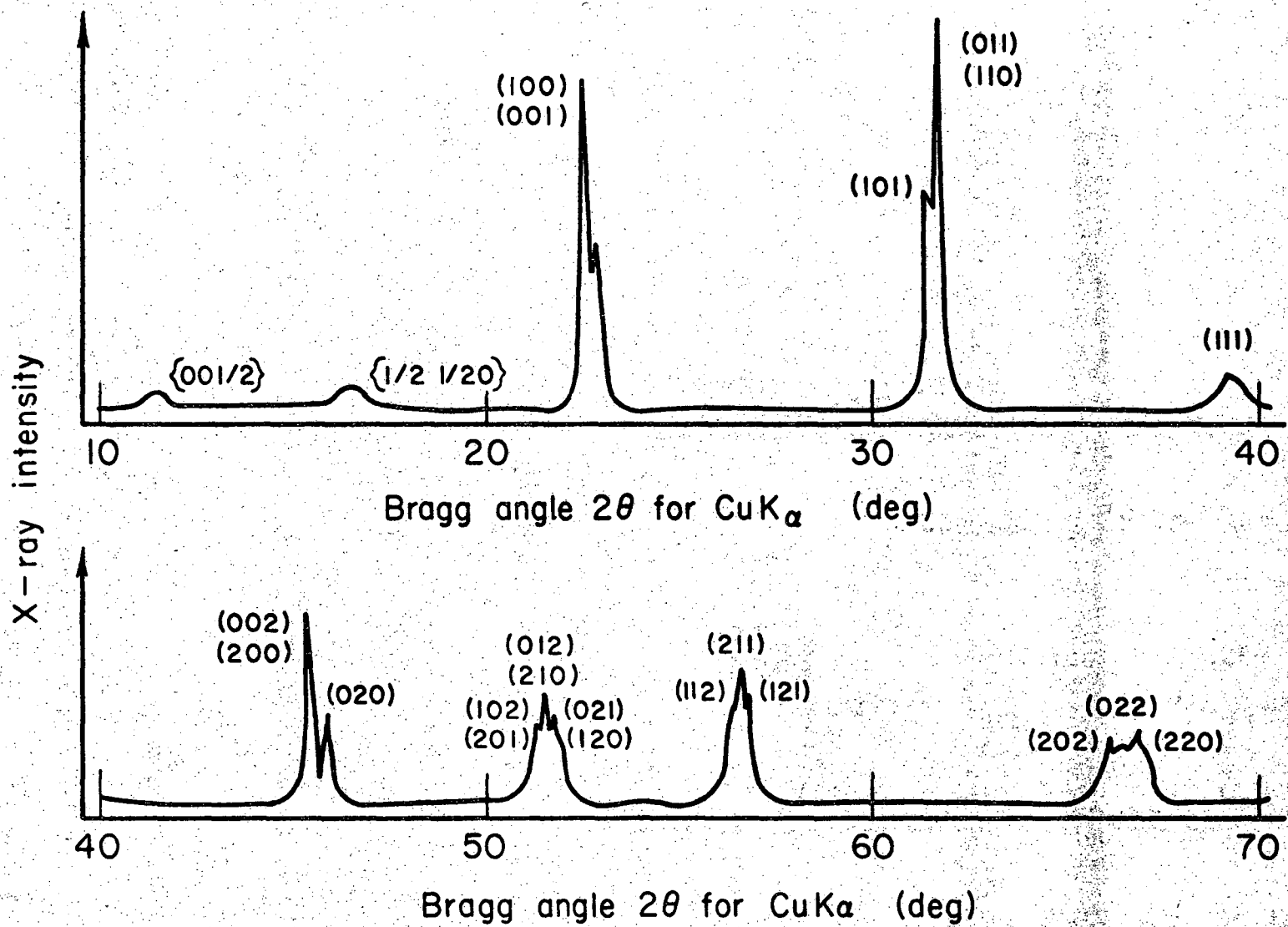
The X-ray diffraction pattern for pure single phase NKN as indexed by Stannek⁴ is shown in Fig. 8. Added to the pattern, however, are two broad peaks at Bragg angles of about 11.2 and 15.8. These peaks were calculated to be caused by diffraction from the multiple cell planes $\{00\ 1/2\}$ and $\{1/2\ 1/20\}$ respectively. This seems reasonable because both end members of the solid solution, NaNbO_3 and KNbO_3 exhibit this multiple cell diffraction phenomenon as shown by E. A. Wood.¹³

Concerning the reactions occurring during the calcining of NKN, it is less complicated to study the NaNbO_3 system for phase identification. Pure NaNbO_3 is shown in Fig. 9, along with a typical calcined specimen broken down into various regions. Note the increasing concentration of the second phase and how similar the gradient is to that of NKN in Fig. 4.

In Fig. 10 the X-ray diffraction pattern of NaNbO_3 with a high concentration of the second phase is shown. Also shown is the pattern for $\text{Na}_2\text{Nb}_8\text{O}_{21}$. It is evident that $\text{Na}_2\text{Nb}_8\text{O}_{21}$ is the second phase present.

Based on the X-ray patterns taken at various temperatures and the DTA patterns, a possible reaction series has been postulated.

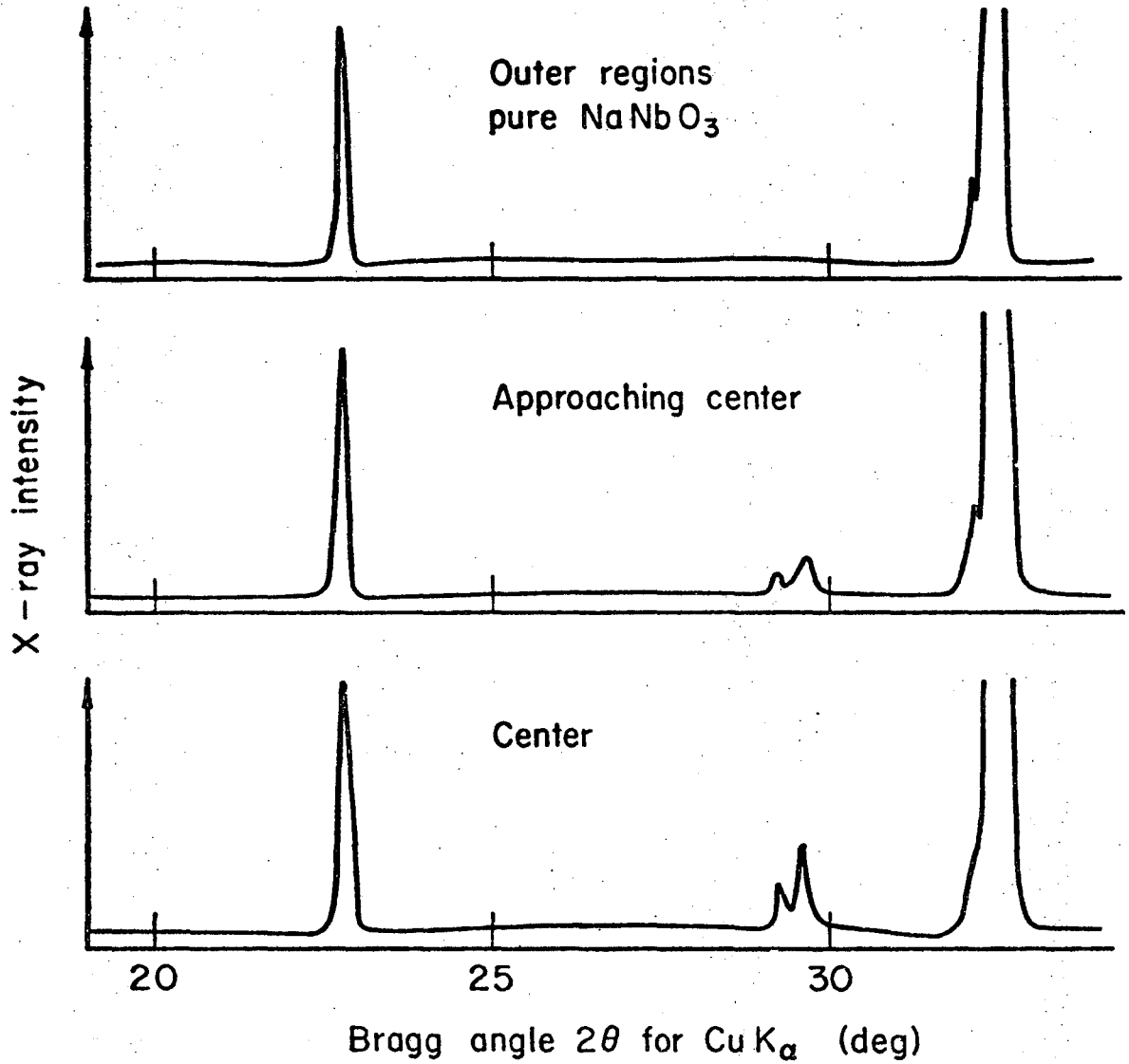
The following is the reaction series. At about 150°C the moisture in the powder evaporates and the system remains unchanged until 240°C when the nitrate compounds melt. As 600°C is approached, the nitrates and Nb_2O_5 start reacting endothermically to form $\text{Na}_2\text{Nb}_8\text{O}_{21}$ for the NaNbO_3 - Nb_2O_5 system and $(\text{NaK})\text{Nb}_8\text{O}_{21}$ for the ternary system. The temperature of this reaction is lower in the gradient run because only NaNbO_3 is present but the order and magnitude of the peaks are the same as the



-18-

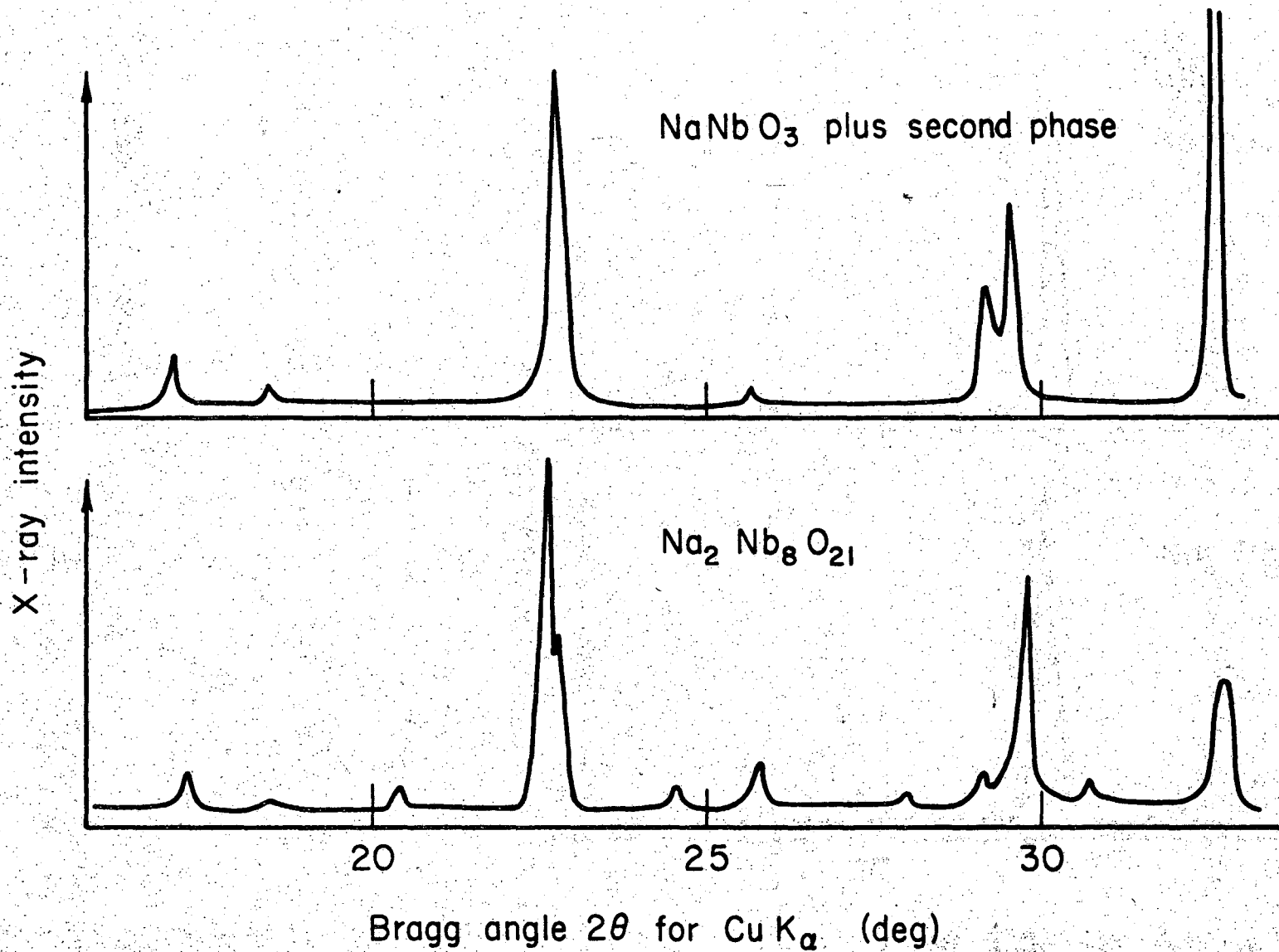
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Fig. 8. Indexed X-ray pattern for $(\text{Na}_{0.5}\text{K}_{0.5})\text{NbO}_3$.



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Fig. 9. X-ray patterns showing concentration gradient of second phase, $\text{Na}_2\text{Nb}_8\text{O}_{21}$, in NaNbO_3 for a calcined compact.



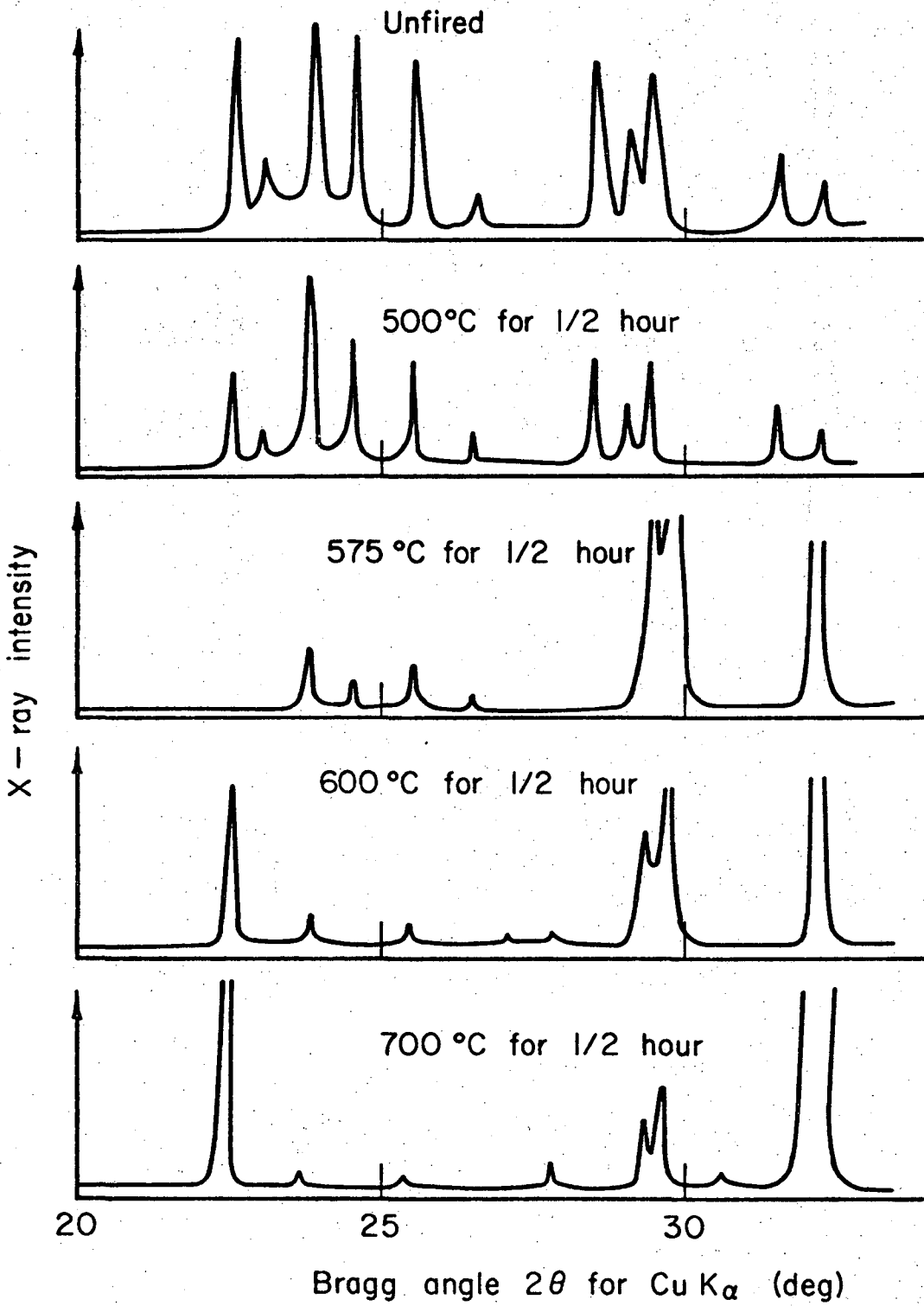
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Figure 10. X-ray patterns for NaNbO_3 (containing second phase) and $\text{Na}_2\text{Nb}_8\text{O}_{21}$.

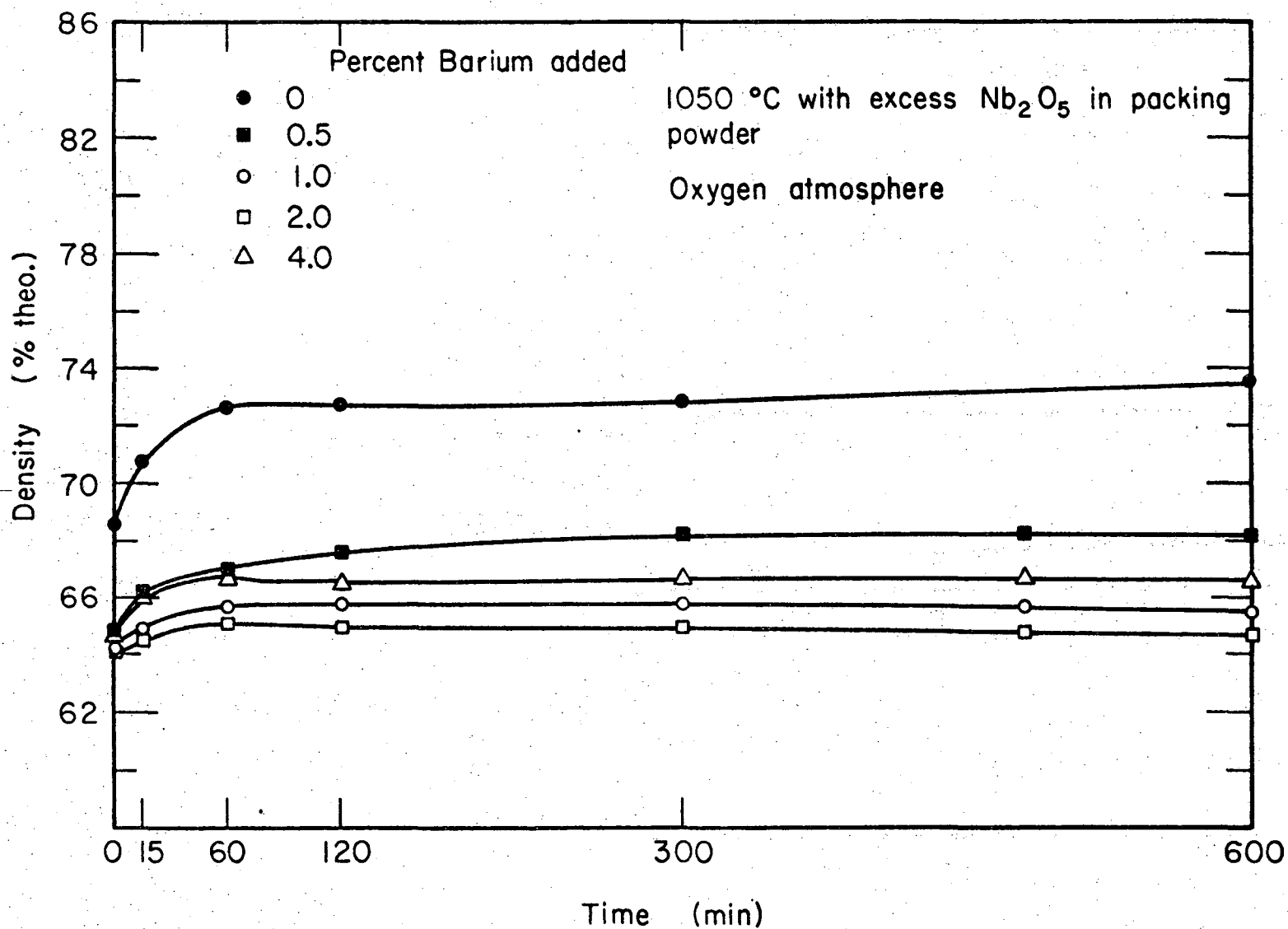
DTA analyses for NKN material. From X-ray patterns shown in Fig. 11, the $(\text{NaK})\text{Nb}_8\text{O}_{21}$ is forming at the expense of Nb_2O_5 and the nitrates. But loss of weight doesn't occur in the NKN system until a slightly higher temperature, 615°C . At some temperature above 600°C the first NKN peaks appear and as temperature increases to 700°C , the NKN phase continued to grow at the expense of the $(\text{NaK})\text{Nb}_8\text{O}_{21}$ phase. If the reaction goes to completion then all the $(\text{NaK})\text{Nb}_8\text{O}_{21}$ should convert to NKN.

The reason for the concentration gradient of $(\text{NaK})\text{Nb}_8\text{O}_{21}$ appearing in this system is a diffusion problem and is shown in Fig. 12. Initially, at just under 600°C the pellet or powder compact of raw materials has formed a solid solution of $(\text{NaK})\text{Nb}_8\text{O}_{21}$ and $(\text{NaK})\text{O}$, or $(\text{NaK})\text{NO}_3$ liquid. As the temperature increases, the nitrate gases leave the system (accounting for the weight loss). Also, $(\text{NaK})\text{O}$ begins to evaporate from the surface resulting in the concentration gradient shown in Fig. 12A. The temperature for the formation of NKN is reached at the surface and the $(\text{NaK})\text{O}$ reacts with the $(\text{NaK})\text{Nb}_8\text{O}_{21}$ at the surface to form NKN. This reaction acts like a sink for $(\text{NaK})\text{O}$ and the system sees the same $(\text{NaK})\text{O}$ concentration gradient as in Part A but with a smaller diameter pellet and less $(\text{NaK})\text{O}$ as shown in Part B. As the reaction temperature moves inward, the above process continues, Part C. The last stage is the point at which the entire pellet has reached the reaction temperature and the remaining $(\text{NaK})\text{O}$ has reacted to form NKN. If there is a deficiency of $(\text{NaK})\text{O}$ in the system due to vaporization, then the presence of the second phase in the center after calcining is explained. The solution is to add a larger quantity of excess NaNO_3 and KNO_3 before calcining.



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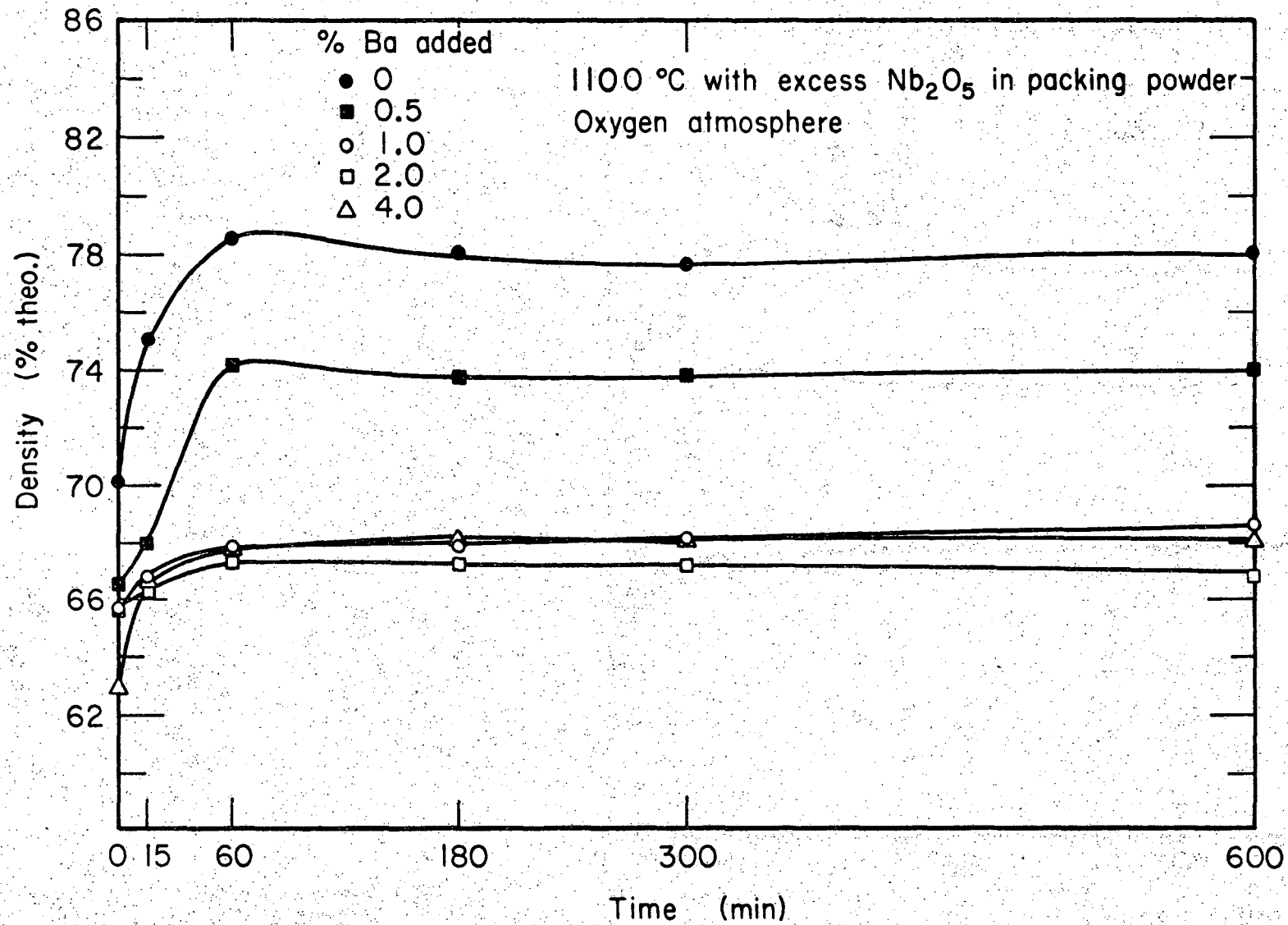
Fig. 11. Calcining history of NKN using X-ray diffraction patterns.



-25-

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Fig. 13. Relative density of NKN pellets versus sintering time at 1050°C.



-26-

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Fig. 14. Relative density of NKN pellets versus sintering time at 1100°C.

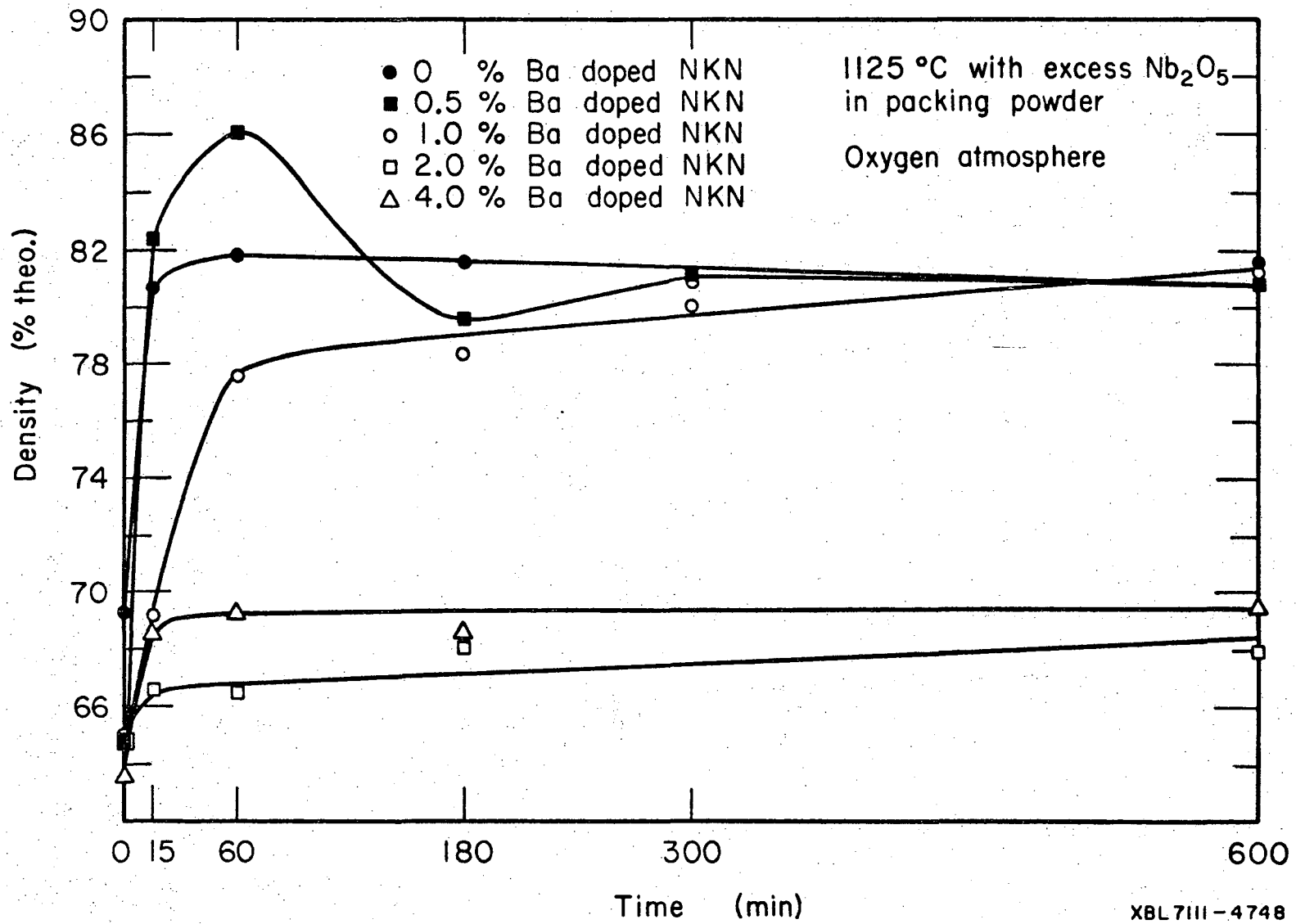


Fig. 15. Relative density of NKN pellets versus sintering time at 1125°C.

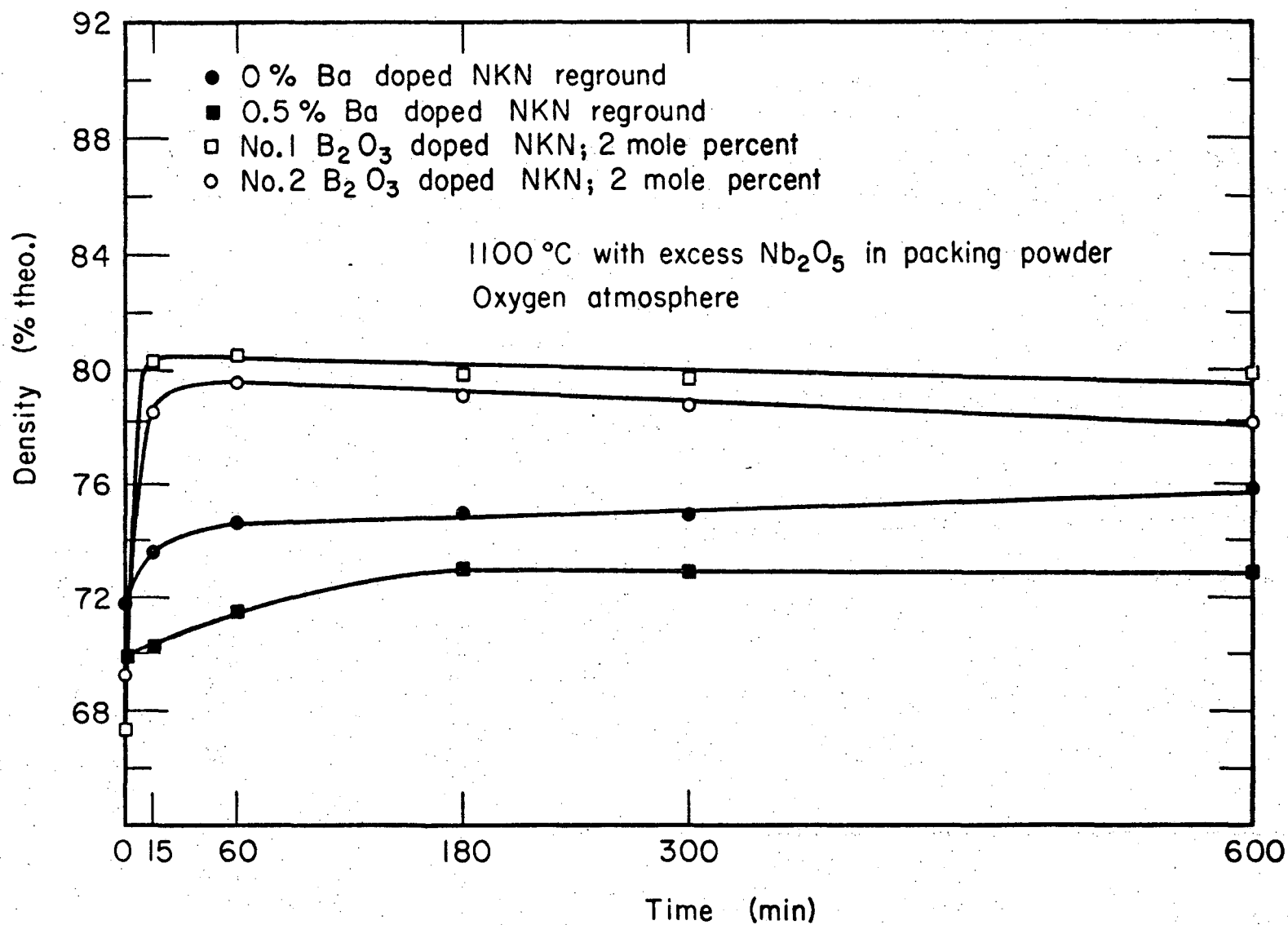


Fig. 16. Relative density of NKN pellets versus sintering time at 1100°C.

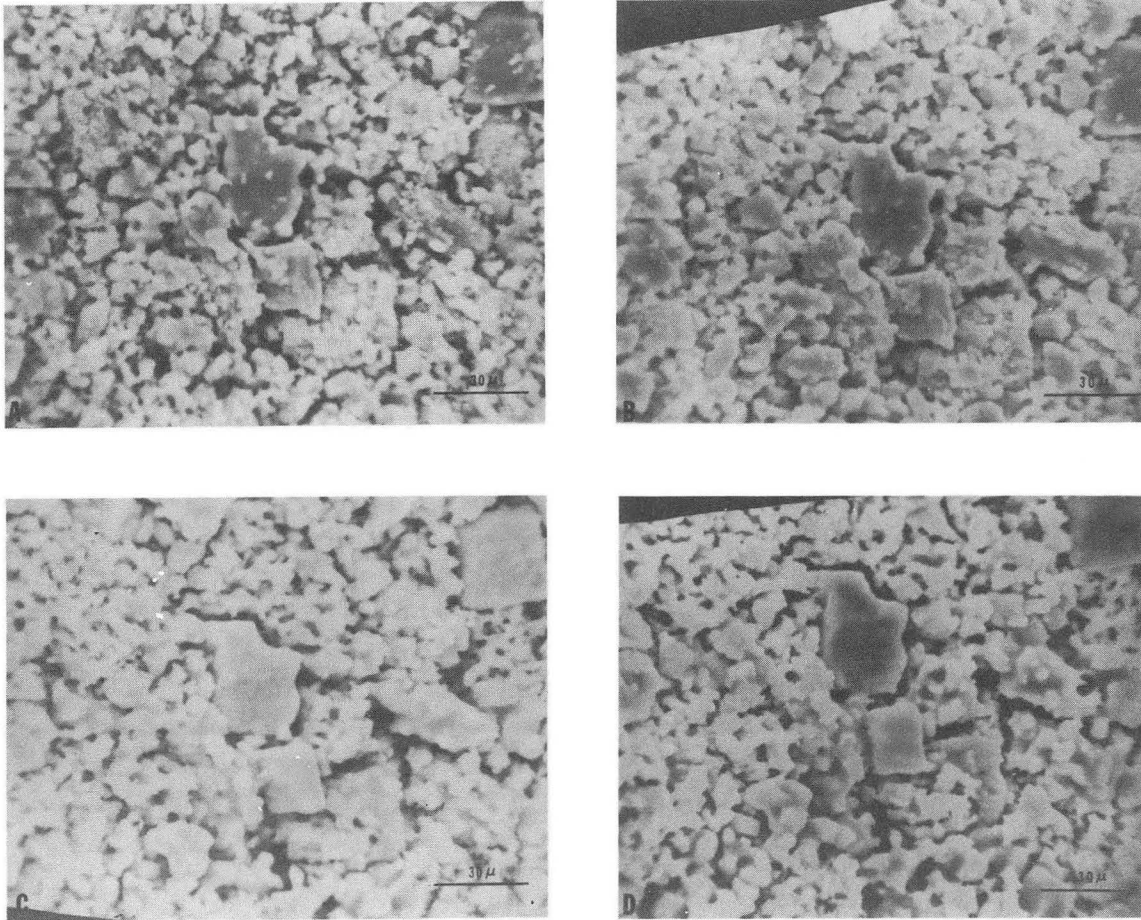
appreciably the densification of PZT ferroelectrics. Undetected impurities in NKN could account for the liquid phase.

B_2O_3 was added to create a liquid phase. Its sintering curves agree with the postulated theory, rapid initial densification only.

Stannek⁴ said that the cubic grains of NKN had a very low surface energy and that this would lead to a small driving force for sintering. This is why densification stops after the rearrangement stage.

Barium was added as a dopant to reduce grain growth. Microstructures of doped and undoped NKN as observed with the scanning electron microscope are shown in Figs. 17, 18, 19, 20, and 21. Figure 17 shows a series of pictures of undoped NKN sintered in the hot stage. These pictures show the disappearance of the smaller grains and some rearrangement. Figures 18, 19, and 20 show the effect of Ba^{+2} additions to NKN at different sintering temperatures. At each temperature the effect of increasing Ba^{+2} additions on reducing grain growth is evident. However, as temperature is increased, the effectiveness of Ba^{+2} as a grain growth inhibitor decreases. The effect of B_2O_3 on microstructure is shown in Fig. 21. It is similar to the undoped NKN in that the liquid phase appears to have been formed.

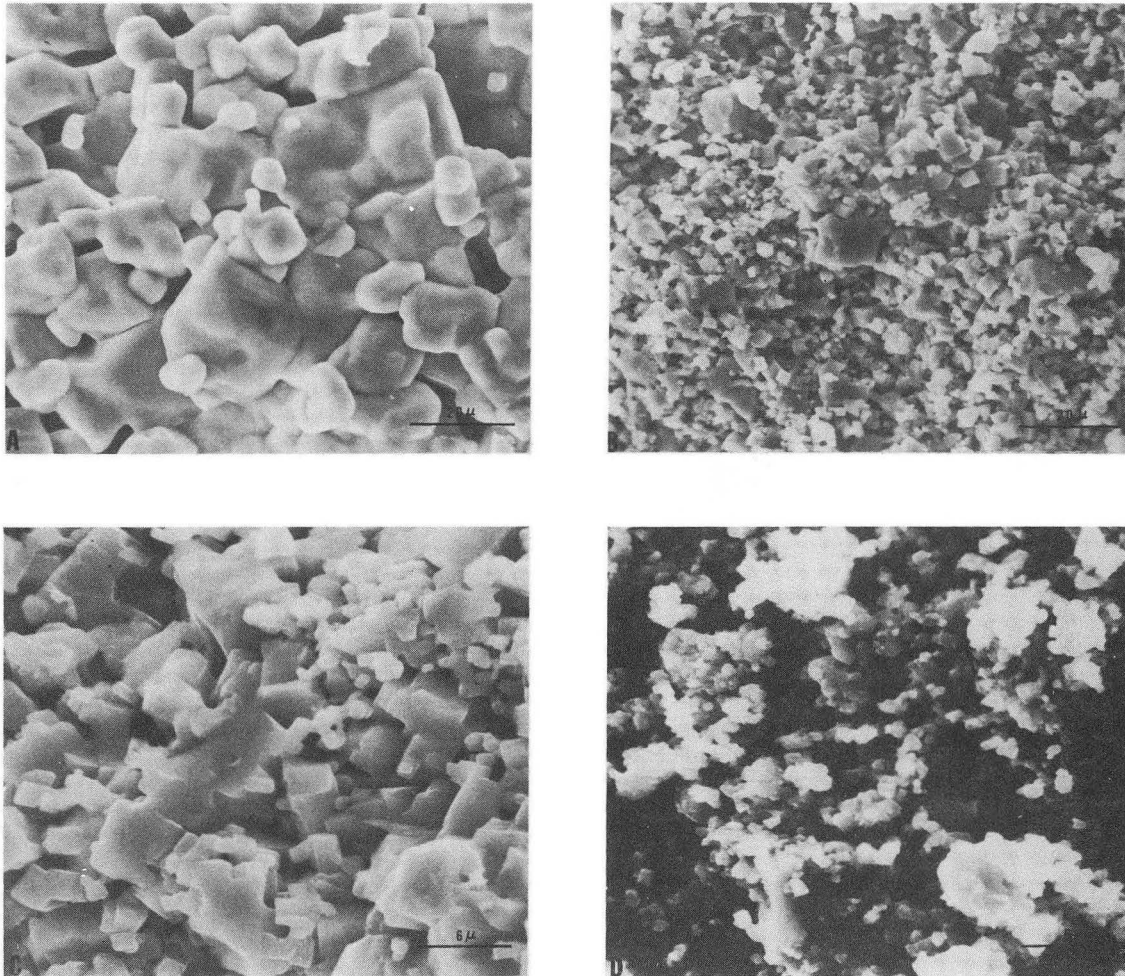
The amount of liquid phase appears to decrease with increasing Ba^{+2} additions. From Kingery's relationship between rearrangement densification and volume fraction liquid, the Ba^{+2} is postulated to prevent formation of a liquid phase, i.e., rearrangement.



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Fig. 17. Scanning electron microscope pictures of NKN in hot stage in vacuum.

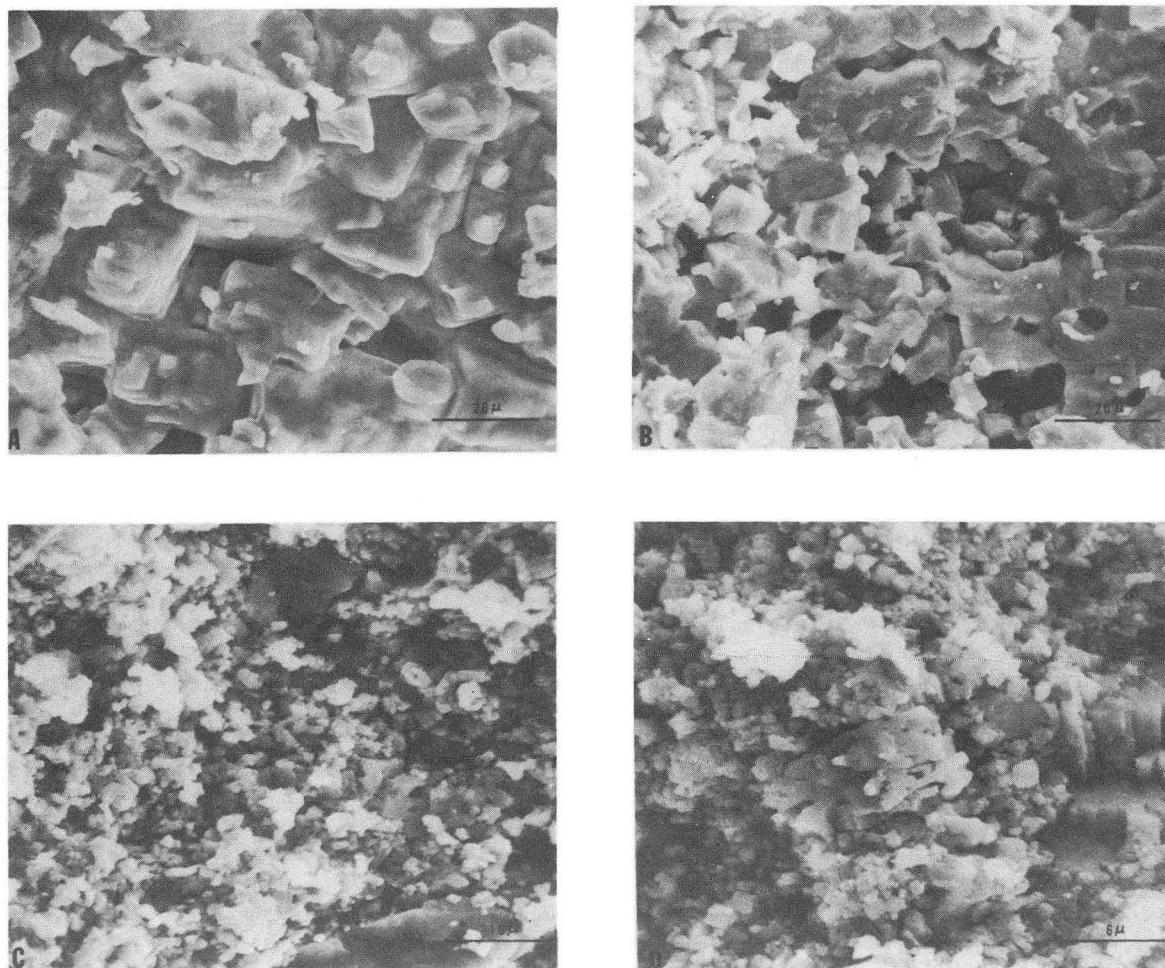
- A. 540°C
- B. 950°C
- C. 1050°C
- D. 1100°C



XBB 7111 5601

Fig. 18. Scanning electron microscope pictures of fracture surfaces of NKN pellets sintered for 10 hours at 1050°C in oxygen.

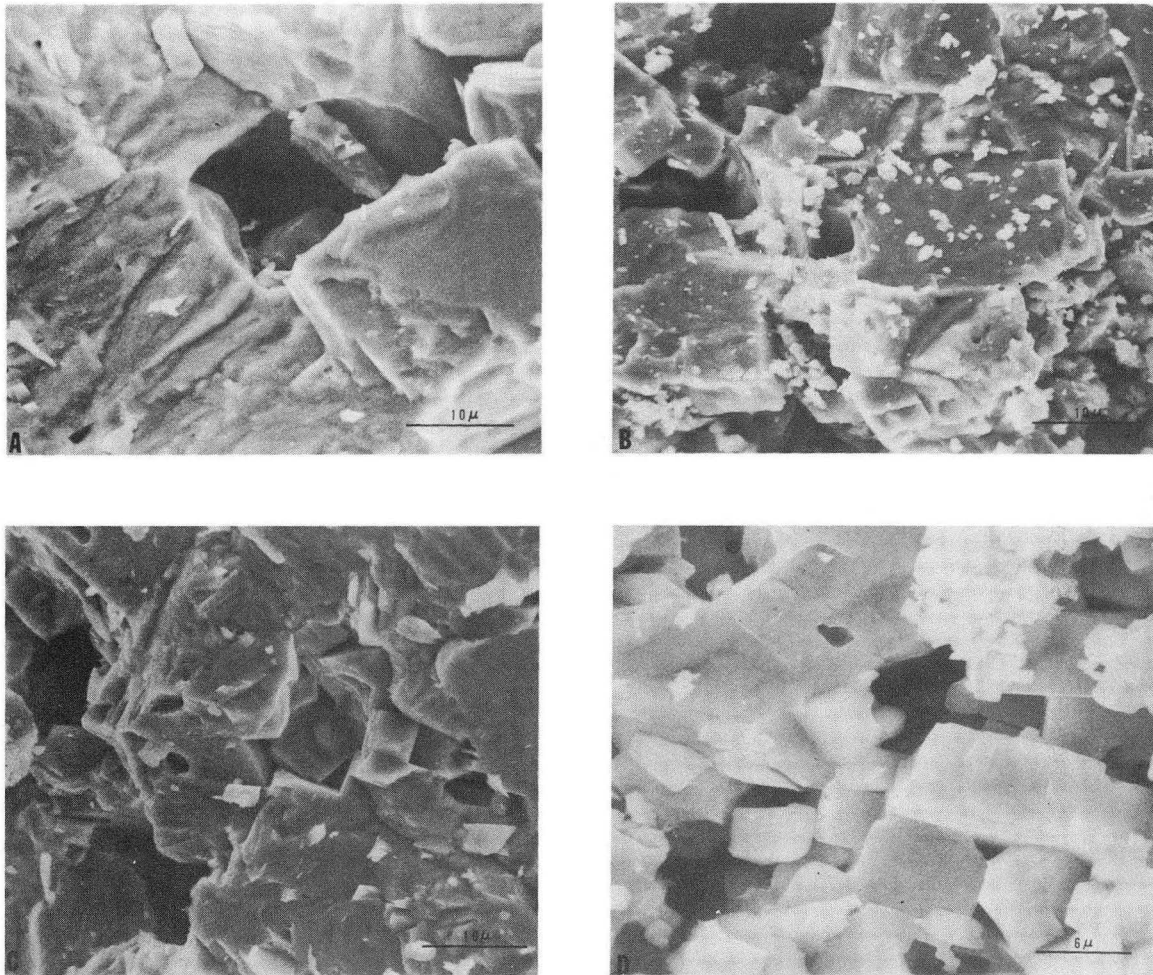
- A. 0.0 mole percent Ba⁺²
- B. 0.5 " " "
- C. 1.0 " " "
- D. 4.0 " " "



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Fig. 19. Scanning electron microscope pictures of fracture surfaces of NKN pellets sintered for 10 hours at 1100°C in oxygen.

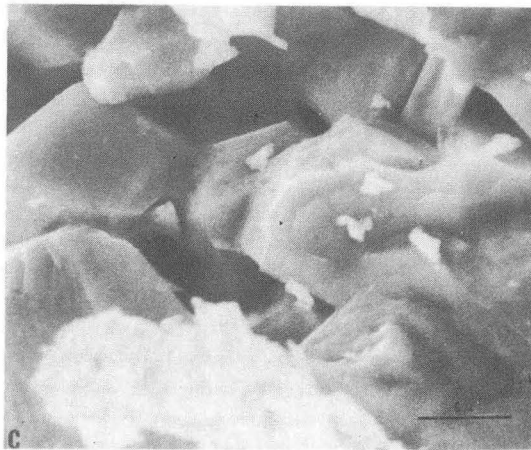
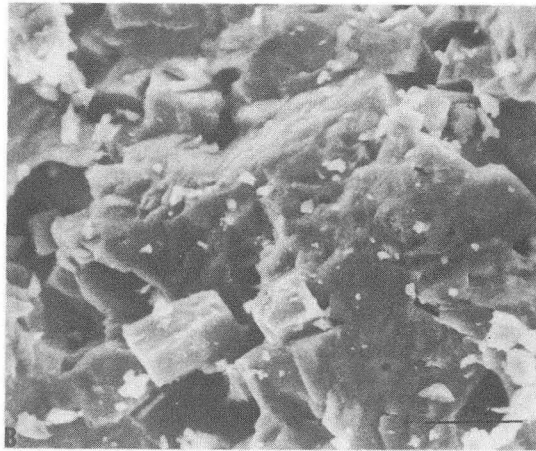
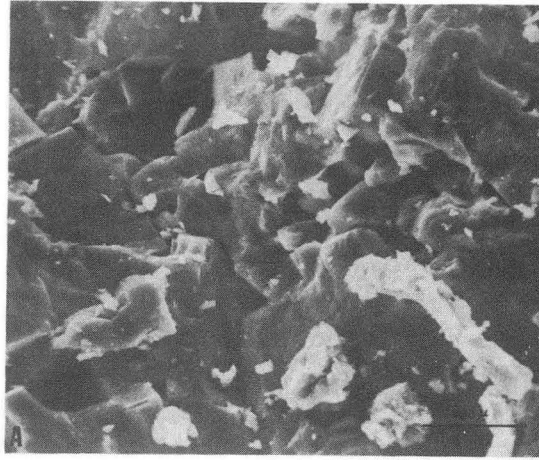
- A. 0.0 mole percent Ba⁺²
- B. 0.5 " " "
- C. 1.0 " " "
- D. 2.0 " " "



XBB 7111 5599

Fig. 20. Scanning electron microscope pictures of fracture surfaces of NKN pellets sintered for 10 hours at 1125°C in oxygen.

- A. 0.0 mole percent Ba⁺²
- B. 0.5 " " "
- C. 1.0 " " "
- D. 2.0 " " "



XBB 7111 5603

Fig. 21. Scanning electron microscope pictures of fracture surfaces of NKN pellets sintered for 10 hours at 1100°C in oxygen. The pellets were doped with 2 mole percent B_2O_3 .

IV. CONCLUSION

The system $(\text{Na}_{0.5}\text{K}_{0.5})\text{NbO}_3$ presents several interesting processing problems which are just beginning to be understood. The reactions taking place during calcining are: the formation of an intermediate compound, the reaction of this compound with sodium and potassium oxide to form NKN. Loss of sodium and potassium oxides due to vaporization during this reaction are significant enough to account for the presence of the intermediate compound in the calcined compact after calcining reactions have ceased.

NKN does not sinter per se. Densification occurs by particle rearrangement in the presence of a liquid phase. The driving force for sintering of NKN is so small that densification of the powder essentially stops after rearrangement although some de-densification is observed. Barium additions effectively reduce grain growth but do not increase sintering. In fact, large additions (2 and 4 mole %) of BaO reduce the rearrangement densification.

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"and the deep and dank tarn at my feet closed sullenly and silently over the fragments of the House of Usher."

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