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Structural Behavior of a Curved 2-Span Reinforced Concrete Box Girder Bridge Model, Vol. 3 -- Detailed Tables of Experiments and Analytical Results

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# STRUCTURAL BEHAVIOR OF A CURVED TWO SPAN REINFORCED CONCRETE BOX GIRDER BRIDGE MODEL

VOL. III – DETAILED TABLES OF  
EXPERIMENTAL AND  
ANALYTICAL RESULTS

by

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P. K. LARSEN

In cooperation with the State of California, Business and  
Transportation Agency, Department of Transportation and  
the U. S. Department of Transportation, Federal Highway  
Administration.

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Department of Civil Engineering  
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and  
Structural Mechanics

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KEYWORDS

Curved box girder bridge; continuous box girder; reinforced concrete model; large scale model; experimental results; theoretical results; reactions, deflections; strains; moments; live loads; overloads.



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## 1. INTRODUCTION

### 1.1 Objective

The present volume is the third of a three volume sequence on the "Structural Behavior of a Curved Two Span Reinforced Concrete Box Girder Bridge Model". The material included in each volume is as follows:

- Vol. I - Design, Construction, Instrumentation and Loading.
- Vol. II - Reduction, Analysis and Interpretation of Results.
- Vol. III - Detailed Tables of Experimental and Analytical Results.

These volumes deal with the complete experimental and analytical study of a 1:2.82 scale box girder bridge model (Fig. 1.1) built and tested in the Structural Engineering Materials Laboratory (S.E.M.L.) of the University of California, Berkeley. The model was 72 ft. long along the longitudinal centerline, 12 ft. wide and 1 ft.  $8 \frac{9}{16}$  in. in depth. It had a radius of curvature in the horizontal plane of 100 ft.

Bridge model dimensions; location and amounts of reinforcing steel; instrumentation and loading used for the model have been described in detail in Vol. I. In Vol. II, the methods of analysis and computer programs used in obtaining theoretical results and in reducing experimental data are described; experimental and theoretical results are compared and discussed in detail; and conclusions and recommendations for implementation are presented. For easy reference in the present volume, Figs. 1.2 and 1.3 depict the general dimensions of the model and the designation of transverse sections and longitudinal girder lines which are of pertinent interest.

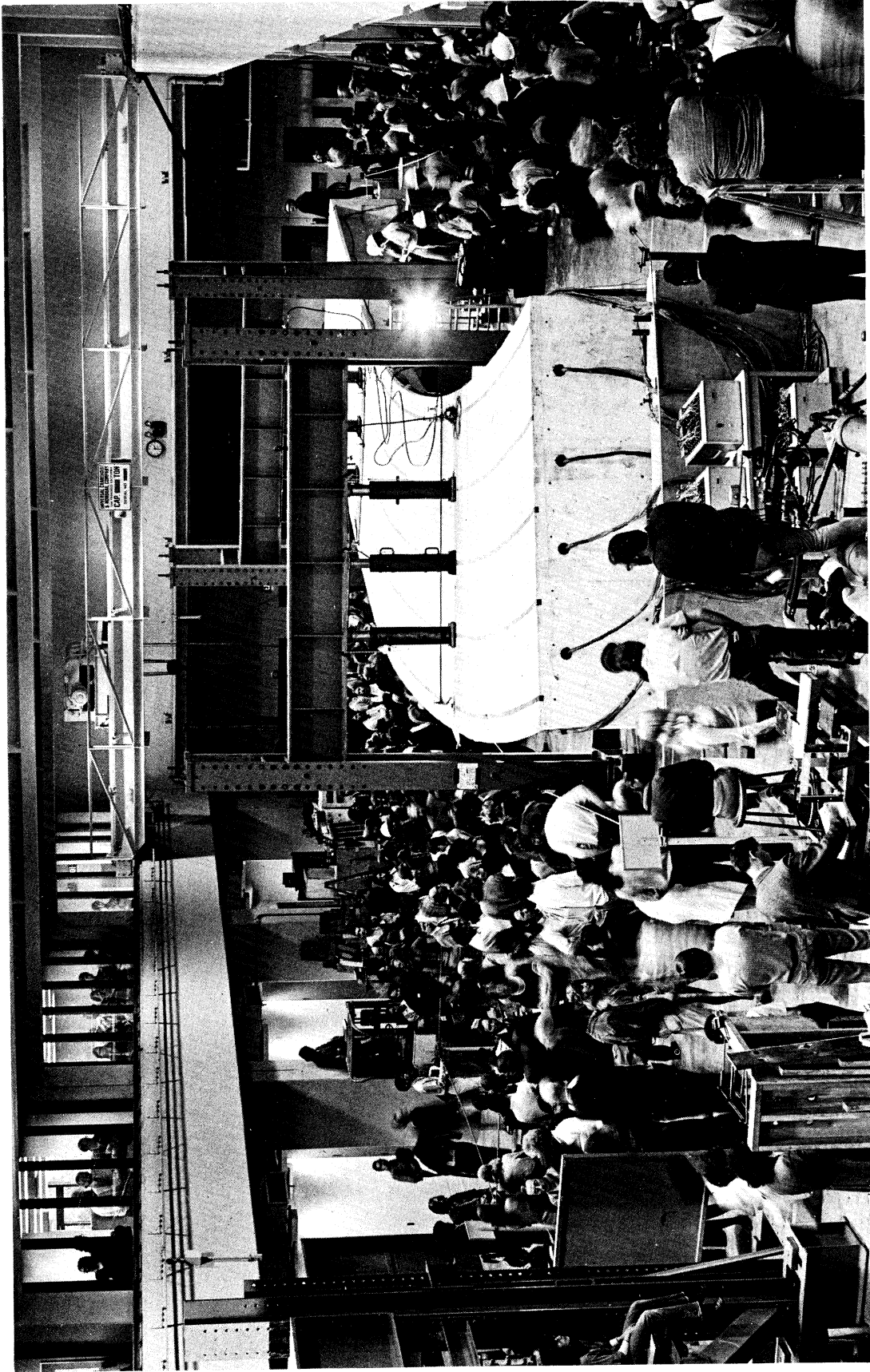
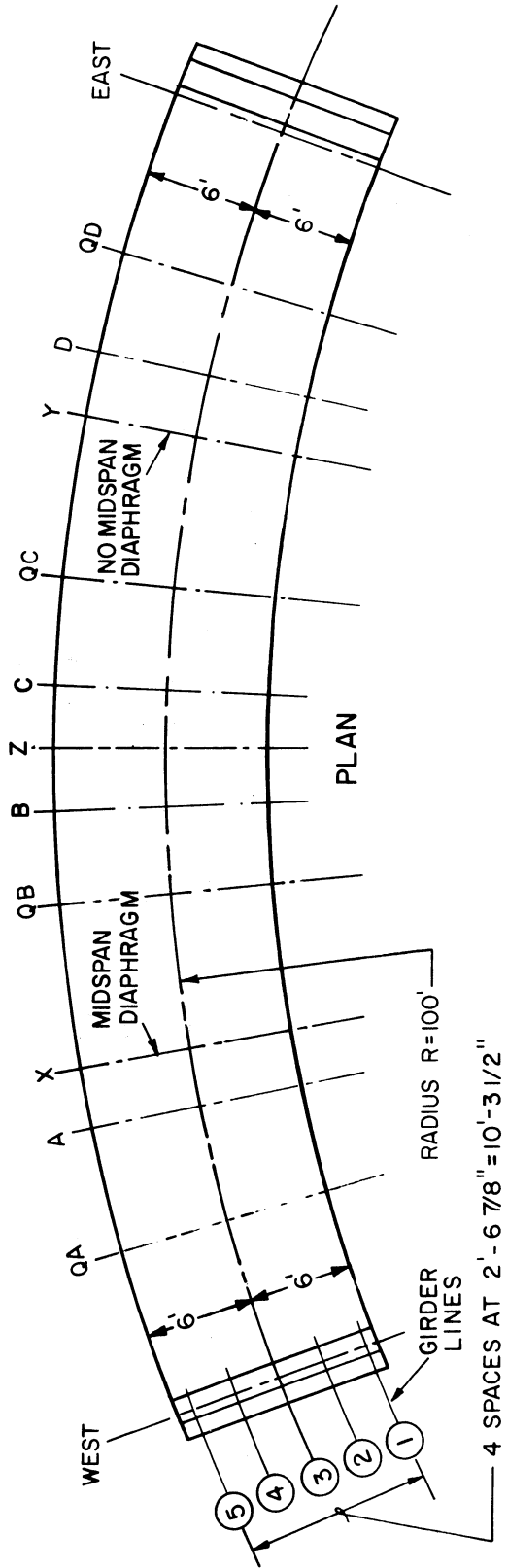
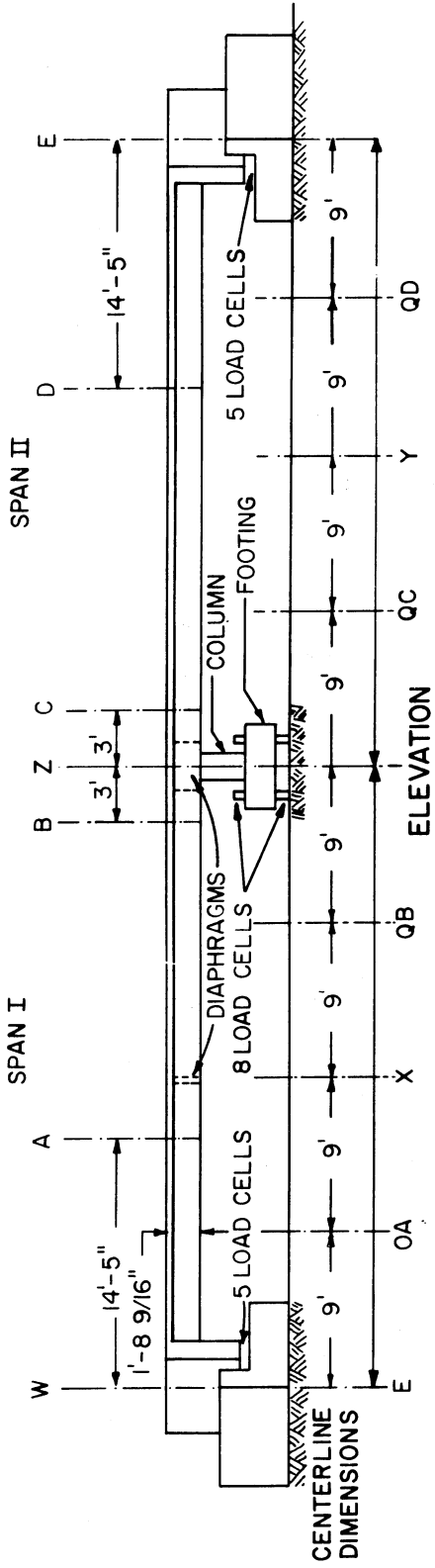


FIG. 1.1 FINAL LOAD TEST ON CURVED BOX GIRDER BRIDGE MODEL



**FIG. 1.2 DIMENSIONS OF BOX GIRDER BRIDGE MODEL WITH LOCATIONS OF TRANSVERSE SECTIONS AND LONGITUDINAL GIRDER LINES**

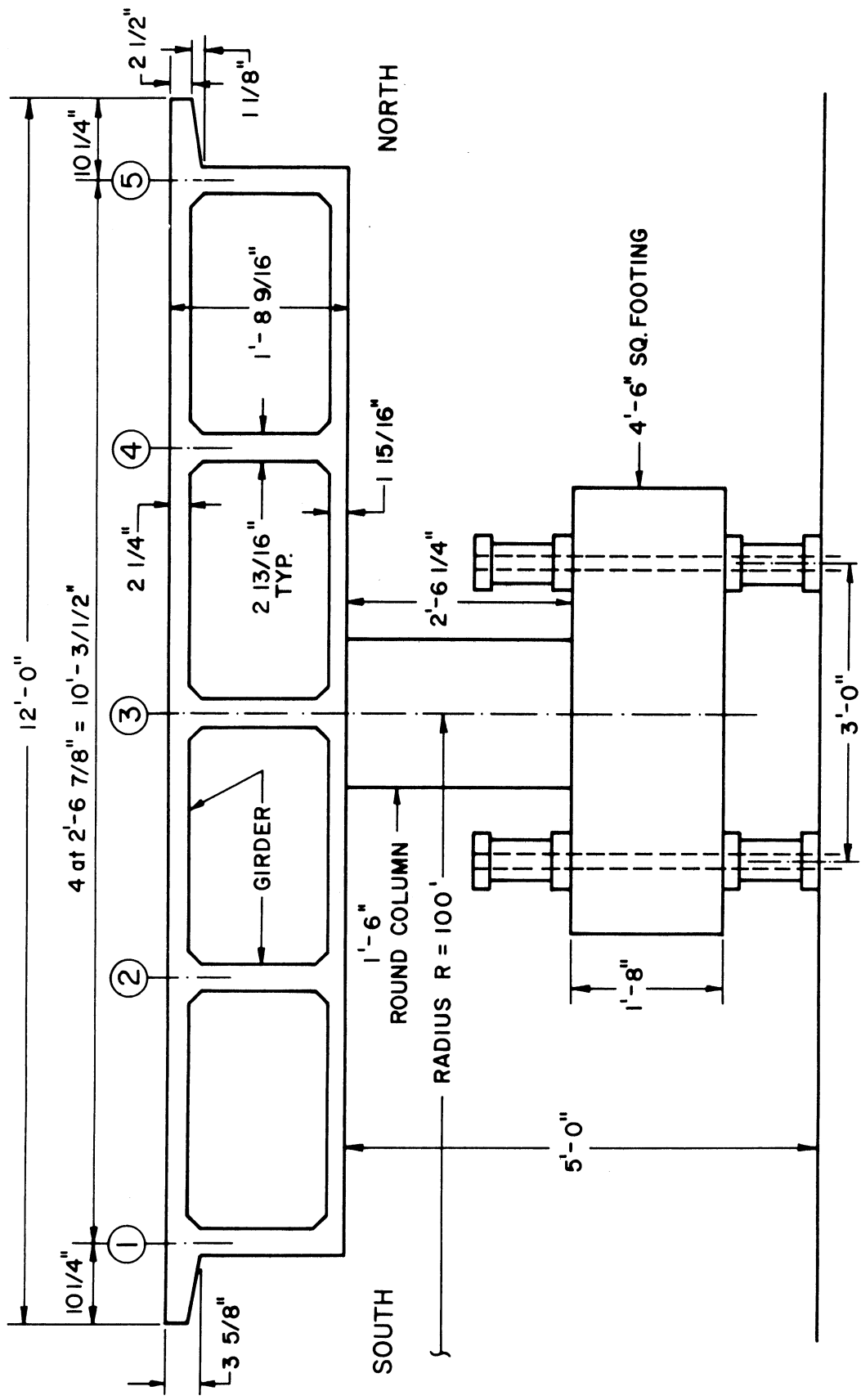


FIG. 1.3 TYPICAL SECTION OF BOX GIRDER BRIDGE MODEL



## 1.2 Scope of Volume III

The present volume contains the detailed tables of experimental and analytical results, many of which have been utilized in Volume II in comparing and interpreting results under various loadings. The tables form a permanent and complete record of the basic results obtained during the research investigation. The responses of the bridge in terms of reactions, deflections, strains and moments are given.

In order that the tables may be easily interpreted and understood within the present volume by itself, Chapter 2 gives a description of the contents of the tables and the loadings considered in each case. A compact summary of the tables is presented in Section 2.6 for easy reference.

## 2. DESCRIPTION OF TABLES

### 2.1 General Remarks

The experimental results presented in the tables have been obtained by using a specially developed set of computer programs described in Chapter 3 of Volume II to convert the raw experimental data to the desired results. The theoretical results presented in the tables in all cases have been obtained by using a finite element computer program, CELL, to analyze the bridge as an uncracked homogeneous structure. Details of the analysis by CELL are given in Chapter 2 of Volume II.

In most cases the theoretical and experimental results presented in the tables have been normalized for purposes of comparison to loads of 100 kips per span. The only exceptions to this are the tables for truck loadings and construction vehicle loadings, in all of which, actual values rather than normalized values are given for the results. In most of the tables computations have been carried out and tabulated with a maximum of three significant figures. It should be recognized, however, that in some cases the number of significant figures should be even less.

For each loading case, described in the succeeding sections of this chapter, a set of 10 tables (A, B, C, D, E, F, G, H, I, J,) are given in the Appendix. A brief description of the contents of each of these tables is given below.

#### A. Summary of Reactions

The individual reactions at each support point at the east (E), center (F), and west (W) supports is given. Applied loads at Section X

(PX), Section Y (PY) and total load (SUMP) are indicated. These may be compared with total reactions at the east (RE), center (RF), and west (RW) supports (obtained by summing individual reactions) as well as the overall total reaction (SUMR). The ratio (SUMR/SUMP) gives a measure of the vertical static check.

In addition to the vertical reactions, the torsional moment reactions at the two end supports (TE and TW) and the longitudinal and torsional moment reactions under the center footing (MF and TF) are tabulated. Experimental values of these quantities are computed from the statical contributions of the individually measured vertical reactions. Theoretical values of TE and TW are computed in a similar manner, however, the total reactions under the center footing (RF, MF, TF,) are output by the CELL program directly. These latter theoretical quantities are then used to calculate the four statically equivalent individual theoretical reactions under the center footing. Also, the total actual experimental load applied at Section X (ACTUAL PX) and at Section Y (ACTUAL PY) is given in this table as well as all other tables.

#### B. Summary of Deflections

Deflections under each girder web are presented for midspan Sections X and Y and quarterspan Sections QB and QC near the center bent, and at Section Z for girders 1, 2, 4 and 5. The ratio of experimental to theoretical deflections (E/T) gives a measure of the effect of cracking in the actual structure which is not taken into account in the theoretical analysis by CELL.

#### C. Summary of Strains at Section A

D. Summary of Strains at Section BE. Summary of Strains at Section CF. Summary of Strains at Section D

Theoretical strains are computed as described in Section 2.8 of Volume II. Measured experimental strains are values obtained directly from the test. Adjusted experimental strains are computed as described in Section 3.5 of Volume II. Normalized and actual values of the applied loads at Sections X and Y (PX and PY), are shown at the bottom of the page. Thus actual strains, if desired, can be obtained by multiplying the normalized strain values tabulated, by the ratio of actual P divided by normalized P.

G. Distribution of Moments to Each Girder (Moments about Compression Flange Mid-depth)H. Distribution of Moments to Each Girder (Moments about Tension Flange Steel)I. Distribution of Moments to Each Girder (Moments about Gross Section Neutral Axis)J. Distribution of Moments to Each Girder (Moments about Girder Experimental Neutral Axis)

In each of these tables, the internal moments taken by each of the five girders and the total internal moment equal to the sum of these is tabulated for sections A, B, C, and D. Computation of these moments and the percentages of total moment at a section taken by each girder are automatically calculated by the computer program CELL for theoretical

values and by MOMENT for experimental values (see Sections 3.6 and 3.9 of Volume II for details).

The actual box girder bridge is first divided into five individual girders consisting of a web and top and bottom flanges. The flanges for the interior girders are taken equal in width to the distance between the midpoint of the cells on adjacent sides of the web. For the exterior girders, on the exterior side of the web the top flange consists of the cantiliver overhang and no bottom flange exists on the exterior side of the web.

The girder moment at any section taken by an individual girder is found by integrating the internal longitudinal stresses over the proper slab and web areas to obtain forces and then multiplying these forces by their respective lever arms to the defined horizontal reference axis. As discussed in Section 3.9 of Volume II, it was observed in reducing the experimental data for the various load cases, that the longitudinal compressive and tensile forces at a section as obtained from the MOMENT program did not balance as statics would require. This indicated that the moduli of elasticity of the concrete and steel used in converting strains to stresses and thence to forces were not representative of the true stiffnesses needed for these conversions.

In order to see if the experimental data was consistent, the unmodified internal forces at Sections A, B, C, and D were calculated from the internal strains and the control specimen moduli of elasticity given for the concrete and steel in Tables 6.4 and 6.6 of Volume I respectively. These experimental forces in the tension and compression flanges are given in Cols. (3) to (10) of Tables 2.1, 2.2 and 2.3 for all conditioning loads and for point load cases 1X, 1Y, 1X + 1Y, 3X, 3Y,

3X + 3Y, 5X, 5Y, 5X + 5Y applied after the 24, 30, 40, 50 and 60 ksi conditioning loads. All values have been normalized to a 100 kip load in the loaded span. A study of these values indicates a general consistency of the experimental data for all load cases and load levels. It can be seen that at Sections A and D, the compression force is consistently higher than the tension force, while at Sections B and C the two forces are much closer. It can also be observed that there is a general increase in the magnitude of the forces at or after increasing conditioning load levels. The differences described above can be attributed to the participation of the concrete between cracks carrying some of the tensile force as well as the steel and the changing position of the neutral axis and moment lever arm under different loadings. See Section 3.9 of Volume II for further discussion of these reasons.

Because of the difference in the experimental tensile and compressive forces at a Section, it was decided to modify these forces to ensure as much as possible that equilibrium was satisfied at the instrumented Sections A, B, C and D. Using the measured reactions and the applied loads and their respective lever arms, an experimental external gross moment at Section A, B, C and D was computed for each load case. Taking the internal moment arm equal to 1.539 ft., the distance between the top and bottom flanges, an equilibrating force (tension equal to compression) was computed by dividing this external moment by 1.539 ft. Results of these calculations for all load cases are given in Cols. (11) to (14) of Tables 2.1, 2.2 and 2.3. Consistency of these experimental results for any load case is a measure of the consistency of the experimental reactions at or after successively higher conditioning load levels. A study of this indicates a greater consistency for these values,

TABLE 2.1 SUMMARY OF EXPERIMENTAL FORCES (KIPS) AT A SECTION OBTAINED FROM INTERNAL STRAIN READINGS AND ALSO FROM THE EXTERNAL MOMENT DIVIDED BY A LEVER ARM OF 1.539 FT

LOAD CASE	AT OR AFTER COND. LOAD (KSI)	UNMODIFIED FORCES AT A SECTION OBTAINED FROM INTERNAL STRAIN READINGS IN THE TOP OR BOTTOM FLANGES												FORCES AT A SECTION IN TOP AND BOTTOM FLANGES FROM EXT. M ÷ 1.539			
		TENSION FLANGE (STEEL)						COMPRESSION FLANGE (CONCRETE + STEEL)						SEC A	SEC B	SEC C	SEC D
		BOT SEC A	TOP SEC B	TOP SEC C	TOP SEC D	BOT SEC A	BOT SEC B	BOT SEC C	TOP SEC A	TOP SEC B	TOP SEC C	TOP SEC D					
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)				
COND. LOAD	24	230	304	267	227	-314	-311	-322	-380	295	305	305	285				
	30	237	313	278	234	-323	-318	-328	-380	297	298	315	274				
	40	244	337	302	251	-312	-322	-327	-371	283	332	351	274				
	50	274	373	333	279	-343	-353	-353	-398	301	292	400	285				
	60	270	366	329	273	-324	-361	-348	-376	283	332	378	275				
1X	24	258	147	98	-31	-399	-161	-121	77	375	104	175	77				
	30	272	152	99	-36	-395	-162	-125	85	357	114	169	75				
	40	279	167	106	-37	-476	-168	-125	90	363	101	162	72				
	50	279	169	101	-36	-514	-174	-127	97	374	78	172	76				
	60	285	161	85	-37	-542	-247	-200	91	366	96	177	78				
1Y	24	-30	112	121	248	50	-115	-162	-471	71	159	138	346				
	30	-36	117	134	267	58	-128	-169	-460	77	174	142	345				
	40	-33	125	156	280	67	-118	-167	-495	79	177	---	339				
	50	-31	131	159	295	72	-126	-177	-524	77	174	180	328				
	60	-34	121	151	295	76	-141	-184	-530	79	179	140	346				
1X + 1Y	24	209	240	207	203	-336	-256	-261	-388	307	228	253	290				
	30	223	277	239	244	-332	-284	-271	-416	296	253	285	277				
	40	237	284	258	239	-413	-283	-276	-417	302	240	261	290				
	50	240	273	243	227	-453	-291	-281	-414	321	196	237	277				
	60	247	281	247	253	-470	-335	-304	-449	311	219	253	278				

TABLE 2.2 SUMMARY OF EXPERIMENTAL FORCES (KIPS) AT A SECTION OBTAINED FROM INTERNAL STRAIN READINGS AND ALSO FROM THE EXTERNAL MOMENT DIVIDED BY A LEVER ARM OF 1.539 FT

LOAD CASE	AFTER COND. LOAD (KSI)	UNMODIFIED FORCES AT A SECTION OBTAINED FROM INTERNAL STRAIN READINGS IN THE TOP OR BOTTOM FLANGES												FORCES AT A SECTION IN TOP AND BOTTOM FLANGES FROM EXT. M ÷ 1.539			
		TENSION FLANGE (STEEL)						COMPRESSION FLANGE (CONCRETE + STEEL)						SEC A	SEC B	SEC C	SEC D
		BOT SEC A	TOP SEC B	TOP SEC C	TOP SEC D	BOT SEC B	BOT SEC C	TOP SEC A	TOP SEC B	TOP SEC C	TOP SEC D	BOT SEC A	BOT SEC B				
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)				
	24	269	162	112	-49	-392	-167	-147	108	377	118	176	78				
	30	292	170	117	-63	-399	-168	-162	132	379	114	156	69				
3X	40	310	191	131	-69	-488	-169	-171	167	385	101	163	72				
	50	306	197	125	-66	-519	-182	-173	166	388	96	161	71				
	60	320	199	125	-68	-554	-192	-195	185	400	68	163	72				
	24	-65	135	135	287	100	-154	-169	-532	79	177	182	349				
	30	-69	142	150	313	107	-168	-179	-536	77	174	199	342				
3Y	40	-83	153	164	342	144	-180	-165	-607	61	137	183	349				
	50	-76	154	166	345	135	-196	-172	-636	73	165	184	349				
	60	-76	155	168	350	142	-221	-191	-647	77	172	205	339				
	24	235	290	255	197	-345	-295	-332	-376	302	288	312	278				
	30	252	319	283	223	-348	-314	-350	-389	296	303	327	283				
3X + 3Y	40	273	351	313	236	-443	-325	-354	-407	290	316	324	277				
	50	267	353	307	248	-462	-345	-361	-448	298	298	311	288				
	60	256	354	306	267	-462	-395	-397	-495	307	278	331	302				



TABLE 2.3 SUMMARY OF EXPERIMENTAL FORCES (KIPS) AT A SECTION OBTAINED FROM INTERNAL STRAIN READINGS AND ALSO FROM THE EXTERNAL MOMENT DIVIDED BY A LEVER ARM OF 1.539 FT

LOAD CASE	AFTER COND. LOAD (KSI)	UNMODIFIED FORCES AT A SECTION OBTAINED FROM INTERNAL STRAIN READINGS IN THE TOP OR BOTTOM FLANGES												FORCES AT SECTION IN TOP AND BOTTOM FLANGES FROM EXT. M ÷ 1.539			
		TENSION FLANGE (STEEL)						COMPRESSION FLANGE (CONCRETE + STEEL)						SEC A	SEC B	SEC C	SEC D
		BOT SEC A	TOP SEC B	TOP SEC C	TOP SEC D	BOT SEC A	BOT SEC B	BOT SEC C	TOP SEC A	TOP SEC B	TOP SEC C	TOP SEC D					
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)				
5X	24	300	195	142	-71	-434	-189	-191	148	375	173	203	90				
	30	316	207	147	-74	-437	-193	-199	161	376	172	195	86				
	40	351	233	170	-95	-522	-196	-224	219	387	147	212	94				
	50	361	246	171	-90	-577	-207	-241	234	377	170	209	93				
5Y	60	362	245	164	-89	-571	-213	-261	253	378	168	207	92				
	24	-65	151	148	276	102	-184	-200	-575	88	198	173	375				
	30	-72	156	159	299	110	-190	-194	-581	80	181	173	375				
	40	-78	172	183	297	134	-207	-188	-608	80	181	181	372				
5X + 5Y	50	-70	173	197	301	125	-206	-209	-639	106	239	192	367				
	60	-76	170	183	306	142	-264	-221	-630	90	205	208	360				
	24	226	353	299	299	-316	-370	-369	-472	310	320	366	296				
	30	240	385	327	244	-325	-392	-389	-490	310	321	400	291				
5X + 5Y	40	274	411	359	226	-389	-400	-402	-487	303	337	470	298				
	50	264	432	368	263	-380	-439	-404	-588	314	311	404	282				
60	268	441	371	273	-388	-487	-434	-602	309	323	422	281					

Cols. (11) to (14), than for the internal forces, Cols. (3) to (10). It should be noted here that the external negative moments at Sections B and C are much more sensitive to small changes in the end reactions than are the external positive moments at Sections A and D.

Using the values given in Tables 2.1, 2.2 and 2.3 a set of "modification factors" was computed by dividing the section forces found from the external moment, Cols. (11) to (14), by the internal section forces found from the strains, Cols. (3) to (10). The results of these calculations are summarized in Tables 2.4, 2.5 and 2.6. Ideally these factors for the tensile or the compressive forces at a particular section for all load cases and load levels would be the same if the effective stiffness for converting the strains to stresses and thence to forces was a constant for each section force. After studying these results, it was decided that for the 24, 30, 40, 50 and 60 ksi conditioning loads, the modification factors shown for each case would be used to modify the experimental internal forces at the sections indicated, thus satisfying equilibrium for these load cases. For all other load cases, with exception of dead load, which is treated separately in Chapter 4 of Vol. II, the modification factors obtained from the 30 ksi conditioning load were used. These other load cases (totalling to 134 cases) which have been described in Table 5.1 of Vol. I, included the point load combinations, designed to produce 24 to 30 ksi total stresses in the reinforcement, which were applied after each conditioning load, as well as the truck load combinations and the moving fork lift loads applied after the 30 ksi conditioning load. All results for experimental internal forces and moments at a section presented in Table G, H, I and J of this Volume have therefore been modified by these factors. However, the experimental re-

TABLE 2.4 SUMMARY OF MODIFICATION FACTORS FOR FORCES AT A SECTION OBTAINED BY DIVIDING FORCE FROM EXTERNAL MOMENT BY FORCE FROM INTERNAL STRAINS

LOAD CASE	AT OR AFTER COND. LOAD (KSI)	FORCE IN TENSION FLANGE (STEEL)				FORCE IN COMPRESSION FLANGE (CONCRETE + STEEL)			
		BOT FL SEC A	TOP FL SEC B	TOP FL SEC C	BOT FL SEC D	TOP FL SEC A	BOT FL SEC B	BOT FL SEC C	TOP FL SEC D
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)
COND. LOAD	24	1.31	1.03	1.16	1.28	0.96	1.00	0.97	0.77
	30	1.26	0.95	1.13	1.17	0.92	0.94	0.96	0.72
	40	1.16	0.98	1.16	1.09	0.91	1.03	1.07	0.74
	50	1.10	0.78	1.20	1.02	0.88	0.83	1.13	0.72
	60	1.05	0.91	1.15	1.01	0.87	0.92	1.08	0.73
1X	24	1.44	0.71	1.79	2.48	0.94	0.65	1.45	1.00
	30	1.31	0.75	1.71	2.80	0.90	0.70	1.35	0.88
	40	1.30	0.61	1.53	1.95	0.76	0.60	1.30	0.80
	50	1.34	0.46	1.70	2.11	0.73	0.45	1.35	0.78
	60	1.28	0.60	2.08	2.11	0.68	0.39	0.89	0.86
1Y	24	2.37	1.42	1.14	1.40	1.42	1.38	0.85	0.74
	30	2.14	1.48	1.06	1.29	1.33	1.36	0.84	0.75
	40	2.39	1.42	-----	1.21	1.18	1.50	-----	0.69
	50	2.48	1.33	1.13	1.11	1.07	1.38	1.01	0.63
	60	2.32	1.48	0.93	1.17	1.04	1.27	0.76	0.65
1X + 1Y	24	1.47	0.95	1.22	1.43	0.91	0.89	0.97	0.75
	30	1.33	0.91	1.19	1.14	0.89	0.89	1.04	0.67
	40	1.27	0.85	1.01	1.21	0.73	0.85	0.95	0.70
	50	1.34	0.72	0.98	1.23	0.71	0.67	0.84	0.67
	60	1.26	0.78	1.02	1.14	0.66	0.65	0.83	0.65

TABLE 2.5 SUMMARY OF MODIFICATION FACTORS FOR FORCES AT  
 A SECTION OBTAINED BY DIVIDING FORCE FROM  
 EXTERNAL MOMENT BY FORCE FROM INTERNAL STRAINS

LOAD CASE	AFTER COND. LOAD (KSI)	FORCE IN TENSION FLANGE (STEEL)				FORCE IN COMPRESSION FLANGE (CONCRETE + STEEL)			
		BOT FL SEC A (3)	TOP FL SEC B (4)	TOP FL SEC C (5)	BOT FL SEC D (6)	TOP FL SEC A (7)	BOT FL SEC B (8)	BOT FL SEC C (9)	TOP FL SEC D (10)
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)
3X	24	1.40	0.73	1.57	1.59	0.96	0.71	1.20	0.72
	30	1.30	0.67	1.33	1.10	0.95	0.68	0.96	0.52
	40	1.24	0.53	1.24	1.04	0.79	0.60	0.95	0.43
	50	1.27	0.49	1.29	1.08	0.75	0.53	0.90	0.43
	60	1.25	0.34	1.32	1.06	0.72	0.35	0.84	0.39
3Y	24	1.13	1.31	1.35	1.22	0.79	1.15	1.08	0.66
	30	1.12	1.23	1.34	1.09	0.72	1.04	1.11	0.64
	40	0.74	0.90	1.12	1.11	0.42	0.76	1.11	0.58
	50	0.96	1.07	1.11	1.01	0.54	0.84	1.07	0.55
	60	1.01	1.11	1.22	0.97	0.54	0.78	1.07	0.52
3X + 3Y	24	1.29	0.99	1.22	1.41	0.88	0.98	0.94	0.74
	30	1.18	0.95	1.16	1.27	0.85	0.97	0.93	0.73
	40	1.06	0.90	1.04	1.17	0.66	0.57	0.92	0.68
	50	1.12	0.84	1.01	1.16	0.65	0.83	0.86	0.64
	60	1.20	0.79	1.08	1.13	0.66	0.70	0.83	0.60

TABLE 2.6 SUMMARY OF MODIFICATION FACTORS FOR FORCES  
AT A SECTION OBTAINED BY DIVIDING FORCE FROM  
EXTERNAL MOMENT BY FORCE FROM INTERNAL STRAINS

LOAD CASE	AFTER COND. LOAD (KSI)	FORCE IN TENSION FLANGE (STEEL)				FORCE IN COMPRESSION FLANGE (CONCRETE + STEEL)													
		TOP FL SEC B		TOP FL SEC C		TOP FL SEC A		TOP FL SEC D											
		(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)										
(1)	(2)																		
5X	24	1.25	0.89	1.43	1.27	0.86	0.92	0.63	0.61										
	30	1.19	0.83	1.33	1.16	0.86	0.89	0.98	0.53										
	40	1.10	0.63	1.25	0.99	0.74	0.75	0.95	0.43										
	50	1.04	0.69	1.22	1.03	0.65	0.82	0.87	0.40										
	60	1.04	0.69	1.26	1.03	0.66	0.79	0.79	0.36										
5Y	24	1.35	1.31	1.17	1.36	0.86	1.08	0.87	0.65										
	30	1.11	1.16	1.09	1.25	0.73	1.95	0.89	0.65										
	40	1.03	1.05	0.99	1.25	0.60	0.87	0.96	0.61										
	50	1.51	1.38	0.98	1.22	0.85	1.16	0.92	0.57										
	60	1.18	1.21	1.08	1.18	0.63	0.78	0.94	0.57										
5X + 5Y	24	1.37	0.90	1.22	1.29	0.98	0.87	0.99	0.63										
	30	1.29	0.83	1.22	1.19	0.95	0.82	1.03	0.59										
	40	1.11	0.82	1.03	1.32	0.78	0.84	0.92	0.61										
	50	1.19	0.72	1.10	1.07	0.83	0.71	1.00	0.48										
	60	1.15	0.73	1.14	1.03	0.80	0.66	0.97	0.47										

actions, deflections, and strains presented in Tables A to F, of course, remain unchanged.

Since a common set of modification factors was used for a large number of cases, perfect equilibrium could not be expected for all these cases. By comparing the modification factors for various load cases in Tables 2.4, 2.5 and 2.6 with the 30 ksi conditioning load factors, the degree to which equilibrium is satisfied can be ascertained. In general, agreement in the loaded span is better than in the unloaded span for point load cases. For the latter, this is due to the fact that at the midspan sections the force reverses sign, indicating for example a closing of the crack in a previous tension zone. These effects can produce changes in the effective stiffness. The modification factor procedure adopted was a compromise, which it was felt gave a more realistic set of effective stiffnesses to be used in converting strains to internal section forces.

For the experimental results, four different horizontal reference axes were considered in calculating moments at a section. These results are given in Tables G, H, I and J. An axis at the compression flange mid-depth (G) puts a greater weight on the experimental stresses measured in the tension steel while an axis at the tension flange steel (H) does just the opposite and emphasizes the experimental stresses measured in the concrete. Axes at the gross-section neutral axis (I) and the individual girder experimental neutral axes (J) tend to weight both the measured steel and concrete stresses more equally. If no experimental discrepancies existed, values for all four reference axes should be relatively close. The differences would be due to the fact that each individual girder could have an axial force existing, thus giving dif-

ferent values for the girder moment depending upon the axis about which moments are calculated. The total internal moment at the section should remain unchanged, however, since the total axial force on the section, which is equal to the sum of the individual girder axial forces, should be zero.

For the theoretical values, the tabulated moments in all cases (G, H, I, J) were obtained from CELL using the entire gross section neutral axis. Also in Volume II, all of the experimental and theoretical values used for purposes of comparison and discussion are taken from tables using this reference axis.

## 2.2 Point Loads on Girder Webs at Midspan (Working Stress)

As described in Volume I the loading program was divided into several phases in which initial conditioning loads were applied to create total maximum tensile stresses in the reinforcement of 24, 30, 40, 50 and 60 ksi. Each of these initial conditioning loads was then followed by a detailed sequence of point loads on the bridge.

One of the prime objectives of the test program was to determine the bridge response at working stress levels. The loading phase involving the initial application of conditioning loads to produce a maximum tensile stress of 30 ksi was chosen to be representative of response at working stress from the point of view of assessing actual box girder bridge behavior for design purposes. An advantage of using the 30 ksi stress level instead of the 24 ksi stress level was that 50% higher values of live load stresses could be registered for a total increase in the bridge model tensile stresses of only 6 ksi. All subsequent point loads in this phase, however, were chosen to produce maxi-

mum stresses, where applied, of the order of the working stresses, i.e. 24 to 30 ksi total maximum tensile stress in the reinforcement.

Because the 30 ksi stress level was chosen to be representative of the box girder bridge behavior for design purposes, a total of 19 point load combinations, 10 basic plus 9 additional point load combinations, were applied after the 30 ksi conditioning loads. However, only the 10 basic point load combinations were used after each of the 24, 40, 50 and 60 ksi conditioning loads. The 10 basic and 9 additional point load combinations are summarized for easy reference in Fig. 2.1.

As described in detail in Volume I, most of the experimental program was carried out for the bridge model with what will hereafter be termed normal support restraints. These consisted of simply supported end abutments and the center bent being supported by a single central column as shown in Figs. 1.1 and 1.2. However, in order to investigate the effect of torsional restraint at the center bent and longitudinal restraint at the two end diaphragms, the 10 basic point load cases were repeated for the 30 ksi working stress phase for each of these two support conditions.

Torsional restraint at the center bent was provided by adding vertical supports under girders 1 and 5 at center Section Z. Longitudinal restraint at the end diaphragms was provided by adding three horizontal reaction supports at each end in line with girders 1, 3, 5. Details of these support conditions are given in Figs. 5.2 and 5.3 of Volume I.

Detailed tabulations of theoretical and experimental results related to reactions, deflections, strains and moments for each of the



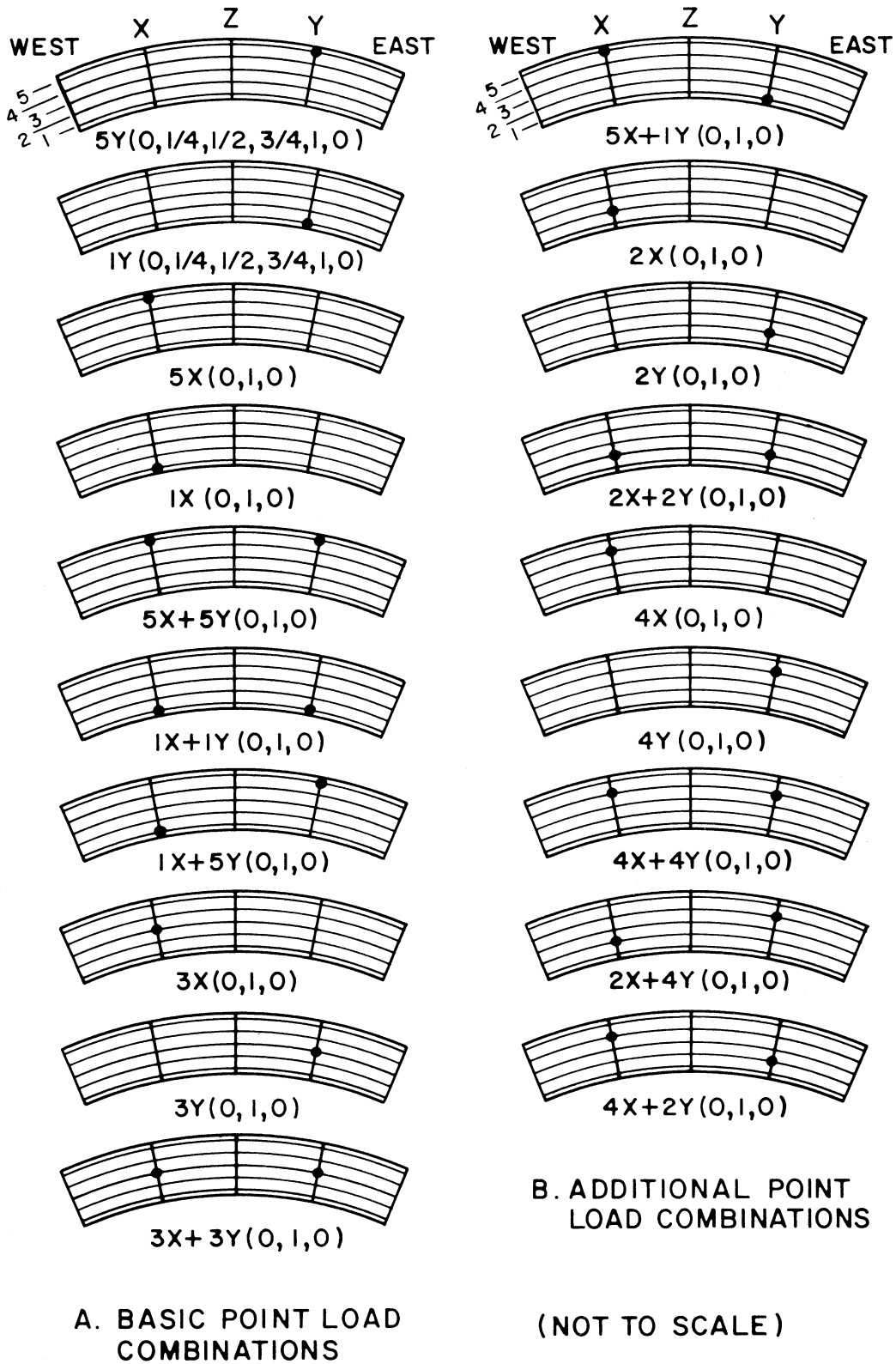


FIG. 2.1 BASIC AND ADDITIONAL POINT LOAD COMBINATIONS APPLIED AFTER CONDITIONING LOADS

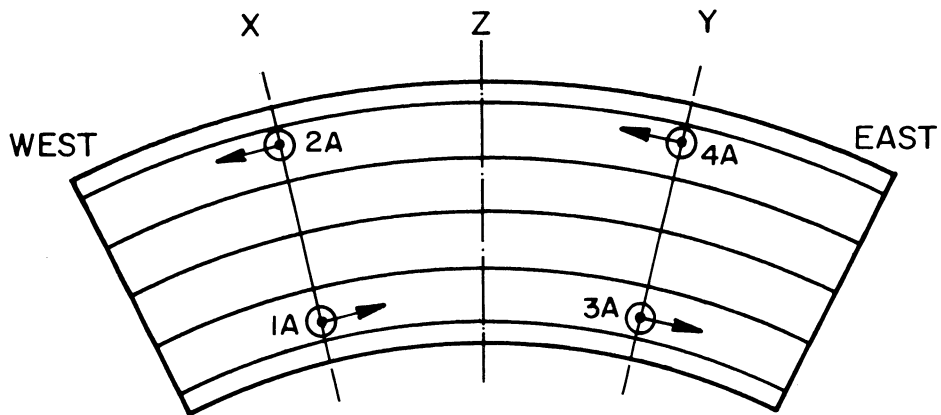
19 point load combinations with normal support restraints are given in Tables 1 to 7 inclusive on the Appendix. All theoretical and experimental values have been normalized for purposes of comparison to loads of 100 kips per span.

Detailed tabulations of only experimental results for point load cases for the torsional and longitudinal restraint cases are given in Table 8 to 15 inclusive in the Appendix. All values have been normalized to loads of 100 kips per span.

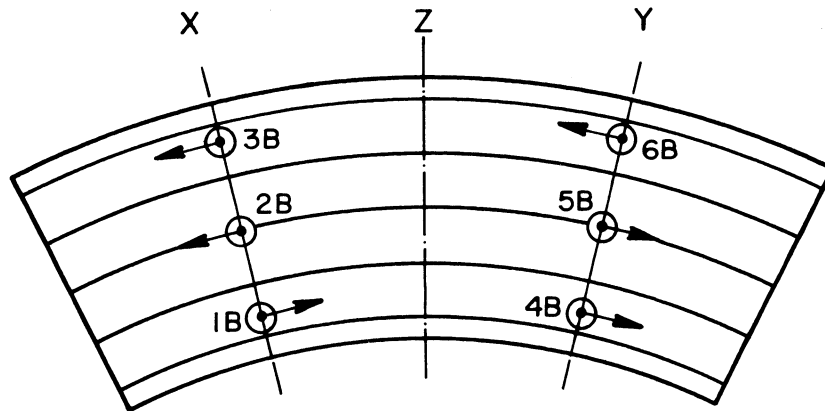
### 2.3 Truck and Construction Vehicle Loads

As described in Volume I, the model was loaded by scaled down versions of the standard AASHO HS 20-44 truck (total load = 72 kips) and a proposed overload construction vehicle class II (total load = 330 kips). All linear dimensions were reduced by the scale factor 1:2.82 and details of wheel positions in the model vehicles can be found in Volume I. Similarity required that the loads be reduced by a factor of 1:8 to produce the same stresses in the model as in the prototype. Thus for the model, the total load for each truck was 9.0 kips and for each construction vehicle was 41.25 kips. Using these loads, a study could be made of the bridge response due to actual design truck live loads placed at various positions on the bridge.

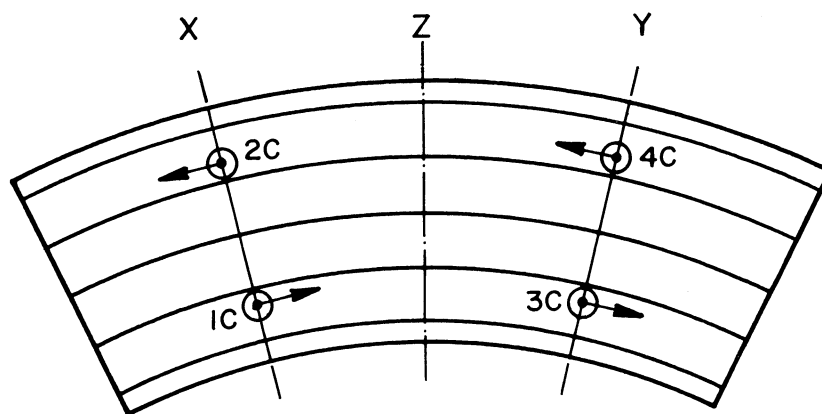
Fig. 2.2 shows the positions and directions of the truck and construction vehicle loads on the bridge. As described in Volume I, a total of 11 combinations of two lane truck loadings, 3 combinations of three lane truck loadings, and 8 combinations of construction vehicle loading were used. Because each vehicle had six wheels and the front wheels had smaller loads than the rear wheels, exact symmetry of loading



(a) TWO LANE TRUCK LOADING (EACH TRUCK = 9.0 KIPS NOMINAL)



(b) THREE LANE TRUCK LOADING (EACH TRUCK = 9.0 KIPS NOMINAL)



(c) CONSTRUCTION VEHICLE LOADING (EACH TRUCK = 41.25 KIPS NOMINAL)

**FIG. 2.2 POSITIONS AND DIRECTIONS OF TRUCK (9.0K) AND CONSTRUCTION VEHICLE (41.25K) LOADS ON THE BRIDGE**

about the bridge longitudinal and transverse centerlines was not maintained, Fig. 2.2.

Detailed tabulations of all experimental results and some theoretical results related to reactions, deflections, strains and moments for these loadings are given in Tables 16 to 23 inclusive in the Appendix.

#### 2.4 Conditioning Loads

As described in Volume I each loading phase was begun by applying initial conditioning loads to create a total maximum nominal tensile stress in the steel reinforcement of 24, 30, 40, 50 and 60 ksi. Each of these was then followed by a detailed sequence of 19 or 10 point load combinations having magnitudes chosen to produce total maximum stresses of the order of 24 to 30 ksi in the reinforcement.

Conditioning loads were obtained by applying equal loads over each of the five girders at both midspan Sections X and Y. Detailed tabulations of theoretical and experimental results related to reactions, deflections, strains and moments for each of the conditioning loads to bring the stress level up to 24, 30, 40, 50 and 60 ksi are given in Tables 24 and 25 in the Appendix. All theoretical values have been normalized for purposes of comparison to total loads of 100 kips per span.

#### 2.5 Point Loads After Conditioning Overloads

Detailed tabulations of theoretical and experimental results related to reactions, deflections, strains and moments are given in Tables 30 to 41 for working stress nominal point loads of 19.3 kips designed to give a total maximum stress of 30 ksi in the reinforcement in each case, subsequent to the application of the conditioning overloads which brought the maximum stress level to 40, 50 and 60 ksi. All theo-

retical and experimental values have been normalized for purposes of comparison to total loads of 100 kips per span. For completeness, reactions, deflections, strains and moments are also given in Tables 26 to 29 for normalized nominal point loads of 12.7 kips applied after the 24 ksi conditioning load.

## 2.6 Summary of Tables

As a convenient reference, a compact summary of all the tables included in the Appendix is given in Tables 2.7, 2.8 and 2.9 which follow this section. Pages in the Appendix are numbered to correspond directly to the Table number, i.e., 1A, 1B, 1C, etc. for easy reference.

TABLE 2.7 SUMMARY OF TABLES FOR WORKING STRESS POINT LOADS AFTER 30 KSI CONDITIONING LOAD

STRESS LEVEL	SUPPORT RESTRAINT	LOAD CASE	TABLE	REACTION	DEFLECTION	STRAINS AT SECTION				MOMENTS ABOUT			
				A	B	A	B	C	D	CF	TF	GNA	ENA
				A	B	C	D	E	F	G	H	I	J
WORKING STRESS OF 30 KSI	NORMAL	1X, 1Y, 1X + 1Y	1	●	●	●	●	●	●	●	●	●	●
		2X, 2Y, 2X + 2Y	2	●	●	●	●	●	●	●	●	●	●
		3X, 3Y, 3X + 3Y	3	●	●	●	●	●	●	●	●	●	●
		4X, 4Y, 4X + 4Y	4	●	●	●	●	●	●	●	●	●	●
		5X, 5Y, 5X + 5Y	5	●	●	●	●	●	●	●	●	●	●
		1X + 5Y, 5X + 1Y	6	●	●	●	●	●	●	●	●	●	●
		2X + 4Y, 4X + 2Y	7	●	●	●	●	●	●	●	●	●	●
	TORSIONAL	1X, 1Y, 1X + 1Y	8	○	○	○	○	○	○	○	○	○	○
		3X, 3Y, 3X + 3Y	9	○	○	○	○	○	○	○	○	○	○
		5X, 5Y, 5X + 5Y	10	○	○	○	○	○	○	○	○	○	○
		1X + 5Y	11	○	○	○	○	○	○	○	○	○	○
	LONGITUDINAL	1X, 1Y, 1X + 1Y	12	○	○	○	○	○	○	○	○	○	○
		3X, 3Y, 3X + 3Y	13	○	○	○	○	○	○	○	○	○	○
		5X, 5Y, 5X + 5Y	14	○	○	○	○	○	○	○	○	○	○
		1X + 5Y	15	○	○	○	○	○	○	○	○	○	○

- BOTH EXPERIMENTAL AND THEORETICAL RESULTS GIVEN
- ONLY EXPERIMENTAL RESULTS GIVEN
- CF COMPRESSION FLANGE
- TF TENSION FLANGE
- GNA UNCRACKED GROSS SECTION NEUTRAL AXIS
- ENA INDIVIDUAL GIRDER EXPERIMENTAL NEUTRAL AXIS

TABLE 2.8 SUMMARY OF TABLES FOR TWO LANE TRUCK LOADING, THREE LANE TRUCK LOADING AND CONSTRUCTION VEHICLE LOADING

STRESS LEVEL	SUPPORT RESTRAINT	LOAD CASE	T A B L E	REACTION	DEFLECTION	STRAINS AT SECTION				MOMENTS ABOUT			
				A	B	A	B	C	D	CF	TF	GNA	ENA
				A	B	C	D	E	F	G	H	I	J
AFTER 30 KSI CONDITIONING LOAD	NORMAL	3A+4A, 1A+2A+3A+4A	16	●	●	●	●	●	●	●	●	●	●
		1A + 2A	16	○	○	○	○	○	○	○	○	○	○
		4A, 2A + 4A	17	●	●	●	●	●	●	●	●	●	●
		2A	17	○	○	○	○	○	○	○	○	○	○
		1A, 3A, 1A + 3A	18	○	○	○	○	○	○	○	○	○	○
		1A + 4A, 2A + 3A	19	○	○	○	○	○	○	○	○	○	○
	NORMAL	4B + 5B + 6B 1B+2B+3B+4B+5B+6B	20	●	●	●	●	●	●	●	●	●	●
		1B + 2B + 3B	20	○	○	○	○	○	○	○	○	○	○
	NORMAL	4c, 2c + 4c	21	●	●	●	●	●	●	●	●	●	●
		2c	21	○	○	○	○	○	○	○	○	○	○
		1C, 3C, 1C + 3C	22	○	○	○	○	○	○	○	○	○	○
		1C + 4C, 2C + 3C	23	○	○	○	○	○	○	○	○	○	○

● BOTH EXPERIMENTAL AND THEORETICAL RESULTS GIVEN

○ ONLY EXPERIMENTAL RESULTS GIVEN

CF COMPRESSION FLANGE

TF TENSION FLANGE

GNA UNCRACKED GROSS SECTION NEUTRAL AXIS

ENA INDIVIDUAL GIRDER EXPERIMENTAL NEUTRAL AXIS

TABLE 2.9 SUMMARY OF TABLES FOR CONDITIONING LOADS AND WORKING STRESS POINT LOADS AFTER VARIOUS CONDITIONING LOADS

STRESS LEVEL	SUPPORT RESTRAINT	LOAD CASE	TABLE	REACTION		DEFLECTION		STRAINS AT SECTION				MOMENTS ABOUT				
				A	B	C	D	A	B	C	D	CF	TF	GNA	ENA	
				A	B	C	D	E	F	G	H	I	J			
COND. LOAD	NORMAL	24, 30, 40 KSI	24	●	●	●	●	●	●	●	●	●	●	●	●	
		50, 60 KSI	25	●	●	●	●	●	●	●	●	●	●	●	●	●
AFTER 24 KSI COND. LOAD	NORMAL	1X, 1Y, 1X + 1Y	26	●	●	●	●	●	●	●	●	●	●	●	●	
		3X, 3Y, 3X + 3Y	27	●	●	●	●	●	●	●	●	●	●	●	●	
		5X, 5Y, 5X + 5Y	28	●	●	●	●	●	●	●	●	●	●	●	●	●
		1X + 5Y	29	●	●	●	●	●	●	●	●	●	●	●	●	●
AFTER 40 KSI COND. LOAD	NORMAL	1X, 1Y, 1X + 1Y	30	●	●	●	●	●	●	●	●	●	●	●	●	
		3X, 3Y, 3X + 3Y	31	●	●	●	●	●	●	●	●	●	●	●	●	
		5X, 5Y, 5X + 5Y	32	●	●	●	●	●	●	●	●	●	●	●	●	●
		1X + 5Y	33	●	●	●	●	●	●	●	●	●	●	●	●	●
AFTER 50 KSI COND. LOAD	NORMAL	1X, 1Y, 1X + 1Y	34	●	●	●	●	●	●	●	●	●	●	●	●	
		3X, 3Y, 3X + 3Y	35	●	●	●	●	●	●	●	●	●	●	●	●	
		5X, 5Y, 5X + 5Y	36	●	●	●	●	●	●	●	●	●	●	●	●	●
		1X + 5Y	37	●	●	●	●	●	●	●	●	●	●	●	●	●
AFTER 60 KSI COND. LOAD	NORMAL	1X, 1Y, 1X + 1Y	38	●	●	●	●	●	●	●	●	●	●	●	●	
		3X, 3Y, 3X + 3Y	39	●	●	●	●	●	●	●	●	●	●	●	●	
		5X, 5Y, 5X + 5Y	40	●	●	●	●	●	●	●	●	●	●	●	●	●
		1X + 5Y	41	●	●	●	●	●	●	●	●	●	●	●	●	●

● BOTH EXPERIMENTAL AND THEORETICAL RESULTS GIVEN

○ ONLY EXPERIMENTAL RESULTS GIVEN

CF COMPRESSION FLANGE

TF TENSION FLANGE

GNA UNCRACKED GROSS SECTION NEUTRAL AXIS

ENA INDIVIDUAL GIRDER EXPERIMENTAL NEUTRAL AXIS



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Copies of most of the research reports [1-14] in the above reference list have been placed on file with the U. S. Department of Commerce and may be obtained on request for cost of reproduction by writing to the following address:

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APPENDIX

Tables of Theoretical and Experimental Results





TABLE 1A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 30 KSI COND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	1X		1Y		1X+1Y	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	8.07	6.61	41.39	23.67	49.45	29.86
2E	.05	1.21	9.57	24.24	9.62	27.20
3E	-1.31	-2.10	-.42	8.94	-1.73	5.92
4E	-2.91	-2.70	-1.17	-6.86	-4.08	-11.95
5E	-9.62	-10.09	-8.32	-10.45	-17.94	-17.79
1F	-16.14	.31	20.53	5.20	4.39	16.98
2F	11.60	25.65	48.71	34.27	60.32	67.19
3F	48.40	34.36	11.88	28.23	60.28	48.65
4F	20.66	7.79	-16.30	1.15	4.35	-.31
1W	37.19	30.38	8.03	6.47	45.23	36.41
2W	11.88	18.64	.12	3.46	11.99	20.26
3W	3.59	6.39	-1.36	-2.12	2.23	7.26
4W	.87	.89	-3.03	-3.62	-2.16	-1.92
5W	-12.33	-15.15	-0.62	-11.36	-21.95	-26.48
RE	-5.72	-7.07	41.05	39.54	35.32	33.24
RF	64.53	68.11	64.82	68.85	129.34	132.51
RW	41.20	41.15	-5.86	-7.17	35.34	35.53
SUMP	100.01	102.19	100.01	101.22	200.00	201.28
PX	-100.00	-100.00	0.	-.33	-100.00	-100.00
PY	0.	.10	-100.00	-100.00	-100.00	-99.05
SUMP	-100.00	-99.90	-100.00	-100.33	-200.00	-199.05
SUMR/SUMP	1.00	1.02	1.00	1.01	1.00	1.01
TW	-283.15	-279.96	-98.93	-109.97	-382.10	-380.69
MF	110.40	24.27	-110.50	-15.13	-.11	-53.73
TF	-83.22	-77.87	-84.56	-84.22	-167.78	-148.77
TE	-98.64	-95.99	-283.43	-255.59	-382.02	-345.93
ACTUAL PX		-19.40		-.06		-19.40
ACTUAL PY		.02		-19.07		-19.22

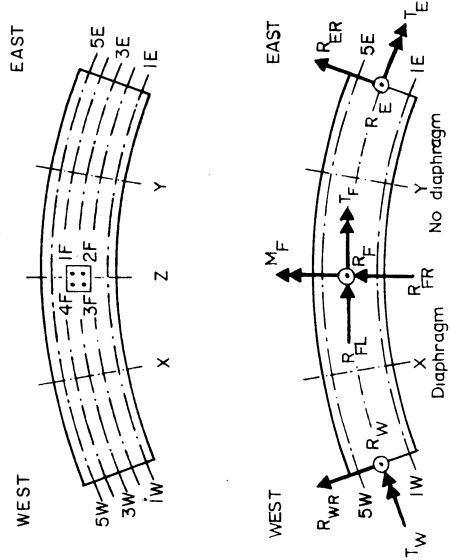
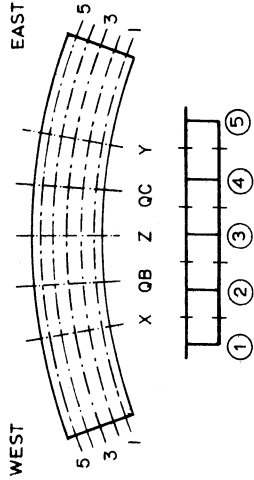


TABLE 1B

SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



DEFLECTION AT POINT	IX		IX+1Y		THEORY		EXPERM		E/T	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X	.942	1.178	1.25	.99	-.153	-.152	.99	.789	1.010	1.28
2X	.806	1.013	1.26	.99	-.198	-.195	.99	.608	.803	1.32
3X	.692	.889	1.28	1.01	-.243	-.244	1.01	.450	.614	1.37
4X	.605	.751	1.24	1.01	-.289	-.293	1.01	.316	.435	1.38
5X	.535	.654	1.22	1.02	-.337	-.342	1.02	.198	.270	1.36
1QB	.625	.818	1.31	1.20	-.090	-.107	1.20	.536	.664	1.24
2QB	.512	.628	1.23	1.05	-.151	-.158	1.05	.361	.447	1.24
3QB	.407	.497	1.22	1.00	-.206	-.207	1.00	.201	.262	1.30
4QB	.329	.434	1.32	.98	-.266	-.260	.98	.063	.099	1.57
5QB	.261	.293	1.12	1.05	-.328	-.344	1.05	-.067	-.079	1.19
1Z	.160	.179	1.12	1.22	.165	.201	1.22	.324	.395	1.22
2Z	.078	.083	1.07	1.11	.080	.089	1.11	.158	.171	1.09
4Z	-.063	-.067	1.07	1.16	-.063	-.073	1.16	-.126	-.141	1.12
5Z	-.129	-.155	1.20	1.14	-.128	-.146	1.14	-.257	-.290	1.13
1QC	-.087	-.087	.99	.934	.682	.934	1.37	.595	.857	1.44
2QC	-.148	-.156	1.05	.677	.529	.677	1.28	.381	.544	1.43
3QC	-.203	-.212	1.05	.398	.398	.455	1.14	.195	.277	1.42
4QC	-.263	-.286	1.08	.314	.314	.355	1.13	.050	.107	2.12
5QC	-.325	-.335	1.03	.277	.255	.277	1.09	-.070	-.032	.46
1Y	-.153	-.156	1.02	1.678	1.101	1.678	1.52	.948	1.516	1.60
2Y	-.197	-.192	.97	.825	.825	1.101	1.33	.629	.943	1.50
3Y	-.239	-.247	1.03	.658	.658	.787	1.20	.419	.608	1.45
4Y	-.283	-.327	1.15	.559	.559	.623	1.11	.276	.400	1.45
5Y	-.329	-.340	1.03	.504	.504	.586	1.16	.175	.281	1.61
LOAD PX	-100.0	-100.0		0.	0.	-.3		-100.0	-100.0	
LOAD PY	0.	.1		-100.0	-100.0			-100.0		
ACTUAL PX		-19.4		-.1						
ACTUAL PY		.0		-19.1						

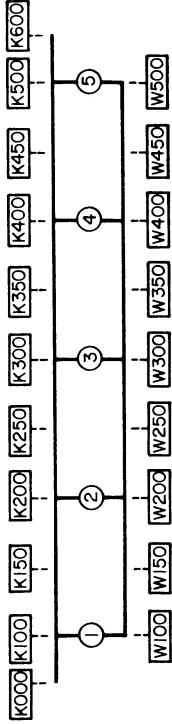
TABLE 1C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LCC.	1X		1Y		1X+1Y	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	-431	-339	56	52	-374	-294
K	K100	-341	-588	48	94	-292	-502
K	K150	-347	-354	42	48	-229	-294
K	K200	-271	-441	44	62	-201	-380
K	K250	-256	-256	44	50	-167	-195
K	K300	-245	-386	44	49	-176	-328
K	K350	-211	-314	51	36	-203	-267
K	K400	-211	-351	58	53	-176	-292
K	K450	-227	-275	58	26	-203	-231
K	K500	-227	-270	58	44	-203	-215
K	K600	-261	-184	58	24	-203	-157
W	W100	1365	1234	-178	-75	1187	1086
W	W150	857	816	-164	-82	895	736
W	W200	1059	1017	-181	-105	789	887
W	W250	919	755	-171	-72	625	793
W	W300	970	896	-187	-116	628	734
W	W350	723	677	-187	-93	628	583
W	W400	796	752	-187	-134	628	610
W	W450	765	659	-187	-87	628	647
W	W500	816	748	-187	-195	628	544
LOAD	PX (KIPS)	-100.0	-100.0	0.	-0.3	-100.0	-100.0
LOAD	PY (KIPS)	0.	.1	-100.0	-100.0	-100.0	-99.1
ACTUAL	PX (KIPS)	-19.4	-19.4	-19.1	-19.1	-19.4	-19.4
ACTUAL	PY (KIPS)	.0	.0	-19.1	-19.1	-19.2	-19.2

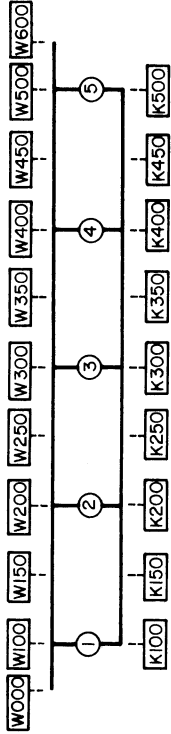
TABLE 1D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	IX		IY		IX+IY	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	184	414	473	327	658	749
W	W100	189	374	427	353	616	740
W	W150	327	367	259	259	593	677
W	W200	185	366	291	339	476	714
W	W250	340	364	206	227	405	559
W	W300	256	383	149	169	405	568
W	W350	147	307	222	145	370	414
W	W400	194	200	178	165	400	401
W	W450	169	198	298	171	428	420
W	W500	130	138	315	167	430	327
W	W600	114	126				316
K	K100	-91	-196	-197	-206	-289	-360
K	K150	-242	-220	-141	-179	-224	-399
K	K200	-82	-157	-182	-181	-328	-373
K	K250	-190	-217	-141	-141	-329	-326
K	K300	-100	-218	-66	-93	-166	-324
K	K350	-194	-195	-111	-111	-316	-324
K	K400	-66	-154	-105	-132	-172	-318
K	K450	-123	-135	-149	-149	-295	-298
K	K500	-58	-123	-129	-149	-187	-284
LOAD	PX (KIPS)	-100.0	-100.0	0.	-0.3	-100.0	-100.0
LOAD	PY (KIPS)	0.	.1	-100.0	-100.0	-100.0	-99.1
ACTUAL	PX (KIPS)	-19.4					-19.4
ACTUAL	PY (KIPS)	.0					-19.2

LOAD	PX (KIPS)	PY (KIPS)
ACTUAL	-19.4	-19.2

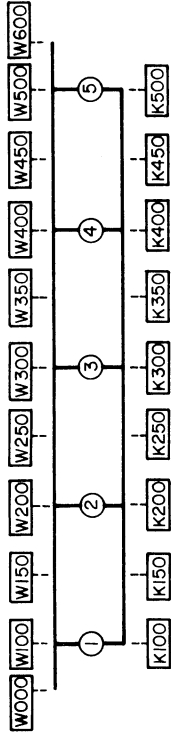
TABLE 1E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

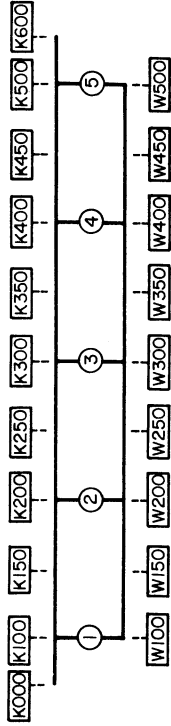


GAGE TYPE	GAGE LOC.	IX		IX+IY		IX		IX+IY		
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
W	W000	425	291	291	302	572	572	728	863	863
W	W100	387	271	267	279	481	503	666	761	778
W	W150		239	236		386	453		626	686
W	W200	280	319	321	203	403	396	484	733	730
W	W250		185	180		332	341		518	526
W	W300	154	224	223	241	327	322	396	573	568
W	W350		148	157		195	214		352	386
W	W400	231	204	209	121	159	164	353	397	417
W	W450		175	177		108	105		287	311
W	W500	304	185	183	95	69	69	400	266	259
W	W600	326	192	192	62	38	38	388	236	236
K	K100	-178	-168	-163	-137	-333	-341	-315	-434	-439
K	K150		-154	-131		-247	-289		-352	-372
K	K200	-134	-144	-142	-95	-206	-212	-229	-322	-335
K	K250		-114	-119		-202	-194		-287	-306
K	K300	-67	-104	-104	-95	-184	-181	-163	-266	-259
K	K350		-141	-134		-137	-141		-259	-258
K	K400	-110	-143	-144	-52	-105	-103	-163	-238	-237
K	K450		-174	-175		-140	-135		-311	-306
K	K500	-133	-171	-169	-37	-119	-118	-171	-287	-284
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	0.	-3	-100.0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	0.	.1	.1	-100.0	-100.0	-99.1	-100.0	-99.1	-99.1
ACTUAL	PX (KIPS)		-19.4			-1			-19.4	
ACTUAL	PY (KIPS)		.0			-19.1			-19.2	

TABLE 1F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

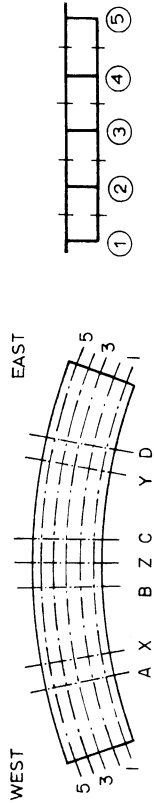
GAGE TYPE	GAGE LOC.	IX		IX+1Y		IX		IX+1Y	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	51	38	-407	-272	-407	-272	-355	-222
K	K100	43	60	-331	-400	-331	-400	-287	-357
K	K150	115	113	-545	-545	-545	-490	-215	-411
K	K200	37	65	-252	-461	-252	-460	-168	-418
K	K250	60	60	-329	-329	-329	-383	-275	-339
K	K300	38	53	-206	-313	-206	-325	-133	-286
K	K350	65	78	-360	-378	-360	-378	-227	-342
K	K400	37	53	-170	-256	-170	-242	-137	-227
K	K450	58	62	-377	-344	-377	-344	-262	-350
K	K500	42	40	-179	-269	-179	-267	-153	-258
K	K600	48	17	-201	-82	-201	-269	-76	-262
W	W100	-183	-58	1480	886	1480	934	1297	825
W	W150	-96	-88	1215	1225	1215	1225	983	1171
W	W200	-164	-114	1147	1133	1147	1110	753	1020
W	W250	-100	-87	853	820	853	820	495	758
W	W300	-177	-106	930	687	930	686	552	642
W	W350	-145	-138	596	594	596	594	450	513
W	W400	-163	-152	715	677	715	666	519	570
W	W450	-117	-127	534	517	534	517	614	431
W	W500	-176	-100	696	663	696	672	825	613
LOAD	PX (KIPS)	-100.0	-100.0	0.	-.3	-100.0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	0.	.1	-100.0	-100.0	-100.0	-100.0	-99.1	-99.1
ACTUAL	PX (KIPS)	-19.4		-.1		-19.1		-19.4	
ACTUAL	PY (KIPS)	.0		-19.1		-19.1		-19.2	

**TABLE 1G**

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



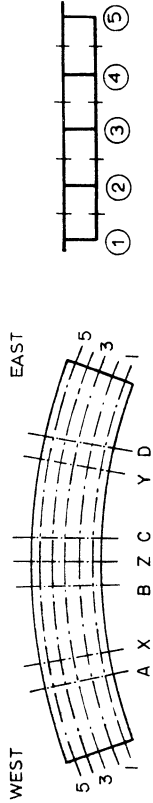
SECTION	GIRDER	IX		IX+IY		IY		IX+IY	
		THEORY K-FT	PCT	THEORY K-FT	PCT	THEORY K-FT	PCT	THEORY K-FT	PCT
A	1	116.1	20.8	87.1	17.4	-15.1	16.2	-5.0	7.7
A	2	139.9	25.1	132.3	26.5	-21.8	22.0	-13.4	20.7
A	3	119.5	21.4	115.6	23.1	-22.1	22.2	-15.5	23.9
A	4	107.1	19.2	104.2	20.9	-22.7	22.8	-17.8	27.5
A	5	74.6	13.4	60.5	12.1	-16.8	16.9	-13.1	20.2
A	SUM	557.1		499.7		-99.4		-64.8	
B	1	-27.6	15.6	-46.6	21.7	-56.6	22.9	-40.4	24.6
B	2	-42.4	24.0	-56.9	26.5	-63.5	25.8	-45.0	27.5
B	3	-53.3	30.2	-57.8	27.0	-39.7	16.1	-30.9	18.8
B	4	-34.5	19.6	-34.7	16.2	-48.1	19.5	-26.2	16.0
B	5	-18.8	10.6	-18.6	8.7	-38.6	15.7	-21.5	13.1
B	SUM	-176.6		-214.6		-246.6		-164.0	
C	1	-47.2	21.3	-34.5	21.0	-39.5	21.9	-67.4	30.3
C	2	-55.4	25.0	-43.6	26.5	-48.2	26.7	-68.7	30.9
C	3	-36.9	16.7	-32.1	19.5	-50.8	28.2	-50.8	22.8
C	4	-45.8	20.6	-30.8	18.8	-28.7	15.9	-27.3	12.3
C	5	-36.4	16.4	-23.4	14.2	-13.2	7.3	-8.4	3.8
C	SUM	-221.7		-154.4		-180.5		-222.5	
D	1	-16.4	16.8	-4.7	7.6	126.4	22.8	85.3	18.5
D	2	-21.8	22.4	-14.0	22.7	148.9	26.9	152.0	33.0
D	3	-21.6	22.2	-13.9	22.5	115.7	20.9	91.6	19.9
D	4	-21.6	22.2	-20.4	32.9	97.4	17.6	84.6	18.4
D	5	-15.9	16.3	-8.9	14.3	65.6	11.8	47.3	10.3
D	SUM	-97.3		-61.9		553.9		460.9	
LCAD	PX (KIPS)	-100.0		-100.0		0.		-100.0	
LCAD	PY (KIPS)	0.		0.		-100.0		-100.0	
ACTUAL	PX (KIPS)	-19.4		-19.4		-1		-19.4	
ACTUAL	PY (KIPS)	0.		0.		-19.1		-19.1	

TABLE IH

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



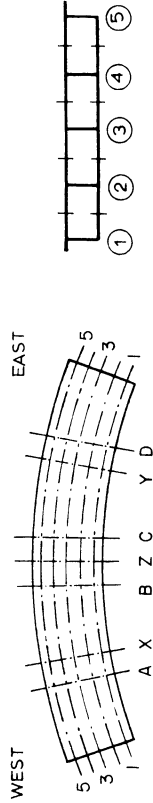
SECTION	GIRDER	IX			IY			IX+IY					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	116.1	20.8	132.5	24.8	-16.1	16.2	-22.1	28.2	100.0	21.8	112.9	25.2
A	2	139.9	25.1	117.5	22.0	-21.8	22.0	-17.7	22.7	118.0	25.8	97.9	21.8
A	3	119.5	21.4	99.5	18.6	-22.1	22.2	-15.6	19.9	97.4	21.3	81.7	18.2
A	4	107.1	19.2	108.7	20.3	-22.7	22.8	-13.5	17.2	84.4	18.4	92.6	20.6
A	5	74.6	13.4	76.0	14.2	-16.8	16.9	-9.4	12.0	57.8	12.6	63.5	14.2
A	SUM	557.1		534.2		-99.4		-78.3		457.7		448.5	
B	1	-27.6	15.6	-35.5	15.8	-56.6	22.9	-32.7	18.3	-80.1	20.0	-61.3	15.5
B	2	-42.4	24.0	-53.7	23.9	-63.5	25.8	-47.8	26.8	-100.5	25.0	-96.1	24.3
B	3	-53.3	30.2	-65.7	29.1	-39.7	16.1	-31.0	17.4	-87.6	21.8	-98.4	24.9
B	4	-34.5	19.6	-47.4	21.0	-48.1	19.5	-39.8	22.4	-78.4	19.5	-89.6	22.7
B	5	-18.8	10.6	-23.0	10.2	-38.6	15.7	-26.9	15.1	-54.7	13.6	-50.0	12.6
B	SUM	-176.6		-225.3		-246.6		-178.2		-401.3		-395.4	
C	1	-47.2	21.3	-25.6	14.5	-39.5	21.9	-56.7	23.9	-86.7	21.5	-70.1	18.3
C	2	-55.4	25.0	-37.9	21.6	-48.2	26.7	-66.3	27.9	-103.4	25.7	-96.7	25.3
C	3	-36.9	16.7	-35.1	19.9	-50.8	28.2	-54.0	22.7	-86.4	21.5	-82.2	21.5
C	4	-45.8	20.6	-45.2	25.7	-28.7	15.9	-35.7	15.0	-75.0	18.6	-76.7	20.1
C	5	-36.4	16.4	-32.0	18.2	-13.2	7.3	-25.1	10.5	-50.8	12.6	-56.2	14.7
C	SUM	-221.7		-175.8		-180.5		-237.9		-402.4		-382.0	
D	1	-16.4	16.8	-20.4	22.3	126.4	22.8	102.9	21.0	110.0	24.1	87.5	19.7
D	2	-21.8	22.4	-22.7	24.8	148.9	26.9	126.1	25.7	127.0	27.8	110.7	25.0
D	3	-21.6	22.2	-18.9	20.7	115.7	20.9	100.9	20.6	94.1	20.6	88.9	20.0
D	4	-21.6	22.2	-17.4	19.0	97.4	17.6	86.1	17.5	75.8	16.6	82.7	18.6
D	5	-15.9	16.3	-12.2	13.3	65.6	11.8	74.4	10.9	49.7	10.9	74.0	16.7
D	SUM	-97.3		-91.5		553.9		490.4		456.6		443.9	
LOAD	PX (KIPS)	-100.0		-100.0		0.		-.3		-100.0		-100.0	
LOAD	PY (KIPS)	0.		.1		-100.0		-100.0		-100.0		-99.1	
ACTUAL	PX (KIPS)			-19.4		-.1		-19.4		-19.4		-19.4	
ACTUAL	PY (KIPS)			.0		.0		.0		.0		.0	



TABLE 11

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

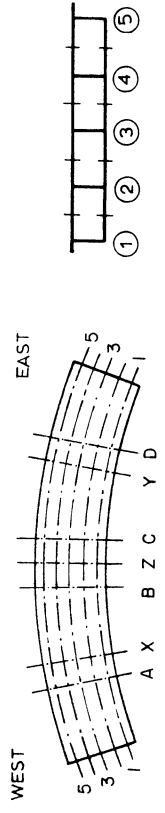


SECTION	GIRDER	IX			IY			IX+IY					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	116.1	20.8	107.4	20.8	-15.1	16.2	-12.6	17.8	100.0	21.8	93.0	21.8
A	2	139.9	25.1	125.7	24.4	-21.8	22.0	-15.4	21.7	118.0	25.8	106.7	25.0
A	3	119.5	21.4	108.5	21.1	-22.1	22.2	-15.5	21.9	97.4	21.3	88.1	20.6
A	4	107.1	19.2	106.2	20.6	-22.7	22.8	-15.9	22.4	84.4	18.4	85.8	20.1
A	5	74.6	13.4	67.4	13.1	-16.8	16.9	-11.4	16.1	57.8	12.6	53.3	12.5
A	SUM	557.1		515.2		-99.4		-70.8		457.7		426.9	
B	1	-27.6	15.6	-40.5	18.3	-56.6	22.9	-36.1	21.0	-80.1	20.0	-73.7	18.7
B	2	-42.4	24.0	-55.2	25.0	-63.5	25.8	-46.6	27.1	-100.5	25.0	-99.3	25.3
B	3	-53.3	30.2	-62.2	28.2	-39.7	16.1	-30.9	18.0	-87.6	21.8	-95.0	24.2
B	4	-34.5	19.6	-41.7	18.9	-48.1	19.5	-33.7	19.6	-78.4	19.5	-78.5	20.0
B	5	-18.8	10.6	-21.0	9.5	-38.6	15.7	-24.5	14.3	-54.7	13.6	-46.8	11.9
B	SUM	-176.6		-220.6		-246.6		-171.9		-401.3		-393.4	
C	1	-47.2	21.3	-29.5	17.3	-39.5	21.9	-61.5	26.6	-86.7	21.5	-84.9	21.8
C	2	-55.4	25.0	-40.5	23.7	-48.2	26.7	-67.4	29.2	-103.4	25.7	-104.2	26.7
C	3	-36.9	16.7	-33.8	19.8	-50.8	28.2	-52.6	22.8	-86.4	21.5	-83.8	21.5
C	4	-45.8	20.6	-38.8	22.7	-28.7	15.9	-32.0	13.8	-75.0	18.6	-71.0	18.2
C	5	-36.4	16.4	-28.2	16.5	-13.2	7.3	-17.6	7.6	-50.8	12.6	-46.3	11.9
C	SUM	-221.7		-170.8		-180.5		-231.1		-402.4		-390.3	
D	1	-16.4	16.8	-11.7	15.6	126.4	22.8	93.2	19.7	110.0	24.1	84.4	19.6
D	2	-21.8	22.4	-17.9	23.8	148.9	26.9	140.5	29.6	127.0	27.8	127.9	29.7
D	3	-21.6	22.2	-16.1	21.5	115.7	20.9	95.8	20.2	94.1	20.6	86.4	20.0
D	4	-21.6	22.2	-19.0	25.3	97.4	17.6	85.3	18.0	75.8	16.6	76.6	17.7
D	5	-15.9	16.3	-10.4	13.8	65.6	11.8	59.4	12.5	49.7	10.9	56.0	13.0
D	SUM	-97.3		-75.1		553.9		474.3		456.6		431.3	
LOAD	PX (KIPS)	-100.0		-100.0		0.		-.		-100.0		-100.0	
LJAD	PY (KIPS)	0.		.1		-100.0		-100.0		-100.0		-99.1	
ACTUAL	PX (KIPS)			-19.4		-.		-.		-19.4		-19.4	
ACTUAL	PY (KIPS)			.0		-19.1		-19.1		-19.1		-19.2	

TABLE 1J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	NORMALIZED POINT LOADS AT											
		1X			1Y			1X+1Y					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	116.1	20.8	101.4	19.9	-16.1	16.2	-14.5	19.6	100.0	21.8	88.1	20.9
A	2	139.9	25.1	127.7	25.0	-21.8	22.0	-15.1	20.4	118.0	25.8	108.8	25.8
A	3	119.5	21.4	110.9	21.7	-22.1	22.2	-15.5	20.9	97.4	21.3	89.7	21.3
A	4	107.1	19.2	105.7	20.7	-22.7	22.8	-16.6	22.5	84.4	18.4	84.6	20.1
A	5	74.6	13.4	64.6	12.7	-16.8	16.9	-12.4	16.7	57.8	12.6	50.3	11.9
A	SUM	557.1		510.3		-99.4		-74.1		457.7		421.5	
B	1	-27.6	15.6	-42.8	19.4	-56.6	22.9	-37.6	22.0	-80.1	20.0	-80.0	20.2
B	2	-42.4	24.0	-56.0	25.4	-63.5	25.8	-46.0	26.9	-100.5	25.0	-101.0	25.5
B	3	-53.3	30.2	-60.7	27.5	-39.7	16.1	-30.9	18.1	-87.6	21.8	-93.5	23.6
B	4	-34.5	19.6	-40.2	18.3	-48.1	19.5	-32.3	18.9	-78.4	19.5	-75.3	19.0
B	5	-18.8	10.6	-20.6	9.4	-39.6	15.7	-24.0	14.1	-54.7	13.6	-46.0	11.6
B	SUM	-176.6		-220.3		-246.6		-170.8		-401.3		-395.8	
C	1	-47.2	21.3	-31.1	18.3	-39.5	21.9	-63.1	27.2	-86.7	21.5	-91.3	22.9
C	2	-55.4	25.0	-41.9	24.6	-48.2	26.7	-67.8	29.2	-103.4	25.7	-108.2	27.2
C	3	-36.9	16.7	-33.0	19.4	-50.8	28.2	-51.9	22.3	-86.4	21.5	-84.7	21.3
C	4	-45.8	20.6	-36.7	21.6	-28.7	15.9	-30.6	13.2	-75.0	18.6	-68.6	17.2
C	5	-36.4	16.4	-27.5	16.2	-13.2	7.3	-18.9	8.1	-50.8	12.6	-45.6	11.4
C	SUM	-221.7		-170.2		-180.5		-232.4		-402.4		-398.3	
D	1	-16.4	16.8	-13.0	17.3	126.4	22.8	90.7	19.3	110.0	24.1	83.5	19.5
D	2	-21.8	22.4	-17.2	22.8	148.9	26.9	144.4	30.7	127.0	27.8	132.7	31.0
D	3	-21.6	22.2	-15.8	20.9	115.7	20.9	94.6	20.1	94.1	20.6	85.8	20.1
D	4	-21.6	22.2	-19.6	26.0	97.4	17.6	85.0	18.1	75.8	16.6	74.7	17.5
D	5	-15.9	16.3	-9.8	13.1	65.6	11.8	55.0	11.7	49.7	10.9	51.1	11.9
D	SUM	-97.3		-75.4		553.9		469.8		456.6		427.8	
LOAD	PX (KIPS)	-100.0		-100.0		0.		-0.3		-100.0		-100.0	
LOAD	PY (KIPS)	0.		.1		-100.0		-100.0		-100.0		-99.1	
ACTUAL	PX (KIPS)			-19.4				.1				-19.4	
ACTUAL	PY (KIPS)			.0				-19.1				-19.2	

TABLE 2A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 30 KSI COND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	2X		2Y		2X+2Y	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	3.98	4.42	13.85	10.26	17.83	14.06
2E	-0.69	-1.75	17.88	20.62	17.20	17.73
3E	-1.31	-2.04	6.48	9.94	5.16	6.99
4E	-2.34	.91	1.64	-5.80	-.69	-2.22
5E	-6.42	-7.69	.03	2.64	-6.39	-5.63
1F	-9.65	-1.24	28.99	29.74	19.34	21.50
2F	4.33	7.55	43.57	46.45	47.90	40.32
3F	43.04	36.15	4.50	3.94	47.54	45.61
4F	29.06	25.34	-10.08	-9.72	18.98	27.22
1W	17.66	18.47	3.90	3.18	21.57	21.43
2W	11.73	10.87	-.63	2.02	11.09	11.22
3W	6.76	5.77	-1.35	-2.59	5.40	6.66
4W	4.59	5.21	-2.42	-2.91	2.17	2.15
5W	-.74	.63	-6.36	-6.77	-7.10	-6.70
RE	-6.78	-6.15	39.88	37.66	33.11	30.93
RF	66.78	67.80	66.98	70.41	133.76	134.65
PW	40.00	40.95	-6.86	-7.07	33.13	34.76
SUMR	100.00	102.60	100.00	101.00	200.00	200.34
PX	-100.00	-100.00	0.	.01	-100.00	-100.00
PY	0.	.06	-100.00	-100.00	-100.00	-96.16
SUMP	-100.00	-99.94	-100.00	-99.99	-200.00	-196.16
SUMR/SUMP	1.00	1.03	1.00	1.01	1.00	1.02
TW	-113.05	-106.36	-57.40	-63.89	-170.48	-168.09
MF	116.15	82.77	-117.22	-122.96	-1.07	16.52
TF	-41.93	-29.40	-43.76	-45.54	-85.68	-55.81
TE	-57.76	-55.47	-112.90	-107.19	-170.66	-152.65
ACTUAL PX		-19.28		0.		-19.67
ACTUAL PY		.01		-19.06		-18.91

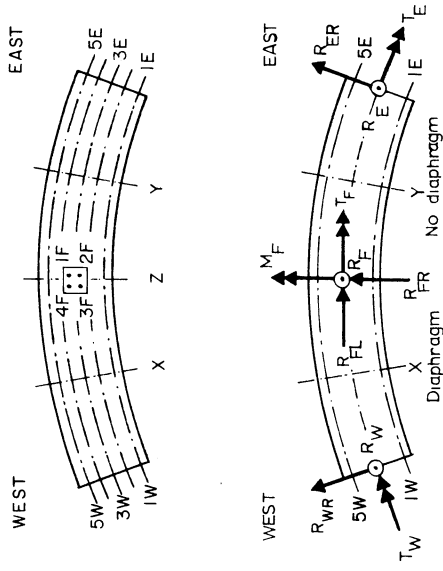
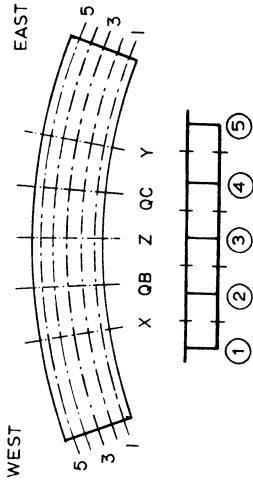


TABLE 2B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



DEFLECTION AT POINT	2X		2Y		2X+2Y	
	THEORY	EXPERM	E/T	THEORY	EXPERM	E/T
1X	.806	1.070	1.33	-.197	-.293	1.49
2X	.790	1.065	1.35	-.224	-.333	1.49
3X	.740	1.017	1.37	-.251	-.366	1.46
4X	.698	.951	1.36	-.281	-.408	1.45
5X	.673	.888	1.32	-.311	-.444	1.43
1QB	.519	.683	1.32	-.150	-.227	1.51
2QB	.483	.627	1.30	-.185	-.263	1.43
3QB	.434	.574	1.32	-.214	-.292	1.37
4QB	.401	.547	1.36	-.250	-.315	1.26
5QB	.375	.470	1.25	-.285	-.379	1.33
1Z	.086	.105	1.22	.087	.112	1.29
2Z	.042	.042	.99	.044	.047	1.08
4Z	-.028	-.034	1.21	-.030	-.030	1.03
5Z	-.059	-.068	1.15	-.061	-.068	1.11
1QC	-.148	-.189	1.28	.534	.740	1.39
2QC	-.182	-.229	1.26	.523	.740	1.41
3QC	-.212	-.260	1.23	.436	.584	1.34
4QC	-.248	-.301	1.21	.380	.529	1.39
5QC	-.284	-.352	1.24	.353	.486	1.38
1Y	-.198	-.270	1.37	.825	.417	.50
2Y	-.224	-.301	1.34	.909	1.361	1.50
3Y	-.249	-.325	1.31	.735	.218	.30
4Y	-.277	-.371	1.34	.646	.869	1.35
5Y	-.306	-.391	1.28	.614	.847	1.38
LOAD PX	-100.0	-100.0		0.	0.	
LOAD PY	0.	.1		-100.0	-100.0	
ACTUAL PX		-19.3		0.	0.	
ACTUAL PY		.0		-19.1	-19.1	
				-100.0	-100.0	
				-100.0	-96.2	
				-19.7	-18.9	

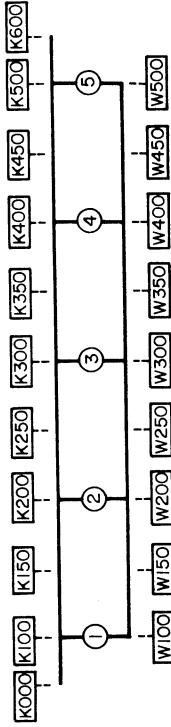
TABLE 20

SUMMARY OF STRAINS (MICR IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	2X		2Y		2X+2Y	
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
K	K000	-339	-290	62	78	-276	-238
K	K100	-310	-496	53	158	-431	-417
K	K150	-338	-339	65	48	-277	-279
K	K200	-269	-444	46	104	-223	-356
K	K250	-286	-288	58	62	-229	-229
K	K300	-257	-390	48	87	-209	-330
K	K350	-225	-328	47	76	-177	-276
K	K400	-293	-385	60	96	-246	-325
K	K450	-243	-342	54	76	-189	-292
K	K500	-272	-298	62	85	-210	-244
K	K600	-195	-195	52	52	-165	-165
W	W100	1188	1096	-196	-187	991	926
W	W150	852	776	-179	-163	859	711
W	W200	1038	956	-179	-201	828	800
W	W250	909	778	-196	-160	764	646
W	W300	1014	958	-184	-215	817	785
W	W350	858	766	-200	-180	673	638
W	W400	887	834	-196	-215	684	667
W	W450	882	734	-200	-169	687	667
W	W500	882	874	-200	-272	685	679
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	.1	-100.0	-100.0	-100.0	-96.2
ACTUAL	PX (KIPS)	-19.3		0.		-19.7	
ACTUAL	PY (KIPS)	.0		-19.1		-18.9	

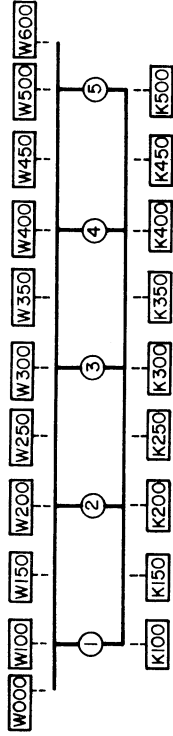
TABLE 2D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



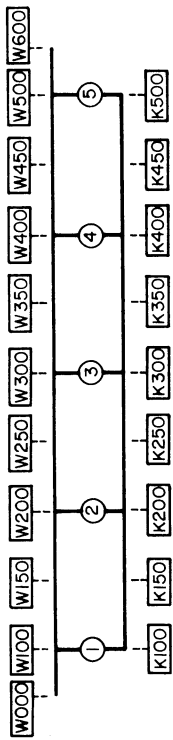
GAGE TYPE	GAGE LOC.	2X		2Y		2X+2Y	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	186	333	465	320	651	648
W	W100	190	307	416	335	606	652
W	W150	277	317	275	315	546	622
W	W200	210	354	320	339	530	697
W	W250	344	379	233	253	479	621
W	W300	296	401	182	217	439	636
W	W350	285	338	186	217	467	545
W	W400	183	242	256	217	441	474
W	W450	209	244	219	247	487	496
W	W500	160	185	326	217	491	398
W	W600	144	176	347	222	491	398
K	K100	-89	-164	-190	-207	-280	-352
K	K150	-197	-183	-153	-218	-247	-389
K	K200	-93	-177	-199	-192	-247	-359
K	K250	-206	-218	-180	-159	-196	-352
K	K300	-116	-224	-79	-145	-203	-351
K	K350	-197	-198	-121	-155	-203	-338
K	K400	-82	-154	-142	-162	-215	-307
K	K450	-138	-147	-161	-164	-293	-301
K	K500	-72	-132	-142	-153	-215	-274
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	.1	-100.0	-100.0	-100.0	-96.2
ACTUAL	PX (KIPS)	-19.3	0.	0.	0.	-19.7	-19.7
ACTUAL	PY (KIPS)	.0	-19.1	-19.1	-19.1	-18.9	-18.9

TABLE 2E

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

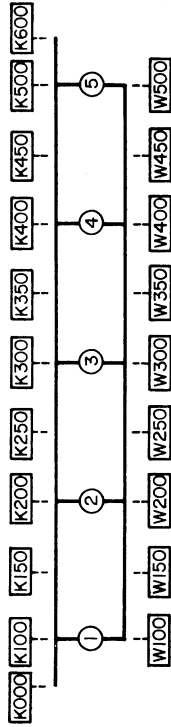


NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	2X		2Y		2X+2Y	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	437	281	238	394	676	693
W	W100	394	253	228	342	622	615
W	W150	232	236	252	344	550	589
W	W200	297	304	252	462	481	771
W	W250	186	186	301	405	421	591
W	W300	180	226	160	411	428	662
W	W350	268	177	121	277	465	457
W	W400	197	248	92	241	370	527
W	W450	344	205	121	179	461	395
W	W500	369	214	92	123	364	357
W	W600	220	220	110	110	461	349
K	K100	-179	-175	-110	-207	-290	-371
K	K150	-142	-165	-114	-209	-256	-361
K	K200	-78	-141	-118	-255	-196	-418
K	K250	-127	-163	-70	-242	-197	-403
K	K300	-151	-127	-52	-228	-204	-356
K	K350	-201	-154	0.	-169	-280	-330
K	K400	-176	-158	-100.0	-117	-276	-276
K	K450	-100.0	-197	-100.0	-136	-340	-334
K	K500	0.	-174	-100.0	-113	-289	-286
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	.1	-100.0	-100.0	-100.0	-96.2
ACTUAL	PX (KIPS)	-19.3	0.	0.	0.	-19.7	-19.7
ACTUAL	PY (KIPS)	0.	-19.1	-19.1	-19.1	-18.9	-18.9

TABLE 2F

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION D

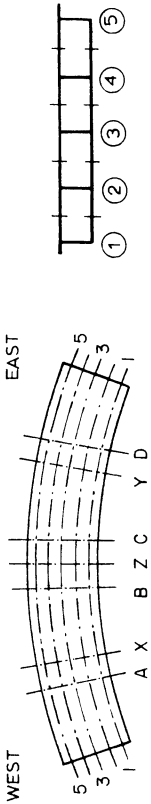
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	2X		2Y		2X+2Y	
		THEORY	MEASR ADJUST	THEORY	MEASR ADJUST	THEORY	MEASR ADJUST
K	K000	56	35	-342	-205	-285	-156
K	K100	48	63	-296	-374	-248	-291
K	K150	136	131	-241	-607	-200	-450
K	K200	41	92	-233	-440	-190	-330
K	K250	70	80	-187	-351	-146	-258
K	K300	42	72	-233	-387	-190	-284
K	K350	105	77	-187	-450	-146	-325
K	K400	40	85	-194	-335	-147	-232
K	K450	125	128	-215	-501	-162	-345
K	K500	46	77	-215	-346	-162	-246
K	K600	52	23	-215	-105	-162	-76
W	W100	-202	-123	1327	919	1124	694
W	W150	-164	-149	1055	1207	873	917
W	W200	-181	-185	1030	1068	836	769
W	W250	-174	-158	793	1010	616	745
W	W300	-194	-177	787	904	596	644
W	W350	-177	-174	823	765	456	503
W	W400	-177	-209	842	876	576	570
W	W450	-191	-181	842	695	456	446
W	W500	-172	-182	842	823	576	584
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	.1	-100.0	-100.0	-100.0	-96.2
ACTUAL	PX (KIPS)	-19.3	0.	0.	0.	-19.7	-19.7
ACTUAL	PY (KIPS)	.0	-19.1	-19.1	-19.1	-18.9	-18.9



TABLE 2G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH



RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

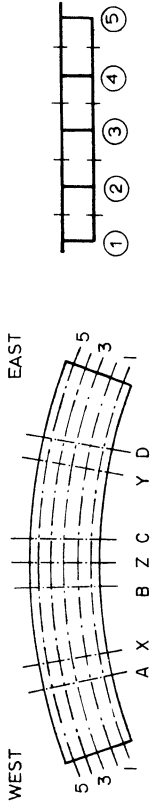
SECTION	GIRDER	2X			2Y			2X+2Y			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	103.3	79.4	15.4	-17.7	-12.7	11.1	85.7	18.8	67.4	16.0
A	2	137.9	127.1	24.6	-23.9	-24.6	21.5	114.1	25.1	106.3	25.2
A	3	125.7	124.8	24.1	-24.0	-28.0	24.5	101.8	22.4	101.5	24.0
A	4	115.5	116.5	22.5	-24.4	-29.6	25.9	91.1	20.0	92.9	22.0
A	5	80.5	69.6	13.4	-18.0	-19.5	17.1	62.5	13.7	54.5	12.9
A	SUM	563.0	517.4		-107.8	-114.4		455.2		422.5	
B	1	-27.6	-38.9	17.7	-51.3	-39.3	21.3	-78.9	17.9	-78.1	19.3
B	2	-46.6	-54.2	24.6	-63.0	-46.9	25.4	-108.6	24.6	-100.3	24.8
B	3	-60.8	-61.4	27.8	-42.7	-36.7	19.9	-100.7	22.8	-97.7	24.1
B	4	-41.6	-41.2	18.7	-50.6	-33.8	18.3	-91.2	20.7	-76.1	18.8
B	5	-22.9	-24.8	11.2	-39.4	-27.8	15.1	-62.1	14.1	-52.7	13.0
B	SUM	-199.5	-220.6		-247.1	-184.4		-441.5		-404.9	
C	1	-48.6	-33.3	19.3	-33.4	-47.2	19.7	-81.1	18.4	-83.2	19.7
C	2	-59.2	-42.3	24.5	-54.6	-70.6	29.5	-111.7	25.3	-113.7	26.9
C	3	-42.4	-33.4	19.3	-61.5	-63.5	26.5	-100.9	22.8	-98.0	23.2
C	4	-53.2	-36.2	21.0	-36.5	-40.2	16.7	-88.7	20.1	-79.7	18.9
C	5	-41.9	-27.5	15.9	-17.3	-18.2	7.6	-59.2	13.4	-47.9	11.3
C	SUM	-245.3	-172.6		-203.3	-239.7		-441.5		-422.5	
D	1	-18.1	-10.4	10.6	113.0	81.0	15.7	94.9	20.8	61.7	16.8
D	2	-24.1	-23.6	24.0	142.1	148.2	28.6	118.0	25.9	109.4	29.7
D	3	-23.6	-22.9	23.2	126.7	117.6	22.7	103.1	22.7	84.0	22.8
D	4	-23.5	-27.1	27.6	107.8	110.0	21.3	84.3	18.5	72.5	19.7
D	5	-17.2	-14.3	14.6	72.2	60.8	11.7	55.0	12.1	40.9	11.1
D	SUM	-106.6	-98.3		561.8	517.5		455.3		368.6	
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.	0.	0.	-100.0	-100.0		-100.0		-96.2	
ACTUAL	PX (KIPS)	0.	-19.3	0.	0.	0.		-19.7		-18.9	
ACTUAL	PY (KIPS)	0.	0.	0.	-19.1	-19.1		-18.9		-18.9	

TABLE 2H:

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

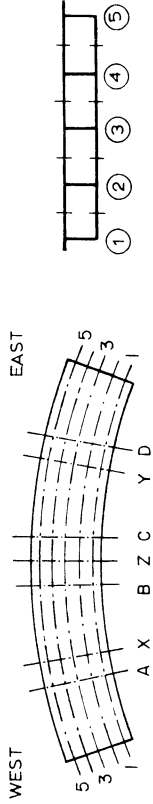


SECTION	GIRDER	NORMALIZED POINT LOADS AT											
		2X		2Y		2X+2Y							
		THEORY K-FT	PCT	THEORY K-FT	PCT	THEORY K-FT	PCT						
A	1	103.3	18.4	116.9	21.8	-17.7	16.4	-37.7	28.2	85.7	18.8	97.2	21.7
A	2	137.9	24.5	117.4	21.9	-23.9	22.1	-24.0	18.0	114.1	25.1	97.3	21.7
A	3	125.7	22.3	104.7	19.6	-24.0	22.2	-23.9	17.9	101.8	22.4	87.0	19.4
A	4	115.5	20.5	114.5	21.4	-24.4	22.6	-27.1	20.3	91.1	20.0	97.2	21.7
A	5	80.5	14.3	81.7	15.3	-18.0	16.7	-20.8	15.6	62.5	13.7	68.7	15.4
A	SUM	563.0		535.2		-107.8		-133.5		455.2		447.3	
B	1	-27.6	13.8	-29.5	13.2	-51.3	20.8	-36.0	17.0	-78.9	17.9	-61.2	14.9
B	2	-46.6	23.4	-54.3	24.4	-63.0	25.5	-54.5	25.6	-108.6	24.6	-103.2	25.1
B	3	-60.8	30.5	-66.8	30.0	-42.7	17.3	-46.1	21.7	-100.7	22.8	-106.0	25.7
B	4	-41.6	20.9	-47.7	21.5	-50.6	20.5	-48.5	22.8	-91.2	20.7	-91.9	22.3
B	5	-22.9	11.5	-24.1	10.8	-39.4	16.0	-27.5	12.9	-62.1	14.1	-49.4	12.0
B	SUM	-199.5		-222.4		-247.1		-212.7		-441.5		-411.6	
C	1	-48.6	19.8	-28.3	13.8	-33.4	16.4	-34.6	14.9	-81.1	18.4	-60.8	14.0
C	2	-59.2	24.1	-48.5	23.6	-54.6	26.9	-69.6	29.9	-111.7	25.3	-115.7	26.7
C	3	-42.4	17.3	-44.3	21.6	-61.5	30.3	-67.3	28.9	-100.9	22.8	-111.8	25.8
C	4	-53.2	21.7	-50.3	24.5	-36.5	18.0	-38.6	16.6	-88.7	20.1	-89.2	20.6
C	5	-41.9	17.1	-34.0	16.6	-17.3	8.5	-22.7	9.7	-59.2	13.4	-56.5	13.0
C	SUM	-245.3		-205.4		-203.3		-232.9		-441.5		-434.0	
D	1	-18.1	17.0	-21.2	16.4	113.0	20.1	105.0	18.8	94.9	20.8	79.9	19.6
D	2	-24.1	22.6	-28.7	22.2	142.1	25.3	128.4	23.0	118.0	25.9	95.5	23.4
D	3	-23.6	22.2	-25.1	19.5	126.7	22.6	117.7	21.1	103.1	22.7	85.8	21.0
D	4	-23.5	22.1	-29.9	23.2	107.8	19.2	110.4	19.8	84.3	18.5	78.2	19.2
D	5	-17.2	16.2	-24.2	18.7	72.2	12.8	97.0	17.4	55.0	12.1	68.7	16.8
D	SUM	-106.6		-129.2		561.8		558.5		455.3		408.0	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-96.2	
ACTUAL	PX (KIPS)	0.		-19.3		0.		0.		-19.7		-18.9	
ACTUAL	PY (KIPS)	0.		0.		-19.1		-19.1		0.		0.	

TABLE 21

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

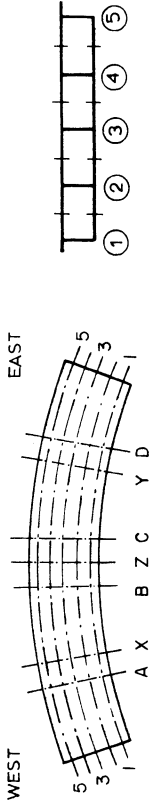
RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	2X			2Y			2X+2Y			
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	
A	1	103.3	18.4	96.2	18.3	-17.7	16.4	-23.9	19.4	85.7	18.8
A	2	137.9	24.5	122.8	23.4	-23.9	22.1	-24.4	19.8	114.1	25.1
A	3	125.7	22.3	115.9	22.1	-24.0	22.2	-26.2	21.3	101.8	22.4
A	4	115.5	20.5	115.7	22.0	-24.4	22.6	-28.5	23.2	91.1	20.0
A	5	80.5	14.3	75.0	14.3	-18.0	16.7	-20.1	16.4	62.5	13.7
A	SUM	563.0		525.5		-107.8		-123.0		455.2	
B	1	-27.6	13.8	-33.7	15.2	-51.3	20.8	-37.5	18.7	-78.9	17.9
B	2	-46.6	23.4	-54.3	24.5	-63.0	25.5	-51.1	25.5	-108.6	24.6
B	3	-60.8	30.5	-64.4	29.0	-42.7	17.3	-41.9	21.0	-100.7	22.8
B	4	-41.6	20.9	-44.9	20.2	-50.6	20.5	-41.9	21.0	-91.2	20.7
B	5	-22.9	11.5	-24.4	11.0	-39.4	16.0	-27.6	13.8	-62.1	14.1
B	SUM	-199.5		-221.7		-247.1		-200.1		-441.5	
C	1	-48.6	19.8	-30.5	16.0	-33.4	16.4	-40.2	17.1	-81.1	18.4
C	2	-59.2	24.1	-45.7	24.0	-54.6	26.9	-70.1	29.7	-111.7	25.3
C	3	-42.4	17.3	-39.5	20.7	-61.5	30.3	-65.7	27.8	-100.9	22.8
C	4	-53.2	21.7	-44.0	23.1	-36.5	18.0	-39.3	16.7	-88.7	20.1
C	5	-41.9	17.1	-31.1	16.3	-17.3	8.5	-20.7	8.8	-59.2	13.4
C	SUM	-245.3		-190.8		-203.3		-236.0		-441.5	
D	1	-18.1	17.0	-15.3	13.6	113.0	20.1	91.8	17.1	94.9	20.8
D	2	-24.1	22.6	-25.9	23.1	142.1	25.3	139.4	26.0	118.0	25.9
D	3	-23.6	22.2	-23.9	21.3	125.7	22.6	117.7	22.0	103.1	22.7
D	4	-23.5	22.1	-28.4	25.3	107.8	19.2	110.2	20.6	84.3	18.5
D	5	-17.2	16.2	-18.7	16.7	72.2	12.8	76.9	14.4	55.0	12.1
D	SUM	-106.6		-112.1		561.8		536.0		455.3	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0	
LOAD	PY (KIPS)	0.		.1		-100.0		-100.0		-100.0	
ACTUAL	PX (KIPS)			-19.3		0.		0.		-19.7	
ACTUAL	PY (KIPS)			.0		-19.1		-18.9		-18.9	

TABLE 2J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )



MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION	GIRDER	2X			2Y			2X+2Y			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	103.3	91.1	17.4	-17.7	-23.8	16.4	85.7	18.8	76.6	17.8
A	2	137.9	124.0	23.7	-23.9	-24.4	22.1	114.1	25.1	103.4	24.1
A	3	125.7	119.1	22.8	-24.0	-26.9	22.2	101.8	22.4	97.3	22.6
A	4	115.5	115.9	22.2	-24.4	-28.8	22.6	91.1	20.0	94.3	21.9
A	5	80.5	72.7	13.9	-18.0	-19.8	16.7	62.5	13.7	58.2	13.5
A	SUM	563.0	522.8		-107.8	-123.7		455.2		429.8	
B	1	-27.6	-35.6	16.1	-51.3	-38.0	20.8	-78.9	17.9	-72.1	17.7
B	2	-46.6	-54.2	24.5	-63.0	-49.6	25.5	-108.6	24.6	-101.3	24.8
B	3	-60.8	-63.3	28.6	-42.7	-40.4	17.3	-100.7	22.8	-100.6	24.7
B	4	-41.6	-43.8	19.8	-50.6	-40.1	20.5	-91.2	20.7	-82.3	20.2
B	5	-22.9	-24.5	11.1	-39.4	-27.7	14.1	-62.1	14.1	-51.4	12.6
B	SUM	-199.5	-221.5		-247.1	-195.8		-441.5		-407.7	
C	1	-48.6	-31.3	16.9	-33.4	-42.5	16.4	-81.1	18.4	-74.9	17.5
C	2	-59.2	-44.5	24.0	-54.6	-70.3	26.9	-111.7	25.3	-114.4	26.8
C	3	-42.4	-37.3	20.2	-61.5	-64.9	30.3	-100.9	22.8	-102.9	24.1
C	4	-53.2	-41.7	22.5	-36.5	-39.7	16.7	-88.7	20.1	-83.0	19.4
C	5	-41.9	-30.4	16.4	-17.3	-20.4	8.5	-59.2	13.4	-51.7	12.1
C	SUM	-245.3	-185.2		-203.3	-237.6		-441.5		-426.8	
D	1	-18.1	-14.2	13.1	113.0	88.0	20.1	94.9	20.8	67.2	17.7
D	2	-24.1	-25.3	23.4	142.1	142.5	25.3	118.0	25.9	105.3	27.7
D	3	-23.6	-23.5	21.8	126.7	117.7	22.6	103.1	22.7	84.6	22.3
D	4	-23.5	-27.9	25.8	107.8	110.1	19.2	84.3	18.5	74.1	19.5
D	5	-17.2	-17.3	16.0	72.2	71.3	12.8	55.0	12.1	49.1	12.9
D	SUM	-106.6	-108.2		561.8	529.6		455.3		380.2	
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.	.1		-100.0			-100.0		-96.2	
ACTUAL	PX (KIPS)		-19.3		0.			-19.7		-18.9	
ACTUAL	PY (KIPS)		0.		-19.1						

TABLE 3A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 30 KSI CONCD. LOADING.  
 TF = MOMENT AT FOOTING ABOUT Y-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	3X		3Y		3X+3Y	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	-0.07	2.16	-2.53	-2.70	-2.60	.22
2E	-1.42	-4.05	8.65	13.32	7.23	8.84
3E	-1.32	-2.48	15.17	11.07	13.86	7.29
4E	-1.78	1.84	9.25	-0.05	7.47	4.42
5E	-3.27	-4.70	8.15	14.48	4.88	9.28
1F	-3.10	2.30	37.97	40.73	34.87	24.62
2F	-3.02	-1.88	38.15	43.43	35.13	21.78
3F	37.65	33.74	-3.40	-6.62	34.26	46.41
4F	37.57	35.52	-3.58	-6.25	34.00	48.24
1W	.98	6.32	-.08	.35	.90	5.37
2W	8.09	2.73	-1.37	.51	6.72	2.24
3W	9.08	5.02	-1.35	-2.91	7.73	6.63
4W	9.17	10.62	-1.83	-2.52	7.34	6.76
5W	11.45	15.32	-3.22	-3.44	8.23	10.32
5E	-7.86	-7.23	38.69	36.12	30.84	30.05
5F	69.10	69.68	69.16	71.29	138.26	141.05
8W	38.77	40.01	-7.85	-8.01	30.92	31.32
SUMP	100.01	102.46	100.00	99.40	200.02	202.42
PX	-100.00	-100.00	0.	.05	-100.00	-100.00
PY	0.	.01	-100.00	-100.00	-100.00	-99.68
SUMP	-100.00	-99.99	-100.00	-99.95	-200.00	-199.68
SUMP/SUMP	1.00	1.02	1.00	.99	1.00	1.01
TW	56.66	66.61	-17.34	-27.30	39.31	36.87
MF	122.04	103.26	-124.65	-145.55	-2.60	72.37
TF	-.24	8.91	-.54	-3.49	-.78	6.99
TE	-17.39	-20.15	56.50	54.01	39.11	35.25
ACTUAL PX		-19.25		.01		-19.22
ACTUAL PY		-0.		-19.21		-19.15

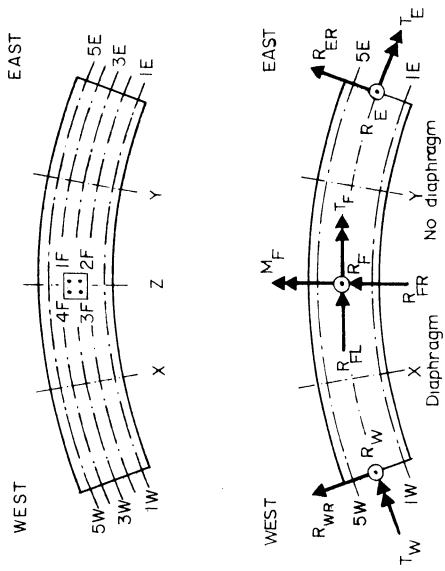
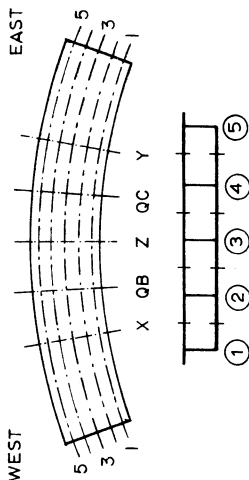


TABLE 3B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



DEFLECTION AT POINT	3X			3Y			3X+3Y		
	THEORY	EXPERM	E/T	THEORY	EXPERM	E/T	THEORY	EXPERM	E/T
1X	.692	.930	1.34	-.239	-.343	1.43	.453	.706	1.56
2X	.740	1.029	1.39	-.249	-.379	1.52	.491	.783	1.59
3X	.793	1.099	1.39	-.260	-.393	1.51	.532	.845	1.59
4X	.809	1.126	1.39	-.273	-.414	1.52	.536	.838	1.56
5X	.831	1.125	1.35	-.288	-.432	1.50	.544	.838	1.54
1QB	.421	.570	1.35	-.207	-.295	1.42	.214	.355	1.66
2QB	.441	.587	1.33	-.215	-.304	1.41	.225	.368	1.63
3QB	.460	.616	1.34	-.222	-.306	1.38	.238	.380	1.59
4QB	.481	.651	1.36	-.235	-.307	1.31	.246	.406	1.65
5QB	.500	.644	1.29	-.245	-.346	1.41	.255	.382	1.50
1Z	.013	.022	1.63	.011	.023	2.13	.024	.056	2.30
2Z	.007	.005	.66	.007	.007	1.04	.014	.021	1.56
4Z	.007	.008	1.15	.006	.011	1.93	.012	.017	1.39
5Z	.012	.017	1.39	.009	.020	2.20	.022	.032	1.47
1QC	-.208	-.260	1.25	.408	.556	1.36	.200	.238	1.19
2QC	-.216	-.276	1.28	.442	.610	1.38	.226	.267	1.18
3QC	-.221	-.287	1.30	.489	.675	1.38	.267	.313	1.17
4QC	-.234	-.297	1.27	.476	.659	1.38	.243	.290	1.19
5QC	-.244	-.308	1.25	.479	.656	1.37	.235	.277	1.18
1Y	-.243	-.325	1.34	.658	.922	1.40	.415	.507	1.22
2Y	-.251	-.339	1.35	.735	1.054	1.43	.484	.605	1.25
3Y	-.260	-.353	1.36	.894	1.314	1.47	.634	.844	1.33
4Y	-.272	-.386	1.42	.793	1.105	1.39	.521	.631	1.21
5Y	-.284	-.380	1.34	.773	1.088	1.41	.489	.602	1.23
LOAD PX	-100.0	-100.0		0.	.1		-100.0	-100.0	
LOAD PY	0.	.0		-100.0	-100.0		-100.0	-100.0	
ACTUAL PX					.0				
ACTUAL PY				-19.2	-19.2				

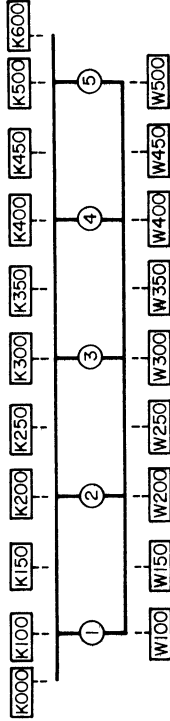
LOAD PX	-100.0	-100.0		0.	.1		-100.0	-100.0	
LOAD PY	0.	.0		-100.0	-100.0		-100.0	-100.0	
ACTUAL PX					.0				
ACTUAL PY				-19.2	-19.2				

TABLE 3C

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	3X		3Y		3X+3Y			
		THEORY	MEASR ADJUST	THEORY	MEASR ADJUST	THEORY	MEASR ADJUST		
K	K000	-314	-271	68	167	-245	-236	-236	-409
K	K100	-277	-465	59	163	-218	-427	-427	-257
K	K150	-307	-308	69	51	-253	-253	-253	-368
K	K200	-251	-414	50	113	-201	-344	-344	-250
K	K250	-304	-304	57	60	-216	-245	-245	-337
K	K300	-268	-393	52	97	-199	-345	-345	-300
K	K350	-346	-345	81	62	-199	-303	-303	-363
K	K400	-249	-412	50	108	-271	-271	-271	-319
K	K450	-315	-364	69	89	-208	-296	-296	-295
K	K500	-266	-334	58	94	-223	-185	-185	-185
K	K600	-289	-208	65	61				
W	W100	1044	969	-217	-224	826	859	859	871
W	W150	812	716	-177	-159	772	716	716	630
W	W200	969	916	-196	-229	836	835	835	800
W	W250	830	767	-186	-173	728	728	728	671
W	W300	1048	998	-211	-238	836	856	856	862
W	W350	838	864	-197	-203	762	727	727	747
W	W400	958	937	-196	-231	801	801	801	800
W	W450	857	814	-194	-188	740	740	740	700
W	W500	982	1055	-210	-274	771	888	888	883
LOAD	PX (KIPS)	-100.0	-100.0	0.	.1	-100.0	-100.0	-100.0	-100.0
LEAD	PY (KIPS)	0.	.0	-100.0	-100.0	-100.0	-99.7	-99.7	-99.7
ACTUAL	PX (KIPS)	-19.2	.0	.0	.0	-19.2	-19.2	-19.2	-19.2
ACTUAL	PY (KIPS)	-0.	-0.	-19.2	-19.2	-19.1	-19.1	-19.1	-19.1

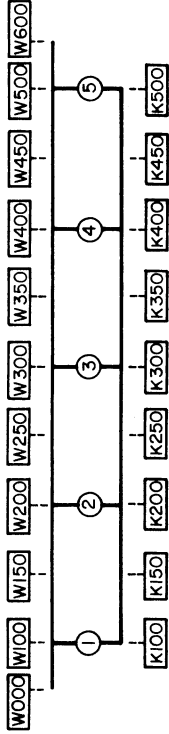
TABLE 3D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



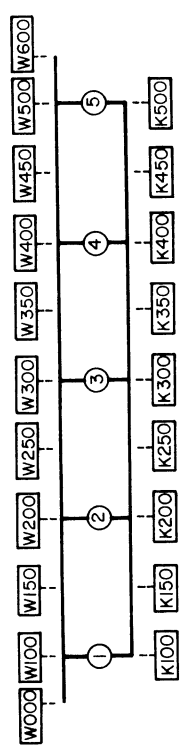
NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	3X			3Y			3X+3Y		
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
W	W000	194	272	272	448	301	301	642	590	590
W	W100	196	271	276	399	297	301	596	590	600
W	W150		241	281		258	293		510	583
W	W200	222	363	358	314	317	318	536	695	692
W	W250		356	399		238	253		604	657
W	W300	335	409	436	214	250	262	549	687	722
W	W350		332	394		227	265		567	660
W	W400	226	311	311	308	277	279	534	610	612
W	W450		279	320		272	310		567	643
W	W500	201	259	263	381	268	270	582	532	538
W	W600	186	266	266	408	276	276	594	554	554
K	K100	-90	-168	-171	-180	-197	-199	-271	-354	-359
K	K150		-172	-166		-226	-214		-376	-360
K	K200	-99	-201	-196	-149	-188	-184	-248	-378	-369
K	K250		-229	-223		-182	-175		-381	-365
K	K300	-133	-237	-241	-92	-177	-176	-225	-382	-385
K	K350		-212	-214		-190	-191		-374	-376
K	K400	-102	-171	-169	-145	-193	-197	-248	-342	-343
K	K450		-170	-172		-180	-186		-340	-345
K	K500	-92	-154	-152	-168	-168	-166	-260	-308	-305
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	0.	.1		-100.0	-100.0	
LOAD	PY (KIPS)	0.	.0		-100.0	-100.0		-100.0	-99.7	
ACTUAL	PX (KIPS)		-19.2			.0			-19.2	
ACTUAL	PY (KIPS)		-0.			-19.2			-19.1	



TABLE 3E

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	3X		3Y		3X+3Y	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	451	287	185	250	636	578
W	W100	403	256	187	229	591	529
W	W150		238		247		523
W	W200	309	301	232	394	541	741
W	W250		212		375		608
W	W300	204	249	368	518	572	806
W	W350		190		353		586
W	W400	309	305	226	356	535	722
W	W450		244		263		544
W	W500	393	267	178	232	571	530
W	W600	421	273	159	240	580	544
K	K100	-182	-194	-87	-143	-269	-339
K	K150		-181		-129		-315
K	K200	-147	-186	-103	-195	-250	-399
K	K250		-163		-276		-472
K	K300	-88	-150	-145	-310	-234	-472
K	K350		-174		-262		-452
K	K400	-146	-175	-100	-169	-247	-358
K	K450		-235		-173		-405
K	K500	-174	-185	-80	-126	-255	-317
LOAD	PX (KIPS)	-100.0	-100.0	0.	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-99.7
ACTUAL	PX (KIPS)		-19.2		0.		-19.2
ACTUAL	PY (KIPS)		-0.		-19.2		-19.1

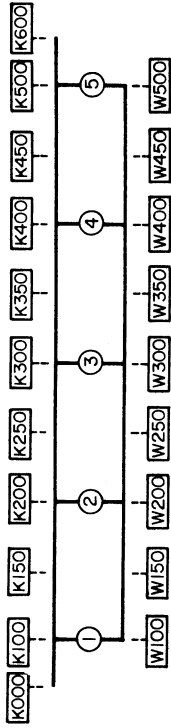
TABLE 3F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION D

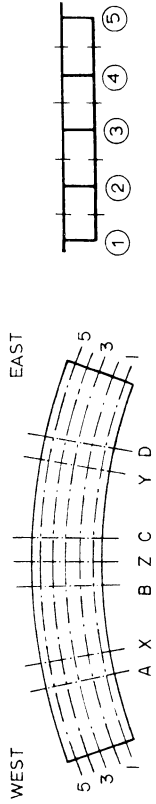
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	3X			3Y			3X+3Y		
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
K	K000	62	35	35	-278	-155	-155	-215	-116	-116
K	K100	53	66	68	-241	-291	-297	-187	-217	-220
K	K150	133	133	126	-231	-530	-498	-186	-389	-364
K	K200	45	98	96	-238	-414	-402	-192	-302	-291
K	K250	74	74	88	-225	-371	-417	-181	-273	-301
K	K300	46	82	87	-250	-357	-391	-176	-256	-282
K	K350	122	122	128	-250	-502	-532	-193	-362	-382
K	K400	44	98	90	-226	-389	-363	-176	-277	-260
K	K450	50	152	143	-250	-586	-527	-176	-419	-381
K	K500	57	99	103	-250	-418	-414	-193	-305	-302
K	K600	31	31	99	-250	-133	-418	-193	-100	-305
W	W100	-224	-134	-138	1042	701	715	818	492	501
W	W150	-199	-195	-174	994	945	876	794	665	617
W	W200	-211	-207	-203	1049	1082	1069	837	780	770
W	W250	-192	-192	-176	958	997	931	766	727	677
W	W300	-206	-201	-200	955	1104	1081	749	771	756
W	W350	-192	-193	-183	0.	861	850	-100.0	596	602
W	W400	0.	-237	-228	-100.0	1082	1074	-100.0	776	773
W	W450	0.	-194	-192	0.	845	841	-100.0	607	600
W	W500	0.	-206	-215	0.	982	1006	-100.0	714	729
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	0.	.1		-100.0	-100.0	
LOAD	PY (KIPS)	0.	0.	0.	-100.0	-100.0		-100.0	-99.7	
ACTUAL	PX (KIPS)		-19.2	0.					-19.2	
ACTUAL	PY (KIPS)		-0.	-19.2					-19.1	

TABLE 3C

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH



RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADINGS.  
SIMPLY SUPPORTED, NO RESTRAINTS.

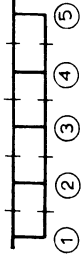
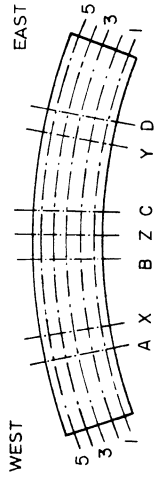
SECTION	GIRDER	3X		3Y		3X+3Y							
		THEORY K-FT	PCT	THEORY K-FT	PCT	THEORY K-FT	PCT						
A	1	92.9	16.3	71.9	13.4	-19.5	16.7	-15.1	12.1	73.4	16.2	63.3	13.6
A	2	129.6	22.8	121.4	22.6	-26.1	22.4	-28.1	22.4	103.5	22.9	106.2	22.9
A	3	130.4	22.9	131.0	24.4	-25.8	22.2	-30.7	24.5	104.6	23.1	113.5	24.5
A	4	127.8	22.5	130.9	24.4	-25.0	22.3	-31.3	24.9	101.8	22.5	112.3	24.2
A	5	88.4	15.5	81.6	15.2	-19.0	16.3	-20.1	16.1	69.4	15.3	68.8	14.8
A	SUM	569.0		536.7		-115.3		-125.4		452.7		464.0	
B	1	-27.5	12.5	-33.3	13.8	-48.8	18.4	-35.9	18.0	-77.0	15.9	-71.5	15.9
B	2	-48.2	22.0	-53.5	22.2	-61.5	23.2	-44.5	22.3	-109.9	22.7	-99.6	22.1
B	3	-66.7	30.4	-67.4	28.0	-48.3	18.3	-41.2	20.7	-113.8	23.5	-110.9	24.6
B	4	-49.2	22.4	-52.1	21.6	-60.0	22.7	-42.8	21.5	-109.2	22.5	-97.3	21.6
B	5	-27.9	12.7	-35.0	14.5	-46.1	17.4	-35.0	17.6	-74.5	15.4	-71.3	15.8
B	SUM	-219.6		-241.2		-264.8		-199.4		-484.4		-450.7	
C	1	-49.2	18.6	-34.4	17.6	-26.8	12.0	-31.5	12.5	-76.4	15.7	-70.9	15.0
C	2	-60.9	23.0	-43.8	22.4	-50.2	22.4	-58.9	23.4	-110.5	22.8	-108.3	22.9
C	3	-46.9	17.7	-37.7	19.3	-72.3	32.3	-72.8	28.9	-116.8	24.1	-115.3	24.3
C	4	-60.4	22.8	-44.7	22.9	-49.2	22.0	-56.1	22.3	-109.0	22.4	-107.6	22.7
C	5	-47.5	17.9	-34.6	17.7	-25.2	11.3	-32.9	13.0	-73.0	15.0	-71.7	15.1
C	SUM	-265.0		-195.3		-223.7		-252.3		-485.8		-473.8	
D	1	-20.0	17.2	-12.0	11.1	92.3	16.2	62.1	11.5	72.3	16.0	43.4	11.3
D	2	-26.5	22.7	-26.4	24.3	132.1	23.2	138.6	25.7	105.6	23.3	99.6	25.9
D	3	-25.8	22.2	-25.3	23.3	131.1	23.0	132.7	24.6	105.3	23.3	93.6	24.3
D	4	-25.6	22.0	-29.0	26.7	127.5	22.4	133.8	24.8	102.0	22.5	95.8	24.9
D	5	-18.5	16.0	-15.9	14.7	85.8	15.1	73.1	13.5	67.2	14.8	52.6	13.7
D	SUM	-116.4		-108.8		563.7		540.3		452.3		385.1	
LOAD	PX (KIPS)	-100.0		-100.0		0.		.1		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-99.7	
ACTUAL	PX (KIPS)	0.		-19.2		.0		.0		-19.2		-19.2	
ACTUAL	PY (KIPS)	-0.		-0.		-19.2		-19.2		-19.1		-19.1	

TABLE 3H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADINGS.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS AT

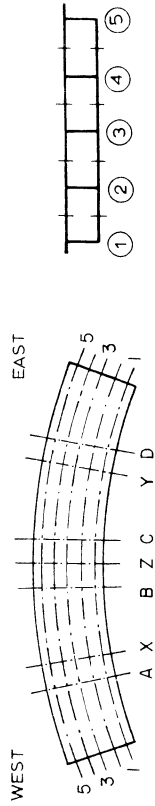
SECTION	GIRDER	3X			3Y			3X+3Y					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	92.9	16.3	106.3	19.7	-19.5	16.7	-39.5	27.3	73.4	16.2	94.2	20.1
A	2	129.6	22.8	112.3	20.8	-26.1	22.4	-25.1	17.3	103.5	22.9	95.8	20.4
A	3	130.4	22.9	109.8	20.4	-25.8	22.2	-25.5	17.6	104.6	23.1	94.0	20.0
A	4	127.8	22.5	122.0	22.6	-26.0	22.3	-30.9	21.3	101.8	22.5	107.5	22.9
A	5	88.4	15.5	88.3	16.4	-19.0	16.3	-23.9	16.5	69.4	15.3	78.3	16.7
A	SUM	569.0		538.7		-116.3		-144.9		452.7		469.8	
B	1	-27.5	12.5	-28.6	12.2	-48.8	18.4	-36.0	15.4	-77.0	15.9	-61.2	14.0
B	2	-48.2	22.0	-56.1	23.9	-61.5	23.2	-55.1	23.6	-109.9	22.7	-104.7	23.9
B	3	-66.7	30.4	-70.3	30.0	-48.3	18.3	-55.6	23.8	-113.8	23.5	-114.6	26.2
B	4	-49.2	22.4	-52.1	22.2	-60.0	22.7	-57.1	24.4	-109.2	22.5	-102.0	23.3
B	5	-27.9	12.7	-27.4	11.7	-46.1	17.4	-29.9	12.8	-74.5	15.4	-54.7	12.5
B	SUM	-219.6		-234.6		-264.8		-233.7		-484.4		-437.3	
C	1	-49.2	18.6	-32.6	14.2	-26.8	12.0	-23.1	9.1	-76.4	15.7	-56.5	11.4
C	2	-60.9	23.0	-55.2	24.0	-50.2	22.4	-57.0	22.5	-110.5	22.8	-115.4	23.3
C	3	-46.9	17.7	-50.0	21.8	-72.3	32.3	-91.6	36.1	-116.8	24.1	-146.7	29.6
C	4	-60.4	22.8	-55.1	24.0	-49.2	22.0	-56.3	22.2	-109.0	22.4	-114.4	23.1
C	5	-47.5	17.9	-36.7	16.0	-25.2	11.3	-25.4	10.0	-73.0	15.0	-62.7	12.7
C	SUM	-265.0		-229.7		-223.7		-253.4		-485.8		-495.8	
D	1	-20.0	17.2	-20.9	14.8	92.3	16.2	84.7	14.8	72.3	16.0	62.8	15.1
D	2	-26.5	22.7	-29.6	20.9	132.1	23.2	121.8	21.3	105.6	23.3	88.5	21.3
D	3	-25.8	22.2	-27.9	19.7	131.1	23.0	122.3	21.4	105.3	23.3	88.4	21.3
D	4	-25.6	22.0	-32.9	23.2	127.5	22.4	127.0	22.2	102.0	22.5	91.2	22.0
D	5	-18.6	16.0	-30.4	21.4	85.8	15.1	115.3	20.2	67.2	14.8	83.9	20.2
D	SUM	-116.4		-141.6		568.7		571.0		452.3		414.8	
LOAD	PX (KIPS)	-100.0		-100.0		0.		.1		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-99.7	
ACTUAL	PX (KIPS)			-19.2				0.				-19.2	
ACTUAL	PY (KIPS)			-0.				-19.2				-19.1	

TABLE 31

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

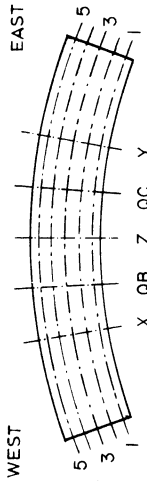
RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COMP. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	3X			3Y			3X+3Y			
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	
A	1	92.9	16.3	97.3	16.7	-26.0	19.4	73.4	16.2	77.1	16.5
A	2	129.6	22.8	117.3	22.4	-26.8	20.0	103.5	22.9	101.6	21.8
A	3	130.4	22.9	121.6	22.6	-28.4	21.2	104.6	23.1	104.8	22.5
A	4	127.8	22.5	127.0	22.3	-31.1	23.2	101.8	22.5	110.2	23.6
A	5	88.4	15.5	84.6	15.7	-21.8	16.3	69.4	15.3	73.1	15.7
A	SUM	569.0		537.8		-115.3		452.7		466.7	
B	1	-27.5	12.5	-30.7	12.9	-48.8	18.4	-77.0	15.9	-65.8	14.8
B	2	-48.2	22.0	-54.9	23.1	-61.5	23.2	-109.9	22.7	-102.5	23.1
B	3	-66.7	30.4	-69.1	29.1	-48.3	18.3	-113.8	23.5	-113.0	25.5
B	4	-49.2	22.4	-52.1	21.9	-60.0	22.7	-109.2	22.5	-99.9	22.5
B	5	-27.9	12.7	-30.8	13.0	-46.1	17.4	-74.5	15.4	-62.2	14.0
B	SUM	-219.6		-237.6		-264.8		-484.4		-443.4	
C	1	-49.2	18.6	-33.4	15.6	-26.8	12.0	-76.4	15.7	-62.9	12.9
C	2	-60.9	23.0	-50.2	23.4	-50.2	22.4	-110.5	22.8	-112.3	23.1
C	3	-46.9	17.7	-44.6	20.8	-72.3	32.3	-116.8	24.1	-132.7	27.3
C	4	-60.4	22.8	-50.5	23.5	-49.2	22.0	-109.0	22.4	-111.4	22.9
C	5	-47.5	17.9	-35.8	16.7	-25.2	11.3	-73.0	15.0	-66.7	13.7
C	SUM	-265.0		-214.4		-223.7		-485.8		-486.1	
D	1	-20.0	17.2	-16.0	13.0	92.3	16.2	72.3	16.0	52.1	13.1
D	2	-26.5	22.7	-27.8	22.5	132.1	23.0	105.6	23.3	94.7	23.8
D	3	-25.8	22.2	-26.5	21.4	131.1	23.1	105.3	23.3	91.3	22.9
D	4	-25.6	22.0	-30.8	24.9	127.5	22.4	102.0	22.5	93.8	23.5
D	5	-18.6	16.0	-22.4	18.1	85.8	15.1	67.2	14.8	66.6	16.7
D	SUM	-116.4		-123.5		568.7		452.3		398.5	
LOAD	PX (KIPS)	-100.0		-100.0		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-99.7	
ACTUAL	PX (KIPS)			-19.2		0.				-19.2	
ACTUAL	PY (KIPS)			-0.		-19.2				-19.1	

TABLE 4B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



DEFLECTION AT POINT	4X		4Y		4X+4Y					
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM				
1X	.604	.808	1.34	1.34	-.283	-.391	1.38	.321	.540	1.68
2X	.698	.954	1.37	1.37	-.277	-.418	1.51	.421	.694	1.65
3X	.809	1.125	1.39	1.39	-.272	-.407	1.50	.538	.873	1.62
4X	.930	1.275	1.37	1.37	-.268	-.416	1.55	.662	1.005	1.52
5X	1.019	1.377	1.35	1.35	-.266	-.423	1.59	.753	1.120	1.49
1QB	.338	.451	1.33	1.33	-.265	-.368	1.39	.073	.168	2.30
2QB	.402	.532	1.32	1.32	-.248	-.348	1.41	.154	.271	1.76
3QB	.474	.631	1.33	1.33	-.231	-.317	1.37	.243	.394	1.62
4QB	.564	.756	1.34	1.34	-.221	-.308	1.39	.342	.530	1.55
5QB	.641	.817	1.28	1.28	-.207	-.307	1.49	.434	.601	1.38
1Z	-.057	-.056	.97	.97	-.059	-.049	.82	-.117	-.098	.84
2Z	-.027	-.027	1.00	1.00	-.028	-.015	.51	-.056	-.041	.73
4Z	.042	.052	1.24	1.24	.043	.050	1.16	.085	.099	1.16
5Z	.085	.111	1.30	1.30	.085	.112	1.32	.170	.213	1.25
1QC	-.269	-.341	1.27	1.27	.317	.437	1.38	.049	.060	1.24
2QC	-.251	-.325	1.30	1.30	.380	.523	1.38	.129	.158	1.22
3QC	-.232	-.300	1.30	1.30	.470	.649	1.38	.238	.291	1.22
4QC	-.221	-.284	1.29	1.29	.593	.824	1.39	.372	.481	1.29
5QC	-.205	-.256	1.25	1.25	.644	.871	1.35	.438	.542	1.24
1Y	-.289	-.392	1.36	1.36	.559	.785	1.41	.270	.337	1.25
2Y	-.281	-.379	1.35	1.35	.646	.907	1.40	.366	.453	1.24
3Y	-.273	-.364	1.33	1.33	.793	1.129	1.42	.520	.693	1.33
4Y	-.268	-.377	1.41	1.41	1.029	1.484	1.44	.761	1.015	1.33
5Y	-.254	-.350	1.32	1.32	1.009	1.428	1.41	.745	.997	1.34
LOAD PX	-100.0	-100.0	0.	0.	0.	0.	-100.0	-100.0	-100.0	-100.0
LOAD PY	0.	0.	1	1	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0
ACTUAL PX			-19.3	-19.3	0.	0.	-19.1	-19.1	-19.1	-19.1
ACTUAL PY			0.	0.	-19.4	-19.4	-19.2	-19.2	-19.2	-19.2

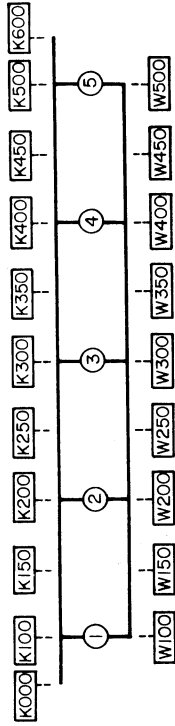
TABLE 4C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LCC.	4X		4Y		4X+4Y	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	-306	-279	76	83	-229	-244
K	K100	-260	-451	65	174	-195	-411
K	K150	-234	-296	55	72	-178	-239
K	K200	-265	-367	56	118	-209	-314
K	K250	-273	-308	54	59	-218	-248
K	K300	-303	-376	62	110	-241	-324
K	K350	-321	-347	69	90	-251	-296
K	K400	972	-428	54	115	-218	-369
K	K450	894	-431	62	82	-241	-284
K	K500	1045	-375	69	106	-251	-331
K	K600	1049	-224	69	70	-251	-194
W	W100	875	893	-241	-251	731	755
W	W150	761	649	-216	-188	678	672
W	W200	894	849	-230	-253	815	762
W	W250	743	724	-210	-217	838	633
W	W300	985	995	-224	-254	914	850
W	W350	839	913	-210	-209	750	729
W	W400	977	998	-224	-237	1109	846
W	W450	872	887	-216	-216	773	750
W	W500	1139	1256	-224	-257	1109	1109
LOAD	PX (KIPS)	-100.0	-100.0	0.	.0	-100.0	-100.0
LCCD	PY (KIPS)	0.	.1	-100.0	-100.0	-100.0	-100.9
ACTUAL	PX (KIPS)	-19.3	.0				-19.1
ACTUAL	PY (KIPS)	.0	.0				-19.2

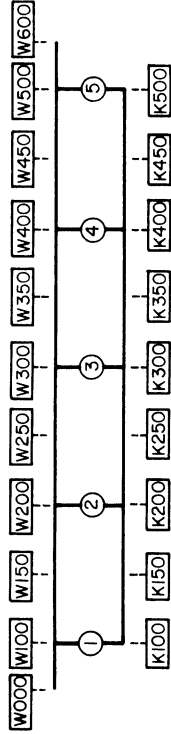
TABLE 4D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	4X		4Y		4X+4Y	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	216	230	456	292	673	556
W	W100	215	254	406	282	622	565
W	W150		254		261		497
W	W200	232	358	309	298	542	700
W	W250		413		246		631
W	W300	359	465	223	276	583	749
W	W350		440		262		658
W	W400	269	379	362	337	632	751
W	W450		397		345		719
W	W500	256	346	456	331	713	687
W	W600	244	362	490	337	734	722
K	K100	-97	-187	-181	-209	-279	-391
K	K150		-167		-244		-399
K	K200	-104	-213	-147	-183	-252	-406
K	K250		-229		-178		-404
K	K300	-143	-248	-97	-188	-240	-407
K	K350		-216		-212		-411
K	K400	-122	-179	-172	-220	-295	-413
K	K450		-205		-196		-408
K	K500	-118	-185	-204	-184	-322	-439
LOAD	PX (KIPS)	-100.0	-100.0	0.	.0	-100.0	-100.0
LOAD	PY (KIPS)	0.	.1	-100.0	-100.0	-100.0	-100.9
ACTUAL	PX (KIPS)		-19.3		.0		-19.1
ACTUAL	PY (KIPS)		.0		-19.4		-19.2



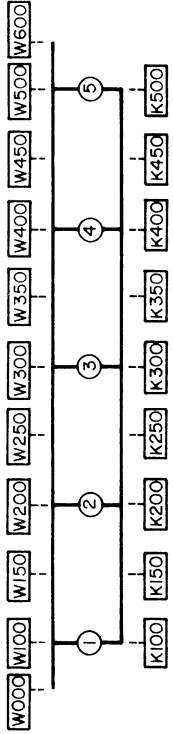
TABLE 4E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LCC.	4X		4Y		4X+4Y	
		THEORY	MEASR.	THEORY	MEASR.	THEORY	MEASR.
W	W000	475	289	173	164	648	524
W	W100	422	253	182	162	605	483
W	W150	321	240	211	187	532	471
W	W200	222	228	359	324	582	598
W	W250	350	216	296	367	647	617
W	W300	450	288	271	348	722	671
W	W350	482	312	266	373	749	734
W	W400	-189	318	-81	405	-270	754
W	W450	-153	-206	-93	-148	-247	-375
W	W500	-97	-191	-142	-133	-239	-348
W	W600	-167	-190	-135	-110	-302	-327
K	K100	-201	-205	-126	-152	-328	-394
K	K150	-189	-186	-142	-240	-398	-461
K	K200	-163	-161	-251	-241	-449	-438
K	K250	-180	-174	-342	-329	-557	-537
K	K300	-189	-183	-228	-239	-433	-439
K	K350	-267	-254	-215	-222	-489	-485
K	K400	-199	-198	-189	-186	-398	-392
K	K450	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0
K	K500	0.	0.	0.	0.	0.	0.

LOAD PX (KIPS) -100.0 -100.0  
 LOAD PY (KIPS) 0. .1

ACTUAL PX (KIPS) -19.3  
 ACTUAL PY (KIPS) .0

-19.1  
 -19.2

TABLE 4F

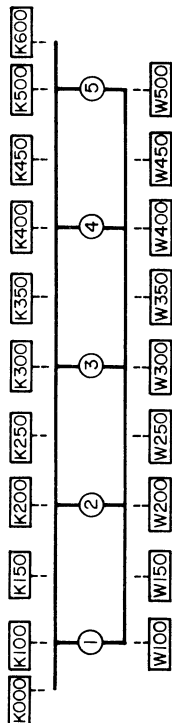
SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION D

TENSION = + K = CONCRETE STRAIN METERS

COMPRESSION = - W = WELDABLE STRAIN GAGES

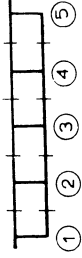
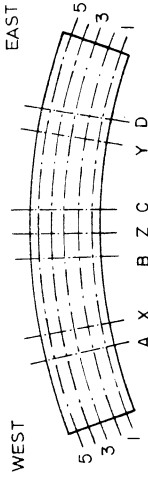


NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	4X		4Y		4X+4Y	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	69	34	-250	-119	-181	-87
K	K100	58	70	-214	-243	-155	-176
K	K150	129	122	-447	-421	-332	-313
K	K200	49	103	-201	-365	-151	-262
K	K250	76	94	-343	-390	-258	-288
K	K300	50	88	-243	-407	-193	-316
K	K350	133	134	-495	-424	-364	-328
K	K400	47	107	-240	-552	-192	-418
K	K450	168	164	-689	-452	-331	-343
K	K500	54	114	-286	-652	-518	-488
K	K600	61	114	-320	-517	-231	-402
W	W100	-247	-154	898	618	650	422
W	W150	-205	-198	820	820	562	509
W	W200	-219	-217	858	909	639	627
W	W250	-212	-196	880	880	620	584
W	W300	-231	-213	1075	1004	844	730
W	W350	-176	-179	1122	1051	887	819
W	W400	-208	-229	1044	1197	835	873
W	W450	-199	-192	1078	1063	825	846
W	W500	-223	-238	1255	1245	1032	963
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	.1	-100.0	-170.0	-100.0	-100.9
ACTUAL	PX (KIPS)	-19.3	.0				-19.1
ACTUAL	PY (KIPS)	.0	-19.4				-19.2

TABLE 4G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH



RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

NORMALIZED POINT LOADS AT

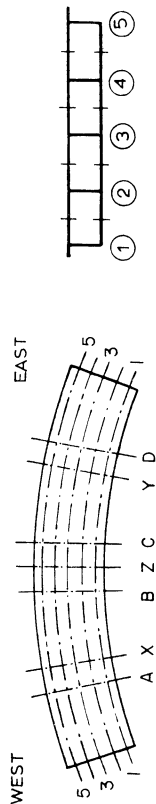
SECTION	GIRDER	4X			4Y			4X+4Y					
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT			
A	1	87.0	15.1	64.6	11.9	-21.6	17.0	-16.9	12.7	65.4	14.6	56.0	11.9
A	2	120.6	20.9	112.0	20.7	-28.7	22.7	-31.0	23.4	91.9	20.5	96.4	20.5
A	3	129.2	22.4	131.1	24.2	-28.1	22.2	-32.8	24.7	101.1	22.5	114.0	24.2
A	4	138.6	24.1	139.9	25.8	-27.9	22.1	-32.4	24.4	110.7	24.6	122.2	25.9
A	5	100.3	17.4	94.3	17.4	-20.3	16.0	-19.6	14.8	80.0	17.8	82.6	17.5
A	SUM	575.7		541.9		-126.6		-132.8		449.2		471.2	
B	1	-29.8	12.1	-29.2	11.1	-50.0	17.1	-34.6	15.8	-79.3	14.9	-67.7	13.5
B	2	-51.0	20.7	-52.6	20.1	-62.2	21.3	-43.3	19.8	-111.9	21.1	-100.0	20.0
B	3	-72.1	29.3	-72.3	27.6	-51.8	17.8	-44.9	20.5	-121.5	22.9	-122.0	24.4
B	4	-58.0	23.6	-62.4	23.8	-71.4	24.5	-52.5	24.0	-128.0	24.1	-118.6	23.7
B	5	-35.2	14.3	-45.5	17.4	-55.1	19.2	-43.8	20.0	-90.7	17.1	-92.0	18.4
B	SUM	-246.1		-261.9		-291.5		-219.1		-531.5		-500.4	
C	1	-51.6	17.8	-35.0	16.3	-25.1	10.3	-21.3	8.0	-77.3	14.5	-64.1	12.3
C	2	-63.9	22.0	-44.5	20.8	-46.3	19.0	-49.7	18.6	-110.3	20.7	-103.7	19.9
C	3	-51.5	17.7	-41.1	19.2	-71.7	29.5	-72.9	27.4	-121.8	22.8	-121.6	23.4
C	4	-69.0	23.7	-52.7	24.6	-62.4	25.7	-72.2	27.1	-130.9	24.6	-134.2	25.8
C	5	-54.8	18.8	-40.9	19.1	-37.6	15.5	-50.3	18.9	-92.6	17.4	-96.8	18.6
C	SUM	-290.8		-214.3		-243.1		-266.5		-532.9		-520.5	
D	1	-22.0	17.3	-13.7	11.9	80.9	14.0	54.6	9.9	58.9	13.1	36.6	9.1
D	2	-29.1	22.8	-29.0	25.2	116.1	20.1	118.0	21.4	87.1	19.3	81.9	20.4
D	3	-28.2	22.2	-26.6	23.2	131.5	22.8	129.8	23.6	103.3	23.0	95.4	23.7
D	4	-27.8	21.8	-28.7	25.0	140.6	24.4	154.9	28.1	112.9	25.1	115.9	28.8
D	5	-20.2	15.9	-16.9	14.7	108.0	18.7	93.9	17.0	87.8	19.5	72.4	18.0
D	SUM	-127.2		-115.0		577.1		551.2		449.9		402.2	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-100.9	
ACTUAL	PX (KIPS)			-19.3		0.		0.		-19.1		-19.1	
ACTUAL	PY (KIPS)			0.		-19.4		-19.4		-19.2		-19.2	

TABLE 4H:

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

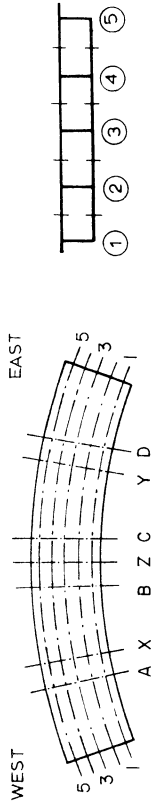
RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	4X			4Y			4X+4Y					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	87.0	15.1	104.6	19.2	-21.6	17.0	-40.8	26.4	65.4	14.6	92.0	19.6
A	2	120.6	20.9	108.7	20.0	-28.7	22.7	-26.4	17.1	91.9	20.5	91.4	19.5
A	3	129.2	22.4	109.8	20.1	-28.1	22.2	-27.6	17.8	101.1	22.5	92.6	19.8
A	4	138.6	24.1	126.6	23.2	-27.9	22.1	-32.6	21.1	110.7	24.6	109.3	23.3
A	5	100.3	17.4	95.3	17.5	-20.3	16.0	-27.3	17.6	80.0	17.8	83.1	17.7
A	SUM	575.7		545.1		-125.6		-154.8		449.2		468.4	
B	1	-29.8	12.1	-31.2	12.5	-50.0	17.1	-39.1	15.6	-79.3	14.9	-68.0	14.1
B	2	-51.0	20.7	-59.1	23.6	-62.2	21.3	-56.0	22.3	-111.9	21.1	-111.7	23.2
B	3	-72.1	29.3	-71.6	28.6	-51.8	17.8	-58.8	23.4	-121.5	22.9	-121.8	25.3
B	4	-58.0	23.6	-55.4	22.1	-71.4	24.5	-64.5	25.7	-128.0	24.1	-115.9	24.1
B	5	-35.2	14.3	-32.8	13.1	-56.1	19.2	-32.8	13.1	-90.7	17.1	-64.1	13.3
B	SUM	-246.1		-250.1		-291.5		-251.2		-531.5		-481.4	
C	1	-51.6	17.8	-35.5	14.4	-25.1	10.3	-23.7	9.0	-77.3	14.5	-62.5	11.6
C	2	-63.9	22.0	-59.2	24.0	-45.3	19.0	-46.5	17.7	-110.3	20.7	-115.1	21.4
C	3	-51.5	17.7	-53.1	21.5	-71.7	29.5	-82.3	31.3	-121.8	22.8	-146.2	27.1
C	4	-69.0	23.7	-58.9	23.9	-62.4	25.7	-76.3	29.0	-130.9	24.6	-139.7	25.9
C	5	-54.8	18.8	-40.2	16.3	-37.6	15.5	-34.1	13.0	-92.6	17.4	-75.0	13.9
C	SUM	-290.8		-246.8		-243.1		-263.0		-532.9		-538.4	
D	1	-22.0	17.3	-20.5	13.5	80.9	14.0	69.3	11.6	58.9	13.1	51.4	11.4
D	2	-29.1	22.8	-30.6	20.1	116.1	20.1	107.2	17.9	87.1	19.3	78.1	17.3
D	3	-28.2	22.2	-29.4	19.4	131.5	22.8	127.0	21.3	103.3	23.0	97.2	21.6
D	4	-27.8	21.8	-36.7	24.2	140.6	24.4	151.0	25.3	112.9	25.1	114.3	25.3
D	5	-20.2	15.9	-34.6	22.8	108.0	18.7	143.3	24.0	87.8	19.5	110.0	24.4
D	SUM	-127.2		-151.9		577.1		597.7		449.9		450.9	
LOAD	PX (KIPS)	-100.0		-100.0		0.		.0		-100.0		-100.0	
LOAD	PY (KIPS)	0.		.1		-100.0		-100.0		-100.0		-100.0	
ACTUAL	PX (KIPS)			-19.3				.0				-19.1	
ACTUAL	PY (KIPS)			.0				-19.4				-19.2	

TABLE 41

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.



RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

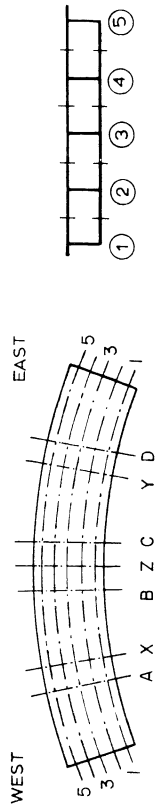
SECTION	GIRDER	4X			4Y			4X+4Y			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	87.0	32.5	15.2	-21.6	-27.6	19.3	65.4	14.6	72.1	15.3
A	2	120.6	110.6	20.3	-28.7	-29.0	20.3	91.9	20.5	94.2	20.0
A	3	129.2	121.7	22.4	-28.1	-30.5	21.4	101.1	22.5	104.5	22.2
A	4	138.6	134.0	24.7	-27.9	-32.5	22.8	110.7	24.6	116.5	24.8
A	5	100.3	94.8	17.4	-20.3	-23.1	16.2	80.0	17.8	82.9	17.6
A	SUM	575.7	543.5		-125.6	-142.6		449.2		470.1	
B	1	-29.8	-30.3	11.9	-50.0	-37.1	15.7	-79.3	14.9	-67.9	13.9
B	2	-51.0	-56.2	22.0	-62.2	-50.3	21.2	-111.9	21.1	-106.5	21.7
B	3	-72.1	-71.9	28.2	-51.8	-52.6	22.2	-121.5	22.9	-121.9	24.9
B	4	-58.0	-58.5	22.9	-71.4	-59.2	25.0	-128.0	24.1	-117.1	23.9
B	5	-35.2	-38.5	15.1	-56.1	-37.7	15.9	-90.7	17.1	-76.6	15.6
B	SUM	-246.1	-255.4		-291.5	-236.9		-531.5		-490.0	
C	1	-51.6	-35.2	15.2	-25.1	-22.6	8.6	-77.3	14.5	-63.2	11.9
C	2	-63.9	-52.7	22.7	-46.3	-48.0	18.1	-110.3	20.7	-110.1	20.7
C	3	-51.5	-47.8	20.6	-71.7	-78.2	29.5	-121.8	22.8	-135.3	25.5
C	4	-69.0	-56.2	24.2	-62.4	-74.5	28.2	-130.9	24.6	-137.3	25.9
C	5	-54.8	-40.5	17.4	-37.6	-41.3	15.6	-92.6	17.4	-84.7	16.0
C	SUM	-290.8	-232.4		-243.1	-264.6		-532.9		-530.6	
D	1	-22.0	-16.8	12.8	80.9	61.2	10.7	58.9	13.1	43.2	10.2
D	2	-29.1	-29.7	22.6	116.1	113.2	19.8	87.1	19.3	80.2	18.9
D	3	-28.2	-27.9	21.2	131.5	128.6	22.5	103.3	23.0	96.2	22.7
D	4	-27.8	-32.3	24.6	140.6	153.2	26.8	112.9	25.1	115.2	27.2
D	5	-20.2	-24.8	18.9	108.0	115.9	20.3	87.8	19.5	89.2	21.0
D	SUM	-127.2	-131.5		577.1	572.2		449.9		424.1	
LOAD	PX (KIPS)	-100.0	0.	0.	0.	0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.	0.	0.	-100.0	-100.0		-100.0		-100.9	
ACTUAL	PX (KIPS)		0.	0.		0.				-19.1	
ACTUAL	PY (KIPS)		0.	0.		-19.4				-19.2	

TABLE 4J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	4X			4Y			4X+4Y					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT		
A	1	87.0	15.1	77.7	14.3	-21.6	17.0	-26.5	18.7	65.4	14.6	68.1	14.4
A	2	120.6	20.9	111.0	20.4	-28.7	22.7	-29.5	20.8	91.9	20.5	94.8	20.1
A	3	129.2	22.4	125.3	23.0	-28.1	22.2	-31.2	22.0	101.1	22.5	108.2	22.9
A	4	138.6	24.1	135.9	25.0	-27.9	22.1	-32.5	22.9	110.7	24.6	118.3	25.1
A	5	100.3	17.4	94.5	17.4	-20.3	16.0	-21.9	15.5	80.0	17.8	82.7	17.5
A	SUM	575.7		544.4		-126.6		-141.6		449.2		472.2	
B	1	-29.8	12.1	-30.1	11.6	-50.0	17.1	-36.5	15.7	-79.3	14.9	-67.8	13.7
B	2	-51.0	20.7	-55.0	21.3	-62.2	21.3	-48.0	20.7	-111.9	21.1	-104.2	21.1
B	3	-72.1	29.3	-72.1	27.9	-51.8	17.8	-50.4	21.7	-121.5	22.9	-121.9	24.7
B	4	-58.0	23.6	-60.1	23.3	-71.4	24.5	-57.3	24.7	-128.0	24.1	-117.7	23.8
B	5	-35.2	14.3	-41.1	15.9	-56.1	19.2	-39.9	17.2	-90.7	17.1	-82.5	16.7
B	SUM	-246.1		-258.3		-291.5		-232.1		-531.5		-494.2	
C	1	-51.6	17.8	-35.2	15.5	-25.1	10.3	-22.5	8.5	-77.3	14.5	-63.4	12.0
C	2	-63.9	22.0	-50.6	22.3	-46.3	19.0	-48.7	18.3	-110.3	20.7	-107.8	20.5
C	3	-51.5	17.7	-45.7	20.1	-71.7	29.5	-76.0	28.6	-121.8	22.8	-130.0	24.7
C	4	-69.0	23.7	-54.8	24.2	-62.4	25.7	-73.6	27.7	-130.9	24.6	-136.0	25.8
C	5	-54.8	18.8	-40.6	17.9	-37.6	15.5	-44.9	15.9	-92.6	17.4	-89.2	16.9
C	SUM	-290.8		-226.9		-243.1		-265.6		-532.9		-526.4	
D	1	-22.0	17.3	-15.9	12.5	80.9	14.0	58.7	10.4	58.9	13.1	40.9	9.8
D	2	-29.1	22.8	-29.5	23.3	115.1	20.1	115.0	20.4	87.1	19.3	80.8	19.4
D	3	-28.2	22.2	-27.5	21.7	131.5	22.8	129.0	22.8	103.3	23.0	95.9	23.0
D	4	-27.8	21.8	-31.2	24.6	140.6	24.4	153.8	27.2	112.9	25.1	115.4	27.7
D	5	-20.2	15.9	-22.7	17.9	108.0	18.7	108.1	19.1	87.8	19.5	83.2	20.0
D	SUM	-127.2		-126.8		577.1		564.5		449.9		416.4	
LJAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LJAD	PY (KIPS)	0.		.1		-100.0		-100.0		-100.0		-100.9	
ACTUAL	PX (KIPS)			-19.3				.0				-19.1	
ACTUAL	PY (KIPS)			.0				-19.4				-19.2	

TABLE 5A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 30 KSI COND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT Y-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	5X		5Y		5X+5Y	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	-8.14	-2.81	-23.25	-20.51	-31.39	-23.42
2E	-2.93	-8.42	-1.70	-6.02	-4.63	-13.09
3E	-1.37	-3.05	2.03	10.44	.67	5.90
4E	-.71	5.46	12.87	9.97	12.16	13.19
5E	2.95	-.91	46.35	42.69	49.30	44.48
1F	10.14	7.72	53.96	55.76	64.09	70.00
2F	-17.30	-18.10	26.17	23.83	8.87	16.16
3F	26.89	31.54	-17.04	-20.24	9.84	5.65
4F	54.33	54.79	10.75	12.85	65.07	59.55
1W	-26.90	-16.13	-8.12	-6.44	-35.03	-20.60
2W	.30	-13.43	-2.90	-2.96	-2.60	-18.67
3W	5.47	.42	-1.39	-3.19	4.08	-1.51
4W	14.38	21.30	-.72	-.33	13.66	19.51
5W	42.90	44.21	3.00	3.75	45.91	49.92
RE	-10.20	-9.73	36.30	36.57	26.11	27.06
RF	74.05	75.95	73.83	72.20	147.88	151.36
FW	36.15	36.37	-10.13	-9.17	26.02	28.65
SUMR	100.00	102.59	100.00	99.60	200.71	207.07
PX	-100.00	-100.00	0.	-.13	-100.00	-100.00
PY	0.	.05	-100.00	-100.00	-100.00	-103.53
SUMP	-100.00	-99.95	-100.00	-100.13	-200.00	-203.53
SUMP/SUMP	1.00	1.03	1.00	.99	1.00	1.02
TW	395.40	399.85	62.83	59.20	458.34	461.12
MF	132.56	145.05	-129.62	-130.47	2.94	-31.43
TF	82.32	73.62	83.37	97.53	165.69	161.61
TE	62.78	45.49	395.63	366.36	458.41	417.02
ACTUAL PX		-19.46		-.02		-18.94
ACTUAL PY		.01		19.08		-19.62

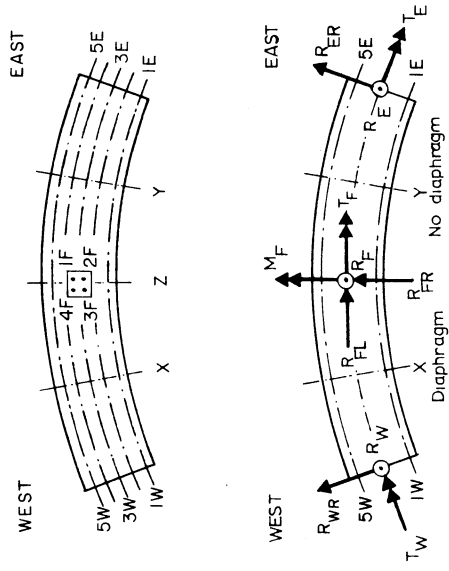
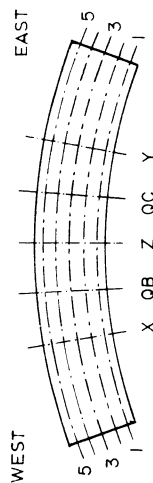


TABLE 5B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



DEFLECTION AT POINT	5X		5Y		5X+5Y	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X	.535	.778	1.45	1.45	1.45	1.45
2X	.673	.992	1.47	1.47	1.47	1.47
3X	.831	1.228	1.48	1.48	1.48	1.48
4X	1.019	1.464	1.44	1.44	1.44	1.44
5X	1.234	1.699	1.38	1.38	1.38	1.38
1QB	.267	.424	1.59	1.59	1.59	1.59
2QB	.372	.544	1.46	1.46	1.46	1.46
3QB	.489	.697	1.43	1.43	1.43	1.43
4QB	.636	.884	1.39	1.39	1.39	1.39
5QB	.791	1.017	1.29	1.29	1.29	1.29
1Z	-.127	-.111	.88	.88	.88	.88
2Z	-.051	-.052	.85	.85	.85	.85
4Z	.078	.079	1.02	1.02	1.02	1.02
5Z	.158	.184	1.16	1.16	1.16	1.16
1QC	-.331	-.420	1.27	1.27	1.27	1.27
2QC	-.287	-.384	1.34	1.34	1.34	1.34
3QC	-.244	-.341	1.40	1.40	1.40	1.40
4QC	-.209	-.305	1.46	1.46	1.46	1.46
5QC	-.168	-.251	1.50	1.50	1.50	1.50
1Y	-.337	-.468	1.39	1.39	1.39	1.39
2Y	-.311	-.434	1.39	1.39	1.39	1.39
3Y	-.288	-.409	1.42	1.42	1.42	1.42
4Y	-.256	-.426	1.60	1.60	1.60	1.60
5Y	-.246	-.371	1.51	1.51	1.51	1.51
LOAD	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	0.	0.	-100.0	-100.0	-100.0	-100.0
ACTUAL	0.	0.	0.	0.	0.	0.
ACTUAL	0.	0.	19.1	19.1	19.1	19.1

NORMALIZED POINT LOADS AT

DEFLECTION AT POINT	5X		5Y		5X+5Y	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X	-.329	-.425	1.29	1.29	1.29	1.29
2X	-.306	-.416	1.36	1.36	1.36	1.36
3X	-.284	-.400	1.41	1.41	1.41	1.41
4X	-.264	-.370	1.40	1.40	1.40	1.40
5X	-.246	-.355	1.44	1.44	1.44	1.44
1QB	-.326	-.408	1.25	1.25	1.25	1.25
2QB	-.283	-.358	1.27	1.27	1.27	1.27
3QB	-.241	-.309	1.28	1.28	1.28	1.28
4QB	-.207	-.261	1.26	1.26	1.26	1.26
5QB	-.166	-.226	1.36	1.36	1.36	1.36
1Z	-.126	-.129	1.03	1.03	1.03	1.03
2Z	-.061	-.060	.98	.98	.98	.98
4Z	.079	.099	1.25	1.25	1.25	1.25
5Z	.162	.216	1.33	1.33	1.33	1.33
1QC	.255	.338	1.33	1.33	1.33	1.33
2QC	.348	.449	1.29	1.29	1.29	1.29
3QC	.468	.601	1.28	1.28	1.28	1.28
4QC	.638	.835	1.31	1.31	1.31	1.31
5QC	.829	1.067	1.29	1.29	1.29	1.29
1Y	.504	.669	1.33	1.33	1.33	1.33
2Y	.614	.803	1.31	1.31	1.31	1.31
3Y	.773	1.011	1.31	1.31	1.31	1.31
4Y	1.009	1.332	1.32	1.32	1.32	1.32
5Y	1.361	1.914	1.41	1.41	1.41	1.41
LOAD	0.	0.	-100.0	-100.0	-100.0	-100.0
LOAD	-100.0	-100.0	0.	0.	0.	0.
ACTUAL	0.	0.	0.	0.	0.	0.
ACTUAL	0.	0.	19.1	19.1	19.1	19.1



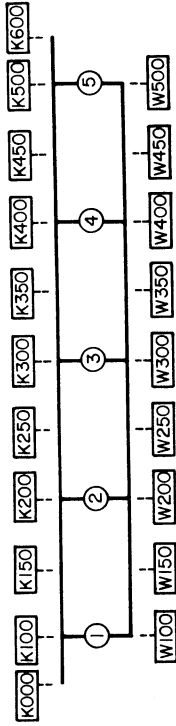
TABLE 5C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	5X		5Y		5X+5Y	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	-303	-287	83	78	-219	-209
K	K100	-250	-466	71	160	-178	-325
K	K150	-228	-293	60	67	-167	-207
K	K200	-228	-371	60	113	-167	-260
K	K250	-262	-316	61	54	-200	-248
K	K300	-280	-391	58	110	-222	-280
K	K350	-335	-365	67	84	-268	-265
K	K400	-412	-481	75	114	-337	-369
K	K450		-377		79		-276
K	K500		-482		103		-385
K	K600		-295		74		-228
W	W100	928	904	-265	-273	663	620
W	W150	862	773	-236	-185	626	568
W	W200	1033	922	-250	-256	782	647
W	W250	1091	768	-228	-225	862	505
W	W300	1315	1051	-243	-255	1071	764
W	W350		890		-205		660
W	W400		1084		-223		828
W	W450		907		-221		639
W	W500		1468		-239		1200
LOAD	PX (KIPS)	-100.0	-100.0	0.0	-0.1	-100.0	-100.0
LOAD	PY (KIPS)	0.0	.1	-100.0	-100.0	-100.0	-103.5
ACTUAL	PX (KIPS)		-19.5		-0.0		-18.9
ACTUAL	PY (KIPS)		.0		19.1		-19.6

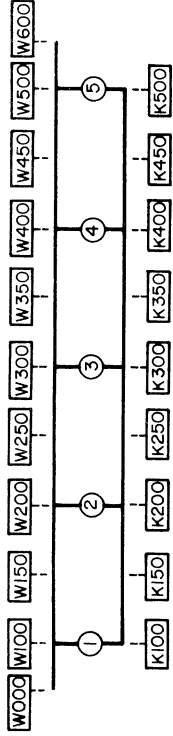
TABLE 5D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	5X			5Y			5X+5Y		
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
W	W000	252	217	217	499	286	286	751	556	556
W	W100	245	244	249	443	278	283	688	572	582
W	W150	249	203	243	325	258	288	574	501	572
W	W200	249	394	381	325	289	292	574	724	716
W	W250	385	385	441	234	241	241	615	658	718
W	W300	382	466	506	232	269	276	615	797	841
W	W350	427	427	495	389	263	305	692	725	838
W	W400	303	454	448	389	343	350	692	851	851
W	W450	429	429	485	526	356	408	845	834	939
W	W500	318	438	448	526	349	350	845	825	838
W	W600	309	475	475	564	355	355	873	868	868
K	K100	-110	-219	-224	-195	-236	-237	-306	-464	-471
K	K150	-166	-166	-169	-155	-274	-255	-268	-460	-445
K	K200	-113	-249	-238	-155	-193	-191	-268	-465	-451
K	K250	-255	-255	-226	-102	-181	-181	-255	-451	-421
K	K300	-153	-242	-250	-102	-188	-186	-255	-450	-456
K	K350	-215	-215	-214	-187	-214	-220	-326	-450	-451
K	K400	-139	-191	-183	-187	-234	-242	-326	-431	-430
K	K450	-264	-264	-246	-236	-197	-212	-384	-470	-465
K	K500	-147	-235	-237	-236	-187	-182	-384	-415	-412
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	0.	-.1	-100.0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	0.	.1	.1	-100.0	-100.0	-100.0	-100.0	-103.5	-103.5
ACTUAL	PX (KIPS)	-19.5	-19.5	-19.5	-.0	-.0	-.0	-.0	-18.9	-18.9
ACTUAL	PY (KIPS)	.0	.0	.0	19.1	19.1	19.1	19.1	-19.6	-19.6

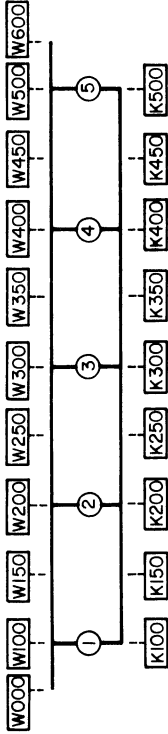
TABLE 5E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	5X		5Y		5X+5Y	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	511	303	199	148	711	500
W	W100	451	274	209	154	661	472
W	W150	255	278	172	164	457	473
W	W200	338	310	217	336	555	717
W	W250	259	261	304	293	591	583
W	W300	240	297	357	508	598	860
W	W350	388	278	310	376	698	692
W	W400	345	425	489	488	988	1004
W	W450	510	371	376	380	886	785
W	W500	545	367	383	484	929	893
W	W600	382	382	527	527	934	934
K	K100	-200	-232	-89	-199	-290	-440
K	K150	-216	-220	-97	-172	-259	-389
K	K200	-161	-236	-97	-172	-259	-404
K	K250	-200	-213	-144	-194	-249	-390
K	K300	-105	-189	-144	-230	-249	-421
K	K350	-185	-198	-145	-355	-331	-562
K	K400	-212	-204	-177	-219	-331	-446
K	K450	-311	-292	-177	-133	-405	-461
K	K500	-228	-216	-177	-277	-405	-473
LOAD	PX (KIPS)	-100.0	-100.0	0.	-.1	-100.0	-100.0
LCAD	PY (KIPS)	0.	.1	-100.0	-100.0	-100.0	-103.5
ACTUAL	PX (KIPS)	-19.5		-.0		-18.9	
ACTUAL	PY (KIPS)	.0		19.1		-19.6	

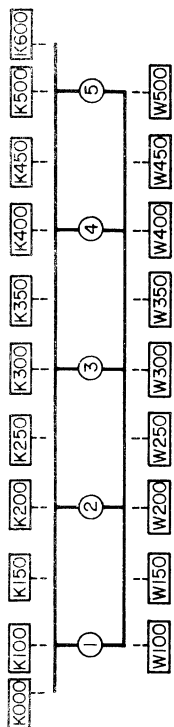
TABLE 5F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION D

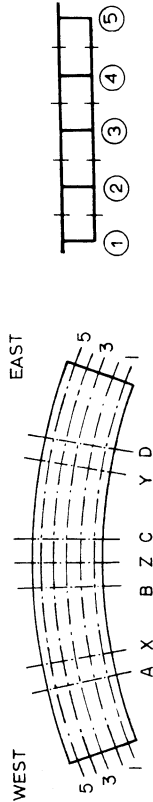
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	5X		5Y		5X+5Y	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	75	38	-243	-121	-167	-94
K	K100	64	76	-205	-234	-141	-178
K	K150	132	123	-453	-426	-135	-369
K	K200	54	117	-190	-342	-171	-269
K	K250	83	104	-320	-354	-212	-257
K	K300	55	104	-226	-377	-171	-313
K	K350	151	151	-499	-541	-420	-463
K	K400	52	125	-264	-479	-212	-426
K	K450	194	197	-721	-787	-259	-630
K	K500	59	136	-318	-531	-312	-459
K	K600	67	44	-379	-219	-181	-459
W	W100	-271	-176	829	544	558	422
W	W150	-232	-232	806	717	566	567
W	W200	-240	-244	806	824	566	650
W	W250	-236	-222	1015	783	762	624
W	W300	-252	-227	1187	874	960	730
W	W350	-187	-194	1386	987	1143	893
W	W400	-226	-247	1386	1394	1143	1267
W	W450	-218	-207	1386	1221	1143	1105
W	W500	-242	-275	1386	684	1143	510
LOAD	PX (KIPS)	-100.0	-100.0	0.	-0.1	-100.0	-100.0
LOAD	PY (KIPS)	0.	.1	-100.0	-100.0	-100.0	-103.5
ACTUAL	PX (KIPS)	-19.5	-0	-0	-0	-18.9	-18.9
ACTUAL	PY (KIPS)	.0	.0	19.1	19.1	-19.6	-19.6

TABLE 5G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )



MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION	GIRDER	5X			5Y			5X+5Y				
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT		
A	1	83.4	66.0	11.3	-23.6	17.2	-18.3	14.0	59.8	13.4	47.4	10.7
A	2	115.8	114.9	19.7	-31.3	22.7	-31.4	24.0	84.5	19.0	86.2	19.5
A	3	126.6	139.2	23.9	-30.5	22.2	-32.2	24.6	96.0	21.6	102.9	23.3
A	4	143.1	154.4	26.5	-30.3	22.0	-30.6	23.4	112.8	25.4	119.1	27.0
A	5	113.2	107.5	18.5	-22.0	16.0	-18.4	14.1	91.3	20.5	86.1	19.5
A	SUM	582.1	582.0		-137.8		-130.9		444.4		441.6	
B	1	-33.3	-27.2	9.3	-54.0	17.1	-33.6	15.4	-87.5	14.9	-66.9	12.3
B	2	-54.8	-54.6	18.7	-65.8	20.8	-41.6	19.1	-120.3	20.5	-102.2	18.8
B	3	-77.2	-79.3	27.1	-54.7	17.3	-43.3	19.9	-130.4	22.2	-130.1	24.0
B	4	-65.5	-73.5	25.1	-77.6	24.5	-53.4	24.5	-142.7	24.3	-134.3	24.7
B	5	-42.9	-57.7	19.7	-64.2	20.3	-46.2	21.2	-107.2	18.2	-109.4	20.1
B	SUM	-273.7	-292.3		-316.3		-218.2		-588.1		-542.9	
C	1	-55.2	-36.8	15.0	-28.0	10.4	-17.7	6.7	-83.5	14.3	-60.1	11.0
C	2	-68.0	-48.0	19.6	-48.5	18.1	-45.7	17.2	-116.3	19.9	-101.9	18.6
C	3	-56.1	-47.1	19.2	-73.3	27.3	-69.7	26.2	-127.8	21.9	-123.9	22.6
C	4	-76.9	-63.2	25.8	-68.5	25.5	-71.9	27.0	-144.5	24.7	-145.4	26.6
C	5	-62.3	-49.8	20.4	-50.4	18.8	-60.9	22.9	-112.2	19.2	-115.9	21.2
C	SUM	-318.5	-244.9		-268.8		-266.0		-584.3		-547.2	
D	1	-24.1	-16.3	12.7	76.3	13.1	47.6	9.2	52.2	11.7	36.3	8.6
D	2	-31.8	-33.0	25.8	108.9	18.7	105.2	20.4	77.1	17.3	82.4	19.6
D	3	-30.7	-28.9	22.6	125.0	21.4	112.7	21.9	94.2	21.2	94.9	22.6
D	4	-30.2	-30.8	24.1	152.7	26.2	172.5	33.5	122.5	27.5	152.7	36.4
D	5	-21.9	-18.9	14.7	120.6	20.7	77.4	15.0	98.7	22.2	53.2	12.7
D	SUM	-138.7	-127.8		583.5		515.3		444.7		419.6	
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.		-100.0		-100.0		-100.0	
LOAD	PY (KIPS)	0.	.1									
ACTUAL	PX (KIPS)	-19.5	-19.5									
ACTUAL	PY (KIPS)	.0	.0									

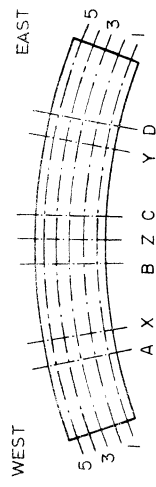
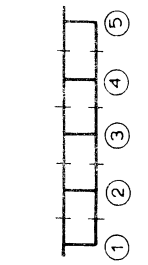


TABLE 80  
DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

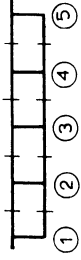
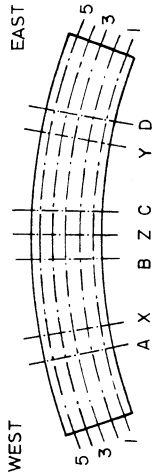
MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION	GIRDER	5X			5Y			5X+5Y					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	83.4	14.3	106.7	18.1	-23.6	17.2	-38.1	25.6	59.8	13.4	75.7	17.3
A	2	115.8	19.9	110.9	18.8	-31.3	22.7	-27.0	18.1	84.5	19.0	80.7	18.4
A	3	126.6	21.7	114.9	19.5	-30.5	22.2	-25.8	17.3	96.0	21.6	86.4	19.7
A	4	143.1	24.6	138.1	23.4	-30.3	22.0	-31.3	21.0	112.8	25.4	103.0	23.5
A	5	113.2	19.5	119.3	20.2	-22.0	16.0	-26.8	18.0	91.3	20.5	92.2	21.1
A	SUM	582.1		589.8		-137.8		-148.9		444.4		437.9	
B	1	-33.3	12.2	-35.1	13.1	-54.0	17.1	-44.8	16.9	-87.5	14.9	-81.7	15.0
B	2	-54.8	20.0	-62.3	23.3	-65.8	20.8	-60.2	22.7	-120.3	20.5	-128.0	23.5
B	3	-77.2	28.2	-70.5	26.4	-54.7	17.3	-59.6	22.5	-130.4	22.2	-135.0	24.8
B	4	-65.5	23.9	-58.1	21.7	-77.6	24.5	-67.9	25.6	-142.7	24.3	-127.6	23.4
B	5	-42.9	15.7	-41.1	15.4	-64.2	20.3	-32.5	12.3	-107.2	18.2	-72.6	13.3
B	SUM	-273.7		-267.2		-316.3		-265.0		-588.1		-544.9	
C	1	-55.2	17.3	-41.3	14.6	-28.0	10.4	-32.4	11.9	-83.5	14.3	-73.7	13.4
C	2	-68.0	21.4	-68.5	24.3	-48.5	18.1	-52.0	19.0	-116.3	19.9	-120.2	21.9
C	3	-56.1	17.6	-61.7	21.8	-73.3	27.3	-78.3	28.7	-127.8	21.9	-139.1	25.3
C	4	-76.9	24.2	-66.2	23.4	-68.5	25.5	-72.7	26.6	-144.5	24.7	-137.4	25.0
C	5	-62.3	19.5	-44.7	15.8	-50.4	18.8	-37.5	13.8	-112.2	19.2	-79.2	14.4
C	SUM	-318.5		-282.3		-268.8		-272.9		-584.3		-549.7	
D	1	-24.1	17.4	-21.5	12.4	76.3	13.1	70.1	11.3	52.2	11.7	56.2	10.7
D	2	-31.8	22.9	-33.2	19.2	108.9	18.7	102.7	16.5	77.1	17.3	81.8	15.6
D	3	-30.7	22.2	-33.1	19.2	125.0	21.4	120.1	19.3	94.2	21.2	100.2	19.1
D	4	-30.2	21.8	-43.2	25.0	152.7	26.2	162.4	26.1	122.5	27.5	140.3	26.7
D	5	-21.9	15.8	-41.5	24.1	123.6	20.7	167.4	26.9	98.7	22.2	146.0	27.8
D	SUM	-138.7		-172.5		583.5		622.7		444.7		524.5	
LOAD	PX (KIPS)	-100.0		-100.0		0.		-0.1		-100.0		-100.0	
LOAD	PY (KIPS)	0.		.1		-100.0		-100.0		-100.0		-103.5	
ACTUAL	PX (KIPS)			-19.5				-0				-18.9	
ACTUAL	PY (KIPS)			.0				19.1				-19.6	

TABLE 5I

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.



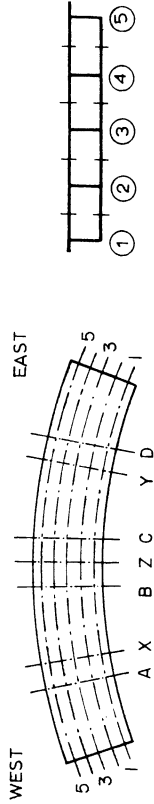
RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION	GIRDER	5X			5Y			5X+5Y		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1	83.4	84.2	14.3	-23.6	-27.1	17.2	59.8	60.0	13.4
A	2	115.8	113.2	19.9	-31.3	-29.5	22.7	84.5	83.7	19.0
A	3	126.6	128.4	21.7	-30.5	-29.3	22.2	96.0	95.6	21.6
A	4	143.1	147.2	24.6	-30.3	-30.9	22.0	112.8	111.9	25.4
A	5	113.2	112.8	19.5	-22.0	-22.2	16.0	91.3	88.8	20.5
A	SUM	582.1	585.7		-137.8	-139.0		444.4	440.1	
B	1	-33.3	-31.6	12.2	-54.0	-39.8	17.1	-87.5	-75.1	14.9
B	2	-54.8	-58.9	20.0	-65.8	-51.9	20.8	-120.3	-116.5	20.5
B	3	-77.2	-74.5	28.2	-54.7	-52.4	17.3	-130.4	-132.9	22.2
B	4	-65.5	-65.0	23.9	-77.6	-61.5	24.5	-142.7	-130.6	24.3
B	5	-42.9	-48.5	15.7	-64.2	-38.6	20.3	-107.2	-89.1	18.2
B	SUM	-273.7	-278.5		-316.3	-244.2		-588.1	-544.1	
C	1	-55.2	-39.3	17.3	-28.0	-25.9	10.4	-83.5	-67.7	14.3
C	2	-68.0	-59.4	21.4	-48.5	-49.2	18.1	-116.3	-112.1	19.9
C	3	-56.1	-55.2	17.6	-73.3	-74.5	27.3	-127.8	-132.4	21.9
C	4	-76.9	-64.9	24.2	-68.5	-72.3	25.5	-144.5	-141.0	24.7
C	5	-62.3	-47.0	19.5	-50.4	-48.0	18.8	-112.2	-95.6	19.2
C	SUM	-318.5	-265.7		-263.8	-269.9		-584.3	-548.8	
D	1	-24.1	-18.6	17.4	76.3	57.7	13.1	52.2	45.2	11.7
D	2	-31.8	-33.1	22.9	108.9	104.1	18.7	77.1	82.1	17.3
D	3	-30.7	-30.8	22.2	125.0	116.0	21.4	94.2	97.3	21.2
D	4	-30.2	-36.3	21.8	152.7	168.0	26.2	122.5	147.2	27.5
D	5	-21.9	-29.0	15.8	120.6	117.6	20.7	98.7	94.7	22.2
D	SUM	-138.7	-147.8		583.5	563.4		444.7	466.6	
LOAD	PX (KIPS)	-100.0	0.		0.	-100.0		-100.0	-100.0	
LOAD	PY (KIPS)	0.	.1		-100.0	-100.0		-100.0	-103.5	
ACTUAL	PX (KIPS)		-19.5						-18.9	
ACTUAL	PY (KIPS)		.0			19.1			-19.6	

TABLE 5J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADINGS.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS AT

SECTION	GIRDER	5X			5Y			5X+5Y					
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT			
A	1	83.4	14.3	79.3	13.5	-23.6	17.2	-25.5	18.5	59.8	13.4	57.0	12.9
A	2	115.8	19.9	113.7	19.4	-31.3	22.7	-30.0	21.8	84.5	19.0	84.5	19.1
A	3	126.6	21.7	132.6	22.7	-30.5	22.2	-30.3	22.0	96.0	21.6	98.5	22.3
A	4	143.1	24.6	149.5	25.5	-30.3	22.0	-30.9	22.4	112.8	25.4	114.3	25.9
A	5	113.2	19.5	110.5	18.9	-22.0	16.0	-21.0	15.3	91.3	20.5	87.6	19.8
A	SUM	582.1		585.6		-137.8		-137.6		444.4		441.9	
B	1	-33.3	12.2	-31.0	10.8	-54.0	17.1	-38.7	16.2	-87.5	14.9	-73.5	13.4
B	2	-54.8	20.0	-57.5	20.1	-65.8	20.8	-49.0	20.5	-120.3	20.5	-112.2	20.5
B	3	-77.2	28.2	-76.4	26.7	-54.7	17.3	-49.9	20.9	-130.4	22.2	-131.8	24.1
B	4	-65.5	23.9	-69.0	24.1	-77.6	24.5	-59.4	24.9	-142.7	24.3	-132.1	24.2
B	5	-42.9	15.7	-52.0	18.2	-64.2	20.3	-41.5	17.4	-107.2	18.2	-97.3	17.8
B	SUM	-273.7		-285.9		-316.3		-238.4		-588.1		-546.8	
C	1	-55.2	17.3	-38.8	14.9	-28.0	10.4	-25.9	9.6	-83.5	14.3	-66.7	12.1
C	2	-68.0	21.4	-56.9	21.8	-48.5	18.1	-47.9	17.7	-116.3	19.9	-108.6	19.7
C	3	-56.1	17.6	-52.7	20.2	-73.3	27.3	-72.2	26.7	-127.8	21.9	-128.8	23.4
C	4	-76.9	24.2	-64.2	24.6	-68.5	25.5	-72.2	26.7	-144.5	24.7	-142.9	26.0
C	5	-62.3	19.5	-47.9	18.4	-50.4	18.8	-52.5	19.4	-112.2	19.2	-103.2	18.8
C	SUM	-318.5		-260.5		-268.8		-270.7		-584.3		-550.2	
D	1	-24.1	17.4	-17.8	12.5	76.3	13.1	54.3	9.8	52.2	11.7	42.3	9.0
D	2	-31.8	22.9	-33.1	23.2	108.9	18.7	104.4	18.7	77.1	17.3	82.2	17.6
D	3	-30.7	22.2	-30.3	21.2	125.0	21.4	115.0	20.6	94.2	21.2	96.6	20.7
D	4	-30.2	21.8	-34.8	24.4	152.7	26.2	169.8	30.5	122.5	27.5	149.6	32.0
D	5	-21.9	15.8	-26.5	18.6	120.6	20.7	113.5	20.4	98.7	22.2	96.8	20.7
D	SUM	-138.7		-142.5		583.5		557.1		444.7		467.5	
LOAD	PX (KIPS)	-100.0		-100.0		0.		-0.1		-100.0		-100.0	
LOAD	PY (KIPS)	0.		.1		-100.0		-100.0		-100.0		-103.5	
ACTUAL	PX (KIPS)			-19.5				-0				-18.9	
ACTUAL	PY (KIPS)			.0				19.1				-19.6	



TABLE 6A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 30 KSI COND. LOADINGS.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	1X+5Y		5X+1Y		THEORY		EXPERM	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	-15.18	-15.72	33.25	21.37				
2E	-1.65	-3.47	6.64	19.90				
3E	.72	7.35	-1.78	5.62				
4E	9.96	8.87	-1.87	-4.41				
5E	36.73	33.75	-5.38	-10.20				
1F	37.82	46.33	30.67	28.34				
2F	37.77	34.52	31.42	28.60				
3F	31.36	22.67	38.77	43.03				
4F	31.41	34.74	38.02	42.60				
1W	29.07	23.74	-18.87	-11.32				
2W	8.98	13.38	.42	-10.11				
3W	2.20	7.45	4.10	2.63				
4W	.15	.78	11.35	15.73				
5W	-9.33	-13.07	33.28	36.15				
RE	30.58	30.78	30.86	32.28				
RF	138.36	138.26	138.87	142.57				
RW	31.07	32.28	30.28	33.08				
SUMR	200.01	201.32	200.01	207.93				
PX	-100.00	-100.00	-100.00	-100.00				
PY	-100.00	-100.18	-100.00	-103.31				
SUMP	-200.00	-200.18	-200.00	-203.31				
SUMR/SUMP	1.00	1.01	1.00	1.02				
TW	-220.32	-221.84	296.48	310.75				
MF	-19.22	-35.18	22.05	43.03				
TF	.15	35.82	-2.24	-1.04				
TE	296.99	286.31	-220.68	-225.00				
ACTUAL PX								-18.78
ACTUAL PY								-19.69

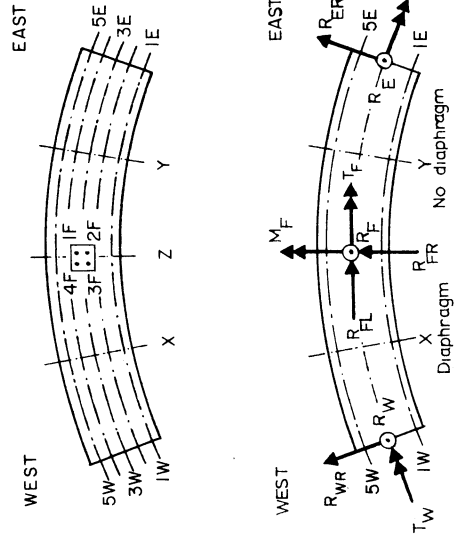
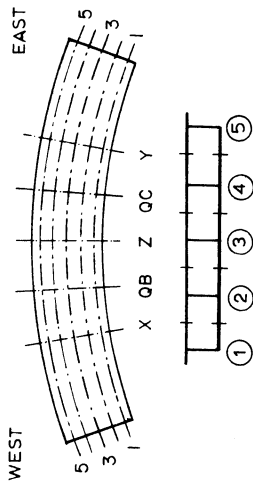


TABLE 6B

SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS AT

5X+1Y

\*\*\*\*\*  
 THEORY EXPERM E/T \*\*\*\*\*  
 \*\*\*\*\*  
 THEORY EXPERM E/T \*\*\*\*\*

DEFLECTION AT POINT  
 \*\*\*\*\*  
 THEORY EXPERM E/T \*\*\*\*\*

DEFLECTION AT POINT	THEORY	EXPERM	E/T	THEORY	EXPERM	E/T
1X	.613	.801	1.31	.382	.528	1.38
2X	.500	.662	1.32	.476	.682	1.43
3X	.408	.557	1.37	.589	.860	1.46
4X	.340	.460	1.35	.730	1.044	1.43
5X	.289	.375	1.30	.897	1.236	1.38
1QB	.300	.384	1.28	.177	.261	1.47
2QB	.230	.296	1.29	.221	.320	1.45
3QB	.166	.225	1.35	.283	.406	1.43
4QB	.122	.185	1.51	.370	.533	1.44
5QB	.094	.127	1.35	.463	.597	1.29
1Z	.034	.033	.97	.038	.084	2.20
2Z	.016	.011	.66	.018	.032	1.74
4Z	.016	.037	2.26	.015	.016	1.10
5Z	.033	.075	2.26	.030	.033	1.10
1QC	.167	.202	1.21	.351	.574	1.64
2QC	.200	.261	1.31	.242	.361	1.49
3QC	.265	.963	3.63	.154	.192	1.24
4QC	.375	1.134	3.02	.105	.143	1.36
5QC	.504	1.946	3.86	.087	.108	1.23
1Y	.351	.434	1.24	.765	1.328	1.74
2Y	.417	.396	.95	.514	.774	1.51
3Y	.535	.728	1.36	.370	.493	1.33
4Y	.726	.358	.49	.292	.338	1.16
5Y	1.032	1.510	1.46	.258	.314	1.22
LOAD PX	-100.0	-100.0		-100.0	-100.0	
LOAD PY	-100.0	-100.2		-100.0	-103.3	
ACTUAL PX		-19.6			-18.8	
ACTUAL PY		-19.7			-19.4	

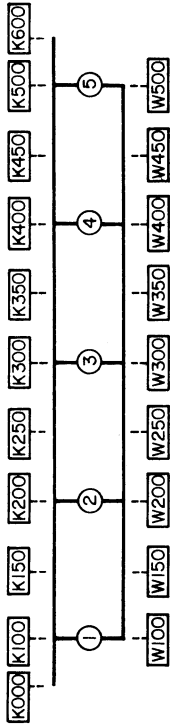
TABLE 6C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	1X+5Y		5X+1Y		MEASR		ADJUST		MEASR		ADJUST	
		THEORY	MEASR	THEORY	MEASR	THEORY	ADJUST	THEORY	ADJUST	THEORY	ADJUST	THEORY	ADJUST
K	K000	-347	-295	-247	-216	-247	-216	-247	-216	-247	-216	-247	-216
K	K100	-269	-491	-201	-347	-201	-347	-201	-347	-201	-347	-201	-347
K	K150		-279		-221		-221		-221		-221		-221
K	K200	-211	-352	-186	-292	-186	-292	-186	-292	-186	-292	-186	-292
K	K250		-201		-250		-250		-250		-250		-250
K	K300	-183	-292	-217	-323	-217	-323	-217	-323	-217	-323	-217	-323
K	K350		-231		-304		-304		-304		-304		-304
K	K400	-152	-258	-236	-412	-236	-412	-236	-412	-236	-412	-236	-412
K	K450		-187		-325		-325		-325		-325		-325
K	K500	-159	-190	-284	-425	-284	-425	-284	-425	-284	-425	-284	-425
K	K600	-186	-132	-354	-263	-354	-263	-354	-263	-354	-263	-354	-263
W	W100	1100	972	749	713	749	713	749	713	749	713	749	713
W	W150		681		616		616		616		616		616
W	W200	823	809	698	747	698	747	698	747	698	747	698	747
W	W250		690		603		603		603		603		603
W	W300	720	675	852	821	852	821	852	821	852	821	852	821
W	W350		532		724		724		724		724		724
W	W400	568	560	919	900	919	900	919	900	919	900	919	900
W	W450		547		727		727		727		727		727
W	W500	573	551	1127	1202	1127	1202	1127	1202	1127	1202	1127	1202
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0
LCAD	PY (KIPS)	-100.0	-100.2	-100.0	-103.3	-100.0	-103.3	-100.0	-103.3	-100.0	-103.3	-100.0	-103.3
ACTUAL	PX (KIPS)		-19.6		-18.8		-18.8		-18.8		-18.8		-18.8
ACTUAL	OY (KIPS)		-19.7		-19.4		-19.4		-19.4		-19.4		-19.4

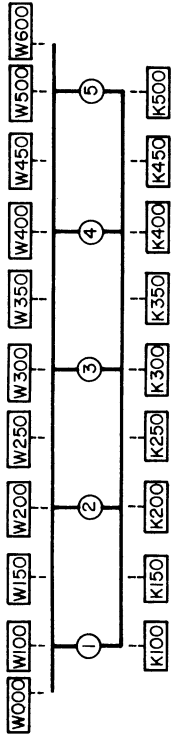
TABLE 6D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



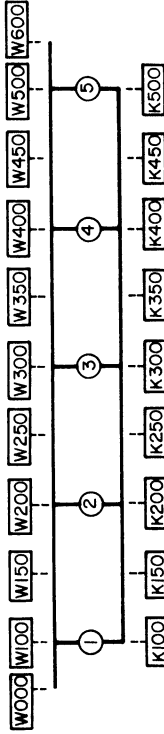
NORMALIZED POINT LOADS AT 5X+1Y

GAGE TYPE	GAGE LOC.	1X+5Y		5X+1Y		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	684	703	726	558	726	558		
W	W100	632	647	672	620	672	630		
W	W150	510	579	541	488	541	561		
W	W200	488	646	532	751	574	735		
W	W250	488	570	532	574	661	650		
W	W300	536	675	526	661	583	667		
W	W350	536	516	526	583	654	649		
W	W400	657	621	616	567	612	669		
W	W450	678	495	624	612	628	628		
W	W500		493		653		653		
W	W600								
K	K100	-287	-394	-308	-410	-308	-419		
K	K150	-238	-479	-255	-350	-255	-347		
K	K200	-202	-333	-219	-444	-219	-424		
K	K250	-253	-340	-245	-401	-245	-346		
K	K300	-295	-378	-276	-351	-276	-359		
K	K350		-391		-338		-338		
K	K400		-366		-330		-325		
K	K450		-308		-416		-399		
K	K500		-295		-379		-380		
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0		
LOAD	PY (KIPS)	-100.0	-100.2	-100.0	-103.3	-100.0	-103.3		
ACTUAL	PX (KIPS)		-19.6		-18.8		-18.8		
ACTUAL	PY (KIPS)		-19.7		-19.4		-19.4		

TABLE 6E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	IX+5Y		5X+1Y		NORMALIZED POINT LOADS AT		*****	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	624	465	814	908	814	908	814	908
W	W100	596	440	730	779	730	779	730	779
W	W150	422	409	541	646	541	646	541	646
W	W200	498	691	482	727	482	727	482	727
W	W250	492	480	593	604	593	604	593	604
W	W300	512	749	482	651	482	651	482	651
W	W350	541	546	509	475	509	475	509	475
W	W400	680	759	606	624	606	624	606	624
W	W450	709	566	607	514	607	514	607	514
W	W500		688		451		451		451
W	W600		728		428		428		428
K	K100	-267	-352	-338	-533	-338	-533	-338	-533
K	K150		-312		-442		-442		-442
K	K200	-232	-318	-257	-415	-257	-415	-257	-415
K	K250		-315		-375		-375		-375
K	K300	-211	-342	-200	-350	-200	-350	-200	-350
K	K350		-500		-317		-317		-317
K	K400	-256	-362	-238	-304	-238	-304	-238	-304
K	K450		-304		-435		-435		-435
K	K500	-310	-433	-266	-331	-266	-331	-266	-331

LOAD	PX (KIPS)	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-103.3
ACTUAL	PX (KIPS)	-19.6	-18.8
ACTUAL	PY (KIPS)	-19.7	-19.4

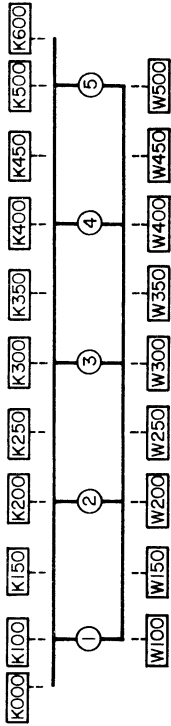
TABLE 6F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



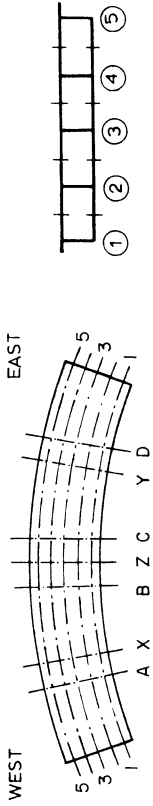
GAGE TYPE	GAGE LOC.	1X+5Y		5X+1Y		NORMALIZED POINT LOADS AT	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	-191	-88	-331	-245	-331	-245
K	K100	-161	-170	-266	-374	-266	-374
K	K150		-324		-485		-438
K	K200	-152	-264	-198	-400	-198	-399
K	K250		-246		-271		-316
K	K300	-187	-305	-151	-259	-151	-266
K	K350		-413		-276		-292
K	K400	-227	-413	-118	-192	-118	-178
K	K450		-619		-266		-237
K	K500	-275	-461	-120	-179	-120	-179
K	K600	-330	-196	-134	-54	-134	-179
W	W100	646	426	1209	712	1209	771
W	W150		555		1057		1096
W	W200	642	657	907	978	907	952
W	W250		639		679		651
W	W300	837	725	678	512	678	516
W	W350		834		467		457
W	W400	1024	1226	489	506	489	493
W	W450		1057		382		381
W	W500	1209	467	453	463	453	473
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-100.2	-100.0	-103.3	-100.0	-103.3
ACTUAL	PX (KIPS)		-19.6		-18.8		-18.8
ACTUAL	PY (KIPS)		-19.7		-19.4		-19.4

TABLE 6G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	1X+5Y		5X+1Y		NORMALIZED POINT LOADS AT		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	92.4	22.0	68.5	18.2	67.3	13.9	52.7	11.2	52.7	11.2
A	2	108.5	25.9	102.6	27.2	94.0	19.5	92.5	19.6	92.5	19.6
A	3	88.9	21.2	86.5	22.9	104.5	21.6	110.7	23.5	110.7	23.5
A	4	76.8	18.3	75.3	20.0	120.5	25.0	127.6	27.1	127.6	27.1
A	5	52.6	12.5	44.4	11.8	96.5	20.0	87.8	18.6	87.8	18.6
A	SUM	419.3		377.4		482.8		471.3		471.3	
B	1	-80.8	16.6	-80.2	18.4	-86.2	17.3	-70.2	15.2	-70.2	15.2
B	2	-106.4	21.9	-97.1	22.2	-113.6	22.7	-100.3	21.7	-100.3	21.7
B	3	-105.0	21.6	-102.3	23.4	-112.3	22.5	-110.2	23.9	-110.2	23.9
B	4	-111.4	22.9	-90.4	20.7	-109.1	21.8	-101.5	22.0	-101.5	22.0
B	5	-83.2	17.1	-66.7	15.3	-78.2	15.7	-79.2	17.2	-79.2	17.2
B	SUM	-486.9		-436.7		-499.3		-461.5		-461.5	
C	1	-76.1	15.6	-55.0	12.3	-96.8	18.9	-108.4	22.5	-108.4	22.5
C	2	-104.4	21.3	-92.1	20.7	-118.8	23.2	-118.3	24.5	-118.3	24.5
C	3	-109.0	22.3	-103.5	23.2	-108.5	21.2	-99.4	20.6	-99.4	20.6
C	4	-113.5	23.2	-108.4	24.3	-109.6	21.4	-94.1	19.5	-94.1	19.5
C	5	-86.5	17.7	-86.5	19.4	-79.1	15.4	-61.9	12.8	-61.9	12.8
C	SUM	-489.5		-445.4		-512.8		-482.1		-482.1	
D	1	59.9	12.3	37.2	9.0	102.3	24.6	73.2	19.7	73.2	19.7
D	2	87.1	17.9	83.8	20.3	117.1	28.2	130.8	35.2	130.8	35.2
D	3	103.4	21.3	94.1	22.8	84.9	20.5	69.7	18.8	69.7	18.8
D	4	131.1	27.0	147.8	35.8	67.2	16.2	63.3	17.1	63.3	17.1
D	5	104.7	21.5	49.4	12.0	43.7	10.5	34.0	9.2	34.0	9.2
D	SUM	486.2		412.4		415.1		371.1		371.1	
LOAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0		-100.0	
LOAD	PY (KIPS)	-100.0		-100.2		-100.0		-103.3		-103.3	
ACTUAL	PX (KIPS)	-19.6		-19.6		-19.6		-19.8		-19.8	
ACTUAL	PY (KIPS)	-19.7		-19.7		-19.7		-19.4		-19.4	



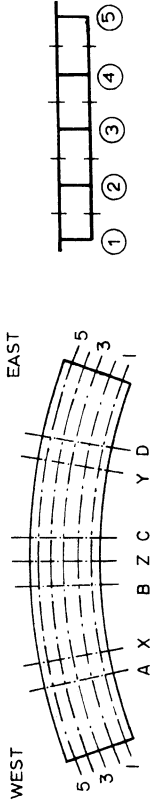


TABLE 6I

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



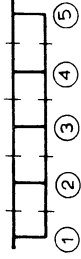
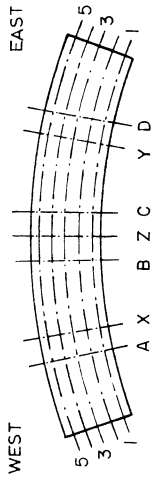
SECTION	GIRDER	1X+5Y				5X+1Y				THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	92.4	22.0	87.6	22.3	67.3	13.9	64.5	13.5	67.3	13.9	64.5	13.5
A	2	108.5	25.9	98.7	25.1	94.0	19.5	89.6	18.8	94.0	19.5	89.6	18.8
A	3	88.9	21.2	81.6	20.7	104.5	21.6	103.3	21.7	104.5	21.6	103.3	21.7
A	4	76.8	18.3	77.1	19.6	120.5	25.0	123.5	25.9	120.5	25.0	123.5	25.9
A	5	52.6	12.5	48.3	12.3	96.5	20.0	96.1	20.1	96.5	20.0	96.1	20.1
A	SUM	419.3		393.3		482.8		476.9		482.8		476.9	
B	1	-80.8	16.6	-76.2	17.1	-86.2	17.3	-67.7	14.9	-86.2	17.3	-67.7	14.9
B	2	-106.4	21.9	-102.0	22.9	-113.6	22.7	-105.7	23.3	-113.6	22.7	-105.7	23.3
B	3	-105.0	21.6	-109.3	24.5	-112.3	22.5	-107.3	23.7	-112.3	22.5	-107.3	23.7
B	4	-111.4	22.9	-100.4	22.5	-109.1	21.8	-100.4	22.1	-109.1	21.8	-100.4	22.1
B	5	-83.2	17.1	-58.5	13.1	-78.2	15.7	-72.6	16.0	-78.2	15.7	-72.6	16.0
B	SUM	-486.9		-446.4		-499.3		-453.6		-499.3		-453.6	
C	1	-76.1	15.6	-55.0	12.3	-96.8	18.9	-98.9	20.4	-96.8	18.9	-98.9	20.4
C	2	-104.4	21.3	-93.1	20.8	-118.8	23.2	-123.4	25.4	-118.8	23.2	-123.4	25.4
C	3	-109.0	22.3	-110.9	24.8	-108.5	21.2	-103.1	21.2	-108.5	21.2	-103.1	21.2
C	4	-113.5	23.2	-112.9	25.2	-109.6	21.4	-95.2	19.6	-109.6	21.4	-95.2	19.6
C	5	-86.5	17.7	-75.6	16.9	-79.1	15.4	-64.7	13.3	-79.1	15.4	-64.7	13.3
C	SUM	-489.5		-447.7		-512.8		-485.3		-512.8		-485.3	
D	1	59.9	12.3	43.0	9.5	102.3	24.6	83.4	21.7	102.3	24.6	83.4	21.7
D	2	87.1	17.9	81.0	17.9	117.1	28.2	121.1	31.5	117.1	28.2	121.1	31.5
D	3	103.4	21.3	95.3	21.0	84.9	20.5	75.2	19.6	84.9	20.5	75.2	19.6
D	4	131.1	27.0	142.1	31.3	67.2	16.2	63.2	16.5	67.2	16.2	63.2	16.5
D	5	104.7	21.5	91.9	20.3	43.7	10.5	41.2	10.7	43.7	10.5	41.2	10.7
D	SUM	486.2		453.4		415.1		384.1		415.1		384.1	
LOAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0		-100.0		-100.0	
LJAD	PY (KIPS)	-100.0		-100.2		-100.0		-103.3		-100.0		-103.3	
ACTUAL	PX (KIPS)			-19.6				-18.8				-18.8	
ACTUAL	PY (KIPS)			-19.7				-19.4				-19.4	

TABLE 6J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS AT

SECTION	GIRDER	1X+5Y			5X+1Y			THEORY			EXPERIMENTAL		
		K-FT	PCT	PCT	K-FT	PCT	PCT	K-FT	PCT	PCT	K-FT	PCT	PCT
A	1	92.4	22.0	82.6	21.2	67.3	13.9	61.0	12.8	67.3	13.9	61.0	12.8
A	2	108.5	25.9	99.8	25.7	94.0	19.5	90.4	19.0	94.0	19.5	90.4	19.0
A	3	88.9	21.2	83.2	21.4	104.5	21.6	106.0	22.3	104.5	21.6	106.0	22.3
A	4	76.8	18.3	76.7	19.7	120.5	25.0	124.8	26.3	120.5	25.0	124.8	26.3
A	5	52.6	12.5	46.6	12.0	96.5	20.0	92.7	19.5	96.5	20.0	92.7	19.5
A	SUM	419.3		388.8		482.8		474.9		482.8		474.9	
B	1	-80.8	16.6	-77.5	17.5	-86.2	17.3	-68.4	15.0	-86.2	17.3	-68.4	15.0
B	2	-106.4	21.9	-100.1	22.6	-113.6	22.7	-103.8	22.8	-113.6	22.7	-103.8	22.8
B	3	-105.0	21.6	-106.8	24.1	-112.3	22.5	-108.4	23.8	-112.3	22.5	-108.4	23.8
B	4	-111.4	22.9	-97.4	22.0	-109.1	21.8	-100.8	22.1	-109.1	21.8	-100.8	22.1
B	5	-83.2	17.1	-61.3	13.8	-78.2	15.7	-74.7	16.4	-78.2	15.7	-74.7	16.4
B	SUM	-486.9		-443.0		-499.3		-456.1		-499.3		-456.1	
C	1	-76.1	15.6	-55.0	12.4	-96.8	18.9	-101.5	21.0	-96.8	18.9	-101.5	21.0
C	2	-104.4	21.3	-92.7	20.8	-118.8	23.2	-121.7	25.2	-118.8	23.2	-121.7	25.2
C	3	-109.0	22.3	-107.6	24.2	-108.5	21.2	-101.7	21.0	-108.5	21.2	-101.7	21.0
C	4	-113.5	23.2	-111.1	25.0	-109.6	21.4	-94.8	19.6	-109.6	21.4	-94.8	19.6
C	5	-86.5	17.7	-79.0	17.7	-79.1	15.4	-64.0	13.2	-79.1	15.4	-64.0	13.2
C	SUM	-489.5		-445.3		-512.8		-483.7		-512.8		-483.7	
D	1	59.9	12.3	41.0	8.9	102.3	24.6	80.7	21.2	102.3	24.6	80.7	21.2
D	2	87.1	17.9	82.0	17.9	117.1	28.2	124.4	32.7	117.1	28.2	124.4	32.7
D	3	103.4	21.3	95.0	20.7	84.9	20.5	73.9	19.4	84.9	20.5	73.9	19.4
D	4	131.1	27.0	144.5	31.5	67.2	16.2	63.3	16.6	144.5	31.5	63.3	16.6
D	5	104.7	21.5	96.1	21.0	43.7	10.5	38.5	10.1	104.7	21.5	38.5	10.1
D	SUM	486.2		458.6		415.1		380.7		415.1		380.7	
LOAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0		-100.0		-100.0	
LOAD	PY (KIPS)	-100.0		-100.2		-100.0		-103.3		-100.0		-103.3	
ACTUAL	PX (KIPS)	-19.6		-19.6		-19.6		-18.8		-19.6		-18.8	
ACTUAL	PY (KIPS)	-19.7		-19.7		-19.7		-19.4		-19.7		-19.4	

TABLE 7A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 30 KSI CCND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OF LOAD	2X+4Y		4X+2Y		THEORY	EXPERM	THEORY	EXPERM
	THEORY	EXPERM	THEORY	EXPERM				
1E	-8.70	-7.85	9.74	8.74				
2E	.55	3.87	15.71	13.56				
3E	6.56	8.11	5.14	6.09				
4E	16.28	6.40	.41	.22				
5E	16.09	21.57	-.12	-.02				
1F	36.38	40.84	32.57	31.96				
2F	36.14	34.61	33.38	21.26				
3F	32.71	30.19	36.67	36.52				
4F	32.95	36.32	35.87	46.74				
1W	13.61	14.27	-9.34	-3.89				
2W	9.60	8.96	3.18	-5.01				
3W	5.39	7.71	6.35	3.41				
4W	3.32	3.75	10.84	11.59				
5W	-.88	-1.93	19.60	26.77				
PF	30.78	32.10	30.88	28.59				
FF	138.18	141.96	138.50	136.48				
PW	31.04	32.76	30.63	32.87				
SUMq	200.00	206.82	200.01	197.94				
PX	-100.00	-100.00	-100.00	-100.00				
PY	-100.00	-103.06	-100.00	-94.85				
SUMP	-200.00	-203.06	-200.00	-194.85				
SUMR/SUMP	1.00	1.02	1.00	1.02				
TW	-90.72	-96.77	168.63	200.43				
MF	-10.29	-13.41	9.89	45.06				
TF	.71	18.52	-2.41	31.38				
TE	168.04	157.90	-90.10	-79.40				
ACTUAL PX		-18.96		-19.44				
ACTUAL FY		-19.54		-18.44				

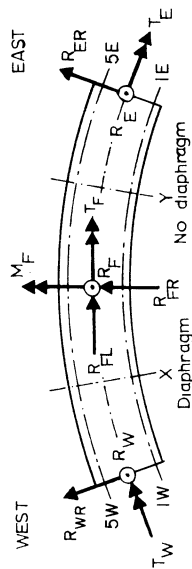
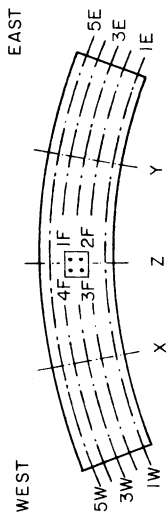
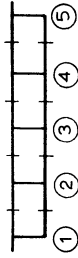
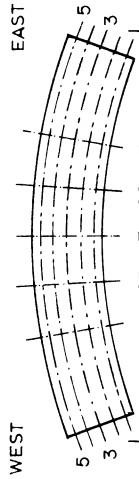


TABLE 7B

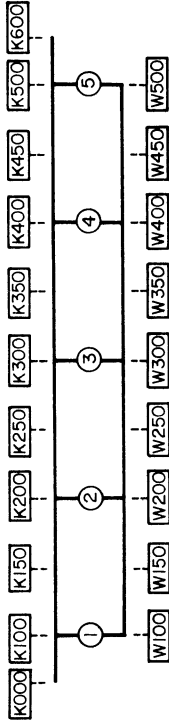
SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



DEFLECTION AT POINT	2X+4Y			4X+2Y			NORMALIZED POINT LOADS AT		
	THEORY	EXPERM	E/T	THEORY	EXPERM	E/T	THEORY	EXPERM	E/T
1X	.523	.733	1.40	.408	.578	1.42	.408	.578	1.42
2X	.514	.729	1.42	.474	.699	1.47	.474	.699	1.47
3X	.468	.682	1.46	.558	.832	1.49	.558	.832	1.49
4X	.430	.612	1.42	.650	.943	1.45	.650	.943	1.45
5X	.407	.553	1.36	.708	1.024	1.45	.708	1.024	1.45
1QB	.254	.369	1.45	.188	.264	1.41	.188	.264	1.41
2QB	.235	.330	1.40	.217	.322	1.48	.217	.322	1.48
3QB	.203	.291	1.43	.260	.386	1.48	.260	.386	1.48
4QB	.179	.259	1.44	.314	.484	1.54	.314	.484	1.54
5QB	.168	.216	1.29	.356	.495	1.39	.356	.495	1.39
1Z	.027	.052	1.93	.029	.052	1.77	.029	.052	1.77
2Z	.014	.023	1.66	.016	.020	1.22	.016	.020	1.22
4Z	.015	.023	1.55	.013	.022	1.76	.013	.022	1.76
5Z	.026	.044	1.68	.024	.050	2.08	.024	.050	2.08
1QC	.170	.228	1.34	.265	.344	1.30	.265	.344	1.30
2QC	.198	.265	1.34	.273	.360	1.32	.273	.360	1.32
3QC	.259	.350	1.35	.204	.228	1.12	.204	.228	1.12
4QC	.345	.488	1.41	.160	.179	1.12	.160	.179	1.12
5QC	.360	.491	1.36	.147	.166	1.13	.147	.166	1.13
1Y	.361	.479	1.33	.537	.736	1.37	.537	.736	1.37
2Y	.422	.555	1.31	.629	.868	1.38	.629	.868	1.38
3Y	.544	.756	1.39	.462	.579	1.25	.462	.579	1.25
4Y	.753	1.054	1.40	.378	.402	1.06	.378	.402	1.06
5Y	.703	.988	1.40	.350	.390	1.11	.350	.390	1.11
LOAD PX	-100.0	-100.0		-100.0	-100.0		-100.0	-100.0	
LOAD PY	-100.0	-103.1		-100.0	-94.8		-100.0	-94.8	
ACTUAL PX		-19.0			-19.4			-19.4	
ACTUAL PY		-19.5			-18.4			-18.4	

TABLE 7C

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	2X+4Y		4X+2Y		NORMALIZED POINT LOADS AT		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR						
K	K000	-262	-239	-243	-228	-243	-228						
K	K100	-245	-430	-206	-375	-206	-360						
K	K150	-273	-273	-188	-237	-188	-236						
K	K200	-214	-346	-188	-306	-188	-327						
K	K250	-225	-225	-217	-249	-217	-255						
K	K300	-200	-316	-217	-322	-217	-319						
K	K350	-170	-261	-225	-295	-225	-301						
K	K400	-170	-298	-225	-367	-225	-371						
K	K450	-181	-226	-248	-286	-248	-327						
K	K500	-202	-232	-259	-323	-259	-325						
K	K600	-202	-152	-259	-193	-259	-193						
W	W100	946	876	777	724	777	751						
W	W150	822	693	715	110	715	453						
W	W200	783	792	848	732	848	703						
W	W250	647	731	864	610	864	591						
W	W300	662	755	939	814	939	821						
W	W350	662	612	939	701	939	763						
W	W400	662	656	939	814	939	831						
W	W450	662	635	939	733	939	740						
W	W500	662	667	939	1050	939	1046						
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0						
L7AD	PY (KIPS)	-100.0	-103.1	-100.0	-94.8	-100.0	-94.8						
ACTUAL	PX (KIPS)	-19.0	-19.0	-19.4	-19.4	-19.0	-19.4						
ACTUAL	PY (KIPS)	-19.5	-19.5	-18.4	-18.4	-19.5	-18.4						

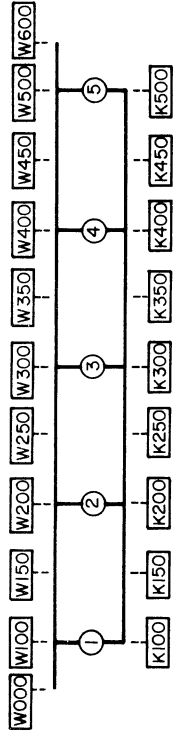
TABLE 7D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	2X+4Y		4X+2Y		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	643	638	681	551	681	551		
W	W100	597	607	631	584	631	594		
W	W150		547		487		557		
W	W200	520	674	553	710	553	699		
W	W250		593		587		650		
W	W300	520	693	542	650	542	692		
W	W350		555		550		636		
W	W400	546	597	525	598	525	596		
W	W450		561		557		628		
W	W500	617	519	583	541	583	551		
W	W600	634	525	591	572	591	572		
K	K100	-271	-372	-288	-379	-288	-386		
K	K150		-433		-366		-357		
K	K200	-241	-368	-258	-413	-258	-399		
K	K250		-371		-398		-361		
K	K300	-214	-405	-222	-363	-222	-368		
K	K350		-404		-348		-349		
K	K400	-255	-372	-243	-328	-243	-326		
K	K450		-336		-360		-355		
K	K500	-277	-313	-261	-322	-261	-320		

LOAD	PX (KIPS)	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-103.1
ACTUAL	PX (KIPS)	-19.0	-19.4
ACTUAL	PY (KIPS)	-19.5	-18.4

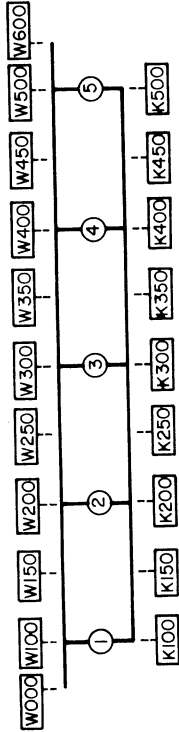
TABLE 7E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

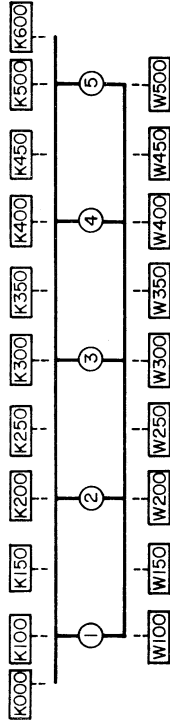


NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	2X+4Y		4X+2Y		THEORY MEASR		ADJUST	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	ADJUST	ADJUST
W	W000	610	494	714	709	714	709		
W	W100	576	466	651	616	651	627		
W	W150	509	452	573	567	573	611		
W	W200	509	694	573	773	573	774		
W	W250	539	542	524	629	524	627		
W	W300	539	774	524	694	524	688		
W	W350	564	547	511	461	511	499		
W	W400	616	763	572	598	572	625		
W	W450	635	562	575	447	575	482		
W	W500	635	607	575	445	575	433		
W	W600	635	639	575	424	575	424		
K	K100	-260	-338	-299	-410	-299	-407		
K	K150	-236	-313	-267	-397	-267	-393		
K	K200	-221	-334	-215	-457	-215	-467		
K	K250	-262	-357	-237	-423	-237	-429		
K	K300	-278	-398	-253	-394	-253	-392		
K	K350	-278	-519	-237	-347	-237	-344		
K	K400	-278	-395	-237	-304	-237	-296		
K	K450	-278	-417	-253	-394	-253	-378		
K	K500	-278	-370	-253	-303	-253	-301		
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0		
LOAD	PY (KIPS)	-100.0	-103.1	-100.0	-94.8	-100.0	-94.8		
ACTUAL	PX (KIPS)	-19.0	-19.0	-19.0	-19.4	-19.0	-19.4		
ACTUAL	PY (KIPS)	-19.5	-19.5	-19.5	-18.4	-19.5	-18.4		

TABLE 7F

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

NORMALIZED POINT LOADS AT  
 4X+2Y

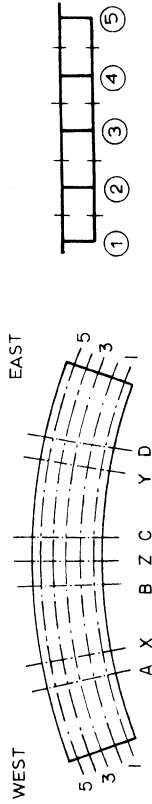
GAGE TYPE	GAGE LOC.	2X+4Y		4X+2Y		THEORY		MEASR		ADJUST	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	ADJUST	
K	K000	-193	-91	-273	-162	-273	-162	-273	-162	-273	-162
K	K100	-166	-180	-237	-298	-237	-298	-237	-298	-237	-298
K	K150	-159	-338	-192	-470	-192	-470	-192	-470	-192	-470
K	K200	-201	-272	-182	-307	-182	-307	-182	-307	-182	-307
K	K250	-200	-335	-139	-444	-139	-444	-139	-444	-139	-444
K	K300	-239	-356	-139	-368	-139	-368	-139	-368	-139	-368
K	K350	-267	-558	-153	-533	-153	-533	-153	-533	-153	-533
K	K400	695	466	1080	673	1080	673	1080	673	1080	673
K	K450	677	605	835	894	835	894	835	894	835	894
K	K500	881	679	798	723	798	723	798	723	798	723
K	K550	867	775	584	695	584	695	584	695	584	695
K	K600	1064	911	564	601	564	601	564	601	564	601
W	W100	466	473	466	473	466	473	466	473	466	473
W	W150	605	562	605	562	605	562	605	562	605	562
W	W200	699	686	699	686	699	686	699	686	699	686
W	W250	679	640	679	640	679	640	679	640	679	640
W	W300	775	768	775	768	775	768	775	768	775	768
W	W350	911	855	911	855	911	855	911	855	911	855
W	W400	927	904	927	904	927	904	927	904	927	904
W	W450	865	846	865	846	865	846	865	846	865	846
W	W500	1032	1058	1032	1058	1032	1058	1032	1058	1032	1058

LOAD PX (KIPS)	-100.0	-100.0
LOAD PY (KIPS)	-100.0	-94.8
ACTUAL PX (KIPS)	-19.0	-19.4
ACTUAL PY (KIPS)	-19.5	-18.4



TABLE 7G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



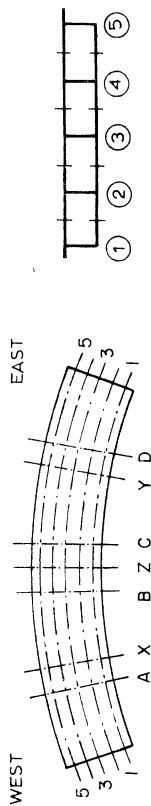
SECTION	GIRDEF	2X+4Y			4X+2Y			NORMALIZED POINT LOADS AT			
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	
A	1	81.8	18.7	64.0	15.7	69.4	14.8	50.4	11.4	50.4	11.4
A	2	109.2	25.0	101.6	25.0	96.7	20.7	88.7	20.0	88.7	20.0
A	3	97.7	22.4	98.2	24.1	105.3	22.5	108.2	24.5	108.2	24.5
A	4	97.6	20.1	89.8	22.1	114.2	24.4	116.6	26.4	116.6	26.4
A	5	60.2	13.8	53.1	13.1	82.3	17.6	78.4	17.7	78.4	17.7
A	SUM	436.4		406.7		467.9		442.2		442.2	
B	1	-76.8	15.9	-75.2	16.8	-81.6	16.6	-68.4	15.5	-68.4	15.5
B	2	-107.0	22.1	-98.9	22.1	-113.9	23.2	-98.2	22.3	-98.2	22.3
B	3	-109.5	22.6	-108.3	24.2	-113.2	23.1	-107.3	24.4	-107.3	24.4
B	4	-111.8	23.1	-95.4	21.3	-107.9	22.0	-94.6	21.5	-94.6	21.5
B	5	-78.7	16.3	-69.5	15.5	-74.5	15.2	-71.6	16.3	-71.6	16.3
B	SUM	-483.8		-447.3		-491.2		-440.2		-440.2	
C	1	-74.1	15.3	-60.4	13.1	-84.5	17.2	-84.8	18.5	-84.8	18.5
C	2	-105.3	21.7	-98.1	21.3	-117.0	23.9	-116.3	25.4	-116.3	25.4
C	3	-112.3	23.1	-109.8	23.8	-110.5	22.6	-104.0	22.7	-104.0	22.7
C	4	-114.6	23.6	-113.1	24.5	-105.3	21.5	-93.7	20.5	-93.7	20.5
C	5	-79.1	16.3	-80.1	17.4	-72.8	14.9	-59.3	12.9	-59.3	12.9
C	SUM	-485.4		-461.4		-491.1		-458.1		-458.1	
D	1	62.8	13.3	40.7	9.4	91.0	20.9	58.9	17.2	58.9	17.2
D	2	92.0	19.6	90.0	20.9	113.0	26.0	103.3	30.1	103.3	30.1
D	3	107.9	22.9	101.4	23.6	98.6	22.7	78.1	22.8	78.1	22.8
D	4	117.1	24.9	122.2	28.4	80.1	18.4	66.2	19.3	66.2	19.3
D	5	90.8	19.3	76.2	17.7	52.0	12.0	36.2	10.6	36.2	10.6
D	SUM	470.5		430.4		434.6		342.8		342.8	
LOAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0		-100.0	
LOAD	PY (KIPS)	-100.0		-103.1		-100.0		-94.8		-94.8	
ACTUAL	PX (KIPS)			-19.0				-19.4		-19.4	
ACTUAL	PY (KIPS)			-19.5				-18.4		-18.4	

TABLE 7H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



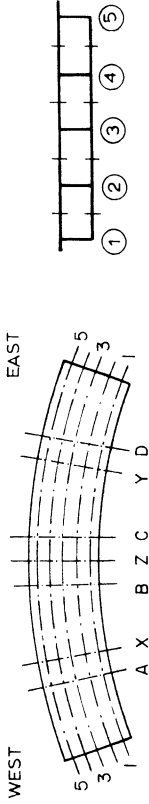
SECTION	GIRDER	2X+4Y		4X+2Y		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	81.8	18.7	97.0	22.5	69.4	14.8	85.5	18.6
A	2	109.2	25.0	95.7	22.2	95.7	20.7	89.2	19.4
A	3	97.7	22.4	83.9	19.4	105.3	22.5	92.3	20.1
A	4	87.6	20.1	91.2	21.1	114.2	24.4	109.0	23.8
A	5	60.2	13.8	63.6	14.8	82.3	17.6	82.7	18.0
A	SUM	436.4		431.4		467.9		458.8	
B	1	-76.8	15.9	-67.4	14.5	-81.6	16.6	-63.6	14.6
B	2	-107.0	22.1	-109.5	23.6	-113.9	23.2	-108.7	24.9
B	3	-109.5	22.6	-121.9	26.2	-113.2	23.1	-109.3	25.0
B	4	-111.8	23.1	-110.6	23.8	-107.9	22.0	-98.0	22.4
B	5	-78.7	16.3	-55.5	11.9	-74.5	15.2	-57.5	13.2
B	SUM	-483.8		-464.8		-491.2		-437.2	
C	1	-74.1	15.3	-54.2	11.2	-84.5	17.2	-69.4	14.6
C	2	-105.3	21.7	-100.7	20.8	-117.0	23.9	-129.6	27.2
C	3	-112.3	23.1	-131.8	27.3	-110.5	22.6	-120.6	25.3
C	4	-114.6	23.6	-128.3	26.6	-105.3	21.5	-95.5	20.1
C	5	-79.1	16.3	-68.2	14.1	-72.8	14.9	-60.6	12.7
C	SUM	-485.4		-483.1		-490.1		-475.7	
D	1	62.8	13.3	52.3	10.9	91.0	20.9	83.9	21.7
D	2	92.0	19.6	82.0	17.0	113.0	26.0	95.1	24.6
D	3	107.9	22.9	103.1	21.4	98.6	22.7	82.3	21.3
D	4	117.1	24.9	123.1	25.6	80.1	18.4	68.2	17.6
D	5	90.8	19.3	120.4	25.0	52.0	12.0	56.9	14.7
D	SUM	470.5		480.9		434.6		386.5	
LOAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0	
LOAD	PY (KIPS)	-100.0		-103.1		-100.0		-94.8	
ACTUAL	PX (KIPS)	-19.0		-19.0		-19.4		-19.4	
ACTUAL	PY (KIPS)	-19.5		-19.5		-18.4		-18.4	

\*\*\*\*\*  
THEORY  
K-FT PCT  
\*\*\*\*\*  
EXPERIMENTAL  
K-FT PCT  
\*\*\*\*\*

TABLE 71

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COMP. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



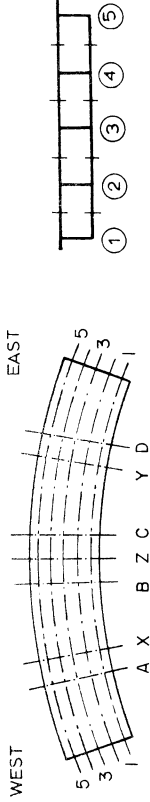
SECTION	GIRDER	2X+4Y				4X+2Y				NORMALIZED POINT LOADS AT			
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
A	1	81.8	18.7	78.7	18.8	69.4	14.8	66.1	14.7	69.4	14.8	66.1	14.7
A	2	109.2	25.0	99.0	23.7	96.7	20.7	88.9	19.8	96.7	20.7	88.9	19.8
A	3	97.7	22.4	91.8	22.0	105.3	22.5	101.2	22.5	105.3	22.5	101.2	22.5
A	4	87.6	20.1	90.5	21.7	114.2	24.4	113.2	25.2	114.2	24.4	113.2	25.2
A	5	60.2	13.8	57.8	13.8	82.3	17.6	80.4	17.9	82.3	17.6	80.4	17.9
A	SUM	436.4		417.9		467.9		449.7		467.9		449.7	
B	1	-76.8	15.9	-70.9	15.5	-81.6	16.6	-65.8	15.0	-81.6	16.6	-65.8	15.0
B	2	-107.0	22.1	-104.8	22.9	-113.9	23.2	-104.1	23.7	-113.9	23.2	-104.1	23.7
B	3	-109.5	22.6	-115.8	25.3	-113.2	23.1	-108.4	24.7	-113.2	23.1	-108.4	24.7
B	4	-111.8	23.1	-103.8	22.7	-107.9	22.0	-96.5	22.0	-107.9	22.0	-96.5	22.0
B	5	-78.7	16.3	-61.8	13.5	-74.5	15.2	-63.8	14.5	-74.5	15.2	-63.8	14.5
B	SUM	-483.8		-457.1		-491.2		-438.7		-491.2		-438.7	
C	1	-74.1	15.3	-57.0	12.0	-84.5	17.2	-76.3	16.3	-84.5	17.2	-76.3	16.3
C	2	-105.3	21.7	-99.5	21.0	-117.0	23.9	-123.7	26.4	-117.0	23.9	-123.7	26.4
C	3	-112.3	23.1	-122.0	25.8	-110.5	22.6	-113.2	24.2	-110.5	22.6	-113.2	24.2
C	4	-114.6	23.6	-121.6	25.7	-105.3	21.5	-94.7	20.2	-105.3	21.5	-94.7	20.2
C	5	-79.1	16.3	-73.5	15.5	-72.8	14.9	-60.0	12.8	-72.8	14.9	-60.0	12.8
C	SUM	-485.4		-473.6		-490.1		-468.0		-490.1		-468.0	
D	1	62.8	13.3	45.9	10.1	91.0	20.9	70.1	19.3	91.0	20.9	70.1	19.3
D	2	92.0	19.6	86.4	19.1	113.0	26.0	99.7	27.5	113.0	26.0	99.7	27.5
D	3	107.9	22.9	102.2	22.6	98.6	22.7	80.0	22.1	98.6	22.7	80.0	22.1
D	4	117.1	24.9	122.6	27.1	80.1	18.4	67.1	18.5	80.1	18.4	67.1	18.5
D	5	90.8	19.3	95.9	21.2	52.0	12.0	45.5	12.6	52.0	12.0	45.5	12.6
D	SUM	470.5		453.1		434.6		362.4		434.6		362.4	
LOAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0		-100.0		-100.0	
LOAD	PY (KIPS)	-100.0		-103.1		-100.0		-94.8		-100.0		-94.8	
ACTUAL	PX (KIPS)	-19.0		-19.0		-19.0		-19.4		-19.0		-19.4	
ACTUAL	PY (KIPS)	-19.5		-19.5		-19.5		-18.4		-19.5		-18.4	

TABLE 7J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	2X+4Y			4X+2Y			THEORY			EXPERIMENTAL		
		K-FT	PCT	PCT	K-FT	PCT	PCT	K-FT	PCT	PCT	K-FT	PCT	PCT
A	1	81.8	18.7	74.5	18.0	69.4	14.8	61.8	13.8	61.8	13.8	61.8	13.8
A	2	109.2	25.0	99.7	24.1	96.7	20.7	88.8	19.8	88.8	19.8	88.8	19.8
A	3	97.7	22.4	94.0	22.7	105.3	22.5	103.8	23.2	103.8	23.2	103.8	23.2
A	4	87.6	20.1	90.3	21.8	114.2	24.4	114.2	25.5	114.2	25.5	114.2	25.5
A	5	60.2	13.8	55.8	13.5	82.3	17.6	79.4	17.7	79.4	17.7	79.4	17.7
A	SUM	436.4		414.4		467.9		448.0		448.0		448.0	
B	1	-76.8	15.9	-72.2	15.9	-81.6	16.6	-66.6	15.2	-66.6	15.2	-66.6	15.2
B	2	-107.0	22.1	-102.6	22.6	-113.9	23.2	-102.0	23.3	-102.0	23.3	-102.0	23.3
B	3	-109.5	22.6	-113.2	25.0	-113.2	23.1	-108.0	24.6	-108.0	24.6	-108.0	24.6
B	4	-111.8	23.1	-101.2	22.3	-107.9	22.0	-95.8	21.8	-95.8	21.8	-95.8	21.8
B	5	-78.7	16.3	-64.3	14.2	-74.5	15.2	-66.4	15.1	-66.4	15.1	-66.4	15.1
B	SUM	-483.8		-453.6		-491.2		-438.9		-438.9		-438.9	
C	1	-74.1	15.3	-57.8	12.4	-84.5	17.2	-78.8	17.0	-78.8	17.0	-78.8	17.0
C	2	-105.3	21.7	-98.9	21.2	-117.0	23.9	-121.3	26.1	-121.3	26.1	-121.3	26.1
C	3	-112.3	23.1	-117.1	25.0	-110.5	22.6	-110.0	23.7	-110.0	23.7	-110.0	23.7
C	4	-114.6	23.6	-118.3	25.3	-105.3	21.5	-94.3	20.3	-94.3	20.3	-94.3	20.3
C	5	-79.1	16.3	-75.6	16.2	-72.8	14.9	-59.8	12.9	-59.8	12.9	-59.8	12.9
C	SUM	-485.4		-467.7		-490.1		-464.2		-464.2		-464.2	
D	1	62.8	13.3	43.9	9.9	91.0	20.9	66.7	18.7	66.7	18.7	66.7	18.7
D	2	92.0	19.6	87.7	19.7	113.0	26.0	100.9	28.3	100.9	28.3	100.9	28.3
D	3	107.9	22.9	101.9	22.9	98.6	22.7	79.5	22.3	79.5	22.3	79.5	22.3
D	4	117.1	24.9	122.5	27.5	80.1	18.4	66.7	18.7	66.7	18.7	66.7	18.7
D	5	90.8	19.3	89.1	20.0	52.0	12.0	42.2	11.9	42.2	11.9	42.2	11.9
D	SUM	470.5		445.2		434.6		356.0		356.0		356.0	
LOAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0		-100.0		-100.0	
LOAD	PY (KIPS)	-100.0		-103.1		-100.0		-94.8		-94.8		-94.8	
ACTUAL	PX (KIPS)	-19.0		-19.0		-19.4		-18.4		-18.4		-18.4	
ACTUAL	PY (KIPS)	-19.5		-19.5		-18.4		-18.4		-18.4		-18.4	

TABLE 8A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KS: COND. LOADING.  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS TORSIONAL RESTRAINT.

REACTION OR LOAD	(1-X)		(1-Y)		(1-X)+(1-Y)	
	THEORY	EXPEPM	THEORY	EXPEPM	THEORY	EXPERM
1E	2.04	19.48	22.32			
2E	-1.55	21.61	21.50			
3E	-2.41	9.53	6.93			
4E	-.62	-4.63	-5.95			
5E	-5.14	-7.34	-10.99			
1F	7.07	-2.76	13.31			
2F	13.07	12.99	26.77			
3F	15.75	11.03	24.20			
4F	9.27	-3.28	10.84			
1W	25.62	1.23	25.22			
2W	14.88	1.22	15.59			
3W	6.51	-2.10	7.49			
4W	2.07	-3.12	.04			
5W	-8.76	-5.39	-14.96			
FE	-7.68	38.65	33.81			
FF	45.16	17.98	75.12			
PW	40.32	-8.16	33.38			
SUMR	77.80	48.47	142.31			
PX	-100.00	-.04	-100.00			
PY	.07	-100.00	-103.38			
SUMP	-99.93	-100.04	-203.38			
SUMR/SUMP	.78	.48	.70			
TW	-209.87	45.23	-246.77			
MF	7.32	-3.72	-7.56			
TF	-18.72	-45.09	-40.23			
TE	-34.55	-205.52	-242.03			
ACTUAL PX	-19.12	-.01	-18.82			
ACTUAL PY	.01	-19.24	-19.46			

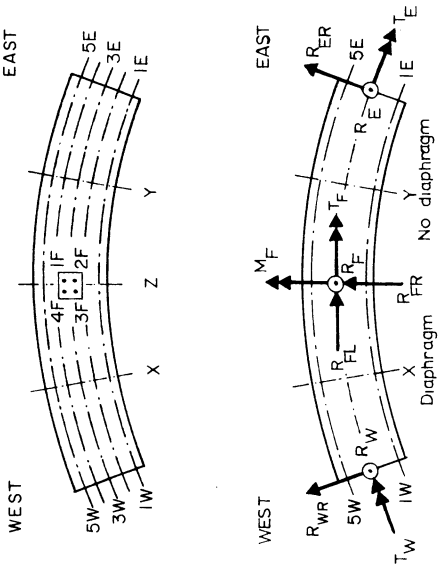
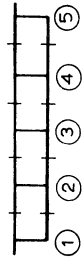
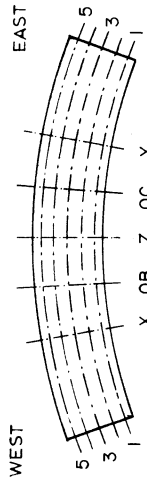


TABLE 8B

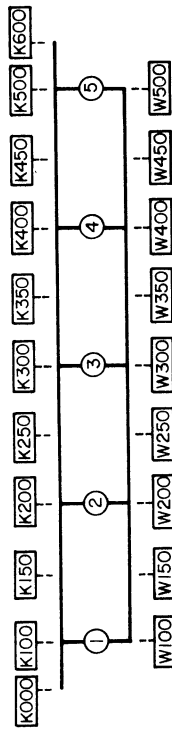
SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 TORSIONAL RESTRAINT.



DEFLECTION AT POINT	(1-X)		(1-Y)		(1-X)+(1-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X	1.156		-2.207		.898	
2X	.994		-2.234		.726	
3X	.894		-2.254		.597	
4X	.778		-2.274		.456	
5X	.687		-2.299		.341	
1QB	.678		-1.194		.475	
2QB	.576		-2.208		.345	
3QB	.498		-2.222		.257	
4QB	.445		-2.244		.168	
5QB	.380		-2.286		.065	
1Z	0.		.001		-.002	
2Z	0.		0.		-.002	
4Z	-.001		.001		-.003	
5Z	0.		-.001		-.004	
1QC	-.177		.820		.650	
2QC	-.201		.621		.434	
3QC	-.208		.445		.245	
4QC	-.229		.370		.155	
5QC	-.246		.307		.060	
1Y	-.211		1.615		1.436	
2Y	-.229		1.063		.845	
3Y	-.242		.772		.538	
4Y	-.247		.644		.391	
5Y	-.279		.608		.316	
LOAD PX	-100.0		-.0		-100.0	
LOAD PY	.1		-100.0		-103.4	
ACTUAL PX	-19.1		-.0		-18.8	
ACTUAL PY	.0		-19.2		-19.5	

TABLE 8C

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 TORSIONAL RESTRAINT.



SECTION A  
 TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		NORMALIZED POINT LOAD APPLIED AT		(1-X)+(1-Y)	
		THEORY	MEASR	THEORY	MEASF	THEORY	ADJUST	THEORY	ADJUST
K	K000	-378	-378	-378	-378	42	42	-331	-331
K	K100	-632	-614	-632	-614	81	78	-564	-548
K	K150	-360	-356	-360	-356	42	42	-305	-302
K	K200	-439	-462	-439	-462	61	65	-382	-402
K	K250	-253	-265	-253	-265	45	46	-210	-209
K	K300	-363	-356	-363	-356	57	57	-303	-296
K	K350	-287	-278	-287	-278	45	47	-234	-223
K	K400	-325	-333	-325	-333	64	65	-257	-266
K	K450	-242	-283	-242	-283	39	49	-186	-224
K	K500	-236	-235	-236	-235	56	56	-174	-172
K	K600	-160	-160	-160	-160	36	36	-123	-123
W	W100	1180	1190	1180	1190	-93	-92	1033	1039
W	W150	854	810	854	810	-82	-79	731	703
W	W200	1009	975	1009	975	-108	-107	856	829
W	W250	909	756	909	756	-80	-77	780	625
W	W300	858	857	858	857	-118	-119	695	691
W	W350	701	664	701	664	-99	-107	556	511
W	W400	741	720	741	720	-121	-123	581	559
W	W450	758	648	758	648	-89	-93	627	508
W	W500	755	742	755	742	-163	-162	561	547
LOAD	PX (KIPS)	-100.0		-100.0				-100.0	
LOAD	PY (KIPS)	.1		.1				-103.4	
ACTUAL	PX (KIPS)	-19.1		-19.1				-18.8	
ACTUAL	PY (KIPS)	.0		.0				-19.5	

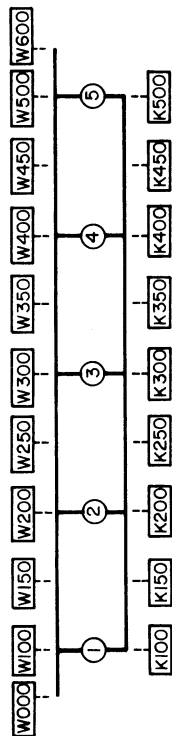
TABLE 8D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. TORSIONAL RESTRAINT.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

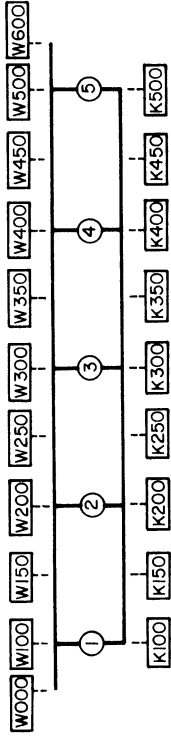


GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	472	472	382	382	841	841
W	W100	408	414	384	390	788	801
W	W150	375	410	315	357	678	757
W	W200	410	415	383	382	765	767
W	W250	362	378	229	246	575	610
W	W300	425	432	212	222	611	627
W	W350	263	310	161	183	407	472
W	W400	217	226	206	205	396	404
W	W450	179	209	199	219	353	404
W	W500	146	142	199	201	317	317
W	W600	132	132	214	214	318	318
K	K100	-274	-278	-267	-270	-519	-526
K	K150	-333	-298	-254	-242	-570	-526
K	K200	-183	-184	-209	-201	-392	-385
K	K250	-184	-227	-151	-129	-330	-350
K	K300	-232	-232	-97	-96	-331	-331
K	K350	-192	-194	-101	-100	-298	-299
K	K400	-137	-139	-111	-113	-251	-255
K	K450	-84	-100	-111	-114	-201	-217
K	K500	-84	-80	-114	-113	-191	-187
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	.1	.1	.1	.1	.1	.1
ACTUAL	PX (KIPS)	-19.1	-19.1	-19.1	-19.1	-18.8	-18.8
ACTUAL	PY (KIPS)	.0	.0	.0	.0	.0	.0



TABLE 8E

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 TORSIONAL RESTRAINT.



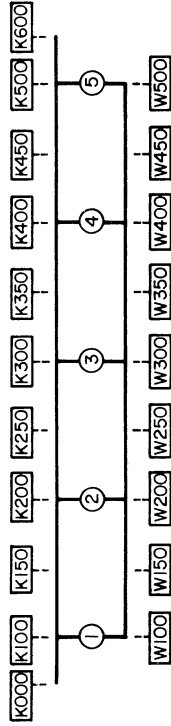
SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR ADJUST	THEORY	MEASR ADJUST	THEORY	MEASR ADJUST
W	W000		343		650		1003
W	W100		303		530		882
W	W150		276		431		700
W	W200		350		436		773
W	W250		209		373		581
W	W300		240		359		590
W	W350		155		209		349
W	W400		234		184		404
W	W450		180		123		290
W	W500		197		96		261
W	W600		210		71		238
K	K100	-220	-217	-381	-386	-587	-578
K	K150	-190	-180	-297	-352	-4720	-568
K	K200	-178	-186	-236	-244	-406	-422
K	K250	-133	-157	-219	-200	-348	-356
K	K300	-104	-99	-182	-179	-286	-280
K	K350	-127	-121	-121	-125	-244	-243
K	K400	-125	-125	-85	-83	-206	-202
K	K450	-151	-150	-104	-101	-264	-256
K	K500	-132	-131	-85	-84	-213	-211
LOAD	PX (KIPS)	-100.0					
LOAD	PY (KIPS)	.1		-100.0		-100.0	-103.4
ACTUAL	PX (KIPS)	-19.1					
ACTUAL	PY (KIPS)	.0					

TABLE 8F

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 TORSIONAL RESTRAINT.



SECTION D

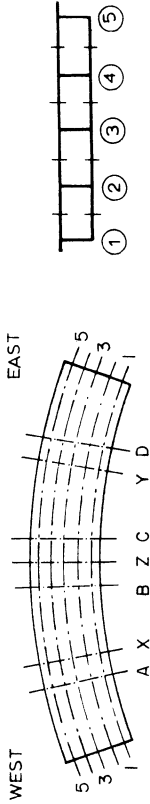
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(1-X)		NORMALIZED POINT LOAD APPLIED AT (1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	30	30	-282	-282	-259	-259
K	K100	47	48	-420	-425	-389	-393
K	K150	84	81	-540	-496	-492	-449
K	K200	62	60	-447	-445	-404	-404
K	K250	53	57	-326	-376	-282	-329
K	K300	53	56	-307	-319	-263	-273
K	K350	70	75	-333	-350	-282	-293
K	K400	56	52	-245	-230	-199	-187
K	K450	72	69	-340	-303	-268	-240
K	K500	54	57	-233	-231	-181	-177
K	K600	23	54	-76	-233	-56	-181
W	W100	-64	-65	830	903	749	821
W	W150	-97	-86	1211	1253	1122	1183
W	W200	-116	-114	1121	1090	1022	995
W	W250	-108	-97	845	808	731	702
W	W300	-113	-111	684	685	572	571
W	W350	-129	-114	597	587	469	464
W	W400	-141	-135	667	653	501	494
W	W450	-115	-117	521	514	389	379
W	W500	-109	-116	613	627	501	504
LOAD	PX (KIPS)	-100.0				-100.0	
LOAD	PY (KIPS)	.1				-103.4	
ACTUAL	PX (KIPS)	-19.1				-18.8	
ACTUAL	PY (KIPS)	.0				-19.5	

TABLE 8G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
TORSIONAL RESTRAINT.

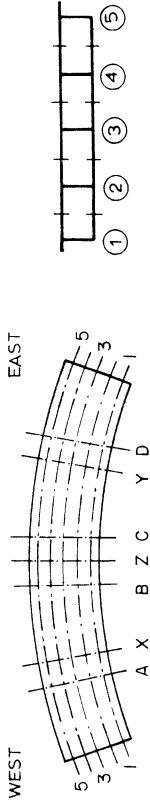


SECTION	GIRDEF	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT
A	1	83.7	17.2	-6.5	10.4	72.8	18.3
A	2	129.0	26.5	-13.3	21.5	109.6	27.6
A	3	112.5	23.1	-15.0	24.2	90.2	22.7
A	4	101.2	20.8	-16.2	26.0	78.5	19.8
A	5	60.3	12.4	-11.2	18.0	45.7	11.5
A	SUM	486.7		-62.2		396.8	
B	1	-50.9	21.9	-45.0	24.0	-95.6	23.6
B	2	-62.1	26.7	-51.2	27.3	-110.0	27.1
B	3	-61.8	26.6	-34.8	18.5	-92.8	22.9
B	4	-37.2	16.0	-30.9	16.4	-64.1	15.8
B	5	-20.2	8.7	-25.9	13.8	-42.7	10.5
B	SUM	-232.2		-187.7		-405.1	
C	1	-40.5	21.9	-68.5	28.4	-118.7	27.4
C	2	-49.5	26.7	-73.0	30.2	-124.5	28.8
C	3	-35.0	18.9	-56.3	23.3	-89.3	20.6
C	4	-34.5	18.6	-31.0	12.8	-64.7	15.0
C	5	-25.6	13.8	-12.6	5.2	-35.4	8.2
C	SUM	-185.1		-241.4		-432.6	
D	1	-5.5	9.0	84.8	18.6	78.7	20.1
D	2	-14.3	23.5	151.5	33.2	138.9	35.4
D	3	-14.4	23.7	91.0	19.9	75.8	19.3
D	4	-17.6	28.9	83.6	18.3	63.1	16.1
D	5	-9.1	14.9	45.6	10.0	35.5	9.1
D	SUM	-50.8		456.5		392.1	
LOAD	PX (KIPS)	-100.0		-0		-100.0	
LOAD	PY (KIPS)	.1		-100.0		-103.4	
ACTUAL	PX (KIPS)	-19.1		-0		-18.8	
ACTUAL	PY (KIPS)	.0		-19.2		-19.5	

TABLE 8H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL  
RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
TORSIONAL RESTRAINT.



NORMALIZED POINT LOAD APPLIED AT

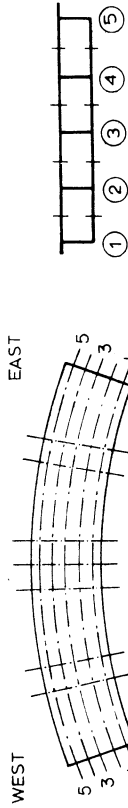
SECTION	GIRDER	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY K-FT	EXPERIMENTAL K-FT	THEORY K-FT	EXPERIMENTAL K-FT	THEORY K-FT	EXPERIMENTAL K-FT
A	1	143.1	27.5	-18.6	22.1	126.3	29.2
A	2	118.6	22.8	-17.5	20.7	100.7	23.3
A	3	95.9	18.4	-16.3	19.3	77.9	18.0
A	4	97.9	18.8	-18.1	21.4	78.5	18.1
A	5	65.0	12.5	-13.9	16.5	49.3	11.4
A	SUM	520.5		-84.4		432.7	
B	1	-51.4	21.5	-45.3	24.8	-92.7	22.1
B	2	-64.2	26.8	-55.4	30.4	-118.3	28.3
B	3	-67.7	28.3	-30.8	16.9	-99.1	23.7
B	4	-41.5	17.3	-31.8	17.5	-74.8	17.9
B	5	-14.7	6.1	-19.2	10.5	-33.8	8.1
B	SUM	-239.5		-182.4		-418.6	
C	1	-35.6	19.0	-67.3	27.9	-102.4	23.8
C	2	-52.0	27.8	-76.4	31.7	-130.8	30.4
C	3	-36.0	19.3	-52.2	21.6	-88.2	20.5
C	4	-38.5	20.6	-28.0	11.6	-65.7	15.3
C	5	-25.0	13.3	-17.1	7.1	-42.8	10.0
C	SUM	-187.1		-241.0		-429.9	
D	1	-14.9	17.5	108.1	22.9	99.3	24.3
D	2	-19.0	22.2	123.7	26.2	111.1	27.2
D	3	-17.9	20.9	97.1	20.6	83.3	20.4
D	4	-17.8	20.8	78.8	16.7	64.8	15.9
D	5	-16.0	18.7	64.0	13.6	49.5	12.1
D	SUM	-85.6		471.6		407.9	
LOAD	PX (KIPS)	-100.0					
LJAD	PY (KIPS)	.1					
ACTUAL	PX (KIPS)	-19.1		-100.0		-103.4	
ACTUAL	PY (KIPS)	.0		.0		-18.8	

TABLE 8I

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE)

MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
TOPSIONAL RESTRAINT.

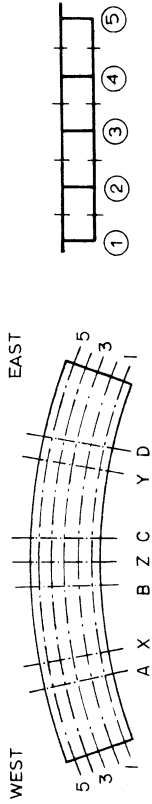


SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1	110.2	22.0		-11.9	16.5		-11.9	16.5	
	2	124.4	24.8		-15.2	21.1		-15.2	21.1	
	3	105.1	20.9		-15.6	21.6		-15.6	21.6	
	4	99.8	19.9		-17.0	23.6		-17.0	23.6	
	5	62.4	12.4		-12.4	17.2		-12.4	17.2	
	SUM	501.9			-72.1			412.9		
B	1	-51.2	21.7		-45.2	24.4		-94.0	22.8	
	2	-63.3	26.8		-53.5	29.0		-114.6	27.8	
	3	-65.1	27.5		-32.6	17.6		-96.3	23.3	
	4	-39.6	16.8		-31.4	17.0		-70.0	17.0	
	5	-17.2	7.3		-22.1	12.0		-37.8	9.2	
	SUM	-236.4			-184.8			-412.7		
C	1	-37.8	20.3		-67.8	28.1		-109.7	25.4	
	2	-50.9	27.3		-74.9	31.1		-128.1	29.7	
	3	-35.6	19.1		-54.0	22.4		-88.7	20.6	
	4	-36.7	19.7		-29.4	12.2		-65.3	15.1	
	5	-25.3	13.6		-15.1	6.3		-39.5	9.2	
	SUM	-186.2			-241.2			-431.2		
D	1	-9.7	13.5		95.2	20.5		87.9	22.0	
	2	-16.4	22.8		139.2	30.0		126.5	31.7	
	3	-15.9	22.2		93.7	20.2		79.2	19.8	
	4	-17.7	24.6		81.5	17.6		63.9	16.0	
	5	-12.1	16.9		53.8	11.6		41.8	10.5	
	SUM	-71.9		463.4			399.3			
LOAD	PX (KIPS)	-100.0								
LOAD	PY (KIPS)	.1								
ACTUAL	PX (KIPS)	-19.1								
ACTUAL	PY (KIPS)	.0								

TABLE 8J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
TORSIONAL RESTRAINT.



NORMALIZED POINT LOAD APPLIED AT

SECTION	GIRDER	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY K-FT	PCT	THEORY K-FT	PCT	THEORY K-FT	PCT
A	1	103.9	20.8	-12.0	16.9	91.3	22.3
A	2	125.7	25.2	-14.9	21.0	106.7	26.1
A	3	107.6	21.6	-15.4	21.7	86.5	21.1
A	4	100.2	20.1	-16.8	23.7	78.5	19.2
A	5	61.5	12.3	-11.9	16.7	46.6	11.4
A	SUM	498.8		-71.1		409.6	
B	1	-51.1	21.8	-45.1	24.3	-94.4	23.0
B	2	-62.7	26.7	-52.6	28.3	-112.7	27.5
B	3	-63.9	27.2	-33.5	18.0	-95.0	23.2
B	4	-38.9	16.6	-31.2	16.8	-68.2	16.6
B	5	-18.2	7.8	-23.5	12.6	-39.4	9.6
B	SUM	-234.8		-186.0		-409.7	
C	1	-38.5	20.7	-68.0	28.1	-112.2	26.0
C	2	-50.3	27.2	-74.2	30.7	-126.8	29.4
C	3	-35.3	19.1	-54.9	22.7	-88.9	20.6
C	4	-35.8	19.3	-30.1	12.4	-65.0	15.1
C	5	-25.4	13.7	-14.7	6.1	-38.8	9.0
C	SUM	-185.4		-241.9		-431.7	
D	1	-9.5	13.6	92.2	20.0	85.4	21.5
D	2	-15.9	22.7	143.5	31.1	130.9	33.0
D	3	-15.6	22.2	92.9	20.1	78.2	19.7
D	4	-17.7	25.2	82.4	17.8	63.6	16.0
D	5	-11.4	16.2	50.5	10.9	39.2	9.9
D	SUM	-70.0		461.6		397.3	
LOAD	PX (KIPS)	-100.0		-0.0		-100.0	
LJAD	PY (KIPS)	.1		-100.0		-103.4	
ACTUAL	PX (KIPS)	-19.1		-0.0		-18.8	
ACTUAL	PY (KIPS)	.0		-19.2		-19.5	

TABLE 9A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 30 KSI COND. LOADS.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS TORSIONAL RESTRAINT.

REACTION OR LOAD	(3-X)		(3-Y)		(3-X)+(3-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	1.59		-3.15		-1.56	
2E	-3.79		12.54		8.75	
3E	-2.74		12.09		9.35	
4E	1.68		.84		2.52	
5E	-4.39		14.04		9.65	
1F	5.55		39.07		44.62	
2F	-.41		40.09		39.68	
3F	24.52		-10.07		14.45	
4F	29.03		-8.25		20.78	
1W	7.11		-.21		6.90	
2W	2.01		.67		2.68	
3W	3.61		-2.42		1.19	
4W	10.21		-2.99		7.22	
5W	17.73		-3.08		14.65	
RE	-7.65		36.36		28.71	
RF	58.69		60.84		119.53	
RW	40.67		-8.03		32.64	
SUMR	91.71		89.17		180.88	
PX	-100.00		.02		-99.98	
PY	.04		-100.00		-99.96	
SUMP	-99.96		-99.98		-199.94	
SUMP/SUMP	.92		.89		.89	
TW	75.51		-24.19		51.32	
MF	72.61		-146.22		-73.61	
TF	15.71		1.20		16.91	
TE	-16.70		-58.35		-75.05	
ACTUAL FX	-19.30		-0.		-19.30	
ACTUAL PY	.01		-19.28		-19.27	

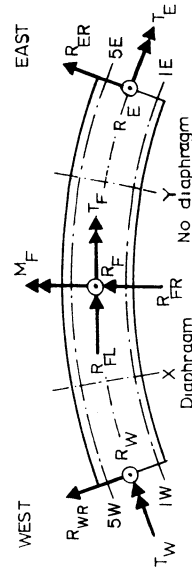
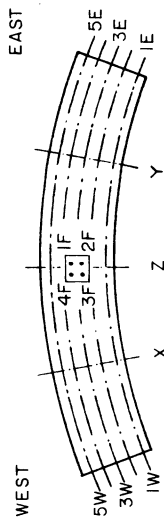
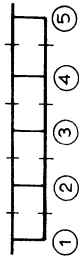
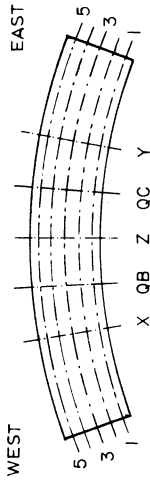


TABLE 9B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 TORSIONAL RESTRAINT.

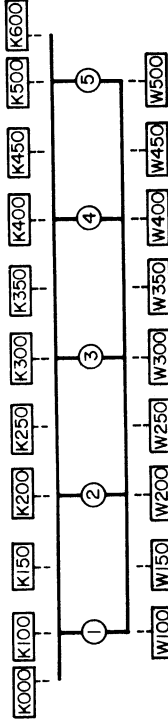


DEFLECTION AT POINT	(3-X)		(3-Y)		(3-X)+(3-Y)	
	THEORY	EXPERM E/T	THEORY	EXPERM E/T	THEORY	EXPERM E/T
1X	.909		-.353		.694	
2X	.983		-.393		.768	
3X	1.077		-.427		.838	
4X	1.097		-.420		.844	
5X	1.108		-.434		.846	
1QB	.542		-.306		.341	
2QB	.564		-.313		.348	
3QB	.609		-.319		.382	
4QB	.631		-.339		.415	
5QB	.628		-.352		.388	
1Z	0.		0.		0.	
2Z	0.		0.		0.	
4Z	0.		0.		0.	
5Z	0.		0.		0.	
1QC	-.252		.560		.209	
2QC	-.260		.611		.258	
3QC	-.261		.680		.334	
4QC	-.272		.669		.288	
5QC	-.292		.647		.243	
1Y	-.297		.914		.503	
2Y	-.316		1.051		.584	
3Y	-.314		1.339		.851	
4Y	-.328		1.126		.640	
5Y	-.373		1.084		.602	
LOAD PX	-100.0		.0		-100.0	
LOAD PY	.0		-100.0		-99.8	
ACTUAL PX	-19.3		-0.		-19.2	
ACTUAL PY	.0		-19.3		-19.2	



TABLE 9C

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 TOPSIDNAL RESTRAINT.



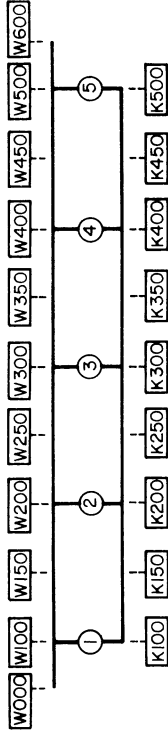
SECTION A  
 TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR ADJUST	THEORY	MEASR ADJUST	THEORY	MEASR ADJUST
K	K000	-273	-273	84	173	-245	-245
K	K100	-479	-462	173	168	-450	-431
K	K150	-300	-293	67	49	-251	-247
K	K200	-379	-400	108	111	-340	-363
K	K250	-298	-305	57	61	-244	-252
K	K300	-380	-377	96	95	-337	-333
K	K350	-328	-326	81	81	-293	-290
K	K400	-389	-394	102	107	-346	-354
K	K450	-303	-345	69	88	-265	-308
K	K500	-318	-319	92	91	-283	-283
K	K600	-196	-196	60	60	-177	-177
W	W100	937	957	-219	-222	841	855
W	W150	800	697	-179	-160	719	633
W	W200	933	888	-225	-217	824	787
W	W250	802	750	-188	-176	719	671
W	W300	974	983	-235	-236	855	862
W	W350	831	858	-196	-204	735	756
W	W400	929	928	-231	-232	816	813
W	W450	856	812	-196	-193	755	710
W	W500	1058	1053	-270	-269	900	897
LOAD	PX (KIPS)	-100.0		.0		-100.0	
LOAD	PY (KIPS)	.0		-100.0		-99.8	
ACTUAL	PX (KIPS)	-19.3		-0.		-19.2	
ACTUAL	PY (KIPS)	.0		-19.3		-19.2	

TABLE 9D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. TORSIONAL RESTRAINT.



SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE L.C.C.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000		278	310	310	607	607
W	W100		284	304	308	602	612
W	W150		249	269	301	527	596
W	W200		379	328	328	718	714
W	W250		361	244	256	608	662
W	W300		443	272	283	728	760
W	W350		335	228	262	570	658
W	W400		325	291	293	632	635
W	W450		284	280	316	574	655
W	W500		270	274	276	543	551
W	W600		281	285	285	577	577
K	K100	-170	-173	-195	-197	-357	-363
K	K150	-177	-171	-229	-215	-384	-366
K	K200	-201	-197	-181	-176	-378	-369
K	K250	-231	-228	-176	-171	-380	-368
K	K300	-239	-243	-172	-172	-382	-386
K	K350	-208	-209	-181	-182	-369	-371
K	K400	-165	-163	-184	-188	-338	-338
K	K450	-164	-166	-171	-177	-335	-340
K	K500	-152	-151	-164	-162	-313	-309
LOAD	PX (KIPS)	-100.0		.0		-100.0	
LOAD	PY (KIPS)	.0		-100.0		-99.8	
ACTUAL	PX (KIPS)	-19.3		-0.		-19.2	
ACTUAL	PY (KIPS)	.0		-19.3		-19.2	

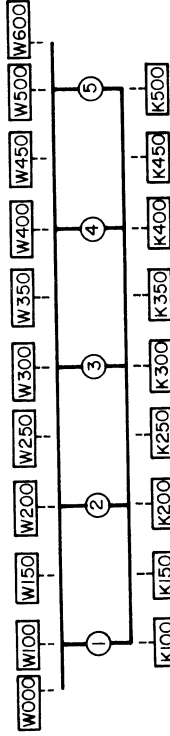
TABLE 9E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. TOPSIONAL RESTRAINT.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOAD APPLIED AT

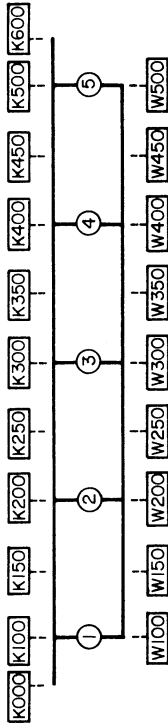
GAGE TYPE	GAGE LCC.	(3-X)		(3-Y)		(3-X)+(3-Y)		ADJUST
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	
W	W000	302	302	259	259	606	606	606
W	W100	254	267	230	230	542	542	545
W	W150	244	261	241	250	515	515	543
W	W200	316	315	398	399	758	758	759
W	W250	222	221	389	378	639	639	626
W	W300	262	260	526	523	835	835	831
W	W350	192	207	328	353	550	550	591
W	W400	312	325	355	369	729	729	751
W	W450	242	257	242	259	522	522	550
W	W500	267	261	236	231	548	548	539
W	W600	278	278	250	250	564	564	564
K	K100	-186	-182	-136	-135	-341	-341	-337
K	K150	-172	-169	-137	-121	-325	-325	-314
K	K200	-178	-187	-181	-185	-385	-385	-399
K	K250	-155	-174	-243	-276	-432	-432	-485
K	K300	-145	-142	-302	-303	-480	-480	-477
K	K350	-168	-160	-259	-254	-465	-465	-452
K	K400	-168	-165	-163	-162	-356	-356	-353
K	K450	-228	-219	-164	-162	-406	-406	-399
K	K500	-179	-177	-118	-116	-317	-317	-312

LOAD	PX (KIPS)	PY (KIPS)	ADJUST
LOAD	-100.0	.0	-100.0
LOAD	.0	-100.0	-99.8
ACTUAL	-19.3	-0.	-19.2
ACTUAL	.0	-19.3	-19.2

TABLE 9F

SUMMARY OF STRAINS (MICPC IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. TORSIONAL RESTRAINT.



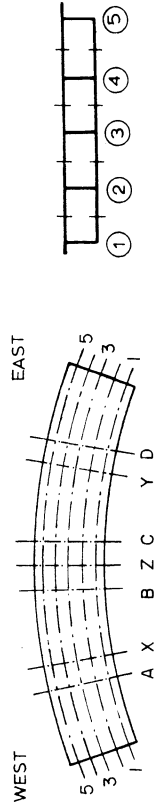
SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	34	34	-151	-151	-110	-110
K	K100	58	60	-275	-282	-205	-210
K	K150	114	110	-498	-472	-371	-350
K	K200	84	82	-401	-385	-302	-288
K	K250	66	75	-373	-418	-282	-316
K	K300	71	73	-343	-358	-250	-264
K	K350	100	105	-481	-438	-360	-322
K	K400	82	76	-384	-370	-279	-268
K	K450	127	122	-559	-504	-401	-363
K	K500	86	90	-395	-390	-288	-283
K	K600	31	86	-134	-395	-99	-288
W	W100	-118	-120	676	694	474	485
W	W150	-167	-155	938	871	666	615
W	W200	-181	-176	1068	1052	784	772
W	W250	-168	-155	1005	944	744	696
W	W300	-159	-160	1085	1066	807	789
W	W350	-166	-160	865	859	608	614
W	W400	-212	-205	1076	1066	771	770
W	W450	-176	-177	853	849	608	600
W	W500	-179	-189	964	990	699	714
LOAD	PX (KIPS)	-100.0		.0		-100.0	
LOAD	PY (KIPS)	.0		-100.0		-99.8	
ACTUAL	PX (KIPS)	-19.3		-0.		-19.2	
ACTUAL	PY (KIPS)	.0		-19.3		-19.2	

TABLE 9G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
TORSIONAL RESTRAINT.



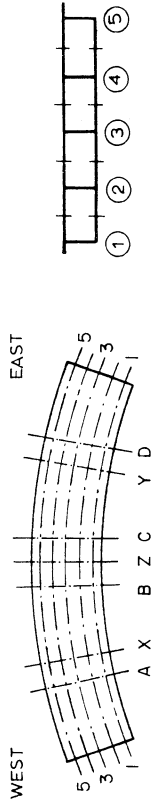
SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1		69.5	13.1		-14.7	11.8		62.2	13.4
A	2		118.1	22.3		-28.0	22.4		105.4	22.6
A	3		129.2	24.4		-30.7	24.5		113.9	24.5
A	4		130.2	24.6		-31.6	25.3		114.2	24.5
A	5		81.6	15.4		-20.1	16.1		70.0	15.0
A	SUM		528.6			-125.2			465.8	
B	1		-34.2	13.7		-36.9	18.0		-73.1	15.9
B	2		-55.0	22.1		-45.7	22.3		-101.8	22.1
B	3		-69.9	28.1		-42.7	20.8		-113.7	24.7
B	4		-53.1	21.4		-44.0	21.4		-99.2	21.5
B	5		-36.4	14.6		-35.9	17.5		-73.1	15.9
B	SUM		-248.5			-205.2			-460.8	
C	1		-36.2	17.9		-32.1	12.6		-73.8	15.2
C	2		-46.2	22.8		-59.8	23.4		-111.7	22.9
C	3		-39.0	19.3		-73.3	28.7		-118.2	24.3
C	4		-46.2	22.9		-57.0	22.3		-110.2	22.6
C	5		-34.7	17.2		-33.0	12.9		-73.1	15.0
C	SUM		-202.2			-255.1			-487.0	
D	1		-10.6	11.1		61.2	11.4		42.7	11.0
D	2		-23.2	24.4		137.9	25.6		100.4	25.8
D	3		-21.0	22.0		132.7	24.6		97.5	25.1
D	4		-26.2	27.5		133.9	24.9		95.8	24.7
D	5		-14.3	15.0		73.0	13.6		52.2	13.4
D	SUM		-95.5			538.6			388.5	
LOAD	PX (KIPS)		-100.0	.0		.0			-100.0	
LOAD	PY (KIPS)		.0	.0		-100.0			-99.8	
ACTUAL	PX (KIPS)		-19.3	.0		-0.			-19.2	
ACTUAL	PY (KIPS)		.0	.0		-19.3			-19.2	

TABLE 9H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
TORSIONAL RESTRAINT.

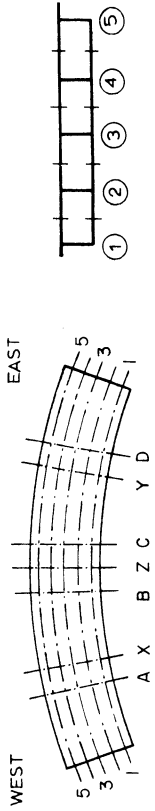


NORMALIZED POINT LOAD APPLIED AT

SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1	107.9	20.7		-40.7	28.2		97.9	21.2	
A	2	108.4	20.8		-24.6	17.0		94.2	20.4	
A	3	106.6	20.4		-25.1	17.4		92.6	20.0	
A	4	115.4	22.1		-30.4	21.1		103.6	22.4	
A	5	83.2	16.0		-23.5	16.3		74.6	16.1	
A	SUM	521.4			-144.2			462.8		
B	1	-29.2	12.5		-35.9	15.9		-61.9	14.2	
B	2	-56.7	24.3		-53.4	23.7		-105.1	24.1	
B	3	-70.3	30.2		-53.3	23.7		-113.9	26.2	
B	4	-50.2	21.5		-53.9	23.9		-99.9	22.9	
B	5	-26.6	11.4		-28.7	12.7		-54.7	12.6	
B	SUM	-232.9			-225.2			-435.5		
C	1	-31.0	14.1		-21.5	8.9		-55.8	11.3	
C	2	-53.0	24.1		-54.7	22.6		-116.2	23.5	
C	3	-47.8	21.8		-89.6	37.0		-148.4	30.0	
C	4	-52.5	23.9		-53.3	22.0		-113.4	22.9	
C	5	-35.4	16.1		-23.4	9.6		-61.5	12.4	
C	SUM	-219.7			-242.6			-495.4		
D	1	-18.5	15.3		80.3	15.0		60.0	15.2	
D	2	-25.3	20.9		117.4	22.0		88.0	22.3	
D	3	-23.5	19.4		109.2	20.4		81.2	20.6	
D	4	-27.5	22.7		118.7	22.2		86.3	21.9	
D	5	-26.3	21.7		108.4	20.3		78.6	19.9	
D	SUM	-121.1			534.1			394.0		
LOAD	PX (KIPS)	-100.0	.0		.0			-100.0		
LOAD	PY (KIPS)	.0			-100.0			-99.8		
ACTUAL	PX (KIPS)	-19.3			.0			-19.2		
ACTUAL	PY (KIPS)	.0			-19.3			-19.2		

TABLE 9I

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE)  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.



RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
TORSIONAL RESTRAINT.

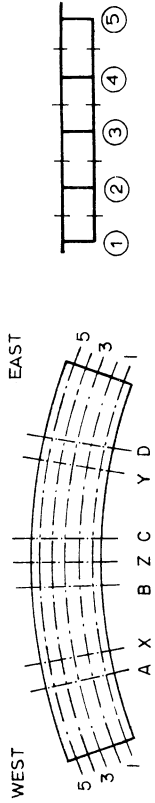
SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1		36.6	16.5		-26.3	19.7		78.2	16.8
A	2		113.8	21.6		-26.5	19.8		100.4	21.6
A	3		119.2	22.7		-28.2	21.1		104.4	22.5
A	4		123.7	23.5		-31.1	23.3		109.5	23.5
A	5		82.3	15.7		-21.6	16.2		72.1	15.5
A	SUM		525.5			-133.7			464.6	
B	1		-31.4	13.1		-36.3	16.8		-66.9	15.0
B	2		-55.9	23.3		-50.0	23.1		-103.6	23.2
B	3		-70.1	29.2		-48.6	22.5		-113.8	25.5
B	4		-51.5	21.5		-49.5	22.9		-99.6	22.3
B	5		-31.0	12.9		-31.9	14.7		-62.9	14.1
B	SUM		-240.0			-216.3			-446.9	
C	1		-33.3	15.7		-26.3	10.6		-63.9	13.0
C	2		-50.0	23.6		-57.0	23.0		-114.2	23.2
C	3		-43.9	20.7		-82.4	33.2		-135.0	27.4
C	4		-49.7	23.5		-55.0	22.1		-112.0	22.8
C	5		-35.1	16.6		-27.6	11.1		-66.7	13.6
C	SUM		-212.0			-248.2			-491.8	
D	1		-14.1	13.2		69.7	13.0		50.4	12.9
D	2		-24.2	22.6		128.8	24.0		94.9	24.3
D	3		-22.1	20.7		122.3	22.8		90.3	23.1
D	4		-26.8	25.1		127.2	23.7		91.6	23.4
D	5		-19.7	18.4		88.8	16.6		64.0	16.4
D	SUM		-106.9			536.8			391.1	
LOAD	PX (KIPS)		-100.0			.0			-100.0	
LOAD	PY (KIPS)		.0			-100.0			-99.8	
ACTUAL	PX (KIPS)		-19.3			.0			-19.2	
ACTUAL	PY (KIPS)		.0			-19.3			-19.2	

TABLE 9J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
TORSIONAL RESTRAINT.



SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1		82.0	15.5		-25.9	19.3		74.2	15.9
A	2		115.1	21.8		-26.9	20.0		101.9	21.9
A	3		122.9	23.3		-29.1	21.7		108.0	23.2
A	4		125.8	23.8		-31.3	23.3		111.0	23.8
A	5		82.0	15.5		-21.0	15.6		71.1	15.3
A	SUM		527.8			-134.1			466.2	
B	1		-32.3	13.3		-36.5	17.2		-68.9	15.3
B	2		-55.6	22.9		-48.4	22.7		-102.9	22.8
B	3		-70.0	28.8		-46.7	22.0		-113.7	25.2
B	4		-52.1	21.5		-47.9	22.5		-99.4	22.0
B	5		-32.9	13.6		-33.2	15.6		-66.5	14.7
B	SUM		-242.9			-212.7			-451.5	
C	1		-34.1	16.4		-28.2	11.2		-66.9	13.7
C	2		-48.7	23.4		-58.2	23.2		-113.2	23.1
C	3		-42.1	20.2		-79.3	31.6		-129.2	26.4
C	4		-48.3	23.2		-55.9	22.2		-111.3	22.7
C	5		-35.0	16.8		-29.7	11.8		-68.8	14.1
C	SUM		-208.2			-251.3			-489.5	
D	1		-13.3	12.8		66.7	12.4		47.9	12.2
D	2		-23.9	23.0		132.4	24.6		97.1	24.8
D	3		-21.8	21.0		126.8	23.5		93.4	23.9
D	4		-26.6	25.6		130.0	24.1		93.3	23.8
D	5		-18.2	17.5		83.0	15.4		59.7	15.2
D	SUM		-103.8			538.9			391.4	
LOAD	PX (KIPS)		-100.0			.0			-100.0	
LOAD	PY (KIPS)		.0			-100.0			-99.8	
ACTUAL	PX (KIPS)		-19.3			.0			-19.2	
ACTUAL	PY (KIPS)		.0			-19.3			-19.2	



TABLE 10A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 30 KSI COND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS TORSIONAL RESTRAINT.

REACTION OR LOAD	(5-X)		NORMALIZED POINT LOAD APPLIED AT (5-Y)		(5-X)+(5-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E		1.27		-19.21		-17.82
2E		-6.48		-3.45		-7.51
3E		-3.34		11.16		6.45
4E		4.19		8.03		10.49
5E		-4.66		39.34		37.44
1F		-10.04		35.73		37.29
2F		-23.10		20.21		-2.81
3F		44.06		-9.66		8.53
4F		53.93		6.97		48.07
1W		-13.34		-1.50		-16.17
2W		-10.79		-2.06		-12.09
3W		.72		-3.05		1.46
4W		19.27		-3.27		16.69
5W		41.88		-.01		41.33
RE		-9.02		35.87		29.05
RF		64.85		53.25		91.08
FW		37.74		-9.89		31.22
SUMR		93.57		79.23		151.35
PX		-100.00		-.04		-100.00
PY		.09		-100.00		-100.36
SUMP		-99.91		-100.04		-200.36
SUMP/SUMP		.94		.79		.76
TW		361.49		4.55		369.70
MF		196.69		-87.94		33.18
TF		34.39		48.22		119.46
TE		-3.06		330.82		330.67
ACTUAL PX		-19.24		-.01		-18.82
ACTUAL PY		.02		-19.37		-19.46

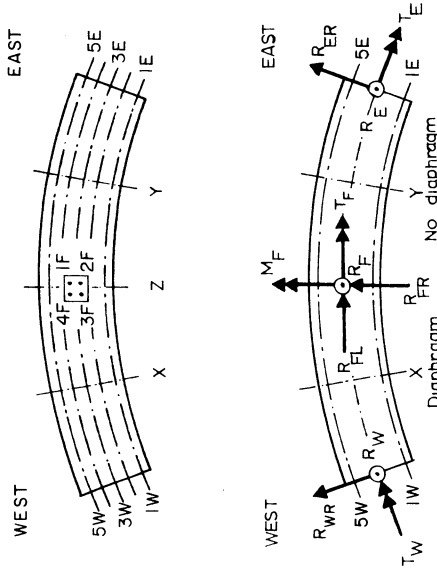
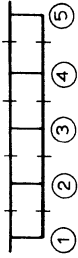
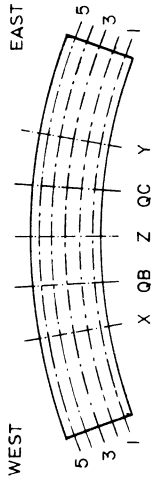


TABLE 10B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 TORSIONAL RESTRAINT.



NORMALIZED POINT LOAD APPLIED AT (5-X)  
 (5-Y)  
 (5-X)+(5-Y)

DEFLECTION AT POINT	(5-X)		(5-Y)		(5-X)+(5-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X	.848		-.350		.382	
2X	1.057		-.359		.561	
3X	1.272		-.366		.765	
4X	1.497		-.352		.983	
5X	1.730		-.361		1.216	
1QB	.497		-.335		.091	
2QB	.602		-.315		.211	
3QB	.732		-.296		.349	
4QB	.887		-.296		.503	
5QB	.988		-.285		.611	
1Z	-.001		-.001		.003	
2Z	0.		-.001		.003	
4Z	0.		-.001		.003	
5Z	0.		-.001		.003	
1QC	-.372		.390		.042	
2QC	-.368		.481		.143	
3QC	-.364		.605		.276	
4QC	-.381		.828		.490	
5QC	-.386		1.016		.678	
1Y	-.445		.718		.292	
2Y	-.455		.838		.402	
3Y	-.460		1.038		.611	
4Y	-.448		1.397		.949	
5Y	-.476		1.993		1.539	
LOAD PX	-100.0		-.0		-100.0	
LOAD PY	.1		-100.0		-100.4	
ACTUAL PX	-19.2		-.0		-18.8	
ACTUAL PY	.0		-19.4		-19.5	

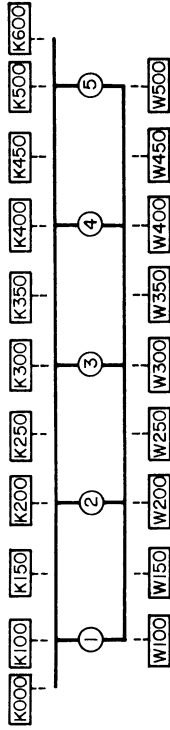
TABLE 10C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. TORSIONAL RESTRAINT.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

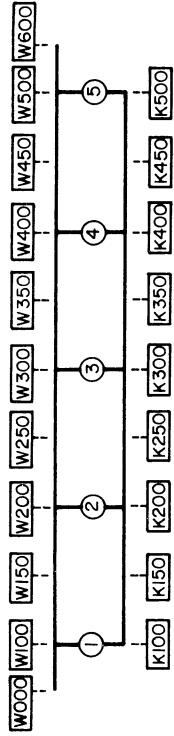


NORMALIZED POINT LOAD APPLIED AT

GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	-291	-291	77	171	-198	-198
K	K100	-491	-469	171	164	-320	-306
K	K150	-284	-281	63	64	-193	-191
K	K200	-374	-401	107	115	-255	-273
K	K250	-309	-321	53	54	-234	-241
K	K300	-393	-394	90	89	-284	-287
K	K350	-369	-383	69	67	-268	-283
K	K400	-493	-491	93	92	-379	-373
K	K450	-395	-433	58	63	-291	-321
K	K500	-496	-502	77	78	-398	-404
K	K600	-313	-313	51	51	-244	-244
W	W100	929	951	-190	-195	620	606
W	W150	814	691	-133	-117	564	537
W	W200	954	906	-191	-181	642	634
W	W250	773	776	-167	-138	469	517
W	W300	1082	1096	-197	-197	762	776
W	W350	939	1033	-161	-158	671	766
W	W400	1159	1191	-185	-182	855	889
W	W450	936	1035	-170	-154	636	763
W	W500	1558	1567	-222	-220	1239	1253
LOAD	PX (KIPS)	-100.0				-100.0	
LOAD	PY (KIPS)	.1				-100.4	
ACTUAL	PX (KIPS)	-19.2				-18.8	
ACTUAL	PY (KIPS)	.0				-19.5	

TABLE 10D

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 TORSIONAL RESTRAINT.



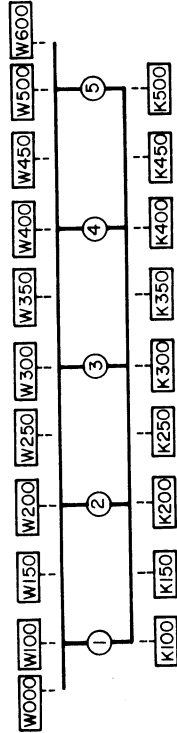
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)		MEASR	ADJUST
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR		
W	W000	185	185	308	308	483	483		
W	W100	229	235	304	308	512	521		
W	W150	184	215	272	299	427	483		
W	W200	404	389	318	322	667	656		
W	W250	372	424	245	253	578	635		
W	W300	487	525	314	320	743	786		
W	W350	428	483	291	331	666	760		
W	W400	494	485	416	420	840	835		
W	W450	440	503	400	458	797	908		
W	W500	456	469	397	402	798	817		
W	W600	504	504	413	413	870	870		
K	K100	-147	-153	-190	-192	-318	-323		
K	K150	-78	-91	-222	-207	-312	-305		
K	K200	-211	-211	-167	-164	-367	-353		
K	K250	-232	-221	-154	-153	-388	-351		
K	K300	-203	-203	-167	-165	-382	-386		
K	K350	-187	-186	-209	-210	-403	-403		
K	K400	-181	-173	-238	-245	-419	-417		
K	K450	-284	-264	-234	-245	-520	-509		
K	K500	-284	-287	-233	-229	-507	-506		
LOAD	PX (KIPS)	-100.0				-100.0			
LOAD	PY (KIPS)	.1		-100.0		-100.4			
ACTUAL	PX (KIPS)	-19.2				-18.8			
ACTUAL	PY (KIPS)	.0				-19.5			

TABLE 10E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. TORSIONAL RESTRAINT.



SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LCC.	(5-X)		(5-Y)		(5-X)+(5-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	312	312	158	158	441	441
W	W100	269	275	175	164	418	418
W	W150	249	273	184	165	400	402
W	W200	326	326	374	377	653	656
W	W250	257	260	312	302	519	512
W	W300	323	321	546	552	804	808
W	W350	259	287	391	416	607	649
W	W400	448	464	586	577	993	994
W	W450	355	376	444	424	748	745
W	W500	397	388	558	565	905	908
W	W600	407	407	628	628	986	986
K	K100	-187	-184	-162	-154	-314	-310
K	K150	-176	-181	-135	-120	-280	-263
K	K200	-195	-206	-148	-157	-315	-330
K	K250	-191	-207	-185	-233	-349	-413
K	K300	-194	-190	-225	-209	-391	-371
K	K350	-221	-213	-382	-361	-574	-546
K	K400	-229	-224	-248	-260	-459	-484
K	K450	-316	-304	-115	-134	-418	-471
K	K500	-250	-248	-339	-348	-575	-563
LOAD	PX (KIPS)	-100.0				-100.0	
LOAD	PY (KIPS)	.1				-100.4	
ACTUAL	PX (KIPS)	-19.2				-18.8	
ACTUAL	PY (KIPS)	.0				-19.5	

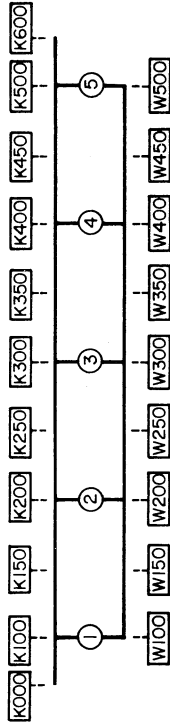
TABLE 10F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
TORSIONAL RESTRAINT.

SECTION D

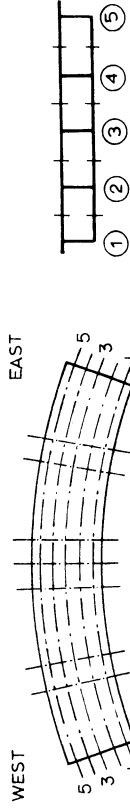
TENSION = + K = CONCRETE STRAIN METERS  
COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		NORMALIZED POINT LOAD APPLIED AT		(5-X)+(5-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000		47		-122		-122		-78
K	K100		82		-221		-221		-143
K	K150		156		-412		-412		-283
K	K200		119		-327		-316		-227
K	K250		91		-310		-349		-225
K	K300		101		-366		-383		-291
K	K350		145		-480		-517		-404
K	K400		120		-487		-481		-395
K	K450		182		-711		-738		-583
K	K500		121		-520		-526		-441
K	K600		43		-230		-520		-188
W	W100	-190	-195	553	564	338	346		
W	W150	-262	-248	733	677	461	418		
W	W200	-270	-265	820	803	550	536		
W	W250	-252	-233	789	751	550	519		
W	W300	-257	-254	869	874	634	642		
W	W350	-228	-222	1033	983	819	776		
W	W400	-279	-273	1445	1392	1203	1151		
W	W450	-232	-231	1315	1171	1094	953		
W	W500	-253	-263	632	656	351	374		
LOAD	PX (KIPS)	-100.0						-100.0	
LOAD	PY (KIPS)	.1		-100.0				-100.4	
ACTUAL	PX (KIPS)	-19.2						-18.8	
ACTUAL	PY (KIPS)	.0		-19.4				-19.5	

TABLE 10G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
TORSIONAL RESTRAINT.



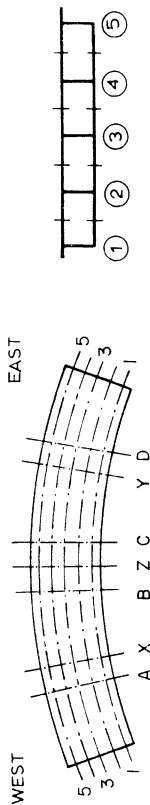
SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1		68.7	11.2		-11.6	11.7		-11.6	11.7
A	2		119.6	19.6		-22.0	22.1		-22.0	22.1
A	3		144.7	23.7		-24.8	25.0		-24.8	25.0
A	4		164.1	26.8		-24.7	24.9		-24.7	24.9
A	5		114.3	18.7		-16.3	16.4		-16.3	16.4
A	SUM		611.4			-99.3			-99.3	
B	1		-25.5	8.6		-36.9	15.1		-36.9	15.1
B	2		-53.3	18.1		-45.0	18.4		-45.0	18.4
B	3		-79.6	27.0		-48.6	19.9		-48.6	19.9
B	4		-76.2	25.9		-61.7	25.2		-61.7	25.2
B	5		-59.7	20.3		-52.3	21.4		-52.3	21.4
B	SUM		-294.3			-244.5			-244.5	
C	1		-37.7	14.8		-19.4	6.6		-19.4	6.6
C	2		-49.3	19.4		-49.2	16.6		-49.2	16.6
C	3		-49.0	19.3		-75.2	25.4		-75.2	25.4
C	4		-66.4	26.1		-82.5	27.9		-82.5	27.9
C	5		-51.5	20.3		-69.7	23.5		-69.7	23.5
C	SUM		-253.8			-296.0			-296.0	
D	1		-17.4	12.5		48.7	9.5		48.7	9.5
D	2		-35.5	25.5		106.2	20.7		106.2	20.7
D	3		-32.2	23.1		115.0	22.4		115.0	22.4
D	4		-34.8	25.0		177.3	34.6		177.3	34.6
D	5		-19.4	13.9		65.6	12.8		65.6	12.8
D	SUM		-139.3			512.7			512.7	
LOAD	PX (KIPS)		-100.0			-			-100.0	
LOAD	PY (KIPS)		.1			-			-	
ACTUAL	PX (KIPS)		-19.2			-			-18.8	
ACTUAL	PY (KIPS)		.0			-			-19.5	

TABLE 10H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
TORSIONAL RESTRAINT.



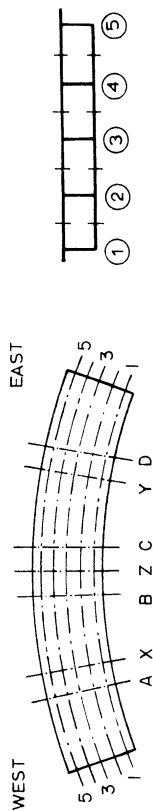
SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1		108.8	18.3		-41.6	30.7		72.5	16.7
A	2		108.4	18.2		-27.0	19.9		75.9	17.4
A	3		114.3	19.2		-22.8	16.9		84.8	19.5
A	4		140.8	23.6		-24.9	18.4		105.5	24.3
A	5		123.1	20.7		-19.1	14.1		96.2	22.1
A	SUM		595.5			-135.3			434.8	
B	1		-19.9	8.5		-34.7	14.1		-53.3	11.2
B	2		-51.9	22.1		-49.5	20.2		-97.1	20.3
B	3		-59.8	25.4		-52.1	21.2		-114.5	23.9
B	4		-55.1	23.5		-69.1	28.2		-125.2	26.2
B	5		-48.2	20.5		-40.0	16.3		-87.9	18.4
B	SUM		-235.0			-245.3			-478.0	
C	1		-32.0	11.7		-25.4	9.6		-51.1	9.9
C	2		-59.6	21.7		-47.3	17.9		-96.7	18.8
C	3		-62.4	22.8		-78.3	29.6		-132.0	25.7
C	4		-70.9	25.9		-72.1	27.3		-144.6	28.1
C	5		-48.9	17.9		-41.4	15.6		-90.0	17.5
C	SUM		-273.8			-264.4			-514.4	
D	1		-25.0	14.7		65.4	11.0		44.0	9.4
D	2		-35.3	20.8		96.9	16.2		69.3	14.8
D	3		-33.5	19.7		115.6	19.4		87.9	18.8
D	4		-39.7	23.3		157.2	26.4		127.8	27.3
D	5		-36.7	21.5		161.5	27.1		138.8	29.7
D	SUM		-170.2			596.6			467.8	
LOAD	PX (KIPS)		-100.0			-.0			-100.0	
LOAD	PY (KIPS)		.1			-100.0			-100.0	
ACTUAL	PX (KIPS)		-19.2			-.0			-18.8	
ACTUAL	PY (KIPS)		.0			-19.4			-19.5	



TABLE 101

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE)  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADINGS.  
TORSIONAL RESTRAINT.



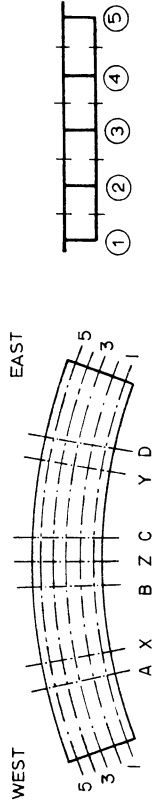
SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1		86.6	14.3		-25.0	21.6		58.7	13.3
A	2		114.7	19.0		-24.2	21.0		81.2	18.4
A	3		131.2	21.7		-23.9	20.7		94.5	21.4
A	4		153.8	25.4		-24.8	21.5		114.5	26.0
A	5		118.2	19.6		-17.5	15.2		92.1	20.9
A	SUM		604.5			-115.4			441.0	
B	1		-22.4	8.6		-35.7	14.6		-56.2	11.5
B	2		-52.6	20.1		-47.5	19.4		-94.6	19.3
B	3		-68.7	26.3		-50.5	20.6		-116.5	23.8
B	4		-64.6	24.7		-65.8	26.9		-126.6	25.9
B	5		-53.3	20.4		-45.5	18.6		-95.7	19.5
B	SUM		-261.5			-245.0			-489.5	
C	1		-34.5	13.0		-22.7	8.2		-52.0	10.1
C	2		-55.0	20.7		-48.2	17.3		-94.1	18.3
C	3		-56.5	21.3		-77.0	27.6		-124.1	24.2
C	4		-68.9	26.0		-76.7	27.5		-142.3	27.7
C	5		-50.1	18.9		-54.0	19.4		-100.9	19.7
C	SUM		-265.0			-278.6			-513.5	
D	1		-20.8	13.6		56.2	10.2		36.0	8.7
D	2		-35.4	23.1		102.1	18.5		69.6	16.7
D	3		-32.8	21.4		115.3	20.9		86.2	20.7
D	4		-37.0	24.2		168.4	30.6		137.9	33.1
D	5		-27.1	17.7		108.4	19.7		86.5	20.8
D	SUM		-153.1			550.3			416.2	
LOAD	PX (KIPS)		-100.0			-			-100.0	
LOAD	PY (KIPS)		.1			-			-100.4	
ACTUAL	PX (KIPS)		-19.2			-			-18.8	
ACTUAL	PY (KIPS)		.0			-			-19.5	

TABLE 10J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
TORSIONAL RESTRAINT.



SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1		82.0	13.5		-25.3	22.0		55.9	12.6
A	2		116.2	19.1		-23.9	20.8		82.5	18.6
A	3		136.7	22.5		-24.2	21.0		97.6	22.0
A	4		157.4	25.9		-24.8	21.5		116.9	26.4
A	5		116.4	19.1		-17.0	14.8		90.6	20.4
A	SUM		608.6			-115.1			443.5	
B	1		-23.3	8.4		-36.1	14.7		-57.2	11.6
B	2		-52.8	19.1		-46.5	19.0		-93.4	18.9
B	3		-74.1	26.8		-49.8	20.3		-117.5	23.8
B	4		-70.7	25.6		-64.4	26.3		-127.2	25.8
B	5		-55.3	20.0		-47.8	19.6		-98.6	20.0
B	SUM		-276.2			-244.6			-493.9	
C	1		-35.4	13.6		-22.3	7.8		-52.2	10.2
C	2		-53.2	20.4		-48.6	17.1		-92.8	18.2
C	3		-54.0	20.7		-76.1	26.7		-119.8	23.4
C	4		-67.9	26.0		-79.2	27.8		-141.1	27.6
C	5		-50.5	19.4		-58.9	20.6		-105.1	20.6
C	SUM		-261.0			-285.1			-511.1	
D	1		-19.7	13.2		53.5	9.7		34.0	8.0
D	2		-35.4	23.8		103.6	18.7		69.7	16.4
D	3		-32.6	21.9		115.2	20.8		85.7	20.1
D	4		-36.2	24.3		172.1	31.1		141.3	33.2
D	5		-25.0	16.8		108.3	19.6		95.4	22.4
D	SUM		-148.9			552.7			426.1	
LOAD	PX (KIPS)		-100.0			-0.0			-100.0	
LOAD	PY (KIPS)		.1			-100.0			-100.4	
ACTUAL	PX (KIPS)		-19.2			-0.0			-18.8	
ACTUAL	PY (KIPS)		.0			-19.4			-19.5	

TABLE 11A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS TORSIONAL RESTRAINT.  
 TF = MOMENT AT FOOTING ABOUT Y-AXIS

\*\*\*\*\*  
 (1-X)+(5-Y)  
 \*\*\*\*\*  
 THEORY EXPERM THEORY EXPERM  
 \*\*\*\*\*  
 THEORY EXPERM  
 \*\*\*\*\*

REACTION  
 NO LOAD  
 1F -17.66  
 2E -4.74  
 3E 8.49  
 4E 10.10  
 5E 35.59  
 1F 36.06  
 2F 15.58  
 3F 7.33  
 4F 28.33

1W 23.07  
 2W 13.17  
 3W 7.67  
 4W .63  
 5W -12.74  
 PE 31.78  
 PF 87.30  
 FW 31.80  
 SUMP 150.88

PX -100.00  
 PY -102.89  
 SUMP -202.89  
 SUMP/SUMP .74

TW -216.54  
 WF -23.97  
 TF 62.22  
 TE 312.20

ACTUAL PX -19.00  
 ACTUAL PY -19.55

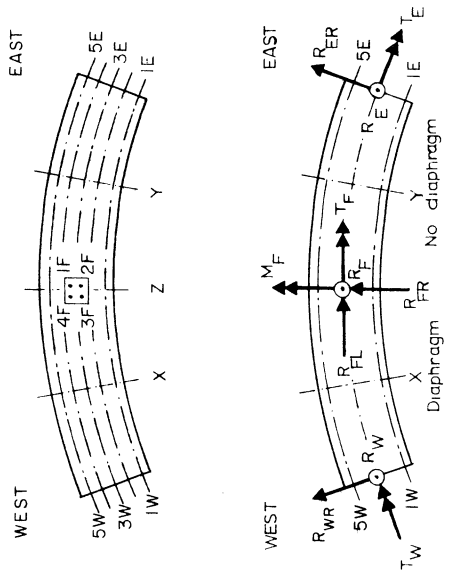
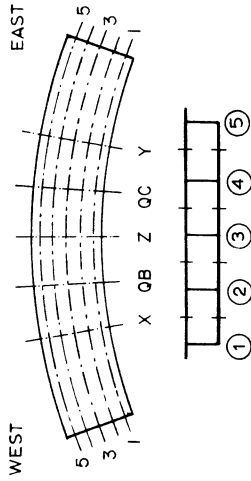


TABLE 11B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 TORSIONAL RESTRAINT.



NORMALIZED POINT LOAD APPLIED AT  
 \*\*\*\*\*  
 THEORY EXPERM E/T \*\*\*\*\*  
 THEORY EXPERM E/T \*\*\*\*\*

(1-X)+(5-Y)  
 \*\*\*\*\*  
 THEORY EXPERM E/T \*\*\*\*\*

DEFLECTION AT POINT  
 1X .814  
 2X .650  
 3X .537  
 4X .419  
 5X .330

1QB .376  
 2QB .273  
 3QB .207  
 4QB .139  
 5QB .084

1Z 0.  
 2Z .001  
 4Z 0.  
 5Z -.001

1QC .187  
 2QC .253  
 3QC .362  
 4QC .543  
 5QC .697

1Y .455  
 2Y .537  
 3Y .719  
 4Y 1.058  
 5Y 1.624

LOAD PX -100.0  
 LOAD PY -102.9  
 ACTUAL PX -19.0  
 ACTUAL PY -19.5

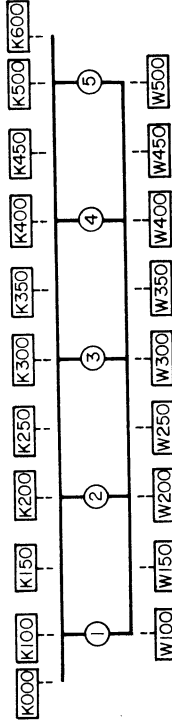
TABLE 11C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. TORSIONAL RESTRAINT.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



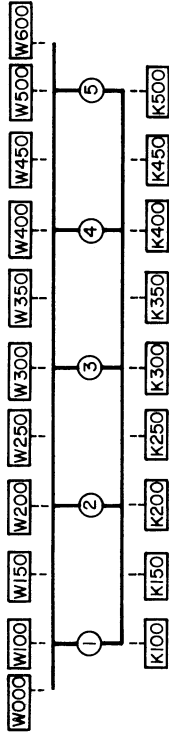
NORMALIZED POINT LOAD APPLIED AT

GAGE TYPE	GAGE LOC.	(1-X) + (5-Y)		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	ADJUST	ADJUST	ADJUST	ADJUST
K	K000	-303	-303				
K	K100	-525	-510				
K	K150	-284	-282				
K	K200	-350	-379				
K	K250	-200	-199				
K	K300	-288	-282				
K	K350	-221	-214				
K	K400	-249	-258				
K	K450	-178	-218				
K	K500	-173	-171				
K	K600	-116	-116				
W	W100	968	975				
W	W150	688	660				
W	W200	799	774				
W	W250	724	585				
W	W300	644	641				
W	W350	517	479				
W	W400	534	514				
W	W450	571	469				
W	W500	520	508				
LCAD	PX (KIPS)	-100.0					
LCAD	PY (KIPS)	-102.9					
ACTUAL	PX (KIPS)	-19.0					
ACTUAL	PY (KIPS)	-19.5					

TABLE 11D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
TORSIONAL RESTRAINT.



SECTION B

TENSION = + K = CONCRETE STRAIN METERS

COMPRESSION = - W = WELDABLE STRAIN GAGES

NORMALIZED POINT LOAD APPLIED AT

GAGE TYPE	GAGE LOC.	(1-X)+(5-Y)		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	ADJUST	ADJUST	ADJUST	ADJUST
W	W000		777				
W	W100		704				
W	W150		632				
W	W200		701				
W	W250		579				
W	W300		722				
W	W350		521				
W	W400		603				
W	W450		556				
W	W500		513				
W	W600		519				
K	K100		-430				-437
K	K150		-529				-479
K	K200		-343				-341
K	K250		-320				-362
K	K300		-391				-389
K	K350		-401				-404
K	K400		-380				-388
K	K450		-332				-358
K	K500		-337				-329

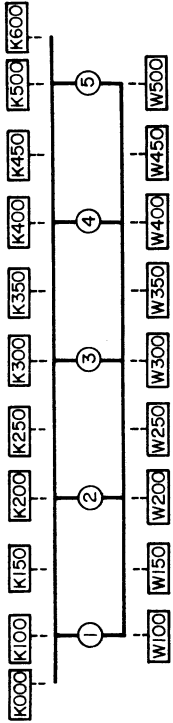
LOAD	PX (KIPS)	-100.0
LOAD	PY (KIPS)	-102.9
ACTUAL	PX (KIPS)	-19.0
ACTUAL	PY (KIPS)	-19.5



TABLE 11F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. TORSIONAL RESTRAINT.



SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

NORMALIZED POINT LOAD APPLIED AT

GAGE TYPE	GAGE LOC.	(1-X)+(5-Y)		THEORY		MEASR		ADJUST	
		THEORY	MEASR	ADJUST	ADJUST	THEORY	MEASR	ADJUST	
K	K000								
K	K100		-96		-96				
K	K150		-180		-185				
K	K200		-327		-306				
K	K250		-270		-260				
K	K300		-247		-279				
K	K350		-307		-320				
K	K400		-400		-431				
K	K450		-424		-420				
K	K500		-612		-642				
K	K600		-461		-468				
K	K600		-204		-461				
W	W100								
W	W150		415		426				
W	W200		557		518				
W	W250		637		622				
W	W300		627		596				
W	W350		696		702				
W	W400		861		825				
W	W450		1262		1212				
W	W500		1149		1006				
W	W500		431		455				
LOAD	PX (KIPS)								
LOAD	PY (KIPS)								
ACTUAL	PX (KIPS)		-100.0		-102.9				
ACTUAL	PY (KIPS)		-19.0		-19.5				



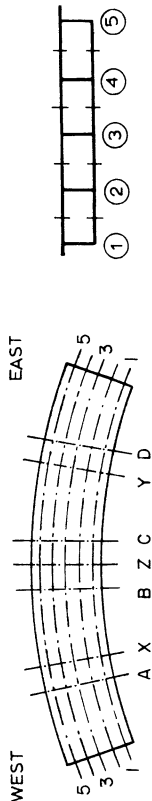


TABLE 11F

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
TORSIONAL RESTRAINT.

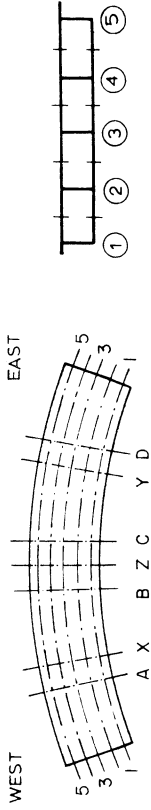


SECTION	GIRDER	(1-X) + (5-Y)		NORMALIZED POINT LOAD APPLIED AT		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	117.1	28.5	117.1	28.5	117.1	28.5	117.1	28.5
A	2	94.9	23.1	94.9	23.1	94.9	23.1	94.9	23.1
A	3	74.6	18.1	74.6	18.1	74.6	18.1	74.6	18.1
A	4	76.3	18.5	76.3	18.5	76.3	18.5	76.3	18.5
A	5	48.8	11.8	48.8	11.8	48.8	11.8	48.8	11.8
A	SUM	411.7		411.7		411.7		411.7	
B	1	-80.0	16.8	-80.0	16.8	-80.0	16.8	-80.0	16.8
B	2	-109.3	22.9	-109.3	22.9	-109.3	22.9	-109.3	22.9
B	3	-117.0	24.5	-117.0	24.5	-117.0	24.5	-117.0	24.5
B	4	-112.5	23.6	-112.5	23.6	-112.5	23.6	-112.5	23.6
B	5	-58.6	12.3	-58.6	12.3	-58.6	12.3	-58.6	12.3
B	SUM	-477.4		-477.4		-477.4		-477.4	
C	1	-57.0	12.3	-57.0	12.3	-57.0	12.3	-57.0	12.3
C	2	-90.0	19.5	-90.0	19.5	-90.0	19.5	-90.0	19.5
C	3	-119.7	25.9	-119.7	25.9	-119.7	25.9	-119.7	25.9
C	4	-123.7	26.8	-123.7	26.8	-123.7	26.8	-123.7	26.8
C	5	-71.7	15.5	-71.7	15.5	-71.7	15.5	-71.7	15.5
C	SUM	-462.0		-462.0		-462.0		-462.0	
D	1	52.7	10.4	52.7	10.4	52.7	10.4	52.7	10.4
D	2	78.3	15.4	78.3	15.4	78.3	15.4	78.3	15.4
D	3	95.6	18.9	95.6	18.9	95.6	18.9	95.6	18.9
D	4	135.3	26.7	135.3	26.7	135.3	26.7	135.3	26.7
D	5	145.0	28.6	145.0	28.6	145.0	28.6	145.0	28.6
D	SUM	506.8		506.8		506.8		506.8	
LOAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0	
LOAD	PY (KIPS)	-102.9		-102.9		-102.9		-102.9	
ACTUAL	PX (KIPS)	-19.0		-19.0		-19.0		-19.0	
ACTUAL	PY (KIPS)	-19.5		-19.5		-19.5		-19.5	

TABLE 111

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
TORSIONAL RESTRAINT.



NORMALIZED POINT LOAD APPLIED AT

\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT

\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT

\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT

SECTION	GIRDER	(1-X)+(5-Y)	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
A	1		90.2	23.2		
A	2		99.1	25.5		
A	3		79.8	20.6		
A	4		74.2	19.1		
A	5		45.1	11.6		
A	SUM		388.5			

B	1		-83.1	17.7		
B	2		-106.4	22.7		
B	3		-111.7	23.9		
B	4		-104.1	22.2		
B	5		-63.0	13.4		
B	SUM		-468.3			

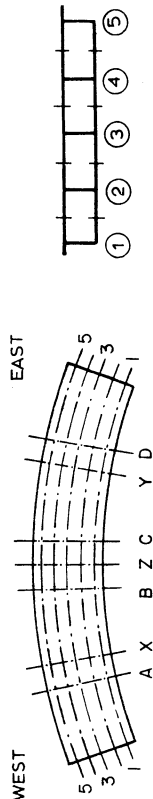
C	1		-58.2	12.5		
C	2		-93.1	20.0		
C	3		-113.9	24.5		
C	4		-119.1	25.6		
C	5		-80.8	17.4		
C	SUM		-465.2			

D	1		43.9	9.6		
D	2		80.5	17.6		
D	3		94.2	20.6		
D	4		145.4	31.9		
D	5		92.5	20.3		
D	SUM		456.5			

LOAD	PX (KIPS)	-100.0
LOAD	PY (KIPS)	-102.9
ACTUAL	PX (KIPS)	-19.0
ACTUAL	PY (KIPS)	-19.5

TABLE 11J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE)  
MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.



RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADINGS.  
TORSIONAL RESTRAINT -

SECTION	GIRDER	(1-X)+(5-Y)		NORMALIZED POINT LOAD APPLIED AT		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	85.2	22.2						
A	2	100.0	26.1						
A	3	81.1	21.1						
A	4	73.7	19.2						
A	5	43.9	11.4						
A	SUM	383.9							
B	1	-84.3	18.2						
B	2	-104.8	22.6						
B	3	-109.2	23.6						
B	4	-100.9	21.8						
B	5	-64.6	13.9						
B	SUM	-463.8							
C	1	-58.5	12.6						
C	2	-94.9	20.4						
C	3	-110.7	23.8						
C	4	-116.9	25.1						
C	5	-84.1	18.1						
C	SUM	-465.1							
D	1	41.6	9.0						
D	2	81.1	17.5						
D	3	93.8	20.2						
D	4	148.8	32.1						
D	5	98.2	21.2						
D	SUM	463.5							
LOAD	PX (KIPS)								
LOAD	PY (KIPS)								
ACTUAL	PX (KIPS)	-100.0							
ACTUAL	PY (KIPS)	-102.9							
ACTUAL	PX (KIPS)	-19.0							
ACTUAL	PY (KIPS)	-19.5							

TABLE 12A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING.  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS  
 TF = MOMENT AT FOOTING ABOUT Y-AXIS

REACTION OR LOAD	(1-X)		(1-Y)		(1-X)+(1-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	5.16	27.08				32.43
2E	2.62	23.39				26.29
3E	-0.71	6.15				5.54
4E	-3.37	-1.21				-4.39
5E	-7.37	-9.24				-16.75
1F	52.49	-22.48				29.85
2F	50.03	-23.87				25.44
3F	-23.62	53.02				29.72
4F	-18.68	51.31				34.07
1W	27.68	6.49				33.22
2W	19.94	2.86				22.74
3W	12.30	-1.35				11.05
4W	0.55	-3.02				-2.20
5W	-14.07	-7.94				-21.71
RE	-3.67	46.17				43.12
RF	60.22	57.98				119.08
RW	46.40	-2.96				43.10
SUMR	102.95	101.19				205.30
PX	-100.00	-0.				-100.00
PY	0.11	-100.00				-101.38
SUMP	-99.89	-100.00				-201.38
SUMP/SUMP	1.03	1.01				1.02
TW	-264.73	-87.07				-346.83
MF	-217.23	226.02				12.75
TF	11.10	-0.48				13.14
TE	-79.69	-250.19				-331.08
ACTUAL FX	-19.24	-0.				-19.13
ACTUAL FY	0.02	-19.43				-19.39

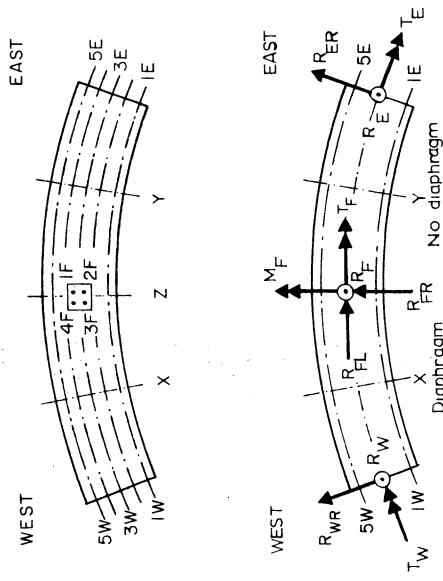
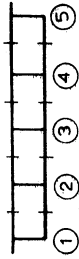
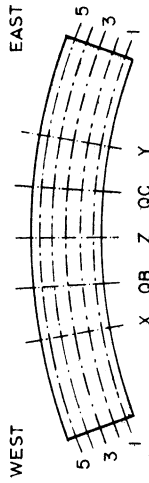


TABLE 12B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 LONGITUDINAL RESTRAINT.



DEFLECTION AT POINT	(1-X)		(1-Y)		NORMALIZED POINT LOAD APPLIED AT (1-X)+(1-Y)	
	THEORY	EXPERM E/T	THEORY	EXPERM E/T	THEORY	EXPERM E/T
1X		1.014		-.098		.901
2X		.822		-.141		.683
3X		.691		-.180		.497
4X		.544		-.220		.316
5X		.423		-.267		.147
1QB		.657		-.034		.608
2QB		.500		-.102		.399
3QB		.378		-.152		.230
4QB		.295		-.202		.075
5QB		.179		-.262		-.094
1Z		.158		.179		.349
2Z		.084		.083		.165
4Z		-.059		-.060		-.120
5Z		-.130		-.135		-.268
1QC		-.031		.789		.758
2QC		-.096		.533		.451
3QC		-.141		.315		.187
4QC		-.202		.229		.022
5QC		-.258		.135		-.138
1Y		-.107		1.438		1.361
2Y		-.140		.865		.740
3Y		-.164		.582		.409
4Y		-.221		.405		.197
5Y		-.271		.356		.072
LOAD PX		-100.0		-0.		-100.0
LOAD PY		.1		-100.0		-101.4
ACTUAL PX		-19.2		-0.		-19.1
ACTUAL PY		.0		-19.4		-19.4



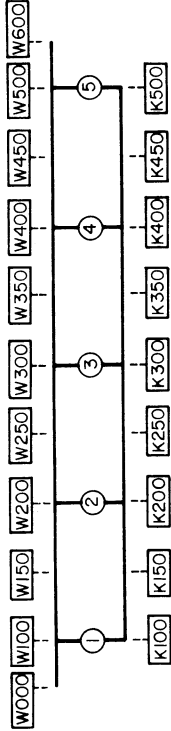




TABLE 12E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. LONGITUDINAL RESTRAINT.

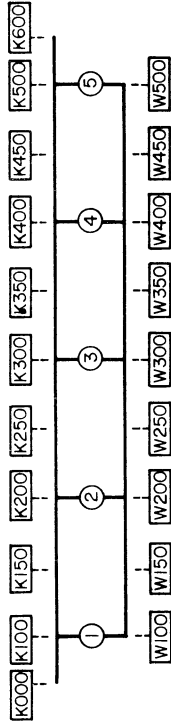


TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASP ADJUST	THEORY	MEASP ADJUST	THEORY	MEASR ADJUST
W	W000	223	223	533	533	773	773
W	W100	273	199	441	440	674	694
W	W150	173	168	344	350	528	595
W	W200	232	234	352	358	599	593
W	W250	93	91	288	299	396	404
W	W300	105	104	285	280	406	403
W	W350	62	61	156	175	226	243
W	W400	102	104	110	116	220	233
W	W450	86	85	61	60	150	167
W	W500	82	82	17	17	105	100
W	W600	83	83	-21	17	63	63
K	K100	-125	-122	-326	-332	-432	-434
K	K150	-110	-88	-257	-308	-351	-384
K	K200	-91	-88	-230	-239	-314	-329
K	K250	-40	-43	-255	-240	-290	-299
K	K300	-19	-20	-241	-239	-256	-251
K	K350	-55	-51	-174	-176	-223	-222
K	K400	-96	-96	-122	-117	-215	-210
K	K450	-140	-138	-152	-144	-290	-281
K	K500	-143	-141	-117	-117	-256	-254
LOAD	PX (KIPS)	-100.0		-0.		-100.0	
LOAD	PY (KIPS)	.1		-100.0		-101.4	
ACTUAL	PX (KIPS)	-19.2		-0.		-19.1	
ACTUAL	PY (KIPS)	.0		-19.4		-19.4	

TABLE 12F

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COMP. LOADING.  
 LONGITUDINAL RESTRAINT.



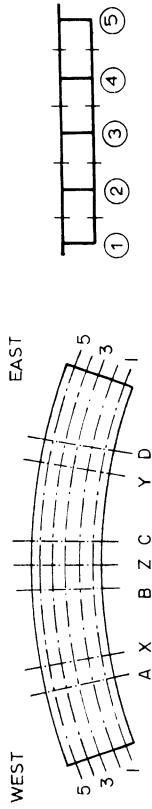
SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	29	29	-292	-292	-256	-256
K	K100	42	43	-439	-443	-398	-401
K	K150	88	87	-551	-502	-485	-435
K	K200	50	46	-450	-450	-409	-413
K	K250	44	44	-306	-362	-262	-322
K	K300	36	40	-286	-295	-253	-257
K	K350	43	54	-306	-317	-270	-271
K	K400	35	34	-209	-197	-177	-171
K	K450	33	36	-274	-251	-233	-225
K	K500	20	20	-171	-170	-150	-144
K	K600	9	20	-55	-171	-45	-150
W	W100	-54	-51	601	671	552	620
W	W150	-84	-78	931	999	845	937
W	W200	-99	-101	828	803	745	725
W	W250	-93	-80	598	573	526	513
W	W300	-96	-90	467	467	378	378
W	W350	-145	-135	367	372	244	274
W	W400	-141	-139	420	415	283	287
W	W450	-105	-115	334	328	231	219
W	W500	-83	-93	428	432	338	334
LOAD	PX (KIPS)	-100.0	-0.			-100.0	
LOAD	PY (KIPS)	.1	-100.0			-101.4	
ACTUAL	PX (KIPS)	-19.2	-0.			-19.1	
ACTUAL	PY (KIPS)	.0	-19.4			-19.4	

TABLE 12G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
LONGITUDINAL RESTRAINT.



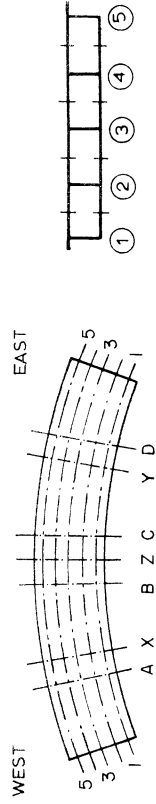
SECTION	GIRDER	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT
A	1	61.7	17.6	-4.3	7.4	56.7	20.6
A	2	96.6	27.5	-12.0	20.7	80.6	29.3
A	3	80.0	22.8	-13.2	22.7	61.2	22.2
A	4	71.9	20.5	-17.2	29.8	50.6	18.4
A	5	41.1	11.7	-11.2	19.4	26.2	9.5
A	SUM	351.3		-57.9		275.3	
B	1	-42.2	24.5	-30.4	32.4	-73.6	27.2
B	2	-49.0	28.5	-30.9	33.0	-80.7	29.8
B	3	-49.2	28.6	-13.2	14.1	-62.1	23.0
B	4	-22.7	13.2	-10.8	11.6	-35.7	13.2
B	5	-9.0	5.2	-8.4	8.9	-18.4	6.8
B	SUM	-172.1		-93.7		-270.6	
C	1	-25.4	27.5	-55.8	31.9	-90.9	31.5
C	2	-29.7	32.2	-57.4	32.8	-92.0	31.9
C	3	-14.5	15.7	-42.2	24.1	-59.7	20.7
C	4	-13.7	14.9	-18.8	10.8	-35.2	12.2
C	5	-9.0	9.7	-.7	.4	-10.5	3.6
C	SUM	-92.4		-175.0		-288.2	
D	1	-4.6	8.0	63.7	19.9	59.6	22.1
D	2	-12.7	21.9	112.4	35.2	102.7	38.2
D	3	-13.2	22.8	60.6	19.0	49.4	18.3
D	4	-19.0	32.9	52.3	16.4	35.5	13.2
D	5	-8.4	14.5	30.3	9.5	22.0	8.2
D	SUM	-57.9		319.2		269.3	
LOAD	PX (KIPS)	-100.0		-0.		-100.0	
LOAD	PY (KIPS)	.1		-100.0		-101.4	
ACTUAL	PX (KIPS)	-19.2		-0.		-19.1	
ACTUAL	PY (KIPS)	.0		-19.4		-19.4	

TABLE 12H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
LONGITUDINAL RESTRAINT.

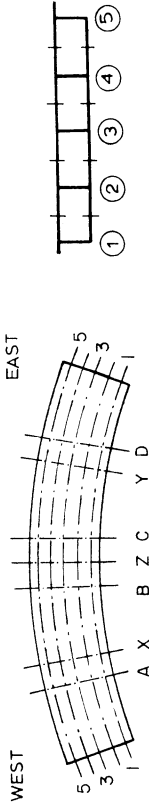


SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1	149.7	29.1		-15.6	29.7		133.9	29.5	
A	2	120.3	23.4		-12.2	23.1		105.8	23.3	
A	3	93.8	18.2		-9.7	18.4		81.5	17.9	
A	4	93.0	18.1		-8.3	15.8		83.1	18.3	
A	5	57.6	11.2		-6.8	13.0		50.2	11.0	
A	SUM	514.4			-52.7			454.5		
B	1	-40.3	15.0		-24.2	24.1		-60.3	16.6	
B	2	-54.4	24.0		-25.8	25.7		-90.0	24.8	
B	3	-85.2	31.7		-3.2	3.2		-88.2	24.3	
B	4	-55.4	20.6		-25.2	25.1		-79.5	21.9	
B	5	-23.1	8.6		-22.0	21.9		-44.8	12.3	
B	SUM	-268.3			-100.4			-362.9		
C	1	-18.4	17.3		-58.3	21.0		-72.1	19.2	
C	2	-21.2	19.9		-76.8	27.7		-98.7	26.2	
C	3	-9.1	8.5		-72.4	26.1		-79.8	21.2	
C	4	-29.7	27.9		-42.5	15.3		-70.8	18.8	
C	5	-28.1	26.4		-27.4	9.9		-54.7	14.5	
C	SUM	-106.6			-277.4			-376.1		
D	1	-15.0	24.5		115.4	25.3		102.1	25.3	
D	2	-16.4	26.8		127.9	28.1		114.6	28.4	
D	3	-12.9	21.1		92.7	20.3		81.2	20.1	
D	4	-10.9	17.8		70.2	15.4		62.3	15.4	
D	5	-6.0	9.8		49.6	10.9		43.6	10.8	
D	SUM	-61.4			455.8			403.8		
LJAD	PX (KIPS)	-100.0			-0.			-100.0		
LOAD	PY (KIPS)	.1			-100.0			-101.4		
ACTUAL	PX (KIPS)	-19.2			-0.			-19.1		
ACTUAL	PY (KIPS)	.0			-19.4			-19.4		

TABLE 1Z1

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
LONGITUDINAL RESTRAINT.



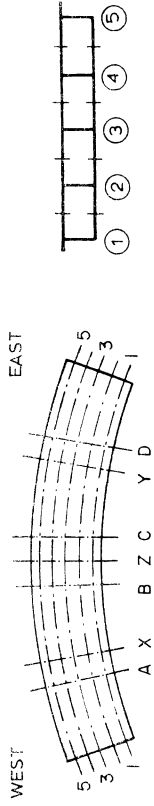
SECTION	GIRDER	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT
A	1	101.0	23.8	-9.4	16.8	91.2	25.7
	2	107.2	25.3	-12.1	21.7	91.9	25.9
	3	86.2	20.3	-11.6	20.9	70.3	19.8
	4	81.3	19.2	-13.3	23.8	65.2	18.3
	5	48.5	11.4	-9.3	16.7	36.9	10.4
A	SUM	424.2		-55.6		355.4	
B	1	-41.2	18.3	-26.9	27.6	-66.2	20.6
	2	-57.6	25.5	-28.1	28.8	-85.9	26.7
	3	-59.1	30.7	-7.7	7.9	-76.6	23.8
	4	-40.8	18.1	-18.8	19.3	-60.0	18.6
	5	-16.8	7.5	-15.9	16.4	-33.0	10.3
B	SUM	-225.5		-97.4		-321.8	
C	1	-21.5	21.5	-57.2	24.7	-80.5	23.9
	2	-25.0	25.0	-68.2	29.4	-95.7	28.4
	3	-11.5	11.5	-58.9	25.4	-70.8	21.0
	4	-22.6	22.5	-31.9	13.8	-54.9	16.3
	5	-19.6	19.6	-15.5	6.7	-35.0	10.4
C	SUM	-100.3		-231.7		-337.0	
D	1	-9.3	15.6	86.8	22.8	78.6	23.9
	2	-14.4	24.2	119.4	31.4	108.1	32.8
	3	-13.1	22.0	74.9	19.7	63.6	19.3
	4	-15.4	25.9	60.3	15.8	47.5	14.4
	5	-7.3	12.3	38.9	10.2	31.7	9.6
D	SUM	-59.5		380.3		329.4	
LOAD	PX (KIPS)	-100.0		-0.		-100.0	
LOAD	PY (KIPS)	.1		-100.0		-101.4	
ACTUAL	PX (KIPS)	-19.2		-0.		-19.1	
ACTUAL	PY (KIPS)	.0		-19.4		-19.4	

TABLE 12J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE)

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
LONGITUDINAL RESTRAINT.



SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1		97.4	23.5		-10.6	17.4		87.6	25.5
A	2		105.7	25.6		-12.1	19.9		90.3	26.3
A	3		85.0	20.5		-12.3	20.2		68.7	20.0
A	4		79.8	19.3		-15.3	25.2		63.7	18.5
A	5		45.8	11.1		-10.5	17.3		33.5	9.8
A	SUM		413.7			-60.8			343.8	
B	1		-41.5	19.0		-28.1	26.8		-68.9	21.6
B	2		-54.5	24.9		-29.2	27.9		-83.9	26.3
B	3		-65.2	29.7		-11.9	11.4		-72.7	22.8
B	4		-40.7	18.6		-18.6	17.8		-59.0	18.5
B	5		-17.2	7.9		-16.8	16.1		-34.2	10.7
B	SUM		-219.1			-104.6			-318.6	
C	1		-22.7	21.4		-56.9	24.4		-83.7	24.6
C	2		-27.4	25.8		-65.2	28.0		-94.4	27.8
C	3		-13.6	12.8		-56.1	24.1		-67.4	19.8
C	4		-21.4	20.1		-30.7	13.2		-52.1	15.3
C	5		-21.1	19.9		-24.0	10.3		-42.2	12.4
C	SUM		-106.3			-232.8			-339.7	
D	1		-9.4	15.2		84.2	22.8		76.3	23.9
D	2		-13.9	22.5		118.0	32.0		107.1	33.5
D	3		-13.1	21.2		73.0	19.8		62.3	19.5
D	4		-17.4	28.2		58.0	15.7		45.5	14.2
D	5		-8.0	12.9		35.8	9.7		28.5	8.9
D	SUM		-61.8			369.1			319.7	
LOAD	PX (KIPS)		-100.0			-0.			-100.0	
LOAD	PY (KIPS)		.1			-100.0			-101.4	
ACTUAL	PX (KIPS)		-19.2			-0.			-19.1	
ACTUAL	PY (KIPS)		.0			-19.4			-19.4	

TABLE 13A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 30 KSI COND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS LONGITUDINAL RESTRAINT.

REACTION OR LOAD	(3-X)		(3-Y)		(3-X)+(3-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	-1.16		1.37		1.06	
2E	-1.23		9.87		8.26	
3E	-1.65		7.46		6.66	
4E	-1.31		9.70		8.08	
5E	-2.18		15.36		12.45	
1F	67.26		-15.21		52.79	
2F	44.21		-35.47		10.11	
3F	-36.44		47.59		9.42	
4F	-11.01		65.29		52.08	
1W	3.18		.03		2.87	
2W	3.57		-1.45		3.31	
3W	10.60		-1.58		9.19	
4W	10.29		-1.33		8.85	
5W	16.95		-2.35		15.05	
RE	-5.53		43.76		36.61	
PF	64.02		62.20		124.40	
PW	44.59		-5.68		39.27	
SUMR	103.08		100.28		200.28	
PX	-100.00		.03		-100.00	
PY	.05		-100.00		-96.78	
SUMP	-99.95		-99.97		-196.78	
SUMR/SUMP	1.03		1.00		1.02	
TW	88.15		-14.51		76.93	
MF	-238.38		245.34		-2.10	
TF	72.72		56.94		129.01	
TE	-10.60		71.55		57.89	
ACTUAL PX	-19.37		-0.		-19.56	
ACTUAL PY	.01		-19.10		-18.93	

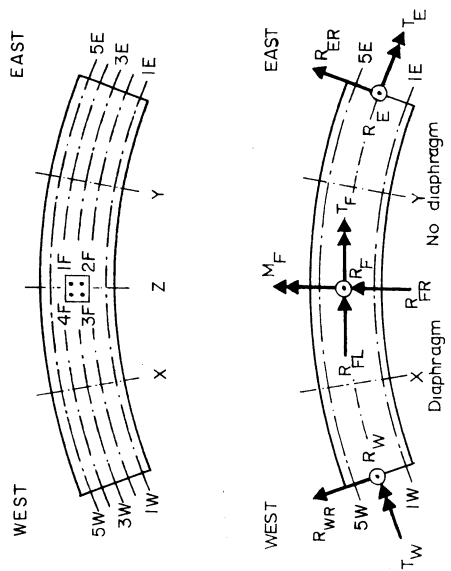
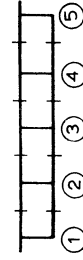
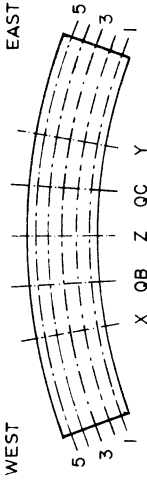


TABLE 13B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTICNS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 LONGITUDINAL RESTRAINT.



DEFLECTION AT POINT	(3-X)		(3-Y)		(3-X)+(3-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X	.667	.667	-.186	-.186	.517	.517
2X	.733	.733	-.202	-.202	.573	.573
3X	.812	.812	-.223	-.223	.658	.658
4X	.823	.823	-.210	-.210	.651	.651
5X	.832	.832	-.229	-.229	.654	.654
1QB	.384	.384	-.165	-.165	.228	.228
2QB	.403	.403	-.172	-.172	.261	.261
3QB	.437	.437	-.168	-.168	.300	.300
4QB	.486	.486	-.169	-.169	.329	.329
5QB	.473	.473	-.178	-.178	.324	.324
1Z	.003	.003	.002	.002	.007	.007
2Z	.006	.006	-.001	-.001	.006	.006
4Z	.020	.020	.014	.014	.033	.033
5Z	.044	.044	.028	.028	.067	.067
1QC	-.173	-.173	.370	.370	.160	.160
2QC	-.163	-.163	.407	.407	.213	.213
3QC	-.149	-.149	.464	.464	.275	.275
4QC	-.162	-.162	.457	.457	.262	.262
5QC	-.190	-.190	.457	.457	.235	.235
1Y	-.196	-.196	.602	.602	.373	.373
2Y	-.202	-.202	.707	.707	.471	.471
3Y	-.185	-.185	.994	.994	.718	.718
4Y	-.205	-.205	.738	.738	.506	.506
5Y	-.213	-.213	.725	.725	.488	.488
LOAD PX	-100.0	-100.0	.0	.0	-100.0	-100.0
LOAD PY	.1	.1	-100.0	-100.0	-96.8	-96.8
ACTUAL PX	-19.4	-19.4	-0.	-0.	-19.6	-19.6
ACTUAL PY	.0	.0	-19.1	-19.1	-18.9	-18.9



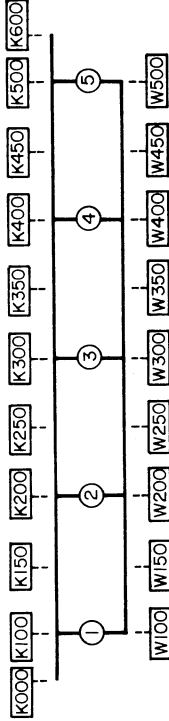
TABLE 13C

SUMMARY CF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. LONGITUDINAL RESTRAINT.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR ADJUST	THEORY	MEASR ADJUST	THEORY	MEASR ADJUST
K	K000	-259	-259	53	53	-233	-233
K	K100	-465	-448	106	103	-432	-414
K	K150	-284	-282	41	31	-244	-244
K	K200	-363	-385	66	67	-324	-347
K	K250	-275	-281	34	37	-234	-242
K	K300	-346	-341	55	55	-313	-307
K	K350	-300	-299	43	43	-271	-268
K	K400	-343	-351	54	56	-308	-317
K	K45)	-250	-295	34	45	-224	-268
K	K500	-265	-265	44	43	-242	-241
K	K600	-160	-160	28	28	-146	-146
W	W100	613	629	-97	-98	541	553
W	W150	550	473	-82	-75	485	418
W	W200	638	604	-106	-101	547	517
W	W250	552	531	-98	-91	484	465
W	W300	682	692	-118	-120	577	587
W	W350	601	625	-101	-104	515	536
W	W400	668	668	-128	-127	570	569
W	W450	620	592	-108	-102	531	506
W	W500	789	786	-148	-149	651	650
LOAD	PX (KIPS)	-100.0		.0		-100.0	
LOAD	PY (KIPS)	.1		-100.0		-96.8	
ACTUAL	PX (KIPS)	-19.4		-0.		-19.6	
ACTUAL	PY (KIPS)	.0		-19.1		-18.9	

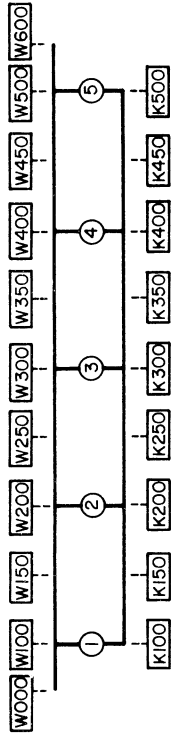
TABLE 13D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. LONGITUDINAL RESTRAINT.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOAD APPLIED AT

GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR ADJUST	THEORY	MEASR ADJUST	THEORY	MEASR ADJUST
W	W000						
W	W100	249	249	205	205	466	466
W	W150	251	256	202	204	469	477
W	W200	216	252	176	201	402	459
W	W250	343	336	199	201	557	553
W	W300	333	378	130	134	474	523
W	W350	399	427	119	123	546	576
W	W400	308	361	121	142	442	513
W	W450	281	279	164	167	469	470
W	W500	243	281	165	189	420	482
W	W600	231	234	165	166	395	400
W	W600	235	235	162	162	406	406
K	K100	-190	-193	-142	-143	-327	-332
K	K150	-226	-216	-148	-140	-367	-350
K	K200	-239	-235	-116	-112	-357	-350
K	K250	-293	-302	-85	-68	-370	-366
K	K300	-330	-335	-53	-50	-382	-384
K	K350	-276	-278	-90	-90	-364	-366
K	K400	-202	-200	-123	-128	-323	-325
K	K450	-178	-182	-119	-127	-301	-311
K	K500	-155	-153	-130	-127	-281	-277
LOAD	PX (KIPS)	-100.0		.0		-100.0	
LOAD	PY (KIPS)	.1		-100.0		-96.8	
ACTUAL	PX (KIPS)	-19.4		-0.		-19.6	
ACTUAL	PY (KIPS)	.0		-19.1		-18.9	

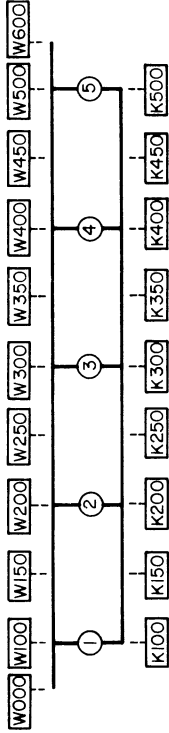
TABLE 13E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. LONGITUDINAL RESTRAINT.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

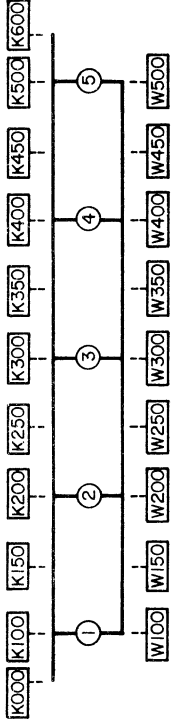


GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	210	210	226	226	449	449
W	W100	199	192	206	204	403	404
W	W150	168	181	201	206	388	403
W	W200	207	207	351	353	570	572
W	W250	122	122	361	348	474	465
W	W300	131	129	510	507	623	620
W	W350	106	120	297	319	413	442
W	W400	191	201	295	309	510	530
W	W450	165	177	206	223	376	401
W	W500	179	174	197	192	377	369
W	W600	176	176	196	196	383	383
K	K100	-144	-142	-157	-155	-295	-291
K	K150	-128	-119	-170	-162	-290	-276
K	K200	-113	-113	-240	-248	-344	-356
K	K250	-92	-60	-341	-374	-382	-426
K	K300	-41	-43	-412	-413	-422	-421
K	K350	-62	-61	-346	-339	-392	-383
K	K400	-114	-110	-208	-204	-316	-308
K	K450	-191	-180	-201	-195	-383	-370
K	K500	-152	-151	-130	-130	-284	-283
LOAD	PX (KIPS)	-100.0		.0		-100.0	
LOAD	PY (KIPS)	.1		-110.0		-96.8	
ACTUAL	PX (KIPS)	-19.4		-0.		-19.6	
ACTUAL	PY (KIPS)	.0		-19.1		-18.9	

TABLE 13F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. LONGITUDINAL RESTRAINT.



SECTION D

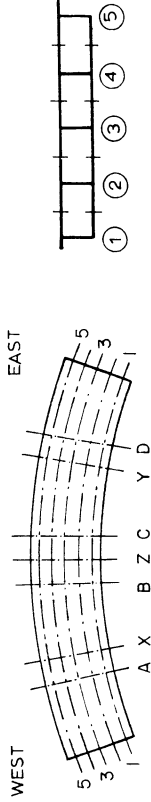
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000		25		-143		-112
K	K100		45		-267		-211
K	K150		83		-479		-378
K	K200		61		-370		-293
K	K250		45		-329		-261
K	K300		50		-300		-236
K	K350		67		-432		-341
K	K400		53		-333		-259
K	K450		79		-462		-367
K	K500		49		-311		-256
K	K600		15		-100		-84
W	W100	-59	-62	375	385	304	310
W	W150	-85	-83	567	522	448	410
W	W200	-97	-95	689	683	553	547
W	W250	-97	-91	675	624	537	495
W	W300	-100	-100	773	751	602	585
W	W350	-101	-98	551	555	419	432
W	W400	-122	-118	708	708	567	569
W	W450	-112	-113	560	561	443	443
W	W500	-98	-105	635	652	510	522
LOAD	PX (KIPS)	-100.0		.0		-100.0	
LOAD	PY (KIPS)	.1		-100.0		-96.8	
ACTUAL	PX (KIPS)	-19.4		-0.		-19.6	
ACTUAL	PY (KIPS)	.0		-19.1		-18.9	

TABLE 13G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI CCND. LOADING.  
LONGITUDINAL RESTRAINT.



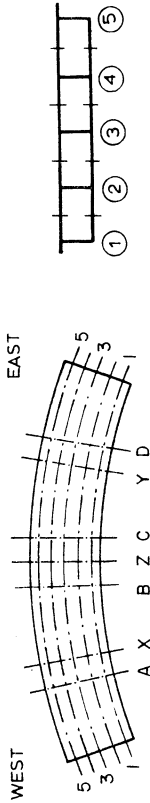
SECTION	GIRDER	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT
A	1	43.5	11.9	-6.1	9.6	37.9	12.1
A	2	79.2	21.6	-13.1	20.9	68.3	21.8
A	3	90.8	24.7	-15.6	24.9	77.6	24.8
A	4	93.3	25.4	-17.0	27.0	79.5	25.4
A	5	60.1	16.4	-11.1	17.6	49.9	15.9
A	SUM	366.8		-62.9		313.2	
B	1	-29.7	13.7	-24.4	20.5	-55.8	16.1
B	2	-48.9	22.5	-27.7	23.3	-78.3	22.6
B	3	-62.5	28.7	-21.2	17.8	-86.6	25.0
B	4	-45.8	21.1	-25.0	20.9	-73.4	21.2
B	5	-30.6	14.0	-20.9	17.5	-52.2	15.1
B	SUM	-217.6		-119.1		-346.2	
C	1	-25.3	19.8	-26.8	12.2	-53.9	15.3
C	2	-29.8	23.3	-51.1	23.3	-82.6	23.4
C	3	-21.0	16.4	-66.7	30.4	-87.1	24.7
C	4	-29.2	22.8	-47.9	21.8	-79.0	22.4
C	5	-22.7	17.7	-27.0	12.3	-50.0	14.2
C	SUM	-128.0		-219.4		-352.7	
D	1	-5.3	9.6	33.2	9.6	26.4	9.7
D	2	-12.5	22.7	86.8	25.2	69.2	25.3
D	3	-12.9	23.5	89.9	26.1	70.2	25.7
D	4	-15.8	28.6	87.2	25.3	69.5	25.5
D	5	-8.6	15.6	47.4	13.8	37.6	13.8
D	SUM	-55.1		344.6		272.9	
LOAD	PX (KIPS)	-100.0	.0	.0		-100.0	
LOAD	PY (KIPS)	.1		-100.0		-96.8	
ACTUAL	PX (KIPS)	-19.4		-0.		-19.6	
ACTUAL	PY (KIPS)	.0		-19.1		-18.9	

TABLE 13H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE)

MOMENTS ABOUT TENSION FLANGE STEEL

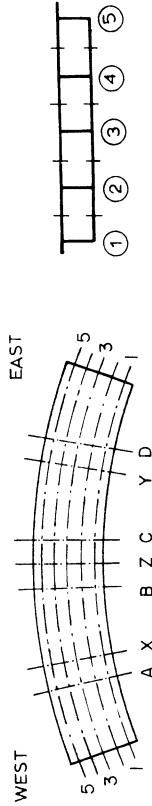
RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
LONGITUDINAL RESTRAINT.



SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1		109.2	22.2		-22.8	28.4		99.3	22.3
A	2		107.5	21.8		-15.6	19.5		95.1	21.4
A	3		100.1	20.3		-14.6	18.2		89.6	20.1
A	4		105.0	21.3		-15.9	19.9		95.6	21.5
A	5		70.5	14.3		-11.2	13.9		65.1	14.6
A	SUM		492.3			-80.1			444.6	
B	1		-35.8	11.9		-25.1	18.8		-59.3	13.9
B	2		-72.8	24.3		-31.3	23.5		-103.3	24.1
B	3		-99.2	33.1		-18.8	14.1		-116.4	27.2
B	4		-63.2	21.1		-35.5	26.7		-97.9	22.9
B	5		-28.5	9.5		-22.5	16.9		-50.9	11.9
B	SUM		-299.6			-133.3			-427.9	
C	1		-23.6	17.8		-27.5	8.4		-49.9	11.2
C	2		-29.6	22.2		-77.1	23.5		-104.8	23.5
C	3		-14.5	10.9		-125.4	38.2		-131.3	29.4
C	4		-34.5	25.9		-70.3	21.4		-101.8	22.8
C	5		-30.9	23.2		-28.2	8.6		-58.8	13.2
C	SUM		-133.1			-328.6			-446.5	
D	1		-14.3	17.3		81.3	16.8		64.0	16.6
D	2		-18.8	22.7		112.4	23.2		88.5	22.9
D	3		-16.6	20.2		98.1	20.3		78.2	20.3
D	4		-17.7	21.5		103.2	21.3		82.4	21.4
D	5		-15.1	18.3		88.5	18.3		72.8	18.9
D	SUM		-82.5			483.5			385.9	
LOAD	PX (KIPS)		-100.0	.0		.0			-100.0	
LOAD	PY (KIPS)		.1			-100.0			-96.8	
ACTUAL	PX (KIPS)		-19.4			-0.			-19.6	
ACTUAL	PY (KIPS)		.0			-19.1			-18.9	

TABLE 131

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )  
 MOMENTS ABOUT ENTIRE GROSS SECTION N.A.  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 LONGITUDINAL RESTRAINT.



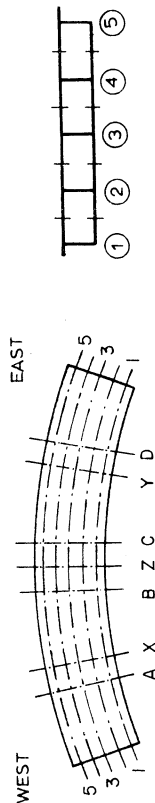
SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1		72.8	17.2		-13.5	19.1		65.3	17.6
A	2		91.8	21.7		-14.2	20.2		80.3	21.6
A	3		95.0	22.5		-15.2	21.5		82.9	22.3
A	4		98.6	23.3		-16.5	23.4		86.7	23.3
A	5		64.7	15.3		-11.1	15.7		56.7	15.2
A	SUM		422.9			-70.6			372.0	
B	1		-33.1	12.6		-24.8	19.5		-57.8	14.8
B	2		-62.2	23.6		-29.7	23.4		-92.2	23.5
B	3		-82.9	31.5		-19.9	15.6		-103.1	26.3
B	4		-55.5	21.1		-30.8	24.3		-87.0	22.2
B	5		-29.5	11.2		-21.8	17.2		-51.5	13.1
B	SUM		-263.1			-127.0			-391.6	
C	1		-24.4	18.6		-27.2	9.7		-51.7	12.8
C	2		-29.7	22.7		-65.5	23.4		-94.9	23.4
C	3		-17.4	13.3		-99.3	35.5		-111.6	27.6
C	4		-32.1	24.6		-60.3	21.5		-91.7	22.6
C	5		-27.2	20.8		-27.7	9.9		-54.9	13.6
C	SUM		-130.9			-279.9			-404.8	
D	1		-9.3	13.8		54.7	13.4		43.2	13.4
D	2		-15.3	22.7		98.3	24.2		77.8	24.1
D	3		-14.6	21.7		93.6	23.0		73.8	22.8
D	4		-16.7	24.7		94.4	23.2		75.3	23.3
D	5		-11.5	17.1		65.8	16.2		53.3	16.5
D	SUM		-67.4			406.7			323.4	
LOAD	PX (KIPS)		-100.0	.0		.0			-100.0	
LJAD	PY (KIPS)		.1	-100.0		-100.0			-96.9	
ACTUAL	PX (KIPS)		-19.4	-0.		-0.			-19.6	
ACTUAL	PY (KIPS)		.0	-19.1		-19.1			-18.9	

TABLE 13J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
LONGITUDINAL RESTRAINT.



SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1		70.8	17.1		-14.6	20.3		64.2	17.6
A	2		90.2	21.7		-14.1	19.7		79.1	21.7
A	3		93.9	22.6		-15.3	21.3		81.7	22.4
A	4		97.4	23.5		-16.7	23.2		85.2	23.4
A	5		62.7	15.1		-11.1	15.4		54.0	14.8
A	SUM		414.9			-71.8			364.3	
B	1		-32.3	12.8		-24.7	19.7		-57.2	15.1
B	2		-58.7	23.3		-29.0	23.1		-88.0	23.2
B	3		-78.7	31.1		-20.5	16.3		-98.5	26.0
B	4		-53.1	21.0		-29.5	23.6		-83.5	22.0
B	5		-29.8	11.8		-21.6	17.2		-51.7	13.6
B	SUM		-252.6			-125.3			-378.8	
C	1		-24.6	18.7		-27.1	10.2		-52.2	13.4
C	2		-29.7	22.7		-61.8	23.2		-91.1	23.4
C	3		-19.4	14.8		-93.1	35.0		-105.0	27.0
C	4		-31.1	23.7		-56.8	21.3		-87.4	22.4
C	5		-26.5	20.2		-27.5	10.3		-53.8	13.8
C	SUM		-131.3			-266.2			-389.6	
D	1		-9.1	14.0		53.2	13.5		41.8	13.4
D	2		-14.9	22.8		95.6	24.3		75.7	24.2
D	3		-14.2	21.7		92.4	23.5		72.6	23.2
D	4		-16.4	25.0		92.2	23.4		73.4	23.5
D	5		-10.7	16.4		60.6	15.4		49.1	15.7
D	SUM		-65.3			393.9			312.7	
LOAD	PX (KIPS)		-100.0	.0		-100.0	.0		-100.0	
LOAD	PY (KIPS)		.1			-0.			-96.8	
ACTUAL	PX (KIPS)		-19.4			-0.			-19.6	
ACTUAL	PY (KIPS)		.0			-19.1			-18.9	



TABLE 14A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 30 KSI CCND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS LONGITUDINAL RESTRAINT.

REACTION OR LOAD	(5-X)		NORMALIZED POINT LOAD APPLIED AT		(5-Y)		(5-X)+(5-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E		-4.87		-17.53		-20.87		-20.87
2E		-4.96		-11.00		-17.34		-17.34
3E		-1.08		5.96		3.83		3.83
4E		.45		17.35		18.67		18.67
5E		2.82		46.55		50.94		50.94
1F		80.80		-2.23		78.13		78.13
2F		37.00		-48.77		-13.10		-13.10
3F		-46.73		36.57		-9.53		-9.53
4F		-1.65		80.70		80.09		80.09
1W		-19.12		-6.76		-21.14		-21.14
2W		-12.46		-3.64		-19.21		-19.21
3W		4.37		-2.33		-1.49		-1.49
4W		19.53		.30		19.92		19.92
5W		50.84		4.41		57.57		57.57
RE		-7.64		41.33		35.23		35.23
RF		69.42		66.27		135.59		135.59
PW		43.16		-8.02		35.65		35.65
SUMR		104.94		99.58		206.47		206.47
PX		-100.00		.06		-100.00		-100.00
PY		.11		-100.00		-101.23		-101.23
SUMP		-99.89		-99.94		-201.23		-201.23
SUMP/SUMP		1.05		1.00		1.03		1.03
TW		442.31		67.62		505.70		505.70
MF		-249.27		252.40		8.30		8.30
TF		133.32		136.00		271.27		271.27
TE		53.49		402.68		462.17		462.17
ACTUAL PX		-19.34		.01		-19.31		-19.31
ACTUAL PY		.02		-19.30		-19.55		-19.55

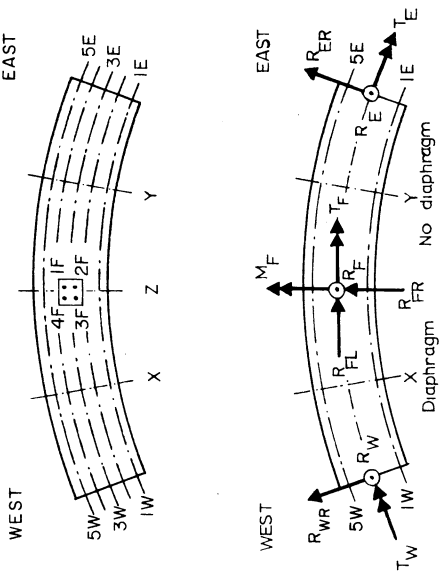
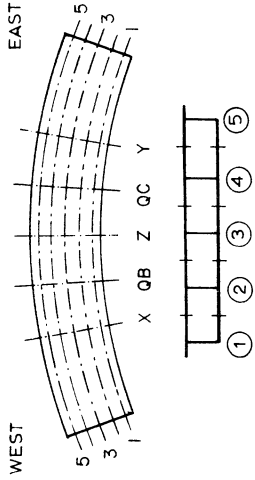


TABLE 14B

SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. LONGITUDINAL RESTRAINT.

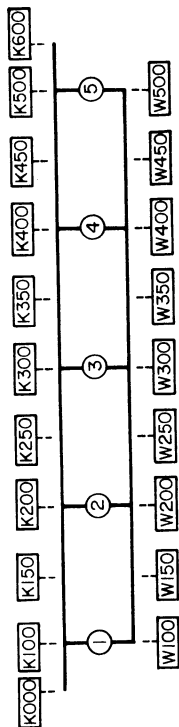


DEFLECTION AT POINT	(5-X)		(5-Y)		(5-X)+(5-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X		.466		-.280		.170
2X		.664		-.248		.395
3X		.876		-.213		.648
4X		1.092		-.183		.906
5X		1.335		-.150		1.179
1QB		.199		-.296		-.131
2QB		.335		-.242		.082
3QB		.483		-.178		.299
4QB		.676		-.127		.549
5QB		.805		-.065		.743
1Z		-.138		-.150		-.298
2Z		-.065		-.070		-.140
4Z		.096		.100		.201
5Z		.198		.219		.417
1QC		-.305		.157		-.112
2QC		-.242		.267		.053
3QC		-.179		.421		.261
4QC		-.132		.671		.568
5QC		-.087		.918		.872
1Y		-.305		.378		.117
2Y		-.260		.507		.295
3Y		-.212		.735		.572
4Y		-.190		1.056		.902
5Y		-.151		1.661		1.555
LOAD PX		-100.0		.1		-100.0
LOAD PY		.1		-100.0		-101.2
ACTUAL PX		-19.3		.0		-19.3
ACTUAL PY		.0		-19.3		-19.5

TABLE 14C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. LONGITUDINAL RESTRAINT.



SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	-261	-261	117	117	-201	-201
K	K100	-431	-412	117	112	-314	-300
K	K150	-249	-250	44	45	-194	-195
K	K200	-319	-344	77	83	-242	-262
K	K250	-275	-288	30	29	-246	-255
K	K300	-328	-330	69	67	-260	-265
K	K350	-334	-324	52	48	-250	-274
K	K400	-408	-405	65	65	-355	-347
K	K450	-307	-339	43	48	-259	-283
K	K500	-408	-414	51	52	-373	-380
K	K600	-244	-244	35	35	-221	-221
W	W100	516	503	-137	-134	402	388
W	W150	503	477	-79	-84	419	392
W	W200	556	547	-135	-136	438	433
W	W250	427	477	-140	-69	300	380
W	W300	674	689	-140	-141	570	584
W	W350	607	705	-112	-96	515	626
W	W400	763	797	-125	-121	657	709
W	W450	593	708	-141	-78	449	600
W	W500	1131	1141	-115	-119	1082	1096
LOAD	PX (KIPS)	-100.0	.1			-100.0	
LOAD	PY (KIPS)	.1	-100.0			-101.2	
ACTUAL	PX (KIPS)	-19.3	.0			-19.3	
ACTUAL	PY (KIPS)	.0	-19.3			-19.5	

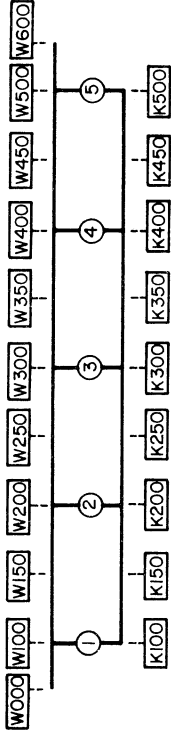
TABLE 14D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. LONGITUDINAL RESTRAINT.

SECTION B

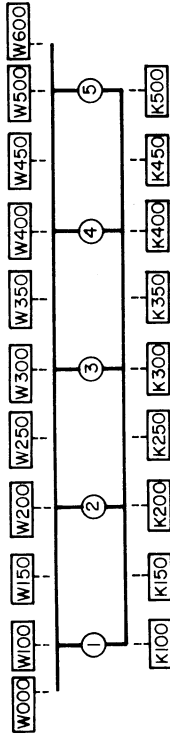
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)		MEASR	ADJUST	THEORY	MEASR	ADJUST
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR					
W	W000	199	199	212	212	424	424	438				
W	W100	231	236	202	204	433	440	465				
W	W150	191	224	193	213	384	407	399				
W	W200	375	362	204	211	579	573	591				
W	W250	367	419	140	137	507	556	547				
W	W300	467	504	167	166	634	670	657				
W	W350	399	458	182	211	581	669	597				
W	W400	425	419	275	283	700	702	711				
W	W450	387	438	269	319	656	737	745				
W	W500	399	408	273	274	672	682	691				
W	W600	426	426	268	268	694	694	720				
K	K100	-234	-239	-189	-190	-423	-429	-415				
K	K150	-226	-223	-203	-189	-429	-412	-422				
K	K200	-288	-277	-129	-127	-417	-404	-420				
K	K250	-335	-318	-86	-79	-421	-397	-422				
K	K300	-345	-354	-75	-70	-420	-424	-415				
K	K350	-289	-289	-134	-136	-423	-425	-421				
K	K400	-228	-220	-178	-187	-406	-407	-408				
K	K450	-275	-260	-152	-170	-427	-430	-409				
K	K500	-237	-239	-166	-160	-403	-399	-434				
LOAD	PX (KIPS)	-100.0		.1		-100.0		-100.0				
LOAD	PY (KIPS)	.1		-100.0		-101.2		-101.2				
ACTUAL	PX (KIPS)	-19.3		.0		-19.3		-19.3				
ACTUAL	PY (KIPS)	.0		-19.3		-19.5		-19.5				

TABLE 14E

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 LONGITUDINAL RESTRAINT.



TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LCC.	(5-X)		(5-Y)		(5-X)+(5-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	222	222	134	134	391	391
W	W100	192	201	153	144	368	367
W	W150	181	206	159	145	357	369
W	W200	211	210	324	326	576	578
W	W250	160	163	284	275	455	455
W	W300	164	162	509	514	688	685
W	W350	157	178	350	374	525	572
W	W400	289	306	476	471	822	838
W	W450	255	277	386	371	636	646
W	W500	275	266	476	480	748	745
W	W600	270	270	528	528	795	795
K	K100	-177	-176	-217	-214	-394	-389
K	K150	-153	-154	-195	-178	-350	-336
K	K200	-142	-148	-228	-234	-376	-376
K	K250	-85	-92	-290	-331	-372	-425
K	K300	-63	-63	-335	-320	-397	-381
K	K350	-76	-76	-450	-430	-534	-512
K	K400	-142	-134	-274	-296	-412	-427
K	K450	-262	-240	-166	-211	-431	-455
K	K500	-178	-178	-306	-299	-488	-480
LOAD	PX (KIPS)	-100.0		.1		-100.0	
LOAD	PY (KIPS)	.1		-100.0		-101.2	
ACTUAL	PX (KIPS)	-19.3		.0		-19.3	
ACTUAL	PY (KIPS)	.0		-19.3		-19.5	

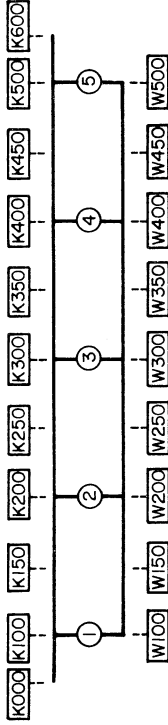
TABLE 14F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. LONGITUDINAL RESTRAINT.

SECTION D

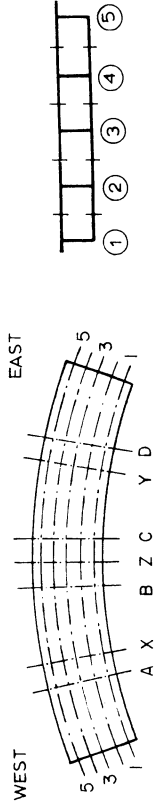
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)		MEASR	ADJUST
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR		
K	K000		28		-115		-115	-88	-88
K	K100		53		-203		-203	-154	-160
K	K150		79		-380		-380	-320	-311
K	K200		74		-289		-289	-241	-228
K	K250		48		-276		-276	-235	-257
K	K300		60		-322		-322	-284	-302
K	K350		84		-416		-416	-379	-426
K	K400		66		-436		-436	-407	-403
K	K450		103		-623		-623	-591	-635
K	K500		69		-447		-447	-413	-424
K	K600		21		-188		-188	-171	-413
W	W100	-77	-81	278	281	214	220		
W	W150	-100	-110	403	356	329	281		
W	W200	-117	-114	477	466	371	361		
W	W250	-117	-109	483	458	379	359		
W	W300	-124	-123	571	575	502	507		
W	W350	-58	-77	776	721	729	661		
W	W400	-123	-125	1076	1028	1006	954		
W	W450	-115	-101	1013	887	945	817		
W	W500	-168	-167	257	278	177	198		
LOAD	PX (KIPS)	-100.0		.1		-100.0			
LOAD	PY (KIPS)	.1		-100.0		-101.2			
ACTUAL	PX (KIPS)	-19.3		.0		-19.3			
ACTUAL	PY (KIPS)	.0		-19.3		-19.5			

TABLE 14G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
LONGITUDINAL RESTRAINT.



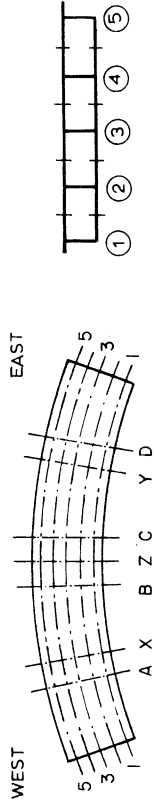
SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	37.4	37.4	9.5	-8.1	-8.1	12.9	-8.1	12.9	30.3	9.0
A	2	73.6	73.6	18.7	-15.1	-15.1	24.1	-15.1	24.1	59.1	17.5
A	3	91.5	91.5	23.3	-15.9	-15.9	25.5	-15.9	25.5	77.9	23.0
A	4	109.8	109.8	27.9	-15.1	-15.1	24.1	-15.1	24.1	96.3	28.5
A	5	80.9	80.9	20.6	-8.3	-8.3	13.3	-8.3	13.3	74.7	22.1
A	SUM	393.3	393.3		-62.5	-62.5		-62.5		338.3	
B	1	-24.8	-24.8	9.2	-24.3	-24.3	15.5	-24.3	15.5	-52.8	11.9
B	2	-50.5	-50.5	18.8	-28.7	-28.7	18.3	-28.7	18.3	-82.2	18.5
B	3	-74.5	-74.5	27.7	-27.3	-27.3	17.4	-27.3	17.4	-106.2	23.9
B	4	-67.0	-67.0	24.9	-41.3	-41.3	26.3	-41.3	26.3	-111.8	25.1
B	5	-51.8	-51.8	19.3	-35.6	-35.6	22.7	-35.6	22.7	-92.0	20.7
B	SUM	-268.5	-268.5		-157.2	-157.2		-157.2		-445.0	
C	1	-27.2	-27.2	16.0	-15.0	-15.0	5.9	-15.0	5.9	-45.6	10.4
C	2	-33.1	-33.1	19.4	-41.6	-41.6	16.5	-41.6	16.5	-79.8	18.2
C	3	-28.5	-28.5	16.8	-67.5	-67.5	26.7	-67.5	26.7	-98.2	22.4
C	4	-45.3	-45.3	26.6	-69.0	-69.0	27.3	-69.0	27.3	-120.0	27.3
C	5	-36.1	-36.1	21.2	-59.8	-59.8	23.6	-59.8	23.6	-95.2	21.7
C	SUM	-170.2	-170.2		-252.9	-252.9		-252.9		-438.7	
D	1	-7.2	-7.2	11.5	23.1	23.1	7.1	23.1	7.1	18.3	6.5
D	2	-15.4	-15.4	24.7	59.6	59.6	18.2	59.6	18.2	46.1	16.3
D	3	-14.3	-14.3	23.0	75.6	75.6	23.1	75.6	23.1	65.8	23.3
D	4	-14.5	-14.5	23.3	132.0	132.0	40.4	132.0	40.4	122.3	43.3
D	5	-10.8	-10.8	17.4	36.2	36.2	11.1	36.2	11.1	29.6	10.5
D	SUM	-62.3	-62.3		326.6	326.6		326.6		282.2	
LOAD	PX (KIPS)	-100.0	-100.0	.1						-100.0	
LOAD	PY (KIPS)	.1	.1							-101.2	
ACTUAL	PX (KIPS)	-19.3	-19.3	.0						-19.3	
ACTUAL	PY (KIPS)	.0	.0							-19.5	

TABLE 14H:

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
LONGITUDINAL RESTRAINT.

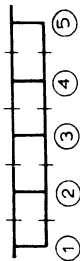
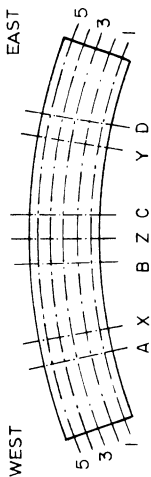


SECTION	GIRDER	(5-X)		(5-Y)		(5-X)+(5-Y)	
		THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT
A	1	102.3	19.6	-28.7	30.3	76.0	17.7
	2	99.1	19.0	-18.3	19.3	79.3	18.5
	3	101.2	19.4	-15.8	16.7	84.7	19.8
	4	117.8	22.6	-18.1	19.1	99.4	23.2
	5	100.7	19.3	-13.8	14.6	89.2	20.8
	SUM	521.0		-94.7		428.5	
B	1	-41.8	12.3	-35.2	19.9	-74.7	14.6
	2	-80.7	23.8	-38.1	21.5	-118.1	23.1
	3	-102.8	30.3	-25.8	14.5	-126.4	24.7
	4	-71.0	20.9	-50.4	28.4	-121.6	23.8
	5	-42.8	12.6	-27.8	15.7	-71.1	13.9
	SUM	-339.1		-177.3		-512.0	
C	1	-30.6	17.7	-38.2	10.6	-68.3	12.9
	2	-40.9	23.6	-73.0	20.3	-112.5	21.2
	3	-21.0	12.1	-112.5	31.3	-133.5	25.2
	4	-42.8	24.7	-92.1	25.6	-134.0	25.3
	5	-37.7	21.8	-43.8	12.2	-82.2	15.5
	SUM	-173.1		-359.5		-530.5	
D	1	-14.6	15.0	64.1	11.7	52.0	10.4
	2	-19.5	20.1	89.9	16.3	75.8	15.2
	3	-18.8	19.3	105.1	19.1	93.8	18.8
	4	-23.5	24.2	143.3	26.0	135.5	27.2
	5	-20.9	21.5	147.6	26.8	140.9	28.3
	SUM	-97.2		550.0		498.0	
LJAD	PX (KIPS)	-100.0		.1		-100.0	
LJAD	PY (KIPS)	.1		-100.0		-101.2	
ACTUAL	PX (KIPS)	-19.3		.0		-19.3	
ACTUAL	PY (KIPS)	.0		-19.3		-19.5	



TABLE 141

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.A.



RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING,  
LONGITUDINAL RESTRAINT.

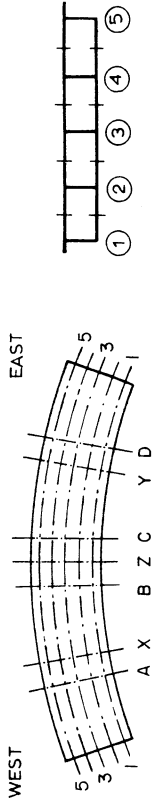
SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1		66.4	14.7		-17.3	22.5		50.7	13.4
A	2		95.0	18.9		-16.5	21.5		68.1	18.0
A	3		95.9	21.3		-15.9	20.7		80.9	21.4
A	4		113.4	25.2		-16.4	21.4		97.7	25.8
A	5		89.7	19.9		-10.8	14.0		81.2	21.4
A	SUM		450.4			-76.9			378.7	
B	1		-34.2	11.1		-30.4	18.0		-65.0	13.5
B	2		-67.2	21.8		-33.9	20.1		-102.1	21.2
B	3		-90.2	29.3		-26.5	15.7		-117.5	24.4
B	4		-69.2	22.5		-46.4	27.5		-117.3	24.3
B	5		-46.8	15.2		-31.3	18.6		-80.4	16.7
B	SUM		-307.7			-168.4			-482.3	
C	1		-29.1	16.9		-27.9	8.9		-58.2	11.9
C	2		-37.4	21.8		-59.0	18.9		-97.9	20.0
C	3		-24.4	14.2		-92.4	29.6		-117.8	24.1
C	4		-44.0	25.6		-81.8	25.2		-127.8	26.1
C	5		-37.0	21.5		-50.9	16.3		-88.0	18.0
C	SUM		-171.9			-312.0			-489.7	
D	1		-10.5	13.5		41.5	9.7		33.4	8.8
D	2		-17.2	22.1		73.1	17.1		59.4	15.7
D	3		-16.3	20.9		88.8	20.8		78.3	20.7
D	4		-18.5	23.8		137.1	32.1		128.2	33.9
D	5		-15.3	19.7		86.0	20.2		79.3	20.9
D	SUM		-77.9			426.5			378.6	
LOAD	PX (KIPS)		-100.0			.1			-100.0	
LOAD	PY (KIPS)		.1			-100.0			-101.2	
ACTUAL	PX (KIPS)		-19.3			.0			-19.3	
ACTUAL	PY (KIPS)		.0			-19.3			-19.5	

TABLE 14J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
LONGITUDINAL RESTRAINT.



SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1		66.6	15.0		-17.5	23.0		50.2	13.5
A	2		83.5	18.8		-16.3	21.5		66.7	17.9
A	3		94.7	21.3		-15.9	21.0		80.0	21.5
A	4		112.5	25.4		-16.1	21.3		97.3	26.1
A	5		86.1	19.4		-10.0	13.2		78.4	21.0
A	SUM		443.4			-75.8			372.7	
B	1		-33.3	11.1		-29.6	17.8		-63.2	13.3
B	2		-63.6	21.2		-32.2	19.4		-97.0	20.5
B	3		-86.2	28.7		-26.8	16.1		-113.8	24.0
B	4		-68.4	22.8		-44.9	27.0		-115.4	24.4
B	5		-48.5	16.2		-32.7	19.7		-84.4	17.8
B	SUM		-299.9			-166.3			-473.7	
C	1		-28.8	16.7		-28.9	9.6		-57.3	12.0
C	2		-36.3	21.0		-54.7	18.2		-92.7	19.5
C	3		-26.4	15.3		-84.7	28.3		-110.8	23.3
C	4		-44.5	25.8		-77.9	26.0		-124.7	26.2
C	5		-36.7	21.3		-53.6	17.9		-90.1	18.9
C	SUM		-172.9			-299.9			-475.6	
D	1		-10.1	13.6		40.6	9.3		32.5	8.2
D	2		-17.0	22.8		70.9	16.2		57.6	14.5
D	3		-15.9	21.3		86.6	19.7		76.3	19.2
D	4		-17.6	23.6		135.3	30.8		126.2	31.7
D	5		-13.8	18.6		105.4	24.0		105.5	26.5
D	SUM		-74.3			438.8			398.1	
LJAD	PX (KIPS)		-100.0			.1			-100.0	
LOAD	PY (KIPS)		.1			-100.0			-101.2	
ACTUAL	PX (KIPS)		-19.3			.0			-19.3	
ACTUAL	PY (KIPS)		.0			-19.3			-19.5	

TABLE 15'A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 30 KSI COND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT Y-AXIS LONGITUDINAL RESTRAINT.

REACTION OR LOAD	(1-X)+(5-Y)		NORMALIZED POINT LOAD APPLIED AT	
	THEORY	EXPERM	THEORY	EXPERM
1E	-14.46			
2E	-6.54			
3E	5.59			
4E	15.94			
5E	39.03			
1F	48.37			
2F	-2.52			
3F	15.83			
4F	65.57			
1W	23.04			
2W	13.45			
3W	9.04			
4W	1.38			
5W	-8.41			
RE	39.56			
RF	127.25			
PW	38.50			
SUMR	205.31			
PX	-100.00			
PY	-101.98			
SUMP	-201.98			
SUMR/SUMP	1.02			
TW	-192.89			
NF	53.23			
TF	150.94			
TE	155.56			
ACTUAL PX	-19.10			
ACTUAL PY	-19.48			

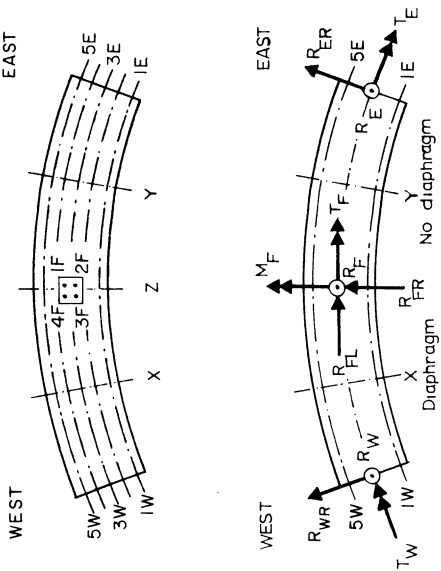
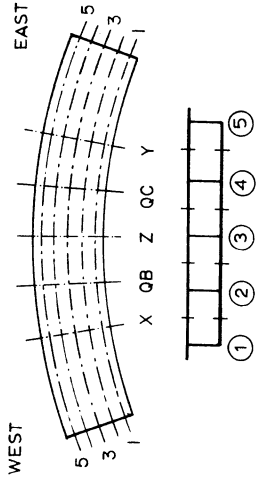


TABLE 15B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 LONGITUDINAL PESTRRAINT.



NORMALIZED POINT LOAD APPLIED AT

\*\*\*\*\*  
 THEORY EXPERM E/T \*\*\*\*\*  
 THEORY EXPERM E/T \*\*\*\*\*

(1-X)+(5-Y)  
 \*\*\*\*\*  
 THEORY EXPERM E/T \*\*\*\*\*

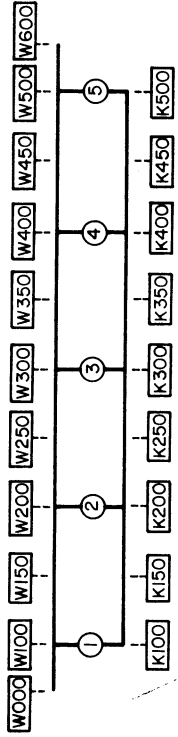
DEFLECTION AT POINT	THEORY	EXPERM	E/T
1X	.726		
2X	.591		
3X	.483		
4X	.384		
5X	.296		
1QB	.348		
2QB	.267		
3QB	.210		
4QB	.167		
5QB	.139		
1Z	-.011		
2Z	-.004		
4Z	.054		
5Z	.120		
1QC	.092		
2QC	.160		
3QC	.276		
4QC	.478		
5QC	.679		
1Y	.249		
2Y	.357		
3Y	.567		
4Y	.853		
5Y	1.445		
LOAD PX	-100.0		
LOAD PY	-102.0		
ACTUAL PX	-19.1		
ACTUAL PY	-19.5		

\*\*\*\*\*  
 THEORY EXPERM E/T \*\*\*\*\*  
 THEORY EXPERM E/T \*\*\*\*\*



TABLE 15D

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 LONGITUDINAL RESTRAINT.



SECTION R  
 TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

NORMALIZED POINT LOAD APPLIED AT

GAGE TYPE	GAGE LCC.	(1-X)+(5-Y)		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	ADJUST	ADJUST	MEASR	ADJUST
W	W000		606				
W	W100		552				
W	W150		488				
W	W200		527				
W	W250		446				
W	W300		539				
W	W350		401				
W	W400		446				
W	W450		409				
W	W500		378				
W	W600		361				
K	K100						
K	K150		-385				
K	K200		-478				
K	K250		-304				
K	K300		-304				
K	K350		-352				
K	K400		-371				
K	K450		-349				
K	K500		-273				
			-282				
LOAD	PX (KIPS)						
LOAD	PY (KIPS)						
ACTUAL	PX (KIPS)		-100.0				
ACTUAL	PY (KIPS)		-102.0				
			-19.1				
			-19.5				

LOAD PX (KIPS)  
 LOAD PY (KIPS)  
 ACTUAL PX (KIPS)  
 ACTUAL PY (KIPS)

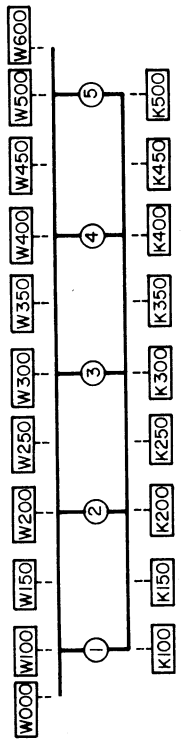
TABLE 15E

SUMMARY OF STRAINS (MICPC IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 30 KSI COND. LOADING. LONGITUDINAL RESTRAINT.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

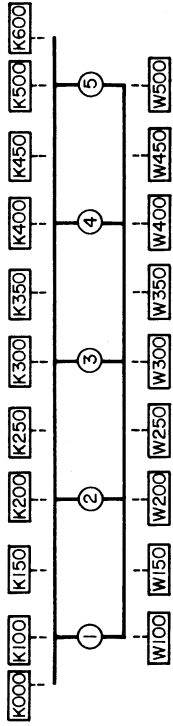


NORMALIZED POINT LOAD APPLIED AT

GAGE TYPE	GAGE LOC.	(1-X)+(5-Y)		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	ADJUST	ADJUST	MEASR	ADJUST
W	W000		361		361		361
W	W100		366		353		353
W	W150		335		317		317
W	W200		572		575		575
W	W250		388		378		378
W	W300		628		633		633
W	W350		425		454		454
W	W400		631		627		627
W	W450		492		472		472
W	W500		590		596		596
W	W600		636		636		636
K	K100	-339		-333			
K	K150	-298		-262			
K	K200	-315		-310			
K	K250	-328		-353			
K	K300	-353		-344			
K	K350	-511		-485			
K	K400	-372		-395			
K	K450	-303		-349			
K	K500	-450		-442			
LOAD	PX (KIPS)						
LOAD	PY (KIPS)			-100.0			
ACTUAL	PX (KIPS)			-102.0			
ACTUAL	PY (KIPS)			-19.1			
ACTUAL	PY (KIPS)			-19.5			

TABLE 15F

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 30 KSI COND. LOADING.  
 LONGITUDINAL RESTRAINT.



SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

NORMALIZED POINT LOAD APPLIED AT

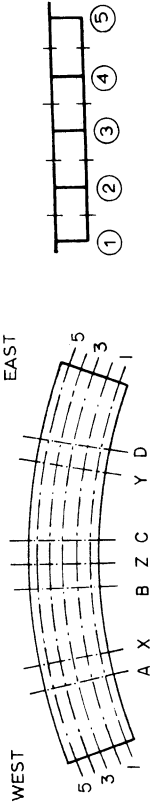
GAGE TYPE	GAGE LOC.	(1-X)+(5-Y)		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	ADJUST	ADJUST	MEASR	ADJUST
K	K000		-83				
K	K100		-155				
K	K150		-296				
K	K200		-250				
K	K250		-231				
K	K300		-289				
K	K350		-389				
K	K400		-410				
K	K450		-606				
K	K500		-442				
K	K600		-185				
W	W100	205					
W	W150	297					
W	W200	381					
W	W250	404					
W	W300	506					
W	W350	669					
W	W400	1023					
W	W450	949					
W	W500	182					

LOAD	PX (KIPS)	-100.0
LOAD	PY (KIPS)	-102.0
ACTUAL	PX (KIPS)	-19.1
ACTUAL	PY (KIPS)	-19.5



TABLE 15G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
LONGITUDINAL RESTRAINT.



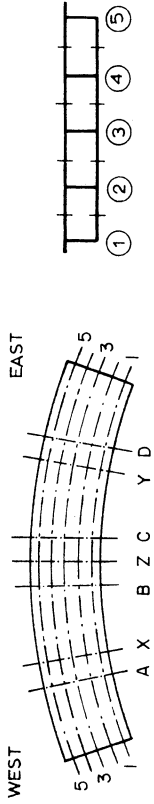
SECTION	GIRDER	(1-X)+(5-Y)		NORMALIZED POINT LOAD APPLIED AT		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	53.1	18.3	53.1	18.3	53.1	18.3	53.1	18.3
A	2	31.1	27.9	31.1	27.9	31.1	27.9	31.1	27.9
A	3	56.5	22.9	56.5	22.9	56.5	22.9	56.5	22.9
A	4	56.0	19.3	56.0	19.3	56.0	19.3	56.0	19.3
A	5	33.9	11.7	33.9	11.7	33.9	11.7	33.9	11.7
A	SUM	290.6		290.6		290.6		290.6	
B	1	-67.2	19.6	-67.2	19.6	-67.2	19.6	-67.2	19.6
B	2	-77.9	22.7	-77.9	22.7	-77.9	22.7	-77.9	22.7
B	3	-78.6	22.9	-78.6	22.9	-78.6	22.9	-78.6	22.9
B	4	-69.5	20.3	-69.5	20.3	-69.5	20.3	-69.5	20.3
B	5	-49.7	14.5	-49.7	14.5	-49.7	14.5	-49.7	14.5
B	SUM	-343.0		-343.0		-343.0		-343.0	
C	1	-41.7	11.5	-41.7	11.5	-41.7	11.5	-41.7	11.5
C	2	-73.5	20.3	-73.5	20.3	-73.5	20.3	-73.5	20.3
C	3	-84.5	23.4	-84.5	23.4	-84.5	23.4	-84.5	23.4
C	4	-88.5	24.5	-88.5	24.5	-88.5	24.5	-88.5	24.5
C	5	-72.8	20.2	-72.8	20.2	-72.8	20.2	-72.8	20.2
C	SUM	-361.1		-361.1		-361.1		-361.1	
D	1	17.2	6.1	17.2	6.1	17.2	6.1	17.2	6.1
D	2	46.8	16.6	46.8	16.6	46.8	16.6	46.8	16.6
D	3	65.7	23.3	65.7	23.3	65.7	23.3	65.7	23.3
D	4	123.2	43.6	123.2	43.6	123.2	43.6	123.2	43.6
D	5	29.2	10.4	29.2	10.4	29.2	10.4	29.2	10.4
D	SUM	232.3		232.3		232.3		232.3	
LOAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0	
LOAD	PY (KIPS)	-102.0		-102.0		-102.0		-102.0	
ACTUAL	PX (KIPS)	-19.1		-19.1		-19.1		-19.1	
ACTUAL	PY (KIPS)	-19.5		-19.5		-19.5		-19.5	

TABLE 15H:

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
LONGITUDINAL RESTRAINT.



NORMALIZED POINT LOAD APPLIED AT

\*\*\*\*\*  
THEORY K-FT PCT  
\*\*\*\*\* EXPERIMENTAL K-FT PCT

\*\*\*\*\*  
THEORY K-FT PCT  
\*\*\*\*\* EXPERIMENTAL K-FT PCT

\*\*\*\*\*  
THEORY K-FT PCT  
\*\*\*\*\* EXPERIMENTAL K-FT PCT

SECTION	GIRDER	(1-X)+(5-Y)	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
A	1		128.5		30.0	
A	2		101.6		23.7	
A	3		77.3		18.1	
A	4		75.3		17.6	
A	5		45.6		10.6	
A	SUM		428.3			

B	1		-73.4		16.8	
B	2		-101.0		23.1	
B	3		-108.8		24.9	
B	4		-104.5		23.9	
B	5		-49.8		11.4	
B	SUM		-437.4			

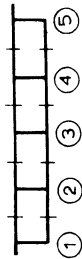
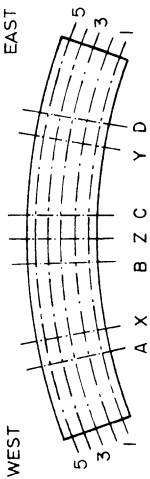
C	1		-55.2		12.1	
C	2		-89.3		19.6	
C	3		-120.1		26.3	
C	4		-121.3		26.6	
C	5		-70.7		15.5	
C	SUM		-456.6			

D	1		48.8		9.7	
D	2		75.5		15.0	
D	3		93.6		18.7	
D	4		135.9		27.1	
D	5		147.9		29.5	
D	SUM		501.7			

LOAD	PX (KIPS)	-100.0
LOAD	PY (KIPS)	-102.0
ACTUAL	PX (KIPS)	-19.1
ACTUAL	PY (KIPS)	-19.5

TABLE 151

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.



RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
LONGITUDINAL RESTRAINT.

NORMALIZED POINT LOAD APPLIED AT

\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

(1-X)+(5-Y)  
\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

SECTION	GIRDER	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
A	1	86.8	24.6		
A	2	90.2	25.6		
A	3	71.4	20.3		
A	4	64.7	18.4		
A	5	39.1	11.1		
A	SUM	352.1			
B	1	-70.7	17.9		
B	2	-90.7	22.9		
B	3	-95.4	24.1		
B	4	-88.9	22.5		
B	5	-49.8	12.6		
B	SUM	-395.4			
C	1	-49.2	11.9		
C	2	-82.3	19.9		
C	3	-104.2	25.2		
C	4	-106.7	25.8		
C	5	-71.7	17.3		
C	SUM	-414.1			
D	1	31.4	8.2		
D	2	59.6	15.7		
D	3	78.2	20.6		
D	4	128.9	33.9		
D	5	32.2	21.6		
D	SUM	380.3			

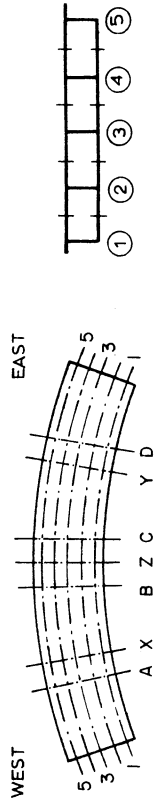
LOAD	PX (KIPS)	PY (KIPS)
LOAD	-100.0	-102.0
ACTUAL	-19.1	-19.5

TABLE 15J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 30 KSI COND. LOADING.  
LONGITUDINAL RESTRAINT.



SECTION	GIRDER	(1-X)+(5-Y)		NORMALIZED POINT LOAD APPLIED AT		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1			83.6	24.3				
A	2			88.9	25.9				
A	3			70.3	20.5				
A	4			63.4	18.5				
A	5			37.1	10.8				
A	SUM			343.4					
B	1			-69.7	18.3				
B	2			-86.3	22.6				
B	3			-90.4	23.7				
B	4			-84.8	22.3				
B	5			-49.7	13.1				
B	SUM			-381.0					
C	1			-48.2	12.1				
C	2			-79.0	19.9				
C	3			-97.1	24.4				
C	4			-101.2	25.5				
C	5			-71.9	18.1				
C	SUM			-397.4					
D	1			30.9	7.7				
D	2			58.1	14.4				
D	3			76.1	18.9				
D	4			126.9	31.5				
D	5			111.1	27.6				
D	SUM			403.1					
LOAD	PX (KIPS)								
LOAD	PY (KIPS)								
ACTUAL	PX (KIPS)			-100.0					
ACTUAL	PY (KIPS)			-102.0					
	PX (KIPS)			-19.1					
	PY (KIPS)			-19.5					

TABLE 16A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS  
 TW = MOMENT AT FOOTING ABOUT Y-AXIS  
 RESULTS FOR TRUCK LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.

REACTION OR LOAD	3A+4A		1A+2A+3A+4A		1A+2A	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	1.73	-0.06	1.69	0.30		0.39
2E	0.94	1.89	0.67	1.43		-0.74
3E	0.43	2.08	0.19	1.34		-0.45
4E	1.32	0.33	1.00	0.82		0.26
5E	2.66	2.79	2.09	1.85		-0.61
1F	6.38	5.66	5.90	5.18		0.16
2F	6.69	5.10	6.18	4.05		-0.24
3F	-0.23	0.50	6.35	7.41		6.29
4F	-0.54	1.32	6.07	8.30		6.31
1W	0.07	-0.11	0.90	1.34		1.37
2W	-0.23	0.10	0.99	0.29		0.46
3W	-0.24	-0.32	0.64	0.86		0.72
4W	-0.34	-0.44	1.12	1.05		1.72
5W	-0.63	-0.59	2.20	2.26		2.86
PE	7.08	7.03	5.64	5.74		-1.35
PF	12.30	12.58	24.50	24.94		12.52
PW	-1.37	-1.36	5.85	5.80		7.13
SUMR	18.01	18.25	35.99	36.48		19.30
PX	-0.	-0.	-18.00	-18.00		-18.00
PY	-18.00	-18.00	-18.00	-18.00		-0.
SUMP	-18.00	-18.00	-36.00	-36.00		-18.00
SUMR/SUMP	1.00	1.01	1.00	1.01		1.02
TW	-3.89	-3.86	7.02	6.69		10.93
WF	-20.78	-13.41	0.50	9.72		19.02
TF	-0.92	2.09	-0.84	3.03		0.64
TE	5.76	10.65	2.91	6.41		-3.86
ACTUAL PX		-0.		-18.06		-18.09
ACTUAL PY		-18.12		-18.06		-0.

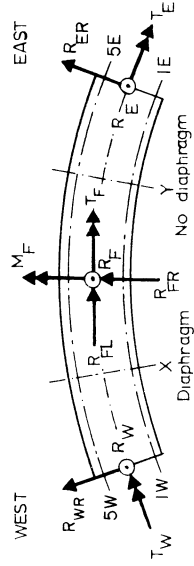
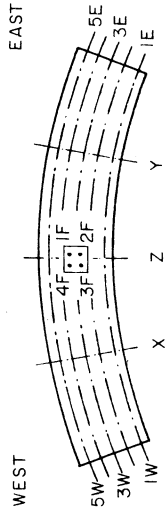
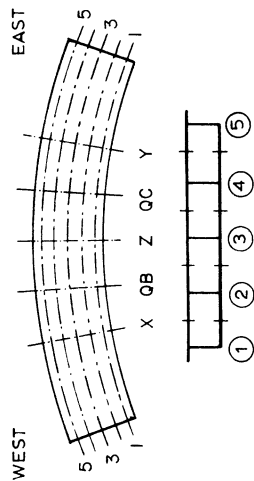


TABLE 16B

SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.



DEFLECTION AT POINT	3A+4A		1A+2A		1A+2A+3A+4A		1A+2A	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X	-.041	-.054	1.32	1.32	.083	.116	1.41	.168
2X	-.043	-.059	1.37	1.37	.083	.120	1.44	.175
3X	-.045	-.064	1.42	1.42	.086	.126	1.47	.181
4X	-.048	-.065	1.35	1.35	.091	.130	1.43	.193
5X	-.051	-.066	1.29	1.29	.097	.139	1.43	.200
1Q8	-.035	-.048	1.39	1.39	.042	.061	1.45	.106
2Q8	-.037	-.048	1.30	1.30	.040	.058	1.45	.105
3Q8	-.038	-.050	1.31	1.31	.039	.059	1.50	.107
4Q8	-.041	-.052	1.27	1.27	.043	.066	1.53	.114
5Q8	-.044	-.053	1.21	1.21	.048	.068	1.42	.117
1Z	.005	.005	1.00	1.00	.007	.011	1.57	.008
2Z	.002	.003	1.30	1.30	.004	.008	2.34	.005
4Z	.001	.002	2.37	2.37	.002	.005	2.37	.001
5Z	.001	.005	3.34	3.34	.004	.008	2.02	.003
1QC	.081	.103	1.28	1.28	.043	.054	1.25	-.045
2QC	.077	.102	1.32	1.32	.038	.051	1.33	-.048
3QC	.075	.097	1.29	1.29	.036	.045	1.26	-.051
4QC	.082	.106	1.29	1.29	.040	.052	1.31	-.056
5QC	.089	.110	1.24	1.24	.046	.054	1.18	-.055
1Y	.132	.178	1.35	1.35	.089	.119	1.34	-.055
2Y	.125	.170	1.37	1.37	.080	.105	1.32	-.059
3Y	.124	.163	1.31	1.31	.078	.094	1.22	-.065
4Y	.135	.183	1.36	1.36	.086	.114	1.31	-.063
5Y	.147	.198	1.35	1.35	.096	.129	1.34	-.071
LOAD PX	-0.	-0.	-18.0	-18.0	-18.0	-18.0	-18.0	-18.0
LOAD PY	-18.0	-18.0	-18.0	-18.0	-18.0	-18.0	-18.0	-18.0
ACTUAL PX	-0.	-0.	-18.1	-18.1	-18.1	-18.1	-18.1	-18.1
ACTUAL PY	-18.1	-18.1	-18.1	-18.1	-18.1	-18.1	-18.1	-18.1

NORMALIZED POINT LOADS AT

1A+2A+3A+4A

1A+2A



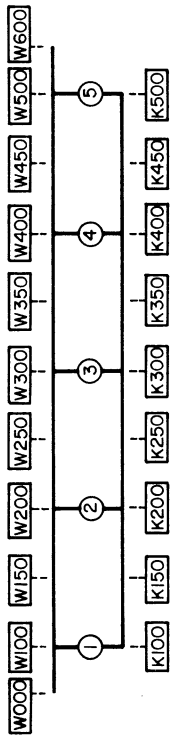
TABLE 16D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	3A+4A		1A+2A+3A+4A		1A+2A		ADJUST
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	
W	W000	82	52	116	105	48	48	48
W	W100	73	55	108	110	49	49	50
W	W150	53	51	89	103	43	50	50
W	W250	38	57	99	123	64	63	63
W	W300	33	41	87	108	55	64	64
W	W350	52	44	90	123	71	75	75
W	W400	69	41	106	107	56	65	65
W	W450	74	47	108	107	55	55	55
W	W500		45		113	41	53	53
W	W600		45		95	47	48	48
K	K100	-33	-35	-49	-67	-31	-32	-32
K	K150	-25	-37	-41	-63	-30	-29	-29
K	K200	-14	-31	-35	-62	-33	-32	-32
K	K250	-25	-27	-42	-58	-35	-35	-35
K	K300	-30	-24	-47	-60	-36	-36	-36
K	K350	-25	-28	-42	-59	-31	-31	-31
K	K400	-30	-30	-47	-57	-26	-26	-26
K	K450	-27	-26	-47	-59	-29	-30	-30
K	K500	-30	-27	-47	-56	-29	-29	-29
LOAD	PX (KIPS)	-0.	-0.	-18.0	-18.0	-18.0	-18.0	-18.0
LOAD	PY (KIPS)	-18.0	-18.0	-18.0	-18.0	-0.	-0.	-0.
ACTUAL	PX (KIPS)	-0.	-18.1	-18.1	-18.1	-18.1	-18.1	-18.1
ACTUAL	PY (KIPS)	-18.1	-18.1	-18.1	-18.1	-0.	-0.	-0.



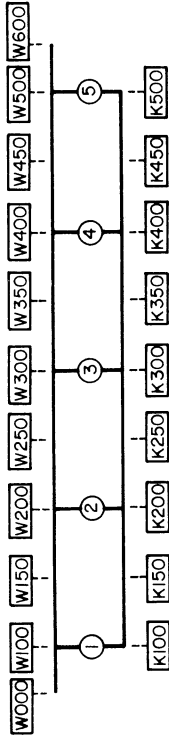
TABLE 16E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	3A+4A		1A+2A+3A+4A		1A+2A	
		THEORY	MEASR ADJUST	THEORY	MEASR ADJUST	THEORY	MEASR ADJUST
W	W000	39	55	119	112	54	54
W	W100	38	50	110	103	48	48
W	W150	45	49	92	98	42	44
W	W200	35	67	89	129	56	56
W	W250	56	55	96	96	38	38
W	W300	51	74	85	125	46	46
W	W350	48	52	87	93	34	34
W	W400	36	58	89	120	56	57
W	W450	42	44	89	93	46	48
W	W500	36	45	106	97	49	48
W	W600	33	45	108	98	49	49
K	K100	-18	-36	-50	-70	-34	-32
K	K150	-30	-30	-61	-60	-30	-30
K	K200	-16	-31	-41	-64	-32	-33
K	K250	-34	-37	-63	-69	-27	-31
K	K300	-20	-34	-35	-61	-26	-25
K	K350	-41	-40	-73	-70	-29	-28
K	K400	-16	-27	-42	-59	-31	-30
K	K450	-24	-26	-65	-67	-41	-40
K	K500	-16	-29	-47	-62	-32	-32
LOAD	PX (KIPS)	-0.	-0.	-18.0	-18.0	-18.0	-18.0
LOAD	PY (KIPS)	-18.0	-18.0	-18.0	-18.0	-0.	-0.
ACTUAL	PX (KIPS)	-0.	-0.	-18.1	-18.1	-18.1	-18.1
ACTUAL	PY (KIPS)	-18.1	-18.1	-18.1	-18.1	-0.	-0.

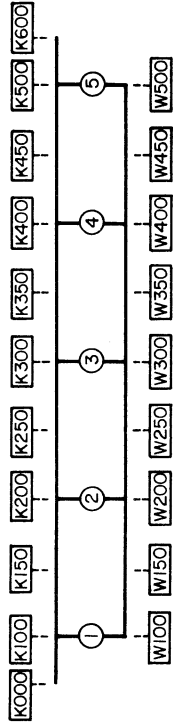
TABLE 16F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.

SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

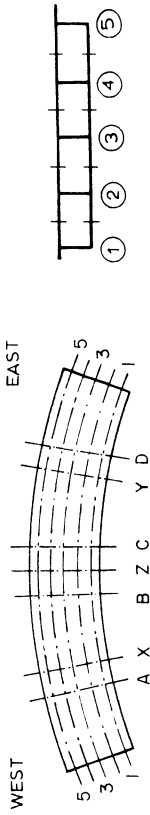


NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	3A+4A		1A+2A+3A+4A		1A+2A	
		THEORY	MEASR ADJUST	THEORY	MEASR ADJUST	THEORY	MEASR ADJUST
K	K000	-55	-32	-43	-24	-24	6
K	K100	-48	-53	-38	-41	-43	10
K	K150	-80	-77	-28	-62	-59	19
K	K200	-36	-66	-28	-52	-51	15
K	K250	-56	-63	-43	-43	-49	12
K	K300	-37	-62	-28	-47	-49	13
K	K350	-71	-75	-29	-56	-59	19
K	K400	-72	-69	-29	-59	-56	15
K	K450	-93	-83	-77	-77	-68	24
K	K500	-44	-72	-35	-60	-60	16
K	K600	-48	-72	-38	-22	-60	5
W	W100	211	125	171	99	102	-24
W	W150	164	156	125	128	122	-35
W	W200	161	163	125	126	123	-35
W	W250	142	136	128	109	104	-34
W	W300	166	136	128	102	103	-36
W	W350	144	138	128	109	105	-34
W	W400	162	144	128	154	150	-40
W	W450	154	153	153	120	118	-33
W	W500	190	197	153	159	163	-35
LOAD	PX (KIPS)	-0.	-0.	-18.0	-18.0	-18.0	-18.0
LCAD	PY (KIPS)	-18.0	-18.0	-18.0	-18.0	-18.0	-18.0
ACTUAL	PX (KIPS)	-0.	-0.	-18.1	-18.1	-18.1	-18.1
ACTUAL	PY (KIPS)	-18.1	-18.1	-18.1	-18.1	-18.1	-18.1

TABLE 16G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



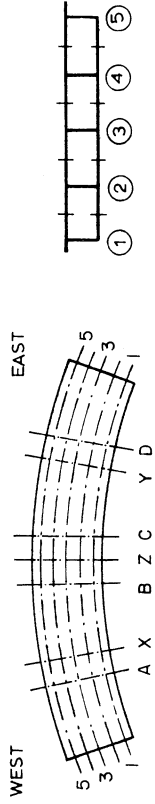
SECTION	GIRDER	3A+4A		1A+2A+3A+4A		1A+2A			
		THEORY K-FT	PCT	THEORY K-FT	PCT	THEORY K-FT	PCT		
A	1	-3.4	16.7	-2.3	11.9	14.4	18.2	12.6	15.9
A	2	-4.5	22.4	-4.3	22.0	18.1	22.9	18.7	23.6
A	3	-4.5	22.2	-4.7	24.3	15.7	21.1	17.7	22.3
A	4	-4.5	22.3	-4.9	25.4	17.1	21.7	18.3	23.0
A	5	-3.3	16.4	-3.2	16.4	12.8	16.2	12.1	15.2
A	SUM	-20.3		-19.5		79.1		79.4	
B	1	-8.8	19.4	-6.4	18.9	-13.1	16.7	-12.9	16.5
B	2	-10.4	23.0	-7.7	22.7	-17.5	22.4	-17.4	22.3
B	3	-7.7	17.0	-6.8	19.9	-17.5	22.3	-18.5	23.8
B	4	-10.2	22.5	-7.2	21.0	-17.6	22.5	-16.6	21.4
B	5	-8.2	18.1	-6.0	17.5	-12.7	16.2	-12.5	16.1
B	SUM	-45.3		-34.1		-73.5		-78.0	
C	1	-4.8	14.5	-6.8	15.9	-13.4	17.1	-13.7	16.8
C	2	-7.2	21.9	-10.0	23.6	-17.6	22.4	-18.8	23.0
C	3	-9.4	28.5	-10.6	25.1	-17.2	22.0	-18.2	22.4
C	4	-7.2	21.7	-9.0	21.3	-17.6	22.3	-18.1	22.2
C	5	-4.4	13.4	-5.9	14.0	-12.7	16.2	-12.7	15.6
C	SUM	-33.1		-42.4		-78.6		-81.5	
D	1	17.9	18.2	11.3	12.8	14.3	18.4	8.9	12.9
D	2	21.7	22.0	21.6	24.4	17.0	21.9	16.7	24.2
D	3	20.6	20.9	18.0	20.4	15.0	20.6	13.6	19.8
D	4	21.7	22.0	23.5	26.5	17.1	22.1	18.3	26.5
D	5	16.6	16.8	14.0	15.9	13.2	17.1	11.3	16.5
D	SUM	98.7		88.4		77.6		68.9	
LOAD	PX (KIPS)	-0.		-0.		-18.0		-18.0	
LOAD	PY (KIPS)	-18.0		-18.0		-18.0		-18.0	
ACTUAL	PX (KIPS)	-0.		-0.		-18.1		-18.1	
ACTUAL	PY (KIPS)	-18.1		-18.1		-18.1		-18.1	

TABLE 16H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

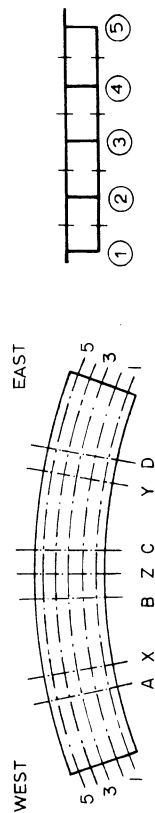
RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



SECTION	GIRDER	3A+4A				NORMALIZED POINT LOADS AT 1A+2A+3A+4A				1A+2A			
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
A	1	-3.4	16.7	-6.2	28.0	14.4	18.2	20.3	25.3	23.5	24.0		
A	2	-4.5	22.4	-4.2	19.0	18.1	22.9	15.7	19.6	19.6	20.0		
A	3	-4.5	22.2	-3.8	17.2	16.7	21.1	14.4	18.0	18.1	18.4		
A	4	-4.5	22.3	-4.5	20.4	17.1	21.7	16.7	20.9	20.7	21.1		
A	5	-3.3	16.4	-3.4	15.5	12.8	16.2	13.0	16.2	16.0	16.4		
A	SUM	-20.3		-22.0		79.1		80.2		97.9			
B	1	-8.8	19.4	-6.1	17.1	-13.1	16.7	-11.2	15.3	-5.3	13.8		
B	2	-10.4	23.0	-8.7	24.1	-17.5	22.4	-17.6	24.0	-9.1	23.9		
B	3	-7.7	17.0	-7.7	21.3	-17.5	22.3	-17.9	24.4	-10.6	27.7		
B	4	-10.2	22.5	-8.7	24.3	-17.6	22.5	-16.8	22.9	-8.1	21.3		
B	5	-8.2	18.1	-4.7	13.1	-12.7	16.2	-9.8	13.4	-5.1	13.4		
B	SUM	-45.3		-35.9		-78.5		-73.3		-38.2			
C	1	-4.8	14.5	-6.1	14.9	-13.4	17.1	-11.5	14.2	-5.6	14.1		
C	2	-7.2	21.9	-9.5	23.3	-17.6	22.4	-19.1	23.6	-9.5	23.9		
C	3	-9.4	28.5	-11.4	27.9	-17.2	22.0	-20.4	25.1	-8.5	21.4		
C	4	-7.2	21.7	-9.1	22.2	-17.6	22.3	-18.9	23.2	-9.6	24.3		
C	5	-4.4	13.4	-4.8	11.7	-12.7	16.2	-11.2	13.9	-6.5	16.3		
C	SUM	-33.1		-40.9		-78.6		-81.1		-39.7			
D	1	17.9	18.2	14.6	15.8	14.3	18.4	11.4	15.4	-3.3	14.5		
D	2	21.7	22.0	19.1	20.7	17.0	21.9	15.0	20.4	-4.7	20.9		
D	3	20.6	20.9	18.6	20.2	16.0	20.6	14.6	19.8	-4.5	20.1		
D	4	21.7	22.0	20.8	22.5	17.1	22.1	16.9	22.9	-5.2	23.0		
D	5	16.6	16.8	19.2	20.8	13.2	17.1	15.9	21.5	-4.8	21.5		
D	SUM	98.7		92.4		77.6		73.8		-22.5			
LOAD	PX (KIPS)			-0.		-18.0		-18.0		-18.0			
LOAD	PY (KIPS)			-18.0		-18.0		-18.0		-18.0			
ACTUAL	PX (KIPS)			-0.		-18.1		-18.1		-18.1			
ACTUAL	PY (KIPS)			-18.1		-18.1		-18.1		-18.1			

TABLE 161

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.  
RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



SECTION	GIRDER	3A+4A			1A+2A+3A+4A			1A+2A			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	-3.4	16.7	-4.0	19.6	14.4	18.2	16.0	20.1	18.6	19.2
A	2	-4.5	22.4	-4.2	20.5	18.1	22.9	17.4	21.8	21.2	21.9
A	3	-4.5	22.2	-4.3	20.9	16.7	21.1	16.2	20.4	20.1	20.7
A	4	-4.5	22.3	-4.7	23.0	17.1	21.7	17.6	22.1	21.8	22.5
A	5	-3.3	16.4	-3.3	16.0	12.8	16.2	12.5	15.6	15.2	15.7
A	SUM	-20.3		-20.6		79.1		79.7		96.9	
B	1	-8.8	19.4	-6.3	17.9	-13.1	16.7	-11.9	15.8	-5.6	14.1
B	2	-10.4	23.0	-8.3	23.5	-17.5	22.4	-17.5	23.2	-9.2	23.1
B	3	-7.7	17.0	-7.3	20.7	-17.5	22.3	-18.2	24.1	-10.9	27.5
B	4	-10.2	22.5	-8.1	22.9	-17.6	22.5	-17.6	22.2	-8.5	21.4
B	5	-8.2	18.1	-5.3	15.0	-12.7	16.2	-11.0	14.6	-5.6	14.0
B	SUM	-45.3		-35.1		-78.5		-75.4		-39.8	
C	1	-4.8	14.5	-6.4	15.4	-13.4	17.1	-12.5	15.4	-5.9	15.7
C	2	-7.2	21.9	-9.7	23.4	-17.6	22.4	-19.0	23.3	-8.9	23.3
C	3	-9.4	28.5	-11.1	26.6	-17.2	22.0	-19.4	23.9	-7.8	20.4
C	4	-7.2	21.7	-9.1	21.8	-17.6	22.3	-18.5	22.8	-9.0	23.6
C	5	-4.4	13.4	-5.3	12.8	-12.7	16.2	-11.9	14.6	-6.4	17.0
C	SUM	-33.1		-41.5		-78.6		-81.3		-38.0	
D	1	17.9	18.2	12.8	14.2	14.3	18.4	10.0	14.1	-2.8	13.2
D	2	21.7	22.0	20.5	22.7	17.0	21.9	16.0	22.4	-4.7	22.6
D	3	20.6	20.9	18.3	20.3	16.0	20.6	14.1	19.8	-4.6	21.9
D	4	21.7	22.0	22.3	24.7	17.1	22.1	17.7	24.8	-5.1	24.6
D	5	16.6	16.8	16.4	18.1	13.2	17.1	13.4	18.8	-3.7	17.7
D	SUM	98.7		90.3		77.6		71.1		-20.8	
LOAD	PX (KIPS)	-0.		-0.		-18.0		-18.0		-18.0	
LOAD	PY (KIPS)	-18.0		-18.0		-18.0		-18.0		-18.0	
ACTUAL	PX (KIPS)	-0.		-0.		-18.1		-18.1		-18.1	
ACTUAL	PY (KIPS)	-18.1		-18.1		-18.1		-18.1		-18.1	



TABLE 17A

SUMMARY OF REACTIONS (KIIPS OR FT-KIIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS

RESULTS FOR TRUCK LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.

NORMALIZED POINT LOADS AT

REACTION OR LOAD	4A		2A+4A		2A	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	-1.65	-1.60	-2.23	-1.82		-0.16
2E	-.06	-.24	-.29	-.76		-.62
3E	.38	.96	.26	.70		-.26
4E	1.40	1.06	1.32	1.16		.25
5E	3.29	3.25	3.45	3.50		0.
1F	4.47	2.04	5.21	5.76		1.73
2F	2.47	-.51	1.23	.59		-.49
3F	-1.23	1.12	1.28	.68		1.63
4F	.77	3.67	5.26	5.84		3.66
1W	-.58	-.55	-2.39	-2.01		-.99
2W	-.23	-.21	-.12	-.94		-1.09
3W	-.12	-.17	.39	.44		.31
4W	-.08	-.17	1.21	1.57		1.42
5W	.16	.23	3.41	3.62		3.90
RE	3.36	3.43	2.51	2.78		-.79
FF	6.49	6.32	12.99	12.87		6.53
PW	-.85	-.87	2.50	2.68		3.55
SUMR	9.00	8.88	18.00	18.33		9.29
PX	-0.	-0.	-9.00	-9.00		-9.00
PY	-9.00	-9.00	-9.00	-9.14		-0.
SUMP	-9.00	-9.00	-18.00	-18.14		-9.00
SUMF / SUMP	1.00	.99	1.00	1.01		1.03
TW	4.19	4.12	33.27	35.43		31.62
MF	-11.10	4.90	.16	.26		6.08
TF	6.01	7.65	11.94	15.49		6.36
TE	30.57	11.84	33.37	32.32		3.06
ACTUAL PX		-0.		-8.88		-8.99
ACTUAL PY		-8.98		-9.02		-0.

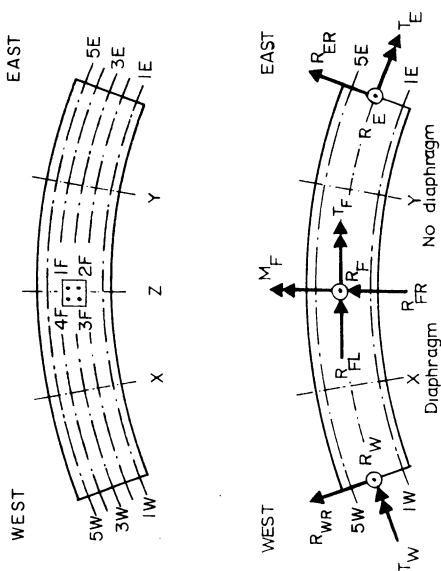
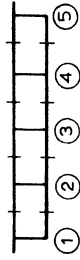
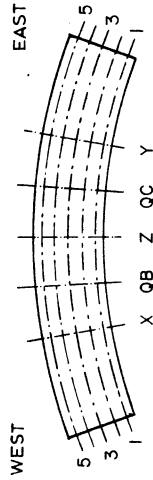


TABLE 17B

SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



DEFLECTION AT POINT	4A		2A+4A		2A		NVRMALIZED POINT LOADS AT	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X	-.027	-.027	.021	.027	1.31	.062		
2X	-.026	-.025	.032	.041	1.28	.079		
3X	-.024	-.024	.045	.060	1.32	.096		
4X	-.023	-.021	.060	.078	1.30	.111		
5X	-.022	-.017	.075	.096	1.28	.128		
1QB	-.026	-.027	-.001	-.004	2.42	.034		
2QB	-.023	-.023	.009	.014	1.48	.042		
3QB	-.020	-.021	.021	.028	1.33	.054		
4QB	-.018	-.019	.035	.048	1.37	.070		
5QB	-.016	-.012	.049	.061	1.26	.081		
1Z	-.009	-.010	-.018	-.022	1.27	-.008		
2Z	-.004	-.004	-.009	-.010	1.20	-.004		
4Z	.006	.007	.012	.014	1.25	.007		
5Z	.012	.015	.023	.030	1.28	.012		
1QC	.024	.019	-.003	-.004	1.37	-.033		
2QC	.031	.030	.007	.010	1.36	-.027		
3QC	.040	.043	.020	.025	1.29	-.023		
4QC	.054	.062	.035	.047	1.32	-.024		
5QC	.056	.072	.050	.064	1.28	-.020		
1Y	.045	.045	.017	.019	1.12	-.033		
2Y	.054	.054	.028	.033	1.18	-.034		
3Y	.067	.073	.042	.053	1.24	-.033		
4Y	.086	.102	.063	.082	1.31	-.029		
5Y	.102	.129	.080	.112	1.39	-.031		
LOAD								
PX	-.0	-.0	-.0	-.0		-.0		
PY	-.9.0	-.9.0	-.9.0	-.9.1		-.0		
ACTUAL								
PX	-.0	-.0	-.8.9	-.9.0		-.0		
PY	-.9.0	-.9.0	-.9.0	-.9.0		-.0		



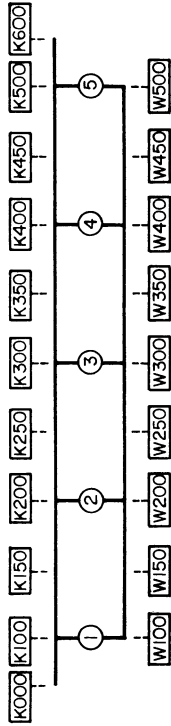
TABLE 17C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	4A		2A+4A		2A	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	7	3	-18	-18	-23	-23
K	K100	6	7	-15	-29	-42	-40
K	K150	4	4	-14	-17	-22	-21
K	K200	5	6	-14	-22	-31	-33
K	K250	3	3	-19	-19	-23	-25
K	K300	5	6	-16	-22	-31	-31
K	K350	4	4	-19	-20	-28	-29
K	K400	4	6	-19	-29	-39	-39
K	K450	4	4	-22	-21	-29	-33
K	K500	5	5	-22	-28	-37	-37
K	K600	6	3	-25	-17	-23	-23
W	W100	-22	-15	58	45	70	72
W	W150	-19	-9	54	45	62	51
W	W200	-21	-15	65	49	72	68
W	W250	-19	-13	72	34	55	57
W	W300	-21	-14	65	57	80	82
W	W350	-19	-12	91	52	70	78
W	W400	-20	-16	91	72	90	92
W	W450	-20	-13	103	51	71	77
W	W500	-20	-16	103	103	125	125

LOAD	PX (KIPS)	PY (KIPS)	ACTUAL PX (KIPS)	ACTUAL PY (KIPS)
	-0.	-9.0	-9.0	-9.0
	-9.0	-9.0	-9.0	-9.0
	-0.	-9.0	-9.0	-9.0
	-0.	-9.0	-9.0	-9.0



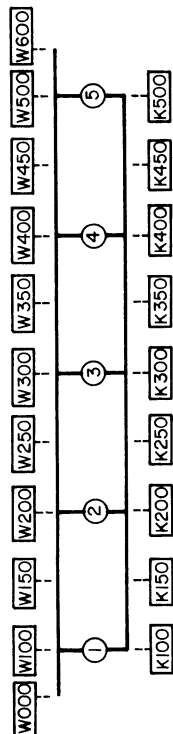
TABLE 17E

SUMMARY OF STRAINS (MICFC IN/IN)

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

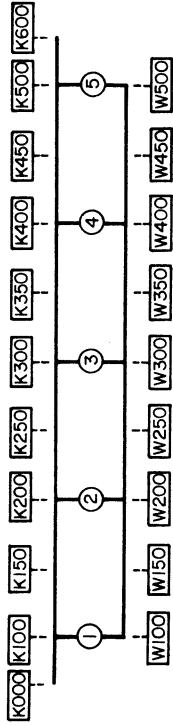
GAGE TYPE	GAGE LOC.	4A		2A+4A		2A	
		THEORY	MEASR. ADJUST	THEORY	MEASR. ADJUST	THEORY	MEASR. ADJUST
W	W000	16	9	58	37	24	24
W	W100	16	12	54	35	21	22
W	W150	18	13	46	36	20	22
W	W200	26	23	46	55	25	25
W	W250	30	22	50	44	20	20
W	W300	30	43	50	67	23	23
W	W350	25	31	58	55	19	21
W	W400	27	40	70	77	32	33
W	W450	27	32	73	61	27	29
W	W500	27	40	73	70	30	29
W	W600	27	43	73	73	29	29
K	K100	-7	-16	-24	-34	-18	-18
K	K150	-8	-13	-21	-29	-16	-17
K	K200	-12	-16	-20	-31	-17	-17
K	K250	-11	-19	-27	-32	-15	-16
K	K300	-12	-23	-20	-34	-14	-13
K	K350	-11	-32	-27	-44	-15	-14
K	K400	-13	-21	-32	-35	-16	-16
K	K450	-13	-14	-32	-38	-25	-23
K	K500	-13	-21	-32	-37	-17	-17
LOAD	PX (KIPS)	-0.	-0.	-9.0	-9.0	-9.0	-9.0
LOAD	PY (KIPS)	-9.0	-9.0	-9.0	-9.1	-0.	-0.
ACTUAL	PX (KIPS)	-0.	-0.	-8.9	-8.9	-9.0	-9.0
ACTUAL	PY (KIPS)	-9.0	-9.0	-9.0	-9.0	-0.	-0.

TABLE 17F

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR TRUCK LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.

SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

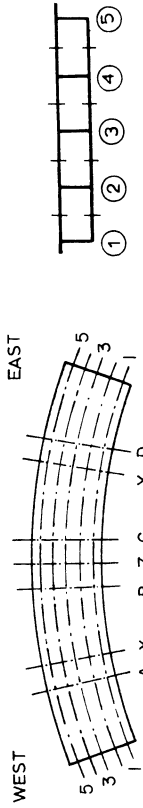
GAGE TYPE	GAGE LOC.	4A		2A+4A		2A		ADJUST
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	
K	K000	-21	-10	-14	-8	-13	2	2
K	K100	-17	-17	-12	-13	-14	5	5
K	K150	-34	-32	-28	-26	-26	9	8
K	K200	-16	-25	-12	-21	-20	7	7
K	K250	-25	-27	-20	-22	-22	6	7
K	K300	-19	-30	-15	-24	-25	7	7
K	K350	-22	-42	-18	-33	-35	10	10
K	K400	-48	-45	-43	-43	-40	8	8
K	K450	-63	-56	-56	-49	-49	14	14
K	K500	-28	-50	-23	-42	-43	10	10
K	K600	-30	-49	-25	-16	-42	3	10
W	W100	73	34	51	28	29	-13	-14
W	W150	48	43	39	39	34	-18	-18
W	W200	70	58	50	45	44	-19	-19
W	W250	56	53	43	43	41	-18	-17
W	W300	87	64	66	51	52	-18	-18
W	W350	84	78	81	75	68	-13	-14
W	W400	100	118	111	111	106	-19	-19
W	W450	96	96	84	84	85	-16	-16
W	W500	129	124	108	104	110	-20	-20
LOAD	PX (KIPS)	-0.	-0.	-9.0	-9.0	-9.0	-9.0	-9.0
LOAD	PY (KIPS)	-9.0	-9.0	-9.0	-9.1	-0.	-0.	-0.
ACTUAL	PX (KIPS)	-0.	-0.	-8.9	-8.9	-9.0	-9.0	-9.0
ACTUAL	PY (KIPS)	-9.0	-9.0	-9.0	-9.0	-0.	-0.	-0.

TABLE 17G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE)

MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



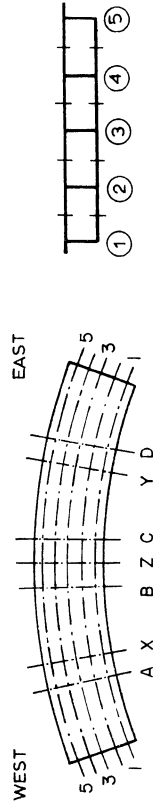
SECTION	GIRDER	4A		2A+4A		2A		2A+4A		2A	
		THEORY K-FT	PCT	THEORY K-FT	PCT	THEORY K-FT	PCT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
A	1	-2.0	17.1	-1.1	13.2	5.2	13.7	3.5	9.9	5.1	11.0
A	2	-2.6	22.8	-1.9	23.9	7.3	19.2	6.7	18.8	8.9	19.2
A	3	-2.6	22.1	-1.9	23.6	8.1	21.4	7.9	22.4	10.8	23.3
A	4	-2.5	22.0	-2.0	24.8	9.6	25.4	10.0	28.3	12.6	27.1
A	5	-1.9	16.0	-1.2	14.5	7.7	20.2	7.3	20.6	9.0	19.4
A	SUM	-11.6		-8.0		37.9		35.5		46.4	
B	1	-4.4	16.9	-2.3	14.5	-6.8	14.7	-5.1	11.9	-2.2	9.1
B	2	-5.4	20.9	-3.1	19.2	-9.4	20.5	-8.1	18.9	-4.5	18.8
B	3	-4.5	17.5	-3.1	19.2	-10.2	22.3	-10.2	23.9	-6.5	27.3
B	4	-6.4	24.7	-4.2	25.9	-11.2	24.4	-10.7	25.2	-5.9	25.0
B	5	-5.2	20.1	-3.4	21.2	-8.3	18.1	-8.6	20.2	-4.7	19.8
B	SUM	-25.8		-16.1		-45.8		-42.6		-23.8	
C	1	-2.1	10.6	-1.3	5.8	-6.6	14.4	-4.6	10.7	-3.0	15.3
C	2	-3.7	18.6	-3.5	16.1	-9.2	20.1	-7.9	18.3	-3.9	20.0
C	3	-5.6	28.2	-5.8	26.8	-10.1	22.2	-9.8	22.8	-3.7	18.8
C	4	-5.0	25.3	-6.0	27.7	-11.3	24.7	-11.5	26.9	-5.0	25.7
C	5	-3.4	17.3	-5.1	23.7	-8.5	18.6	-9.1	21.2	-4.0	20.2
C	SUM	-19.7		-21.7		-45.7		-42.8		-19.5	
D	1	6.7	13.1	3.0	7.1	4.7	11.8	2.4	6.8	-1.3	12.6
D	2	9.6	18.6	7.4	17.6	6.9	17.4	5.7	15.9	-2.6	25.8
D	3	10.9	21.2	8.5	20.2	8.3	20.9	7.0	19.6	-2.3	23.3
D	4	13.3	25.9	14.4	34.3	10.8	27.1	12.9	36.0	-2.4	24.1
D	5	10.9	21.2	8.8	20.9	9.0	22.8	7.8	21.8	-1.4	14.1
D	SUM	51.3		42.1		39.6		35.8		-10.0	
LOAD	PX (KIPS)	-0.		-0.		-9.0		-9.0		-9.0	
LJAD	PY (KIPS)	-9.0		-9.0		-9.0		-9.0		-0.	
ACTUAL	PX (KIPS)	-0.		-0.		-8.9		-8.9		-9.0	
ACTUAL	PY (KIPS)	-9.0		-9.0		-9.0		-9.0		-0.	

TABLE 17H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

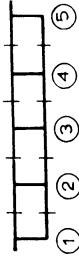
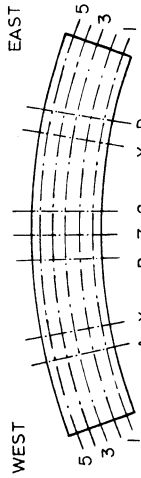
RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



SECTION	GIRDER	4A		2A+4A		2A		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	-2.0	17.1	-1.9	23.8	5.2	13.7	6.8	19.4	9.3	19.5
A	2	-2.6	22.8	-1.5	19.4	7.3	19.2	6.6	18.8	8.8	18.5
A	3	-2.6	22.1	-1.5	18.5	8.1	21.4	6.9	19.7	9.1	19.2
A	4	-2.5	22.0	-1.7	21.5	9.6	25.4	8.1	23.0	11.2	23.5
A	5	-1.9	16.0	-1.3	16.8	7.7	20.2	6.7	19.1	9.2	19.3
A	SUM	-11.6		-7.9		37.9		35.0		47.6	
B	1	-4.4	16.9	-3.3	18.3	-6.8	14.7	-6.4	15.1	-2.8	12.8
B	2	-5.4	20.9	-4.1	22.3	-9.4	20.5	-9.9	23.4	-5.3	23.6
B	3	-4.5	17.5	-3.6	20.0	-10.2	22.3	-10.4	24.7	-6.1	27.4
B	4	-6.4	24.7	-4.7	25.9	-11.2	24.4	-9.9	23.3	-4.8	21.6
B	5	-5.2	20.1	-2.5	13.6	-8.3	18.1	-5.7	13.5	-3.3	14.6
B	SUM	-25.8		-18.2		-45.8		-42.3		-22.3	
C	1	-2.1	10.6	-2.8	10.8	-6.6	14.4	-5.8	13.0	-3.3	15.1
C	2	-3.7	18.6	-5.0	19.7	-9.2	20.1	-9.6	21.7	-5.2	23.8
C	3	-5.6	28.2	-7.7	30.3	-10.1	22.2	-11.3	25.4	-4.5	20.7
C	4	-5.0	25.3	-6.9	27.0	-11.3	24.7	-11.3	25.4	-5.2	23.8
C	5	-3.4	17.3	-3.1	12.2	-8.5	18.6	-6.4	14.5	-3.6	16.6
C	SUM	-19.7		-25.5		-45.7		-44.5		-21.8	
D	1	6.7	13.1	5.5	11.0	4.7	11.8	4.4	10.5	-1.4	11.9
D	2	9.6	18.6	8.0	16.2	6.9	17.4	6.5	15.5	-2.3	18.5
D	3	10.9	21.2	9.3	18.8	8.3	20.9	7.8	18.6	-2.4	19.7
D	4	13.3	25.9	13.4	27.0	10.8	27.1	11.7	27.8	-3.0	24.8
D	5	10.9	21.2	13.3	26.9	9.0	22.8	11.6	27.6	-3.1	25.2
D	SUM	51.3		49.5		39.6		42.1		-12.1	
LOAD	PX (KIPS)	-0.		-0.		-9.0		-9.0		-9.0	
LOAD	PY (KIPS)	-9.0		-9.0		-9.0		-9.0		-9.0	
ACTUAL	PX (KIPS)	-0.		-0.		-8.9		-8.9		-9.0	
ACTUAL	PY (KIPS)	-9.0		-9.0		-9.0		-9.0		-0.	

TABLE 171

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.



RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.

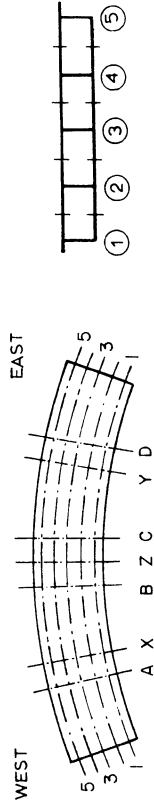
SECTION	GIRDER	4A				2A+4A				2A			
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
A	1	-2.0	17.1	-1.4	17.9	5.2	13.7	5.0	14.1	7.0	14.8	7.0	14.8
A	2	-2.6	22.8	-1.8	21.9	7.3	19.2	6.6	18.8	8.9	18.9	8.9	18.9
A	3	-2.6	22.1	-1.7	21.3	8.1	21.4	7.5	21.2	10.1	21.4	10.1	21.4
A	4	-2.5	22.0	-1.9	23.3	9.6	25.4	9.2	26.0	12.0	25.5	12.0	25.5
A	5	-1.9	16.0	-1.2	15.5	7.7	20.2	7.0	19.9	9.1	19.3	9.1	19.3
A	SUM	-11.6		-8.0		37.9		35.3		46.9		46.9	
B	1	-4.4	16.9	-2.9	16.7	-6.8	14.7	-5.8	13.6	-2.5	11.0	-2.5	11.0
B	2	-5.4	20.9	-3.6	21.0	-9.4	20.5	-9.1	21.4	-4.9	21.4	-4.9	21.4
B	3	-4.5	17.5	-3.4	19.7	-10.2	22.3	-10.3	24.4	-6.3	27.4	-6.3	27.4
B	4	-6.4	24.7	-4.5	25.9	-11.2	24.4	-10.2	24.1	-5.3	23.1	-5.3	23.1
B	5	-5.2	20.1	-2.9	16.7	-8.3	18.1	-7.0	16.5	-3.9	17.0	-3.9	17.0
B	SUM	-25.8		-17.3		-45.8		-42.5		-23.0		-23.0	
C	1	-2.1	10.6	-2.1	8.8	-6.6	14.4	-5.3	12.0	-3.2	15.2	-3.2	15.2
C	2	-3.7	18.6	-4.3	18.3	-9.2	20.1	-8.9	20.2	-4.6	22.2	-4.6	22.2
C	3	-5.6	28.2	-6.9	28.8	-10.1	22.2	-10.6	24.3	-4.1	19.9	-4.1	19.9
C	4	-5.0	25.3	-6.5	27.2	-11.3	24.7	-11.4	26.1	-5.1	24.6	-5.1	24.6
C	5	-3.4	17.3	-4.0	16.9	-8.5	18.6	-7.6	17.4	-3.8	18.1	-3.8	18.1
C	SUM	-19.7		-23.8		-45.7		-43.8		-20.8		-20.8	
D	1	6.7	13.1	4.1	9.0	4.7	11.8	3.3	8.6	-1.4	12.3	-1.4	12.3
D	2	9.6	18.6	7.7	16.9	6.9	17.4	6.1	15.7	-2.4	22.2	-2.4	22.2
D	3	10.9	21.2	8.9	19.5	8.3	20.9	7.4	19.1	-2.4	21.5	-2.4	21.5
D	4	13.3	25.9	14.0	30.8	10.8	27.1	12.4	32.0	-2.7	24.5	-2.7	24.5
D	5	10.9	21.2	10.8	23.8	9.0	22.8	9.5	24.6	-2.2	19.6	-2.2	19.6
D	SUM	51.3		45.5		39.6		38.6		-11.0		-11.0	
LOAD	PX (KIPS)	-0.		-0.		-9.0		-9.0		-9.0		-9.0	
LOAD	PY (KIPS)	-9.0		-9.0		-9.0		-9.1		-0.		-0.	
ACTUAL	PX (KIPS)	-0.		-0.		-8.9		-8.9		-9.0		-9.0	
ACTUAL	PY (KIPS)	-9.0		-9.0		-9.0		-9.0		-0.		-0.	

TABLE 17J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



SECTION	GIRDER	4A		2A+4A		2A	
		THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT
A	1	-2.0	17.1	5.2	13.7	4.8	13.4
A	2	-2.6	22.8	7.3	19.2	6.7	18.6
A	3	-2.6	22.1	8.1	21.4	7.7	21.4
A	4	-2.5	22.0	9.6	25.4	9.5	26.5
A	5	-1.9	16.0	7.7	20.2	7.2	20.0
A	SUM	-11.6		37.9		35.7	
B	1	-4.4	16.9	-6.8	14.7	-5.7	13.2
B	2	-5.4	20.9	-9.4	20.5	-8.7	20.4
B	3	-4.5	17.5	-10.3	22.3	-10.3	24.0
B	4	-6.4	24.7	-11.2	24.4	-10.4	24.4
B	5	-5.2	20.1	-8.3	18.1	-7.6	17.9
B	SUM	-25.8		-45.8		-42.8	
C	1	-2.1	10.6	-6.6	14.4	-5.2	11.8
C	2	-3.7	18.6	-9.2	20.1	-8.5	19.6
C	3	-5.6	28.2	-10.1	22.2	-10.3	23.5
C	4	-5.0	25.3	-11.3	24.7	-11.5	26.3
C	5	-3.4	17.3	-8.5	18.6	-8.2	18.7
C	SUM	-19.7		-45.7		-43.6	
D	1	6.7	13.1	4.7	11.8	3.1	8.2
D	2	9.6	18.6	6.9	17.4	5.9	15.8
D	3	10.9	21.2	8.3	20.9	7.3	19.3
D	4	13.3	25.9	10.8	27.1	12.6	33.3
D	5	10.9	21.2	9.0	22.8	8.9	23.6
D	SUM	51.3		39.6		37.7	
LOAD	PX (KIPS)	-0.		-9.0		-9.0	
LOAD	PY (KIPS)	-9.0		-9.0		-9.1	
ACTUAL	PX (KIPS)	-0.		-8.9		-9.0	
ACTUAL	PY (KIPS)	-9.0		-9.0		-9.0	



TABLE 18A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR TRUCK LOADS APPLIED  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS AFTER 30 KSI COND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED NO RESTRAINT.

REACTION OR LOAD	1A		3A		1A+3A	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	.50			1.65		2.21
2E	.03			2.11		2.06
3E	-.23			.78		.72
4E	-.08			-.41		-.46
5E	-.80			-.55		-1.29
1F	.28			1.14		1.50
2F	1.91			3.05		3.94
3F	2.67			1.73		4.21
4F	.98			.01		1.87
1W	2.57			.35		3.05
2W	1.17			.40		1.40
3W	.81			-.04		.74
4W	.16			-.36		.07
5W	-.84			-1.00		-1.75
RE	-.58			3.58		3.24
RF	5.84			5.93		11.52
PW	3.87			-.65		3.51
SUMR	9.13			8.86		18.27
PX	-9.00			-0.		-9.00
PY	-0.			-9.00		-8.99
SUMP	-9.00			-9.00		-17.99
SUMR/SUMP	1.01			.98		1.02
TW	-20.15			-8.90		-28.12
MF	2.20			-3.66		-.94
TF	-4.96			-5.45		-7.17
TE	-6.97			-17.80		-24.49
ACTUAL PX	-9.06			-0.		-8.93
ACTUAL PY	-0.			-9.04		-8.92

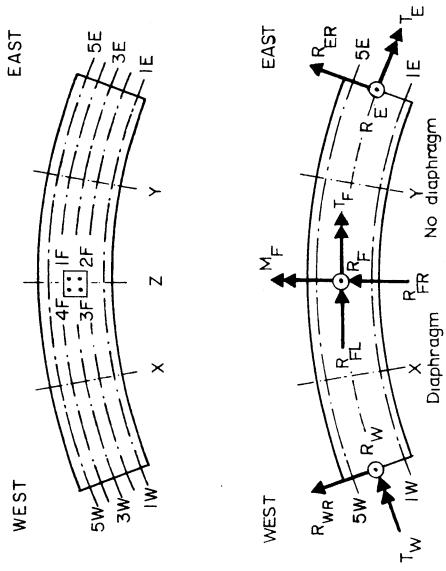
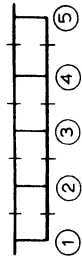
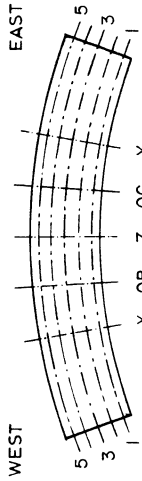


TABLE 18B

SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.



DEFLECTION AT POINT	1A		3A		1A+3A	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X	.098		-.018			.075
2X	.089		-.022			.062
3X	.080		-.027			.050
4X	.071		-.032			.037
5X	.064		-.034			.026
1QB	.067		-.012			.052
2QB	.055		-.017			.037
3QB	.046		-.022			.023
4QB	.039		-.028			.010
5QB	.031		-.032			-.001
1Z	.015		.016			.030
2Z	.008		.010			.015
4Z	-.005		-.005			-.009
5Z	-.011		-.010			-.018
1QC	-.009		.072			.057
2QC	-.015		.060			.040
3QC	-.019		.043			.020
4QC	-.027		.031			.007
5QC	-.028		.024			-.004
1Y	-.016		.123			.099
2Y	-.018		.100			.072
3Y	-.022		.071			.042
4Y	-.027		.059			.028
5Y	-.033		.057			.017
LOAD PX		-9.0		-0.		-9.0
LOAD PY		-0.		-9.0		-9.0
ACTUAL PX		-9.1		-0.		-8.9
ACTUAL PY		-0.		-9.0		-8.9

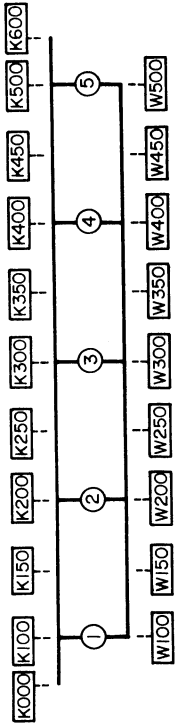
TABLE 18C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	1A		3A		1A+3A	
		THEORY	MEASR ADJUST	THEORY	MEASR ADJUST	THEORY	MEASR ADJUST
K	K000						
K	K100	-40	-81	5	5	-32	-69
K	K150	-81	-78	11	10	-69	-67
K	K200	-27	-27	4	4	-22	-18
K	K250	-47	-51	6	7	-39	-41
K	K300	-23	-23	4	5	-18	-17
K	K350	-33	-33	5	5	-26	-26
K	K400	-27	-26	4	4	-20	-19
K	K450	-31	-32	5	5	-24	-25
K	K500	-24	-28	3	3	-17	-22
K	K600	-24	-23	4	4	-18	-17
K		-17	-17	2	2	-12	-12
W	W100	143	143	-10	-10	129	129
W	W150	76	69	-10	-10	63	58
W	W200	104	101	-12	-12	90	87
W	W250	78	63	-8	-9	66	53
W	W300	73	73	-14	-14	58	58
W	W350	60	57	-12	-13	46	42
W	W400	62	60	-16	-17	47	46
W	W450	65	56	-10	-12	51	31
W	W500	61	60	-22	-23	45	45
LOAD	PX (KIPS)	-9.0		-0.		-9.0	
LOAD	PY (KIPS)	-0.		-9.0		-9.0	
ACTUAL	PX (KIPS)	-9.1		-0.		-8.9	
ACTUAL	PY (KIPS)	-0.		-9.0		-8.9	

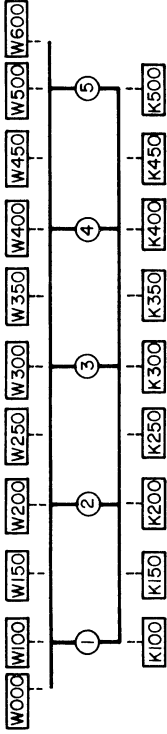
TABLE 18D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	1A		3A		1A+3A	
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
W	W000	32	32	27	27	58	58
W	W100	29	30	30	30	58	59
W	W150	25	28	23	26	46	53
W	W200	29	30	31	31	58	57
W	W250	26	29	17	19	43	47
W	W300	31	32	15	16	44	46
W	W350	20	23	12	14	30	36
W	W400	16	16	15	15	28	28
W	W450	10	14	13	15	27	30
W	W500	11	11	14	14	22	22
W	W600	9	9	13	13	21	21
K	K100	-16	-16	-16	-16	-28	-29
K	K150	-19	-17	-14	-14	-30	-28
K	K200	-14	-14	-15	-14	-26	-26
K	K250	-15	-18	-13	-10	-25	-25
K	K300	-18	-18	-8	-8	-24	-24
K	K350	-16	-16	-9	-9	-24	-24
K	K400	-13	-13	-11	-11	-22	-22
K	K450	-11	-11	-11	-12	-20	-22
K	K500	-11	-11	-12	-12	-22	-21
LOAD	PX (KIPS)	-9.0	-9.0	-0.	-0.	-9.0	-9.0
LOAD	PY (KIPS)	-0.	-0.	-9.0	-9.0	-9.0	-9.0
ACTUAL	PX (KIPS)	-9.1	-9.1	-0.	-0.	-8.9	-8.9
ACTUAL	PY (KIPS)	-0.	-0.	-9.0	-9.0	-8.9	-8.9

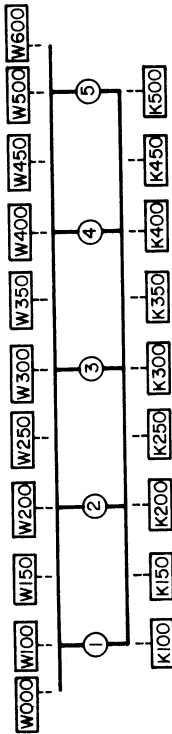
TABLE 18E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	1A		3A		1A+3A	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000		24		44		67
W	W100		22		37		59
W	W150		19		30		48
W	W200		28		36		62
W	W250		14		30		44
W	W300		18		28		44
W	W350		11		16		26
W	W400		18		13		29
W	W450		14		8		21
W	W500		15		5		17
W	W600		15		2		15
K	K100	-15	-15	-22	-22	-33	-33
K	K150	-13	-12	-18	-20	-28	-30
K	K200	-13	-14	-17	-18	-29	-30
K	K250	-10	-12	-17	-16	-27	-28
K	K300	-9	-8	-16	-15	-24	-23
K	K350	-12	-12	-11	-11	-21	-21
K	K400	-13	-13	-8	-8	-20	-20
K	K450	-16	-16	-10	-10	-25	-25
K	K500	-15	-15	-9	-9	-23	-23
LOAD	PX (KIPS)	-9.0	-9.0	-0.	-0.	-9.0	-9.0
LOAD	PY (KIPS)	-0.	-0.	-9.0	-9.0	-0.	-0.
ACTUAL	PX (KIPS)	-9.1	-9.1	-0.	-0.	-8.9	-8.9
ACTUAL	PY (KIPS)	-0.	-0.	-9.0	-9.0	-0.	-0.

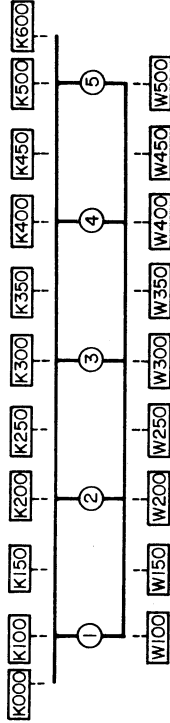
TABLE 18F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.

SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

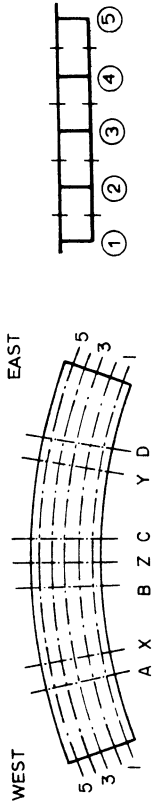


NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	IA		3A		IA+3A	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000						
K	K100	2	2	-20	-20	-17	-17
K	K150	4	4	-33	-33	-28	-28
K	K200	9	9	-49	-49	-38	-38
K	K250	6	5	-39	-39	-32	-32
K	K300	5	5	-27	-33	-21	-26
K	K350	5	5	-29	-29	-22	-23
K	K400	5	6	-33	-33	-24	-24
K	K450	4	4	-24	-22	-16	-16
K	K500	5	5	-35	-31	-22	-21
K	K600	3	3	-23	-23	-16	-16
K	K600	1	3	-8	-23	-5	-16
W	W100						
W	W150	-8	-8	78	81	63	67
W	W200	-13	-13	105	101	87	87
W	W250	-10	-11	96	93	76	74
W	W300	-11	-9	74	71	56	54
W	W350	-15	-15	63	63	43	43
W	W400	-16	-13	48	50	28	32
W	W450	-19	-19	60	59	36	36
W	W500	-13	-13	47	46	30	28
W	W500	-18	-18	59	60	40	40
LOAD	PX (KIPS)						
LOAD	PY (KIPS)	-9.0	-9.0	-0.	-0.	-9.0	-9.0
ACTUAL	PX (KIPS)						
ACTUAL	PY (KIPS)	-9.1	-9.1	-0.	-0.	-8.9	-8.9

TABLE 18G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



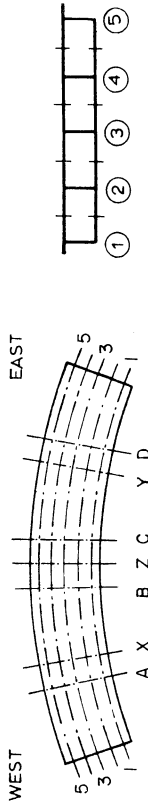
SECTION	GIRDER	1A			3A			1A+3A		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1	8.8	20.0		-7	9.0		7.8	22.4	
A	2	12.1	27.5		-1.6	19.9		10.4	29.7	
A	3	9.6	21.7		-1.9	23.9		7.5	21.5	
A	4	8.6	19.5		-2.2	27.6		5.9	17.0	
A	5	5.0	11.4		-1.6	19.7		3.3	9.3	
A	SUM	44.0			-8.0			34.9		
B	1	-3.7	21.7		-3.5	24.6		-7.0	23.4	
B	2	-4.5	26.6		-4.1	28.6		-8.2	27.5	
B	3	-4.7	27.7		-2.7	18.8		-7.1	23.6	
B	4	-2.7	15.9		-2.3	15.9		-4.7	15.6	
B	5	-1.4	8.1		-1.7	12.2		-3.0	9.9	
B	SUM	-17.0			-14.2			-29.9		
C	1	-2.8	21.1		-5.3	28.2		-8.0	25.6	
C	2	-3.7	27.5		-6.0	31.8		-9.3	29.9	
C	3	-2.5	18.5		-4.5	24.1		-6.8	21.7	
C	4	-2.5	18.8		-2.3	12.0		-4.8	15.3	
C	5	-1.9	14.1		-7	3.9		-2.3	7.4	
C	SUM	-13.3			-18.9			-31.2		
D	1	-8	10.5		7.3	18.2		6.1	20.8	
D	2	-1.6	19.9		12.8	32.1		10.3	35.0	
D	3	-1.8	23.0		8.2	20.5		5.7	19.3	
D	4	-2.3	29.6		7.4	18.6		4.6	15.4	
D	5	-1.3	17.0		4.3	10.6		2.8	9.5	
D	SUM	-7.9			39.9			29.5		
LOAD	PX (KIPS)	-9.0			-0.			-9.0		
LOAD	PY (KIPS)	-0.			-9.0			-9.0		
ACTUAL	PX (KIPS)	-9.1			-0.			-8.9		
ACTUAL	PY (KIPS)	-0.			-9.0			-8.9		

TABLE 18H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



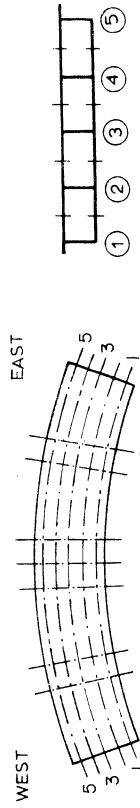
SECTION	GIRDER	1A		3A		1A+3A	
		THEORY K-FT	PCT	THEORY K-FT	PCT	THEORY K-FT	PCT
A	1	18.6	33.5	-2.5	29.1	15.5	35.7
A	2	11.4	20.6	-1.9	22.5	8.6	19.7
A	3	8.8	15.9	-1.6	18.5	6.7	15.4
A	4	9.8	17.6	-1.5	17.6	7.5	17.3
A	5	6.9	12.4	-1.1	12.3	5.2	11.9
A	SUM	55.5		-8.6		43.5	
B	1	-3.0	15.1	-2.6	17.5	-4.8	15.6
B	2	-4.7	24.0	-3.8	25.7	-7.6	24.7
B	3	-5.5	28.3	-2.8	19.0	-7.6	24.6
B	4	-4.2	21.5	-3.4	22.8	-6.8	22.1
B	5	-2.2	11.1	-2.2	15.1	-4.0	13.0
B	SUM	-19.5		-14.8		-30.7	
C	1	-2.4	14.5	-3.7	19.9	-5.5	16.8
C	2	-3.8	23.1	-5.3	28.6	-8.6	26.2
C	3	-3.2	19.6	-4.7	25.0	-7.5	22.9
C	4	-4.1	24.9	-2.9	15.7	-6.5	19.8
C	5	-3.0	17.9	-2.0	10.8	-4.7	14.3
C	SUM	-16.5		-18.6		-32.7	
D	1	-1.6	20.9	9.1	20.7	7.5	22.2
D	2	-2.0	25.8	11.3	25.6	9.1	26.9
D	3	-1.6	20.8	9.0	20.5	7.0	20.7
D	4	-1.5	19.5	7.9	17.9	5.6	16.7
D	5	-1.0	13.0	6.7	15.2	4.6	13.5
D	SUM	-7.5		44.1		33.7	
LOAD	PX (KIPS)	-9.0		-0.		-9.0	
LOAD	PY (KIPS)	-0.		-9.0		-9.0	
ACTUAL	PX (KIPS)	-9.1		-0.		-8.9	
ACTUAL	PY (KIPS)	-0.		-9.0		-8.9	



TABLE 181

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



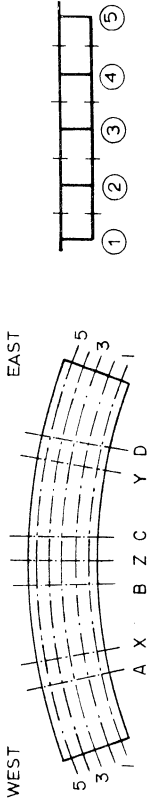
SECTION	GIRDER	1A		3A		1A+3A	
		THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT
A	1	13.2	26.8	-1.5	18.3	11.3	29.0
A	2	11.8	24.0	-1.8	21.1	9.6	24.7
A	3	9.2	18.8	-1.8	21.4	7.2	18.5
A	4	9.1	18.5	-1.9	23.0	6.7	17.2
A	5	5.8	11.9	-1.4	16.2	4.1	10.6
A	SUM	49.1		-8.3		38.8	
B	1	-3.3	17.8	-3.0	20.6	-5.8	19.0
B	2	-4.6	25.1	-3.9	27.0	-7.9	25.9
B	3	-5.2	28.1	-2.7	18.8	-7.3	24.1
B	4	-3.5	19.2	-2.9	19.8	-5.9	19.3
B	5	-1.8	9.9	-2.0	13.8	-3.5	11.7
B	SUM	-18.4		-14.5		-30.4	
C	1	-2.6	17.1	-4.4	23.7	-6.6	20.6
C	2	-3.7	24.8	-5.6	30.0	-8.9	27.8
C	3	-2.9	19.2	-4.6	24.6	-7.2	22.4
C	4	-3.4	22.5	-2.6	14.0	-5.7	17.9
C	5	-2.5	16.4	-1.4	7.7	-3.6	11.3
C	SUM	-15.1		-18.7		-32.0	
D	1	-1.2	15.0	8.1	19.4	6.7	21.4
D	2	-1.7	22.5	12.1	29.0	9.8	31.1
D	3	-1.7	22.1	8.6	20.5	6.3	20.0
D	4	-2.0	25.2	7.7	18.3	5.0	16.0
D	5	-1.2	15.2	5.3	12.8	3.6	11.4
D	SUM	-7.7		41.8		31.4	
LOAD	PX (KIPS)	-9.0		-0.		-9.0	
LOAD	PY (KIPS)	-0.		-9.0		-9.0	
ACTUAL	PX (KIPS)	-9.1		-0.		-8.9	
ACTUAL	PY (KIPS)	-0.		-9.0		-8.9	

TABLE 18J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE)

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



SECTION	GIRDER	1A		3A		1A+3A	
		THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT
A	1	12.2	25.5	-1.6	18.8	10.5	27.7
A	2	11.9	24.7	-1.7	19.8	9.8	25.9
A	3	9.3	19.4	-1.8	20.9	7.3	19.2
A	4	9.0	18.8	-2.0	23.5	6.5	17.2
A	5	5.5	11.5	-1.5	17.0	3.8	10.0
A	SUM	48.0		-8.7		37.9	
B	1	-3.4	18.9	-3.2	21.8	-6.3	20.5
B	2	-4.6	25.2	-4.0	27.3	-8.0	26.2
B	3	-5.0	27.6	-2.7	18.6	-7.2	23.6
B	4	-3.4	18.5	-2.7	18.8	-5.6	18.4
B	5	-1.8	9.8	-2.0	13.5	-3.5	11.3
B	SUM	-18.1		-14.6		-30.6	
C	1	-2.6	18.0	-4.7	24.7	-7.1	22.0
C	2	-3.7	25.4	-5.8	30.1	-9.1	28.1
C	3	-2.7	18.5	-4.6	23.9	-7.0	21.7
C	4	-3.2	21.6	-2.5	13.2	-5.4	16.9
C	5	-2.4	16.5	-1.5	8.0	-3.7	11.3
C	SUM	-14.6		-19.1		-32.3	
D	1	-1.1	13.9	7.8	19.0	6.5	21.2
D	2	-1.7	21.2	12.4	30.0	9.9	32.3
D	3	-1.8	21.8	8.4	20.5	6.1	19.9
D	4	-2.2	27.1	7.6	18.4	4.9	15.9
D	5	-1.3	16.0	4.9	12.0	3.3	10.7
D	SUM	-8.0		41.1		30.8	
LOAD	PX (KIPS)	-9.0		-0.		-9.0	
LJAD	PY (KIPS)	-0.		-9.0		-9.0	
ACTUAL	PX (KIPS)	-9.1		-0.		-8.9	
ACTUAL	PY (KIPS)	-0.		-9.0		-8.9	

TABLE 19A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR TRUCK LOADS APPLIED  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS AFTER 30 KSI COND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED NO RESTRAINT.

REACTION OR LOAD	1A+4A		2A+3A		THEORY EXPERM	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	-1.25			1.68		
2E	.08			1.49		
3E	.64			.48		
4E	.60			-.39		
5E	2.76			-.29		
1F	4.84			3.70		
2F	4.05			2.28		
3F	1.39			2.24		
4F	2.32			3.87		
1W	2.02			-.90		
2W	1.02			-.50		
3W	.65			.45		
4W	.22			1.24		
5W	-.89			2.70		
RE	2.83			2.97		
RF	12.60			12.09		
RW	3.02			2.99		
SUMR	18.45			18.05		
PX	-9.00			-9.00		
PY	-9.15			-8.96		
SUMP	-18.15			-17.96		
SUMR/SUMP	1.02			1.01		
TW	-17.03			23.00		
MF	-7.77			.20		
TF	2.57			4.56		
TE	21.97			-14.97		
ACTUAL PX	-8.94			-9.00		
ACTUAL PY	-9.09			-8.96		

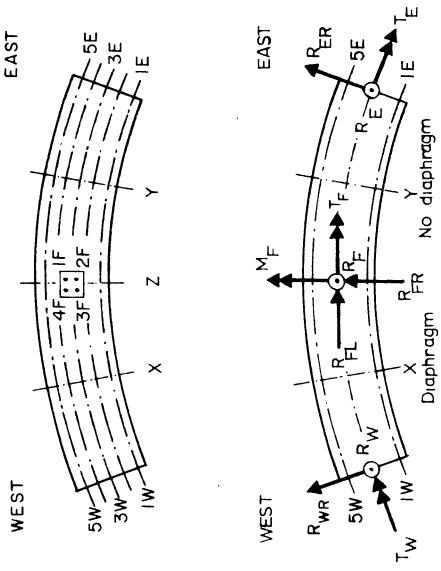
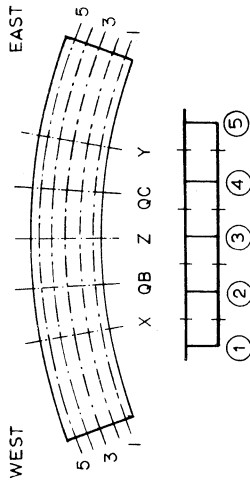


TABLE 19B

SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



NORMALIZED POINT LOADS AT  
2A+3A  
\*\*\*\*\*  
THEORY EXPERM E/T \*\*\*\*\*  
THEORY EXPERM E/T \*\*\*\*\*

1A+4A  
\*\*\*\*\*  
THEORY EXPERM E/T \*\*\*\*\*  
THEORY EXPERM E/T \*\*\*\*\*

DEFLECTION AT POINT	1A+4A THEORY	1A+4A EXPERM	1A+4A E/T	2A+3A THEORY	2A+3A EXPERM	2A+3A E/T
1X		.058			.036	
2X		.048			.045	
3X		.041			.056	
4X		.036			.071	
5X		.029			.080	
1QB		.030			.014	
2QB		.024			.022	
3QB		.017			.028	
4QB		.013			.039	
5QB		.009			.043	
1Z		.005			.004	
2Z		.004			.003	
4Z		.004			.001	
5Z		.004			.004	
1QC		.021			.036	
2QC		.025			.028	
3QC		.033			.015	
4QC		.047			.009	
5QC		.055			.005	
1Y		.046			.076	
2Y		.052			.057	
3Y		.067			.034	
4Y		.089			.023	
5Y		.115			.020	
LOAD PX		-9.0			-9.0	
LOAD PY		-9.1			-9.0	
ACTUAL PX		-8.9			-9.0	
ACTUAL PY		-9.1			-9.0	

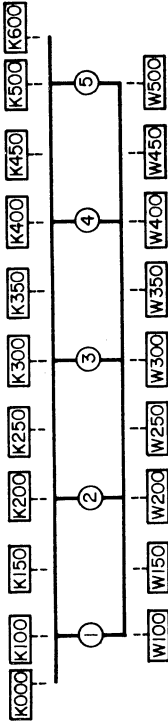
TABLE 19C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

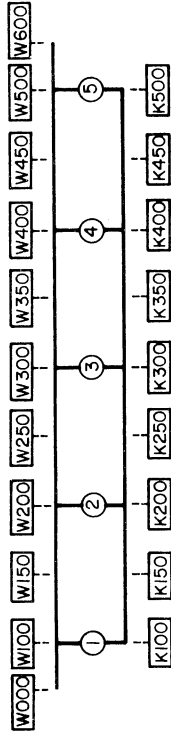
GAGE TYPE	GAGE LOC.	1A+4A		2A+3A		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	-32	-68	-11	-26	-11	-26		
K	K100	-68	-66	-26	-26	-26	-26		
K	K150	-21	-17	-9	-11	-9	-11		
K	K200	-37	-39	-16	-17	-16	-17		
K	K250	-17	-17	-9	-11	-9	-11		
K	K300	-23	-23	-17	-17	-17	-17		
K	K350	-17	-17	-15	-15	-15	-15		
K	K400	-20	-21	-25	-25	-25	-25		
K	K450	-14	-17	-17	-20	-17	-20		
K	K500	-14	-14	-23	-24	-23	-24		
K	K600	-10	-10	-14	-14	-14	-14		
W	W100	120	119	56	56	56	56		
W	W150	58	52	50	44	50	44		
W	W200	83	81	57	55	57	55		
W	W250	58	48	45	48	45	48		
W	W300	53	53	63	64	63	64		
W	W350	42	40	57	64	57	64		
W	W400	44	43	75	78	75	78		
W	W450	45	38	60	64	60	64		
W	W500	45	44	100	100	100	100		
LOAD	PX (KIPS)	-9.0		-9.0		-9.0			
LOAD	PY (KIPS)	-9.1		-9.0		-9.0			
ACTUAL	PX (KIPS)	-8.9		-9.0		-9.0			
ACTUAL	PY (KIPS)	-9.1		-9.0		-9.0			

TABLE 19D

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR TRUCK LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT  
 2A+3A

GAGE TYPE	GAGE LOC.	1A+4A		2A+3A		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000		57		50				
W	W100		54		54				
W	W150		48		43				
W	W200		58		63				
W	W250		48		51				
W	W300		58		55				
W	W350		44		49				
W	W400		50		52				
W	W450		46		53				
W	W500		42		51				
W	W600		41		56				
K	K100	-33	-34	-19	-19				
K	K150	-39	-36	-13	-14				
K	K200	-29	-28	-19	-19				
K	K250	-28	-31	-22	-21				
K	K300	-33	-33	-15	-15				
K	K350	-33	-33	-13	-13				
K	K400	-30	-31	-14	-14				
K	K450	-25	-27	-19	-17				
K	K500	-26	-25	-17	-17				
LOAD	PX (KIPS)								
LCAD	PY (KIPS)	-9.0	-9.0	-9.0	-9.0				
ACTUAL	PX (KIPS)	-8.9	-8.9	-9.0	-9.0				
ACTUAL	PY (KIPS)	-9.1	-9.1	-9.0	-9.0				

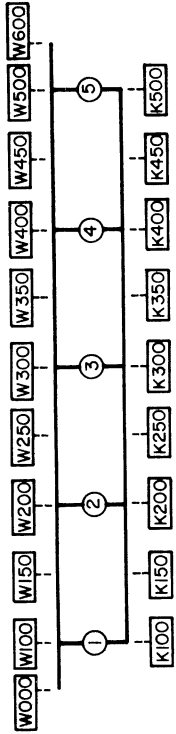
TABLE 19E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	1A+4A		2A+3A		THEORY		MEASR		ADJUST	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	ADJUST	
W	W000		38		73						
W	W100		37		62						
W	W150		36		53						
W	W200		58		62						
W	W250		41		51						
W	W300		63		53						
W	W350		44		39						
W	W400		63		48						
W	W450		47		39						
W	W500		55		37						
W	W600		60		35						
K	K100		-29		-28						
K	K150		-25		-22						
K	K200		-26		-26						
K	K250		-26		-32						
K	K300		-28		-26						
K	K350		-41		-39						
K	K400		-31		-32						
K	K450		-28		-30						
K	K500		-34		-33						

LOAD	PX (KIPS)	-9.0
LOAD	PY (KIPS)	-9.1
ACTUAL	PX (KIPS)	-8.9
ACTUAL	PY (KIPS)	-9.1

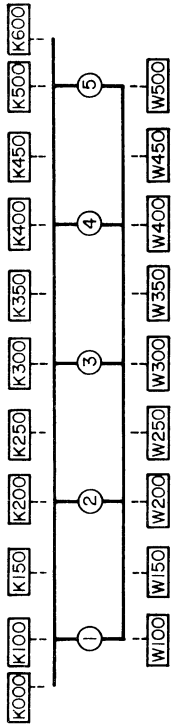
TABLE 19F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO PEDESTAL.

SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT  
 2A+3A

1A+4A  
 \*\*\*\*\*  
 THEORY MEASR ADJUST \*\*\*\*\*  
 \*\*\*\*\*  
 THEORY MEASR ADJUST \*\*\*\*\*  
 \*\*\*\*\*  
 THEORY MEASR ADJUST \*\*\*\*\*

GAGE TYPE	GAGE LOC.	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
K	K000		-7	-7		-11	-11
K	K100		-14	-15		-21	-22
K	K150		-30	-28		-30	-30
K	K200		-24	-23		-26	-26
K	K250		-22	-25		-16	-20
K	K300		-28	-29		-16	-16
K	K350		-39	-41		-18	-18
K	K400		-48	-45		-11	-10
K	K450		-67	-61		-16	-13
K	K500		-51	-52		-6	-6
K	K600		-18	-51		1	-6

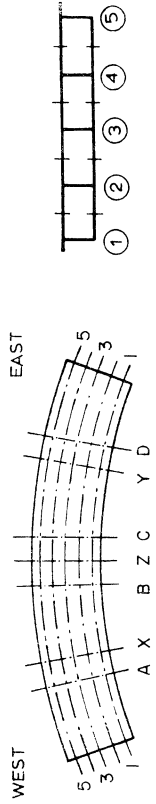
GAGE TYPE	GAGE LOC.	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
W	W100	39	40	40	63	66	66
W	W150	52	48	48	89	85	85
W	W200	60	58	58	73	71	71
W	W250	58	54	54	53	51	51
W	W300	64	64	64	43	43	43
W	W350	79	75	75	35	35	35
W	W400	121	117	117	39	38	38
W	W450	93	92	92	32	32	32
W	W500	126	130	130	35	36	36

LOAD	PX (KIPS)	PY (KIPS)
LOAD	-9.0	-9.0
ACTUAL PX (KIPS)	-9.1	-9.0
ACTUAL PY (KIPS)	-8.9	-9.0
ACTUAL PY (KIPS)	-9.1	-9.0



TABLE 19G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )  
 MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
 RESULTS FOR TRUCK LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.



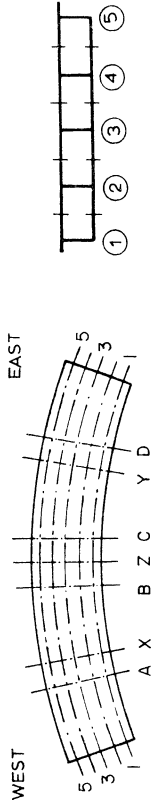
SECTION	GIRDER	1A+4A		2A+3A		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	7.1	21.4	4.3	11.1	4.3	11.1	4.3	11.1
A	2	9.5	28.7	7.6	19.6	7.6	19.6	7.6	19.6
A	3	6.9	20.9	8.8	22.9	8.8	22.9	8.8	22.9
A	4	6.0	18.1	10.6	27.5	10.6	27.5	10.6	27.5
A	5	3.6	10.8	7.3	19.0	7.3	19.0	7.3	19.0
A	SUM	33.1		38.6		38.6		38.6	
B	1	-6.8	17.9	-6.5	16.0	-6.5	16.0	-6.5	16.0
B	2	-8.5	22.6	-9.0	21.9	-9.0	21.9	-9.0	21.9
B	3	-8.9	23.5	-9.6	23.5	-9.6	23.5	-9.6	23.5
B	4	-7.9	20.9	-8.7	21.3	-8.7	21.3	-8.7	21.3
B	5	-5.7	15.2	-7.0	17.2	-7.0	17.2	-7.0	17.2
B	SUM	-37.8		-40.8		-40.8		-40.8	
C	1	-4.7	12.4	-9.1	21.7	-9.1	21.7	-9.1	21.7
C	2	-7.9	20.9	-10.4	24.9	-10.4	24.9	-10.4	24.9
C	3	-8.8	23.4	-8.7	20.9	-8.7	20.9	-8.7	20.9
C	4	-9.2	24.4	-8.2	19.7	-8.2	19.7	-8.2	19.7
C	5	-7.2	18.9	-5.3	12.8	-5.3	12.8	-5.3	12.8
C	SUM	-37.8		-41.7		-41.7		-41.7	
D	1	3.5	8.3	6.1	20.5	6.1	20.5	6.1	20.5
D	2	7.7	18.1	10.1	33.6	10.1	33.6	10.1	33.6
D	3	8.5	19.9	5.8	19.4	5.8	19.4	5.8	19.4
D	4	14.1	33.0	5.1	17.1	5.1	17.1	5.1	17.1
D	5	8.9	20.8	2.8	9.4	2.8	9.4	2.8	9.4
D	SUM	42.8		29.9		29.9		29.9	
LOAD	PX (KIPS)	-9.0		-9.0		-9.0		-9.0	
LOAD	PY (KIPS)	-9.1		-9.0		-9.0		-9.0	
ACTUAL	PX (KIPS)	-8.9		-9.0		-9.0		-9.0	
ACTUAL	PY (KIPS)	-9.1		-9.0		-9.0		-9.0	

TABLE 19H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

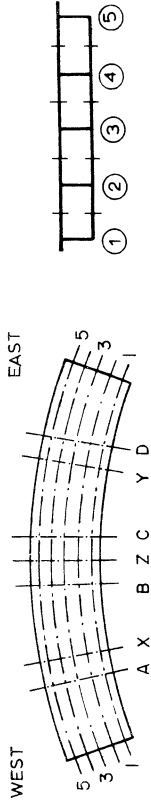
RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NC RESTRAINT.



SECTION	GIRDER	1A+4A		2A+3A		NORMALIZED POINT LOADS AT		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	15.3	38.4	6.3	23.8	6.3	23.8	6.3	23.8	6.3	23.8
A	2	8.2	20.5	4.1	15.5	4.1	15.5	4.1	15.5	4.1	15.5
A	3	6.1	15.2	4.3	16.0	4.3	16.0	4.3	16.0	4.3	16.0
A	4	6.2	15.6	6.4	24.1	6.4	24.1	6.4	24.1	6.4	24.1
A	5	4.1	10.3	5.5	20.6	5.5	20.6	5.5	20.6	5.5	20.6
A	SUM	39.9		26.6		26.6		26.6		26.6	
B	1	-6.2	16.0	-2.5	13.4	-2.5	13.4	-2.5	13.4	-2.5	13.4
B	2	-9.0	23.2	-5.0	26.6	-5.0	26.6	-5.0	26.6	-5.0	26.6
B	3	-9.9	25.7	-4.7	24.6	-4.7	24.6	-4.7	24.6	-4.7	24.6
B	4	-9.1	23.5	-4.0	20.9	-4.0	20.9	-4.0	20.9	-4.0	20.9
B	5	-4.5	11.6	-2.8	14.5	-2.8	14.5	-2.8	14.5	-2.8	14.5
B	SUM	-38.7		-19.0		-19.0		-19.0		-19.0	
C	1	-4.5	12.1	-3.8	18.9	-3.8	18.9	-3.8	18.9	-3.8	18.9
C	2	-7.8	20.7	-5.8	29.3	-5.8	29.3	-5.8	29.3	-5.8	29.3
C	3	-9.7	25.8	-4.0	20.1	-4.0	20.1	-4.0	20.1	-4.0	20.1
C	4	-10.0	26.6	-3.5	17.8	-3.5	17.8	-3.5	17.8	-3.5	17.8
C	5	-5.6	14.9	-2.8	13.9	-2.8	13.9	-2.8	13.9	-2.8	13.9
C	SUM	-37.6		-19.8		-19.8		-19.8		-19.8	
D	1	4.5	9.2	5.7	24.1	5.7	24.1	5.7	24.1	5.7	24.1
D	2	7.2	14.9	7.2	30.4	7.2	30.4	7.2	30.4	7.2	30.4
D	3	8.9	18.4	5.0	21.3	5.0	21.3	5.0	21.3	5.0	21.3
D	4	13.8	28.5	3.7	15.5	3.7	15.5	3.7	15.5	3.7	15.5
D	5	14.1	29.1	2.0	8.6	2.0	8.6	2.0	8.6	2.0	8.6
D	SUM	48.3		23.7		23.7		23.7		23.7	
LOAD	PX (KIPS)	-9.0		-9.0		-9.0		-9.0		-9.0	
LOAD	PY (KIPS)	-9.1		-9.1		-9.1		-9.1		-9.1	
ACTUAL	PX (KIPS)	-8.9		-8.9		-8.9		-8.9		-8.9	
ACTUAL	PY (KIPS)	-9.1		-9.1		-9.1		-9.1		-9.1	

TABLE 191

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.  
RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



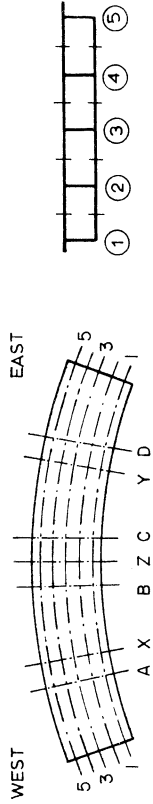
SECTION	GIRDER	1A+4A		2A+3A		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	10.8	29.8	5.2	15.6	5.2	15.6	5.2	15.6
A	2	8.9	24.7	6.0	18.1	6.0	18.1	6.0	18.1
A	3	6.6	18.1	6.8	20.4	6.8	20.4	6.8	20.4
A	4	6.1	16.9	8.8	26.3	8.8	26.3	8.8	26.3
A	5	3.8	10.6	6.5	19.5	6.5	19.5	6.5	19.5
A	SUM	36.2		33.3		33.3		33.3	
B	1	-6.4	16.8	-4.3	15.0	-4.3	15.0	-4.3	15.0
B	2	-8.8	23.0	-6.8	23.6	-6.8	23.6	-6.8	23.6
B	3	-9.5	24.8	-6.9	23.9	-6.9	23.9	-6.9	23.9
B	4	-8.6	22.3	-6.1	21.2	-6.1	21.2	-6.1	21.2
B	5	-5.0	13.2	-4.7	16.2	-4.7	16.2	-4.7	16.2
B	SUM	-38.3		-28.7		-28.7		-28.7	
C	1	-4.6	12.2	-6.1	20.6	-6.1	20.6	-6.1	20.6
C	2	-7.8	20.8	-7.8	26.5	-7.8	26.5	-7.8	26.5
C	3	-9.3	24.7	-6.1	20.6	-6.1	20.6	-6.1	20.6
C	4	-9.6	25.6	-5.6	19.0	-5.6	19.0	-5.6	19.0
C	5	-6.3	16.7	-3.9	13.2	-3.9	13.2	-3.9	13.2
C	SUM	-37.7		-29.6		-29.6		-29.6	
D	1	4.0	8.7	5.9	21.9	5.9	21.9	5.9	21.9
D	2	7.5	16.5	8.8	32.4	8.8	32.4	8.8	32.4
D	3	8.7	19.2	5.5	20.2	5.5	20.2	5.5	20.2
D	4	13.9	30.8	4.5	16.4	4.5	16.4	4.5	16.4
D	5	11.2	24.8	2.5	9.1	2.5	9.1	2.5	9.1
D	SUM	45.2		27.1		27.1		27.1	
LOAD	PX (KIPS)								
LOAD	PY (KIPS)	-9.0		-9.0		-9.0		-9.0	
ACTUAL	PX (KIPS)	-9.1		-9.0		-9.0		-9.0	
ACTUAL	PY (KIPS)	-8.9		-9.0		-9.0		-9.0	

TABLE 19J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



SECTION	GIRDER	1A+4A		2A+3A		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	10.0	28.2	4.9	13.6	4.9	13.6	4.9	13.6
A	2	9.1	25.5	6.7	18.7	6.7	18.7	6.7	18.7
A	3	6.7	18.8	7.9	21.8	7.9	21.8	7.9	21.8
A	4	6.1	17.1	9.6	26.6	9.6	26.6	9.6	26.6
A	5	3.7	10.4	7.0	19.3	7.0	19.3	7.0	19.3
A	SUM	35.6		36.1		36.1		36.1	
B	1	-6.5	17.1	-5.5	15.4	-5.5	15.4	-5.5	15.4
B	2	-8.7	22.8	-8.0	22.4	-8.0	22.4	-8.0	22.4
B	3	-9.3	24.3	-8.6	24.0	-8.6	24.0	-8.6	24.0
B	4	-8.4	21.9	-7.7	21.5	-7.7	21.5	-7.7	21.5
B	5	-5.3	13.8	-6.0	16.7	-6.0	16.7	-6.0	16.7
B	SUM	-38.1		-35.8		-35.8		-35.8	
C	1	-4.6	12.3	-7.5	20.6	-7.5	20.6	-7.5	20.6
C	2	-7.9	20.9	-9.2	25.2	-9.2	25.2	-9.2	25.2
C	3	-9.1	24.2	-7.7	21.2	-7.7	21.2	-7.7	21.2
C	4	-9.5	25.2	-7.4	20.3	-7.4	20.3	-7.4	20.3
C	5	-6.6	17.5	-4.6	12.7	-4.6	12.7	-4.6	12.7
C	SUM	-37.6		-36.5		-36.5		-36.5	
D	1	3.8	8.5	6.0	21.3	6.0	21.3	6.0	21.3
D	2	7.6	17.0	9.3	32.7	9.3	32.7	9.3	32.7
D	3	8.6	19.4	5.6	19.7	5.6	19.7	5.6	19.7
D	4	14.0	31.6	4.8	16.9	4.8	16.9	4.8	16.9
D	5	10.4	23.4	2.7	9.4	2.7	9.4	2.7	9.4
D	SUM	44.3		28.4		28.4		28.4	
LOAD	PX (KIPS)	-9.0		-9.0		-9.0		-9.0	
LOAD	PY (KIPS)	-9.1		-9.1		-9.1		-9.1	
ACTUAL	PX (KIPS)	-8.9		-8.9		-8.9		-8.9	
ACTUAL	PY (KIPS)	-9.1		-9.1		-9.1		-9.1	

TABLE 10A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS

RESULTS FOR JACK LOADS APPLIED  
 AFTER 30 KSI CONJ. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.

REACTION OR LOAD	48+5B+6B		NORMALIZED POINT LOADS AT ALL SIX TRUCKS		1B+2R+3R	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	.96	-.37	.95	.32		.61
2E	1.97	2.98	1.60	2.20		-1.14
3E	1.71	3.32	1.36	2.12		-.70
4E	2.26	.49	1.79	1.31		.67
5E	3.67	3.46	2.81	2.62		-1.30
1F	9.88	11.22	9.21	7.69		-.41
2F	9.93	11.82	9.29	6.95		-1.29
3F	-.62	-2.22	9.28	11.40		10.20
4F	-.67	-2.07	9.21	11.86		10.33
1W	-.02	-.06	.91	1.54		1.73
2W	-.36	.16	1.60	.87		1.18
3W	-.35	-.61	1.42	1.41		.90
4W	-.48	-.80	1.82	1.87		2.85
5W	-.85	-.80	2.75	2.68		4.06
RE	10.57	9.88	8.51	8.57		-1.86
RF	18.51	18.75	37.00	37.90		18.83
RW	-2.06	-2.11	8.50	8.37		10.72
SUMR	27.02	26.52	54.01	54.84		27.69
PX	-0.	-0.	-27.00	-27.00		-27.00
PY	-27.00	-27.00	-27.00	-27.73		-0.
SUMP	-27.00	-27.00	-54.00	-54.73		-27.00
SUMR/SUMP	1.00	.98	1.00	1.00		1.03
TW	-4.58	-6.28	10.03	8.44		16.29
MF	-31.65	-41.00	-.01	12.94		33.34
TF	-.14	-.68	-.22	1.80		1.50
TE	14.69	13.30	10.06	9.55		5.17
ACTUAL PX		-0.		-26.68		-26.98
ACTUAL PY		-27.79		-27.40		-0.

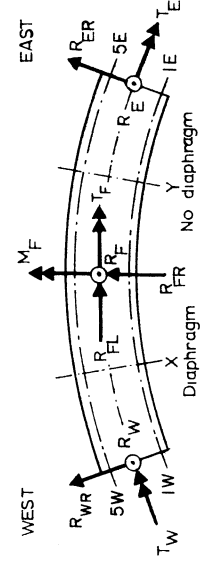
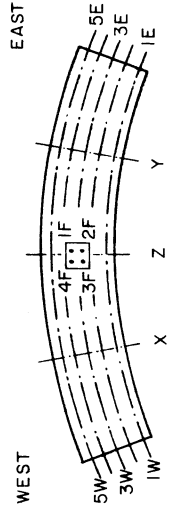
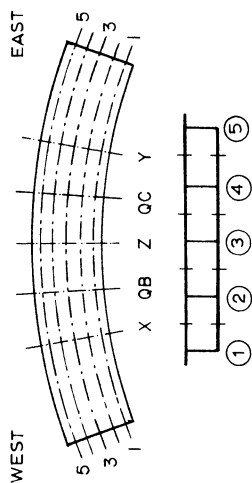


TABLE 20B

SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.



DEFLECTION AT POINT	4B+5B+6B		ALL SIX TRUCKS		IB+2B+3B		
	THEORY	EXPERM	THEORY	E/T	THEORY	EXPERM	E/T
1X	-.062	-.092	.119	.175	1.47	.252	
2X	-.065	-.102	.123	.185	1.50	.266	
3X	-.068	-.109	.128	.191	1.49	.280	
4X	-.072	-.111	.135	.201	1.49	.291	
5X	-.075	-.113	.143	.209	1.47	.301	
1QB	-.054	-.080	.058	.089	1.53	.156	
2QB	-.056	-.083	.058	.089	1.52	.157	
3QB	-.058	-.085	.059	.093	1.56	.164	
4QB	-.061	-.089	.064	.100	1.57	.172	
5QB	-.064	-.092	.069	.099	1.43	.176	
1Z	.004	.008	.008	.016	1.99	.008	
2Z	.002	.005	.004	.010	2.36	.005	
4Z	.002	.005	.004	.006	1.60	.002	
5Z	.004	.005	.007	.011	1.44	.004	
1QC	.114	.161	.060	.079	1.33	-.073	
2QC	.115	.165	.059	.079	1.33	-.077	
3QC	.117	.167	.059	.077	1.29	-.078	
4QC	.124	.173	.063	.083	1.31	-.086	
5QC	.133	.176	.069	.078	1.14	-.093	
1Y	.185	.268	.122	.167	1.37	-.090	
2Y	.190	.273	.124	.164	1.32	-.098	
3Y	.196	.278	.128	.167	1.31	-.101	
4Y	.205	.294	.134	.180	1.34	-.101	
5Y	.216	.305	.142	.188	1.32	-.110	
LOAD PX	-0.	-0.	-27.0	-27.0		-27.0	
LOAD PY	-27.0	-27.0	-27.0	-27.7		-0.	
ACTUAL PX	-0.	-0.	-26.7	-27.0		-0.	
ACTUAL PY	-27.8	-27.8	-27.4	-27.4		-0.	

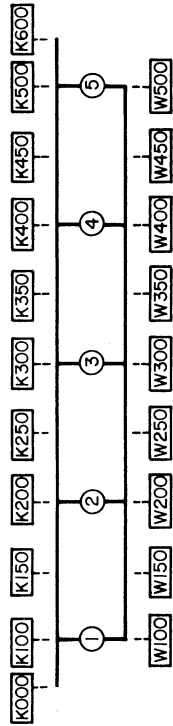
TABLE 20C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	4B+5B+6B		ALL SIX TRUCKS		1B+2B+3B	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	18	22	-68	-71	-80	-80
K	K100	15	44	-60	-132	-142	-138
K	K150	16	16	-63	-57	-80	-74
K	K200	13	27	-52	-91	-105	-109
K	K250	14	14	-63	-64	-81	-81
K	K300	13	24	-52	-80	-96	-95
K	K350	13	20	-50	-70	-85	-85
K	K400	13	26	-50	-85	-101	-102
K	K450	15	18	-55	-67	-81	-89
K	K500	15	23	-55	-73	-86	-86
K	K600	17	15	-61	-46	-55	-55
W	W100	-57	-56	237	263	302	306
W	W150	-45	-45	198	181	216	192
W	W200	-51	-57	198	227	268	258
W	W250	-48	-48	206	183	220	201
W	W300	-55	-59	206	213	259	260
W	W350	-51	-50	191	175	215	222
W	W400	-51	-57	183	200	245	246
W	W450	-50	-50	211	183	223	215
W	W500	-55	-68	211	237	293	290

LOAD	PX (KIPS)	PY (KIPS)	ACTUAL PX (KIPS)	ACTUAL PY (KIPS)
	-0.	-27.0	-26.7	-27.0
	-27.0	-27.7	-27.4	-0.
	-27.0	-27.0	-27.4	-0.

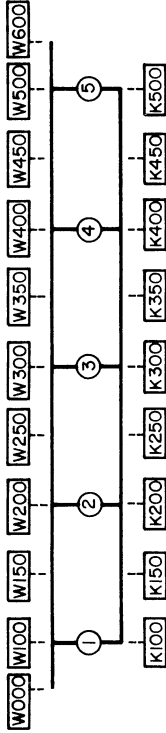
TABLE 200

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	4B+5B+6B		ALL SIX TRUCKS		1B+2B+3B	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	121	80	171	159	171	159
W	W100	108	85	159	167	159	167
W	W150		79		156		156
W	W200	81	89	136	189	136	189
W	W250		63		169		169
W	W300	52	71	135	195	135	195
W	W350		60		167		167
W	W400	80	77	137	166	137	166
W	W450		73		173		173
W	W500	103	72	156	143	156	143
W	W600	110	73	159	148	159	148
K	K100	-49	-52	-72	-97	-72	-97
K	K150		-57		-97		-97
K	K200	-38	-48	-63	-98	-63	-98
K	K250		-44		-95		-95
K	K300	-22	-42	-55	-94	-55	-94
K	K350		-45		-92		-92
K	K400	-38	-47	-64	-86	-64	-86
K	K450		-42		-86		-86
K	K500	-45	-41	-70	-83	-70	-83
LOAD	PX (KIPS)	-0.	-0.	-27.0	-27.0	-27.0	-27.0
LOAD	PY (KIPS)	-27.0	-27.0	-27.0	-27.7	-27.0	-27.7
ACTUAL	PX (KIPS)	-0.	-0.	-26.7	-27.4	-27.0	-27.0
ACTUAL	PY (KIPS)	-27.8	-27.8	-27.4	-27.4	-27.0	-27.4

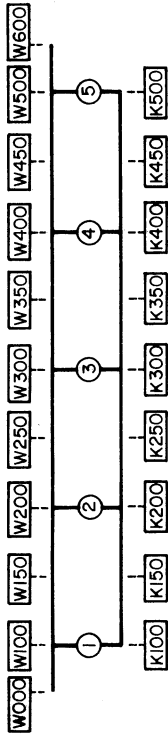


TABLE 20E

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR TRUCK LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	4B+5B+6B		ALL SIX TRUCKS		1B+2B+3B	
		THEORY	MEASR ADJUST	THEORY	MEASR ADJUST	THEORY	MEASR ADJUST
W	W000	54	78	173	166	81	81
W	W100	54	71	161	154	73	74
W	W150	66	71	136	145	65	68
W	W200	56	103	136	199	87	87
W	W250	90	88	135	152	59	58
W	W300	82	118	136	200	72	72
W	W350	77	83	136	146	53	57
W	W400	56	94	136	194	88	90
W	W450	65	68	137	143	68	71
W	W500	51	66	155	147	75	74
W	W600	46	68	158	148	75	75
K	K100	-25	-46	-73	-100	-50	-49
K	K150	-40	-38	-63	-88	-45	-44
K	K200	-25	-44	-63	-97	-47	-50
K	K250	-50	-55	-55	-98	-42	-48
K	K300	-32	-55	-55	-102	-39	-38
K	K350	-25	-59	-63	-112	-45	-44
K	K400	-25	-39	-63	-89	-45	-45
K	K450	-36	-38	-69	-99	-60	-59
K	K500	-23	-38	-69	-90	-48	-47
LOAD	PX (KIPS)	-0.	-0.	-27.0	-27.0	-27.0	-27.0
LOAD	PY (KIPS)	-27.0	-27.0	-27.0	-27.7	-0.	-0.
ACTUAL	PX (KIPS)	-0.	-0.	-26.7	-26.7	-27.0	-27.0
ACTUAL	PY (KIPS)	-27.8	-27.8	-27.4	-27.4	-0.	-0.

TABLE 20F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR TRUCK LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.



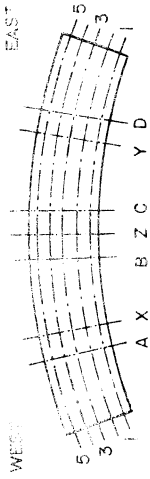
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	4B+5B+6B		ALL SIX TRUCKS		1B+2B+3B	
		THEORY	MEASR ADJUST	THEORY	MEASR ADJUST	THEORY	MEASR ADJUST
K	K000	-76	-45	-60	-35	-35	9
K	K100	-66	-77	-52	-61	-59	16
K	K150	-119	-114	-91	-87	-91	34
K	K200	-57	-97	-45	-77	-77	25
K	K250	-91	-101	-70	-78	-70	20
K	K300	-58	-96	-46	-71	-71	22
K	K350	-114	-121	-87	-93	-87	31
K	K400	-56	-100	-45	-79	-79	25
K	K450	-140	-127	-108	-97	-108	39
K	K500	-64	-106	-51	-84	-85	26
K	K600	-70	-106	-55	-85	-32	9
W	W100	288	197	229	147	151	-39
W	W150	256	242	196	193	182	-53
W	W200	248	258	206	178	195	-56
W	W250	261	226	206	179	169	-49
W	W300	240	240	194	170	179	-55
W	W350	230	222	220	228	165	-53
W	W400	244	289	178	178	223	-63
W	W450	235	233	220	225	175	-51
W	W500	274	281	220	225	231	-55
LOAD	PX (KIPS)	-0.	-0.	-27.0	-27.0	-27.0	-27.0
LOAD	PY (KIPS)	-27.0	-27.0	-27.0	-27.7	-0.	-0.
ACTUAL	PX (KIPS)	-0.	-0.	-26.7	-27.4	-27.0	-27.0
ACTUAL	PY (KIPS)	-27.8	-27.8	-27.4	-27.4	-0.	-0.

TABLE 206

COMPRESSION FLANGES OF MEMBERS 10 EACH GIRDED  
 50 PERCENT AREA PERCENTAGE

MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH



RESULTS FOR TRUCK LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.

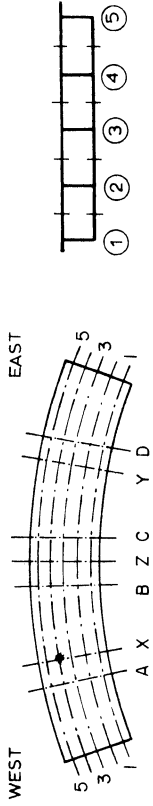
SECTION	GIRDER	4B+5B+6B			VPMALIZED POINT LOADS AT ALL SIX TRUCKS			1B+2B+3B			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	-5.1	16.7	-3.8	12.0	20.4	17.5	18.0	15.0	21.1	14.6
A	2	-6.9	22.4	-7.1	22.2	26.7	22.8	27.9	23.3	33.3	23.0
A	3	-6.8	22.2	-7.8	24.5	25.6	21.9	28.0	23.4	34.1	23.5
A	4	-6.8	22.3	-8.0	25.2	25.6	21.9	28.0	23.3	34.3	23.7
A	5	-5.0	16.3	-5.1	16.1	18.5	15.9	18.0	15.0	22.2	15.3
A	SUM	-30.6		-31.8		116.9		119.8		145.0	
B	1	-13.0	19.0	-9.9	18.2	-19.4	16.4	-19.5	16.2	-9.1	14.1
B	2	-15.8	23.1	-12.2	22.4	-26.6	22.5	-26.6	22.1	-14.2	22.0
B	3	-11.9	17.4	-11.1	20.4	-26.9	22.7	-29.1	24.2	-17.9	27.7
B	4	-15.4	22.6	-11.7	21.4	-26.7	22.5	-25.8	21.4	-13.9	21.5
B	5	-12.2	17.9	-9.6	17.5	-18.9	15.9	-19.2	16.0	-9.6	14.7
B	SUM	-68.3		-54.5		-118.4		-120.3		-64.8	
C	1	-6.8	13.5	-9.6	14.8	-19.6	16.5	-20.3	16.1	-9.8	17.6
C	2	-11.1	22.1	-15.4	23.5	-26.7	22.6	-28.9	23.0	-12.4	22.4
C	3	-14.9	29.7	-17.0	26.1	-26.8	22.6	-28.9	22.9	-10.7	19.3
C	4	-11.0	21.9	-14.3	21.9	-26.6	22.4	-28.3	22.5	-12.9	23.2
C	5	-6.4	12.7	-9.0	13.8	-18.7	15.8	-19.4	15.4	-9.8	17.6
C	SUM	-50.3		-65.4		-118.5		-125.9		-55.6	
D	1	25.1	17.0	17.6	12.5	19.9	17.0	13.2	12.4	-3.5	11.7
D	2	33.2	22.5	34.8	24.7	26.3	22.5	26.2	24.6	-7.3	24.4
D	3	32.4	22.0	31.0	22.0	25.6	21.9	23.0	21.7	-7.0	23.3
D	4	32.7	22.2	36.2	25.8	26.0	22.2	27.5	25.9	-7.9	26.3
D	5	24.1	16.3	21.0	14.9	19.2	16.4	16.3	15.3	-4.3	14.3
D	SUM	147.5		140.5		117.0		106.2		-30.1	
LOAD	PX (KIPS)	-0.		-0.		-27.0		-27.0		-27.0	
LOAD	PY (KIPS)	-27.0		-27.0		-27.0		-27.0		-0.	
AL FUAL	PX (KIPS)	-0.		-0.		-26.7		-26.7		-27.0	
AL FUAL	PY (KIPS)	-27.0		-27.0		-27.0		-27.0		-0.	

TABLE 20H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.

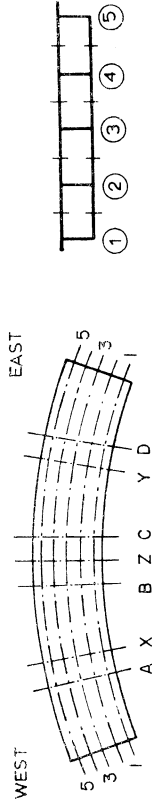


SECTION	GIRDER	4B+5B+53				ALL SIX TRUCKS				1B+2B+3B			
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
A	1	-5.1	16.7	-10.7	28.1	20.4	17.5	27.4	23.3	27.4	23.3	30.8	22.1
A	2	-6.9	22.4	-7.0	18.5	26.7	22.8	23.5	20.0	23.5	20.0	28.6	20.6
A	3	-6.8	22.2	-6.4	16.8	25.6	21.9	22.4	19.1	22.4	19.1	27.4	19.7
A	4	-6.8	22.3	-7.8	20.6	25.6	21.9	25.3	21.5	25.3	21.5	29.8	21.5
A	5	-5.0	16.3	-6.1	16.0	18.5	15.9	19.0	16.1	19.0	16.1	22.3	16.1
A	SUM	-30.6		-38.0		116.9		117.5		117.5		139.0	
B	1	-13.0	19.0	-9.2	16.3	-19.4	16.4	-16.4	14.7	-16.4	14.7	-7.4	13.4
B	2	-15.8	23.1	-13.6	23.9	-26.6	22.5	-26.8	24.1	-26.8	24.1	-13.4	24.2
B	3	-11.9	17.4	-13.1	23.0	-26.9	22.7	-28.0	25.2	-28.0	25.2	-15.8	28.4
B	4	-15.4	22.6	-13.7	24.1	-26.7	22.5	-25.6	23.0	-25.6	23.0	-11.9	21.3
B	5	-12.2	17.9	-7.2	12.7	-18.9	15.9	-14.5	13.0	-14.5	13.0	-7.1	12.8
B	SUM	-68.3		-56.8		-118.4		-111.3		-111.3		-55.6	
C	1	-6.8	13.5	-7.5	13.1	-19.6	16.5	-16.3	13.3	-16.3	13.3	-8.3	13.9
C	2	-11.1	22.1	-13.2	23.0	-26.7	22.6	-28.9	23.6	-28.9	23.6	-14.2	24.0
C	3	-14.9	29.7	-17.2	30.0	-26.8	22.6	-32.5	26.6	-32.5	26.6	-13.1	22.1
C	4	-11.0	21.9	-12.8	22.4	-26.6	22.4	-28.5	23.2	-28.5	23.2	-14.2	24.0
C	5	-6.4	12.7	-6.5	11.4	-18.7	15.8	-16.5	13.4	-16.5	13.4	-9.4	15.9
C	SUM	-50.3		-57.2		-118.5		-122.7		-122.7		-59.2	
D	1	25.1	17.0	20.9	15.0	19.9	17.0	16.3	15.1	16.3	15.1	-5.4	14.6
D	2	33.2	22.5	28.9	20.8	26.3	22.5	22.4	20.7	22.4	20.7	-7.7	20.9
D	3	32.4	22.0	29.4	21.1	25.6	21.9	22.8	21.1	22.8	21.1	-7.3	19.8
D	4	32.7	22.2	31.6	22.7	26.0	22.2	24.4	22.6	24.4	22.6	-8.5	23.0
D	5	24.1	16.3	28.4	20.4	19.2	16.4	22.3	20.6	22.3	20.6	-8.0	21.7
D	SUM	147.5		139.1		117.0		108.2		108.2		-36.9	
LOAD	PX (KIPS)	-0.		-0.		-27.0		-27.0		-27.0		-27.0	
LOAD	PY (KIPS)	-27.0		-27.0		-27.0		-27.7		-27.7		-0.	
ACTUAL	PX (KIPS)	-0.		-0.		-26.7		-26.7		-26.7		-27.0	
ACTUAL	PY (KIPS)	-27.8		-27.8		-27.4		-27.4		-27.4		-0.	

TABLE 201

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



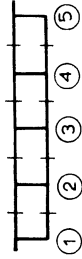
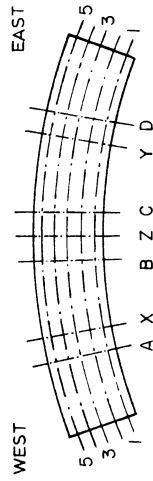
SECTION	GIRDER	48+58+68			NORMALIZED POINT LOADS AT ALL SIX TRUCKS			18+28+38			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	-5.1	16.7	-6.9	19.9	20.4	17.5	22.2	18.7	25.5	17.9
A	2	-6.9	22.4	-7.1	20.4	26.7	22.8	26.0	21.8	31.2	21.9
A	3	-6.8	22.2	-7.2	20.7	25.6	21.9	25.5	21.5	31.1	21.9
A	4	-6.8	22.3	-7.9	22.9	25.6	21.9	26.8	22.5	32.3	22.7
A	5	-5.0	16.3	-5.6	16.1	18.5	15.9	18.4	15.5	22.2	15.6
A	SUM	-30.6		-34.6		116.9		118.8		142.4	
B	1	-13.0	19.0	-9.6	17.1	-19.4	16.4	-17.8	15.4	-8.2	13.7
B	2	-15.8	23.1	-13.0	23.3	-26.6	22.5	-26.7	23.2	-13.8	23.1
B	3	-11.9	17.4	-12.2	21.9	-26.9	22.7	-28.5	24.7	-16.7	28.0
B	4	-15.4	22.6	-12.8	22.9	-26.7	22.5	-25.7	22.3	-12.8	21.4
B	5	-12.2	17.9	-8.3	14.8	-18.9	15.9	-16.6	14.4	-8.2	13.7
B	SUM	-68.3		-55.8		-118.4		-115.3		-59.7	
C	1	-6.8	13.5	-8.4	13.9	-19.6	16.5	-18.1	14.6	-8.9	15.5
C	2	-11.1	22.1	-14.1	23.3	-26.7	22.6	-28.9	23.3	-13.4	23.3
C	3	-14.9	29.7	-17.1	28.1	-26.8	22.6	-30.9	24.9	-12.0	20.9
C	4	-11.0	21.9	-13.5	22.2	-26.6	22.4	-28.4	22.9	-13.6	23.7
C	5	-6.4	12.7	-7.7	12.6	-18.7	15.8	-17.8	14.3	-9.6	16.6
C	SUM	-50.3		-60.8		-118.5		-124.2		-57.6	
D	1	25.1	17.0	19.1	13.6	19.9	17.0	14.6	13.6	-4.3	13.1
D	2	33.2	22.5	32.2	23.0	26.3	22.5	24.5	22.9	-7.5	22.6
D	3	32.4	22.0	30.2	21.6	25.6	21.9	22.9	21.4	-7.2	21.6
D	4	32.7	22.2	34.1	24.4	25.0	22.2	26.1	24.4	-8.2	24.7
D	5	24.1	16.3	24.3	17.4	19.2	16.4	19.0	17.7	-5.9	18.0
D	SUM	147.5		139.9		117.0		107.1		-33.1	
LOAD	PX (KIPS)	-0.		-0.		-27.0		-27.0		-27.0	
LOAD	PY (KIPS)	-27.0		-27.0		-27.0		-27.0		-27.0	
ACTUAL	PX (KIPS)	-0.		-0.		-26.7		-26.7		-27.0	
ACTUAL	PY (KIPS)	-27.8		-27.8		-27.4		-27.4		-0.	

TABLE 20J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR TRUCK LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



SECTION	GIRDER	4R+5B+6B			NORMALIZED POINT LOADS AT ALL SIX TRUCKS			1B+2B+3B			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	-5.1	16.7	-6.7	19.5	20.4	17.5	21.0	17.6	24.1	16.8
A	2	-6.9	22.4	-7.1	20.4	26.7	22.8	26.6	22.2	31.9	22.2
A	3	-6.8	22.2	-7.4	21.4	25.6	21.9	26.5	22.2	32.3	22.5
A	4	-6.8	22.3	-7.9	23.0	25.6	21.9	27.1	22.7	33.0	23.0
A	5	-5.0	16.3	-5.4	15.6	18.5	15.9	18.2	15.3	22.2	15.5
A	SUM	-30.6		-34.5		115.9		119.4		143.6	
B	1	-13.0	19.0	-9.7	17.5	-19.4	16.4	-18.4	15.7	-8.5	13.8
B	2	-15.8	23.1	-12.7	22.9	-26.6	22.5	-26.7	22.8	-14.0	22.6
B	3	-11.9	17.4	-11.9	21.4	-26.9	22.7	-28.8	24.6	-17.3	28.0
B	4	-15.4	22.6	-12.4	22.5	-26.7	22.5	-25.7	22.0	-13.3	21.5
B	5	-12.2	17.9	-8.7	15.7	-18.9	15.9	-17.5	15.0	-8.7	14.0
B	SUM	-68.3		-55.4		-118.4		-117.0		-61.7	
C	1	-6.8	13.5	-8.8	14.1	-19.6	16.5	-18.7	15.0	-9.2	16.1
C	2	-11.1	22.1	-14.7	23.5	-26.7	22.6	-28.9	23.2	-13.1	23.1
C	3	-14.9	29.7	-17.1	27.3	-26.8	22.6	-30.1	24.2	-11.5	20.3
C	4	-11.0	21.9	-13.9	22.1	-26.6	22.4	-28.4	22.8	-13.4	23.5
C	5	-6.4	12.7	-8.1	13.0	-18.7	15.8	-18.3	14.7	-9.6	17.0
C	SUM	-50.3		-62.5		-118.5		-124.4		-56.8	
D	1	25.1	17.0	18.5	13.2	19.9	17.0	14.1	13.2	-4.1	12.7
D	2	33.2	22.5	33.2	23.7	26.3	22.5	25.1	23.5	-7.4	23.1
D	3	32.4	22.0	30.5	21.8	25.6	21.9	23.0	21.5	-7.1	22.0
D	4	32.7	22.2	35.0	25.0	26.0	22.2	26.7	25.0	-8.1	25.1
D	5	24.1	16.3	23.0	16.4	19.2	16.4	17.9	16.8	-5.5	17.0
D	SUM	147.5		140.2		117.0		106.8		-32.2	
LOAD	PX (KIPS)	-0.		-0.		-27.0		-27.0		-27.0	
LOAD	PY (KIPS)	-27.0		-27.0		-27.0		-27.7		-0.	
ACTUAL	PX (KIPS)	-0.		-0.		-26.7		-26.7		-27.0	
ACTUAL	PY (KIPS)	-27.8		-27.8		-27.4		-27.4		-0.	

TABLE 21A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR VEHICLE LOADS APPLIED AFTER 30 KSI JOINT LOADING.  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS  
 TF = MOMENT AT FOOTING ABOUT Y-AXIS  
 SIMPLY SUPPORTED NO RESTRAINT.

REACTION OR LOAD	NORMALIZED VEHICLE LOAD APPLIED AT			
	4C		2C+4C	
	THEORY	EXPERM	THEORY	EXPERM
1E	-6.18	-4.29	-8.50	-4.28
2E	.02	-1.52	-.92	-3.60
3E	2.26	4.24	1.77	2.48
4E	6.37	3.61	6.03	5.06
5E	13.39	13.02	13.99	12.63
1F	19.02	22.16	22.44	22.99
2F	10.98	13.58	6.42	5.03
3F	-4.58	-7.60	6.45	6.46
4F	3.47	1.62	22.48	23.89
1W	-2.31	-1.65	-8.97	-4.72
2W	-.93	-.75	-.37	-3.50
3W	-.50	-.73	2.03	-1.19
4W	-.35	-.90	5.65	6.90
5W	.59	.58	13.99	15.46
RE	15.86	15.06	12.37	12.29
RF	28.89	29.76	57.80	58.37
RW	-3.50	-3.45	12.33	12.95
SUMR	41.25	41.37	82.50	83.61
PX	-0.	-0.	-41.25	-41.25
PY	-41.25	-41.25	-41.25	-41.27
SUMP	-41.25	-41.25	-82.50	-82.52
SJMR/SUMP	1.00	1.00	1.00	1.01
TW	16.42	11.09	133.64	130.60
MF	-46.67	-62.59	.10	3.50
TF	24.13	26.69	48.07	53.07
TE	117.04	102.27	133.61	109.30
ACTUAL PX		-.15		-40.97
ACTUAL PY		-40.88		-41.00

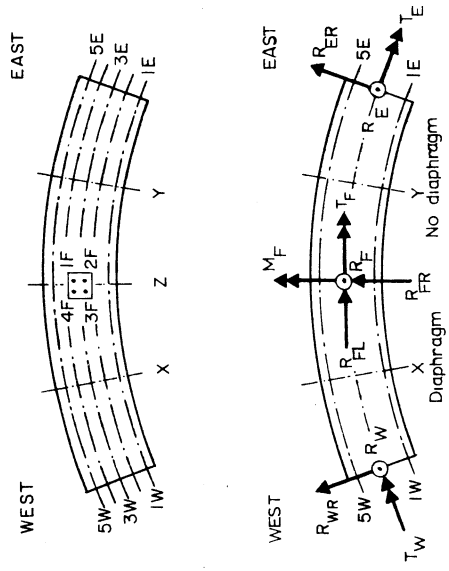
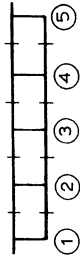
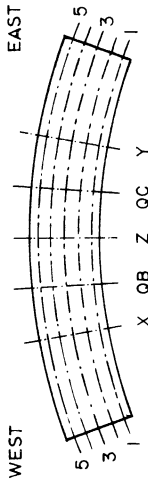


TABLE 21B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR VEHICLE LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.



DEFLECTION AT POINT	4C		2C+4C		2C	
	THEORY	EXPERM E/T	THEORY	EXPERM E/T	THEORY	EXPERM E/T
1X	-.112	-.190 1.69	.086	.127 1.48		.295
2X	-.106	-.192 1.81	.130	.197 1.51		.376
3X	-.101	-.189 1.87	.180	.277 1.54		.462
4X	-.096	-.181 1.87	.233	.354 1.52		.548
5X	-.092	-.172 1.86	.287	.431 1.50		.629
1QB	-.108	-.187 1.73	-.004	-.004 .85		.163
2QB	-.097	-.169 1.75	.037	.063 1.68		.212
3QB	-.086	-.151 1.76	.084	.133 1.58		.275
4QB	-.077	-.141 1.83	.140	.214 1.53		.363
5QB	-.067	-.126 1.89	.196	.288 1.47		.432
1Z	-.035	-.051 1.47	-.070	-.090 1.29		-.043
2Z	-.017	-.025 1.45	-.034	-.042 1.24		-.019
4Z	.024	.035 1.50	.047	.065 1.39		.029
5Z	.048	.072 1.52	.095	.134 1.41		.062
1QC	.100	.156 1.56	-.009	-.030 3.36		-.166
2QC	.129	.203 1.57	.032	.031 .98		-.156
3QC	.169	.274 1.62	.083	.117 1.40		-.143
4QC	.222	.370 1.67	.145	.239 1.65		-.133
5QC	.269	.445 1.66	.203	.327 1.61		-.120
1Y	.188	.278 1.48	.075	.074 1.00		-.177
2Y	.223	.338 1.52	.116	.139 1.20		-.174
3Y	.275	.434 1.58	.173	.257 1.48		-.168
4Y	.338	.567 1.68	.242	.404 1.67		-.165
5Y	.391	.643 1.64	.300	.492 1.64		-.161
LCAD LOAD	-0.	-0.	-41.2	-41.2		-41.2
LOAD	-41.2	-41.2	-41.2	-41.2		-0.
ACTUAL	-0.	-0.	-41.0	-41.0		-41.0
ACTUAL	-41.0	-41.0	-41.0	-41.0		0.

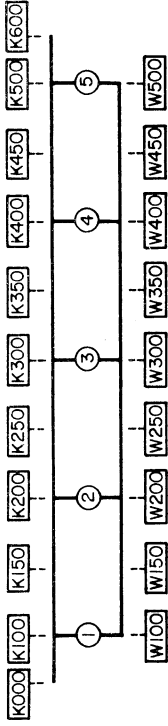


TABLE 21C

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR VEHICLE LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED VEHICLE LOAD APPLIED AT

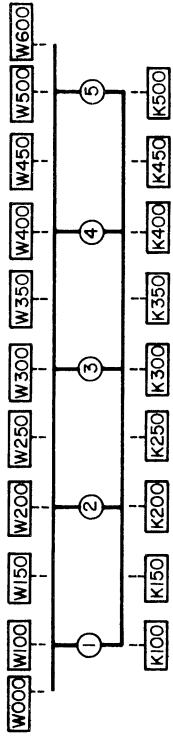
GAGE TYPE	GAGE LOC.	4C		2C+4C		2C	
		THEORY	MEASR	THEORY	MEASF	THEORY	MEASR
K	K000	29	36	-75	-70	-75	-70
K	K100	25	82	-63	-117	-113	-146
K	K150	26	17	-58	-75	-71	-102
K	K200	21	50	-58	-90	-96	-118
K	K250	21	21	-70	-84	-87	-109
K	K300	21	46	-78	-104	-108	-141
K	K350	20	35	-78	-80	-77	-116
K	K400	20	48	-95	-151	-143	-199
K	K450	23	33	-101	-101	-106	-134
K	K500	26	47	-101	-134	-137	-162
K	K600	26	32	-101	-80	-80	-101
W	W100	-93	-103	237	216	211	303
W	W150	-82	-75	221	207	196	272
W	W200	-87	-99	273	227	226	316
W	W250	-80	-97	300	182	190	269
W	W300	-85	-103	382	291	296	389
W	W350	-80	-83		244	264	323
W	W400	-80	-90		384	389	468
W	W450	-85	-97		274	284	362
W	W500	-85	-96		499	497	568
LOAD	PX (KIPS)	-0.	-0.	-41.2	-41.2	-41.2	-41.2
LOAD	PY (KIPS)	-41.2	-41.2	-41.2	-41.3	-41.3	-0.
ACTUAL	PX (KIPS)	-0.2	-0.2	-41.0	-41.0	-41.0	-41.0
ACTUAL	PY (KIPS)	-40.9	-40.9	-41.0	-41.0	-41.0	-0.

TABLE 21D

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR VEHICLE LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.

SECTION B

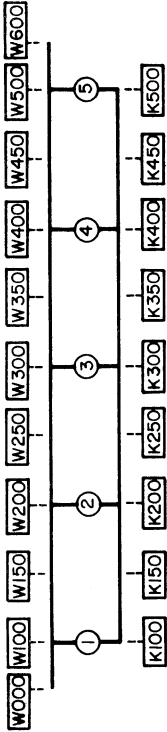
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	4C		2C+4C		2C		*****		
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
W	W000	168	112	112	243	174	174	61	61	61
W	W100	151	106	106	227	187	190	77	77	79
W	W150		24	24		169	190	69	69	80
W	W200	114	119	121	193	249	246	144	144	140
W	W250		96	98		220	207	137	137	158
W	W300	83	123	124	207	291	305	196	196	210
W	W350		111	127		257	295	162	162	185
W	W400	138	157	161	230	319	319	191	191	188
W	W450		149	174		298	340	172	172	197
W	W500	182	144	145	271	297	302	182	182	186
W	W600	195	146	146	277	317	317	201	201	201
K	K100	-66	-81	-82	-101	-147	-150	-64	-64	-66
K	K150		-99	-90		-144	-139	-34	-34	-39
K	K200	-54	-69	-66	-90	-148	-144	-85	-85	-82
K	K250		-63	-64		-145	-136	-81	-81	-71
K	K300	-36	-74	-74	-85	-147	-149	-68	-68	-72
K	K350		-86	-87		-149	-149	-56	-56	-53
K	K400	-66	-86	-89	-107	-148	-147	-77	-77	-75
K	K450		-74	-80		-158	-156	-99	-99	-97
K	K500	-82	-73	-71	-123	-151	-151	-102	-102	-102
LOAD	PX (KIPS)	-0.	-0.		-41.2	-41.2		-41.2		
LOAD	PY (KIPS)	-41.2	-41.2		-41.2	-41.3		-0.		
ACTUAL	PX (KIPS)		-0.2		-41.0			-41.0		
ACTUAL	PY (KIPS)		-40.9		-41.0			.0		

TABLE 21E

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR VEHICLE LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.



SECTION C

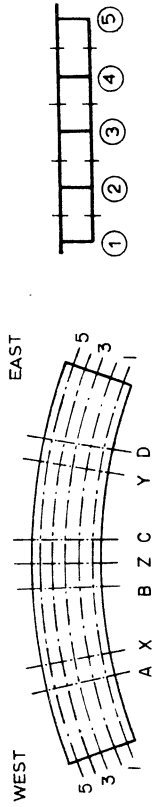
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	4C		2C+4C		2C	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	62	39	233	154	122	122
W	W100	66	49	219	151	111	115
W	W150		60		153	102	113
W	W200	72	124	189	247	130	130
W	W250		114		202	103	103
W	W300	122	199	206	323	130	129
W	W350		140		237	101	109
W	W400	97	209	233	397	186	191
W	W450		151		289	141	149
W	W500	100	189	279	346	156	153
W	W600	96	207	288	356	151	151
K	K100	-29	-57	-97	-139	-85	-84
K	K150		-43		-118	-75	-79
K	K200	-32	-44	-88	-125	-79	-83
K	K250		-56		-130	-71	-76
K	K300	-48	-72	-85	-145	-70	-70
K	K350		-114		-195	-76	-74
K	K400	-44	-78	-109	-153	-85	-82
K	K450		-58		-169	-128	-121
K	K500	-47	-99	-128	-183	-93	-92
LOAD	PX (KIPS)	-0.	-0.	-41.2	-41.2	-41.2	-41.2
LOAD	PY (KIPS)	-41.2	-41.2	-41.2	-41.3	-0.	-0.
ACTUAL	PX (KIPS)		-0.2		-41.0		-41.0
ACTUAL	PY (KIPS)		-40.9		-41.0		-41.0



TABLE 21G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
RESULTS FOR VEHICLE LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



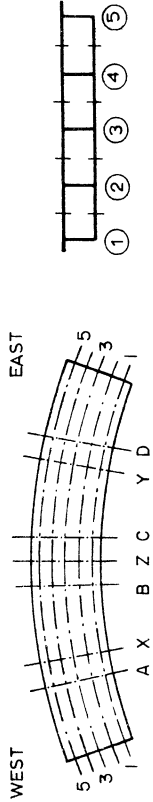
SECTION	GIRDER	4C						2C+4C						2C					
		THEORY		EXPERIMENTAL		PCT		THEORY		EXPERIMENTAL		PCT		THEORY		EXPERIMENTAL		PCT	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	-8.3	17.2	-6.8	12.8	21.3	13.5	16.8	10.0	21.3	13.5	16.8	10.0	23.0	10.7	40.3	18.8	23.0	10.7
A	2	-11.0	22.8	-12.6	23.9	30.0	19.1	30.9	18.3	30.0	19.1	30.9	18.3	40.3	18.8	50.0	23.3	40.3	18.8
A	3	-10.7	22.2	-13.3	25.2	33.9	21.6	37.6	22.3	33.9	21.6	37.6	22.3	50.0	23.3	60.6	28.2	50.0	23.3
A	4	-10.6	22.0	-12.6	23.8	40.0	25.5	49.1	29.0	40.0	25.5	49.1	29.0	60.6	28.2	40.7	19.0	60.6	28.2
A	5	-7.7	15.9	-7.6	14.3	32.0	20.3	34.6	20.5	32.0	20.3	34.6	20.5	40.7	19.0	214.7		40.7	19.0
A	SUM	-48.3		-52.9		157.1		169.1		157.1		169.1		214.7				214.7	
B	1	-17.9	16.7	-8.3	10.0	-27.4	14.9	-21.9	11.4	-27.4	14.9	-21.9	11.4	-8.7	7.7			-8.7	7.7
B	2	-22.4	20.8	-13.1	15.7	-38.2	20.7	-35.0	18.3	-38.2	20.7	-35.0	18.3	-19.5	17.4			-19.5	17.4
B	3	-19.0	17.6	-18.7	22.5	-41.3	22.5	-46.3	24.1	-41.3	22.5	-46.3	24.1	-31.1	27.7			-31.1	27.7
B	4	-26.7	24.8	-23.7	28.5	-44.5	24.2	-49.2	25.6	-44.5	24.2	-49.2	25.6	-29.3	26.1			-29.3	26.1
B	5	-21.7	20.2	-19.4	23.3	-32.7	17.7	-39.5	20.6	-32.7	17.7	-39.5	20.6	-23.7	21.1			-23.7	21.1
B	SUM	-107.7		-83.2		-184.1		-192.0		-184.1		-192.0		-112.4				-112.4	
C	1	-8.2	10.8	-5.6	5.4	-26.4	14.4	-19.7	9.8	-26.4	14.4	-19.7	9.8	-15.4	15.2			-15.4	15.2
C	2	-14.7	19.2	-17.2	16.4	-37.4	20.3	-35.2	17.5	-37.4	20.3	-35.2	17.5	-19.9	19.6			-19.9	19.6
C	3	-22.3	29.1	-27.7	26.5	-41.2	22.4	-45.8	22.7	-41.2	22.4	-45.8	22.7	-19.4	19.1			-19.4	19.1
C	4	-19.0	24.8	-30.1	28.7	-45.3	24.6	-56.7	28.1	-45.3	24.6	-56.7	28.1	-26.7	26.3			-26.7	26.3
C	5	-12.4	16.2	-24.1	23.0	-33.7	18.3	-44.3	22.0	-33.7	18.3	-44.3	22.0	-20.2	19.9			-20.2	19.9
C	SUM	-76.5		-104.7		-184.1		-201.7		-184.1		-201.7		-101.6				-101.6	
D	1	28.0	14.9	19.2	10.0	19.6	14.0	10.5	7.7	19.6	14.0	10.5	7.7	-5.8	12.1			-5.8	12.1
D	2	39.0	20.7	40.2	20.9	27.9	19.9	24.0	17.5	27.9	19.9	24.0	17.5	-12.1	25.1			-12.1	25.1
D	3	41.8	22.2	43.5	22.6	31.2	22.3	30.8	22.5	31.2	22.3	30.8	22.5	-11.3	23.4			-11.3	23.4
D	4	45.3	24.1	58.0	30.1	34.8	24.9	46.7	34.1	34.8	24.9	46.7	34.1	-11.8	24.6			-11.8	24.6
D	5	34.1	18.1	31.7	16.5	26.5	18.9	24.8	18.1	26.5	18.9	24.8	18.1	-7.1	14.8			-7.1	14.8
D	SUM	188.2		192.7		139.9		136.9		139.9		136.9		-48.1				-48.1	
LOAD	PX (KIPS)	-0.		-0.		-41.2		-41.2		-41.2		-41.2		-41.2				-41.2	
LOAD	PY (KIPS)	-41.2		-41.2		-41.2		-41.2		-41.2		-41.2		-41.2				-41.2	
ACTUAL	PX (KIPS)	-.		-.		-.		-.		-.		-.		-.				-.	
ACTUAL	PY (KIPS)	-41.0		-41.0		-41.0		-41.0		-41.0		-41.0		-41.0				-41.0	
		.0		.0		.0		.0		.0		.0		.0				.0	

TABLE 21H:

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR VEHICLE LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.

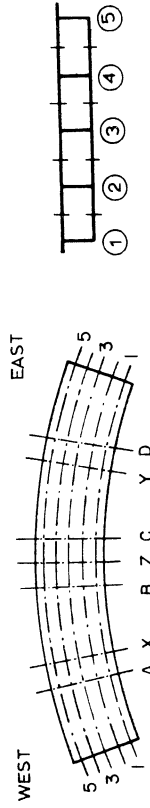


NORMALIZED VEHICLE LOAD APPLIED AT

SECTION	GIRDER	4C			2C+4C			2C		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1	-8.3	-18.9	17.2	21.3	27.0	18.1	27.0	34.1	17.4
A	2	-11.0	-10.0	22.8	30.0	27.2	18.2	27.2	35.5	18.2
A	3	-10.7	-10.7	22.2	33.9	28.6	19.2	28.6	38.2	19.6
A	4	-10.6	-13.5	22.0	40.0	35.2	23.6	35.2	48.4	24.7
A	5	-7.7	-12.2	15.9	32.0	31.1	20.9	31.1	39.3	20.1
A	SUM	-48.3	-65.2		157.1	149.2		149.2	195.4	
B	1	-17.9	-15.5	16.7	-27.4	-25.7	14.4	-25.7	-9.2	10.8
B	2	-22.4	-20.9	20.8	-38.2	-40.5	22.8	-40.5	-19.5	22.8
B	3	-19.0	-23.0	17.6	-41.3	-43.6	24.5	-43.6	-19.0	22.2
B	4	-26.7	-25.1	24.8	-44.5	-42.5	23.9	-42.5	-20.9	24.4
B	5	-21.7	-12.4	20.2	-32.7	-25.5	14.4	-25.5	-17.0	19.9
B	SUM	-107.7	-96.9		-184.1	-177.9		-177.9	-85.5	
C	1	-8.2	-9.0	10.8	-26.4	-23.3	12.2	-23.3	-14.6	13.8
C	2	-14.7	-12.5	19.2	-37.4	-39.3	20.6	-39.3	-24.0	22.6
C	3	-22.3	-24.0	29.1	-41.2	-48.4	25.4	-48.4	-22.3	21.1
C	4	-19.0	-25.4	24.8	-45.3	-49.2	25.8	-49.2	-26.2	24.7
C	5	-12.4	-14.1	16.2	-33.7	-30.4	15.9	-30.4	-18.9	17.8
C	SUM	-76.5	-85.1		-184.1	-190.5		-190.5	-105.9	
D	1	28.0	23.9	14.9	19.6	15.7	11.2	15.7	-8.0	12.0
D	2	39.0	36.4	20.7	27.9	24.5	17.5	24.5	-12.4	18.6
D	3	41.8	41.0	22.2	31.2	30.9	22.1	30.9	-12.6	18.9
D	4	45.3	43.5	24.1	34.8	33.8	24.2	33.8	-17.5	26.2
D	5	34.1	41.4	18.1	26.5	34.6	24.8	34.6	-16.2	24.3
D	SUM	188.2	186.2		139.9	139.5		139.5	-66.7	
LOAD	PX (KIPS)	-0.	-0.		-41.2	-41.2		-41.2	-41.2	
LOAD	PY (KIPS)	-41.2	-41.2		-41.2	-41.3		-41.3	-0.	
ACTUAL	PX (KIPS)	-0.2	-0.2		-41.0	-41.0		-41.0	-41.0	
ACTUAL	PY (KIPS)	-40.9	-40.9		-41.0	-41.0		-41.0	-0.	

TABLE 211

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.  
RESULTS FOR VEHICLE LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



NORMALIZED VEHICLE LOAD APPLIED AT

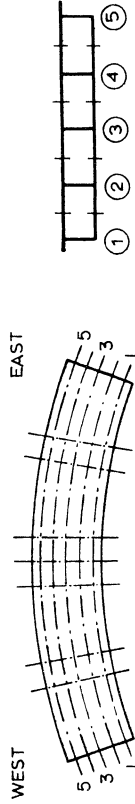
SECTION	GIRDER	4C			2C+4C			2C			
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	
A	1	-8.3	17.2	-12.2	20.8	21.3	13.5	21.4	13.3	27.9	13.6
A	2	-11.0	22.8	-11.5	19.6	30.0	19.1	29.2	18.3	38.2	18.5
A	3	-10.7	22.2	-12.2	20.8	33.9	21.6	33.6	21.0	44.8	21.7
A	4	-10.6	22.0	-13.0	22.3	40.0	25.5	42.9	26.8	55.2	26.8
A	5	-7.7	15.9	-9.6	16.5	32.0	20.3	33.1	20.6	40.1	19.4
A	SUM	-48.3		-58.4		157.1		160.2		206.2	
B	1	-17.9	16.7	-12.3	13.6	-27.4	14.9	-24.0	13.0	-9.0	9.2
B	2	-22.4	20.8	-17.4	19.1	-38.2	20.7	-38.1	20.7	-19.5	20.0
B	3	-19.0	17.6	-21.1	23.2	-41.3	22.5	-44.8	24.3	-24.4	25.0
B	4	-26.7	24.8	-24.5	27.0	-44.5	24.2	-45.5	24.7	-24.6	25.3
B	5	-21.7	20.2	-15.5	17.1	-32.7	17.7	-31.8	17.3	-20.0	20.5
B	SUM	-107.7		-90.8		-184.1		-184.2		-97.5	
C	1	-8.2	10.8	-7.5	8.0	-26.4	14.4	-21.7	11.1	-15.0	14.4
C	2	-14.7	19.2	-14.6	15.6	-37.4	20.3	-37.5	19.2	-22.1	21.3
C	3	-22.3	29.1	-25.7	27.4	-41.2	22.4	-47.3	24.2	-21.0	20.2
C	4	-19.0	24.8	-27.5	29.3	-45.3	24.6	-52.5	26.9	-26.4	25.4
C	5	-12.4	16.2	-18.5	19.7	-33.7	18.3	-36.6	18.7	-19.5	18.7
C	SUM	-76.5		-93.8		-184.1		-195.6		-104.0	
D	1	28.0	14.9	21.3	11.2	19.6	14.0	12.8	9.3	-6.8	12.1
D	2	39.0	20.7	38.5	20.3	27.9	19.9	24.2	17.5	-12.2	21.7
D	3	41.8	22.2	42.4	22.3	31.2	22.3	30.9	22.3	-11.9	21.0
D	4	45.3	24.1	51.6	27.2	34.8	24.9	41.0	29.7	-14.3	25.4
D	5	34.1	18.1	36.1	19.0	26.5	18.9	29.2	21.1	-11.2	19.8
D	SUM	188.2		199.9		139.9		138.1		-56.4	
LOAD	PX (KIPS)	-0.		-0.		-41.2		-41.2		-41.2	
LOAD	PY (KIPS)	-41.2		-41.2		-41.2		-41.3		-0.	
ACTUAL	PX (KIPS)	-.		-.		-41.0		-41.0		-41.0	
ACTUAL	PY (KIPS)	-40.9		-40.9		-41.0		-41.0		.0	

TABLE 21J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE)

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR VEHICLE LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



SECTION	GIRDER	4C		2C+4C		2C					
		THEORY K-FT	EXPERIMENTAL K-FT	THEORY K-FT	EXPERIMENTAL K-FT	THEORY K-FT	EXPERIMENTAL K-FT				
A	1	-8.3	17.2	-12.0	20.6	21.3	13.5	20.4	12.4	26.5	12.6
A	2	-11.0	22.8	-11.7	20.1	30.0	19.1	29.8	18.1	38.9	18.5
A	3	-10.7	22.2	-12.5	21.5	33.9	21.6	35.2	21.4	46.9	22.4
A	4	-10.6	22.0	-12.9	22.2	40.0	25.5	45.3	27.5	57.1	27.2
A	5	-7.7	15.9	-9.1	15.6	32.0	20.3	33.9	20.6	40.4	19.3
A	SUM	-48.3		-58.3		157.1		164.6		209.7	
B	1	-17.9	16.7	-11.5	12.9	-27.4	14.9	-23.6	12.5	-8.9	8.5
B	2	-22.4	20.8	-15.8	17.6	-38.2	20.7	-37.0	19.7	-19.5	18.6
B	3	-19.0	17.6	-20.3	22.9	-41.3	22.5	-45.5	24.2	-28.0	26.8
B	4	-26.7	24.8	-24.2	27.3	-44.5	24.2	-47.1	25.0	-26.9	25.7
B	5	-21.7	20.2	-17.1	19.2	-32.7	17.7	-34.8	18.5	-21.4	20.4
B	SUM	-107.7		-88.9		-184.1		-188.0		-104.7	
C	1	-8.2	10.8	-7.5	7.5	-26.4	14.4	-21.4	10.8	-15.1	14.6
C	2	-14.7	19.2	-16.0	16.1	-37.4	20.3	-36.6	18.4	-21.5	20.8
C	3	-22.3	29.1	-26.8	26.8	-41.2	22.4	-46.6	23.4	-20.4	19.8
C	4	-19.0	24.8	-28.7	28.8	-45.3	24.6	-54.5	27.5	-26.6	25.7
C	5	-12.4	16.2	-20.7	20.7	-33.7	18.3	-39.5	19.9	-19.7	19.1
C	SUM	-76.5		-99.7		-184.1		-198.7		-103.2	
D	1	28.0	14.9	20.5	10.7	19.6	14.0	12.1	8.7	-6.5	11.9
D	2	39.0	20.7	39.1	20.4	27.9	19.9	24.1	17.4	-12.2	22.4
D	3	41.8	22.2	42.8	22.4	31.2	22.3	30.9	22.3	-11.7	21.5
D	4	45.3	24.1	54.7	28.6	34.8	24.9	43.9	31.6	-13.7	25.3
D	5	34.1	18.1	34.4	18.0	26.5	18.9	27.7	20.0	-10.2	18.9
D	SUM	188.2		191.5		139.9		138.6		-54.3	
LOAD	PX (KIPS)	-0.		-0.		-41.2		-41.2		-41.2	
LOAD	PY (KIPS)	-41.2		-41.2		-41.2		-41.3		-0.	
ACTUAL	PX (KIPS)			-.2		-41.0		-41.0		-41.0	
ACTUAL	PY (KIPS)			-40.9		-41.0		-41.0		.0	



TABLE 22A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR VEHICLE LOADS APPLIED  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS AFTER 30 KSI COND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED NO RESTRAINT.

REACTION OR LOAD	NORMALIZED VEHICLE LOAD APPLIED AT			
	1C		3C	
	THEORY	EXPERM	THEORY	EXPERM
1E	2.08	6.79	8.71	8.71
2E	-.46	8.50	8.04	8.04
3E	-1.05	3.69	2.42	2.42
4E	.33	-1.03	-1.01	-1.01
5E	-3.15	-1.60	-4.01	-4.01
1F	-3.52	11.80	3.66	3.66
2F	3.43	22.87	19.59	19.59
3F	17.60	1.50	23.98	23.98
4F	9.51	-8.47	7.57	7.57
1W	9.62	1.17	10.52	10.52
2W	6.12	1.32	6.64	6.64
3W	2.20	-.48	2.62	2.62
4W	1.20	-1.68	-.29	-.29
5W	-1.84	-2.82	-5.85	-5.85
PE	-2.25	16.35	14.15	14.15
RF	27.02	27.70	54.80	54.80
RW	17.30	-2.49	14.22	14.22
SUMR	42.07	41.56	83.17	83.17
PX	-41.25	-0.	-41.25	-41.25
PY	-0.	-41.23	-41.11	-41.11
SUMP	-41.25	-41.23	-82.36	-82.36
SUMR/SUMP	1.02	1.01	1.01	1.01
TW	-71.63	-28.25	-100.57	-100.57
MF	40.80	-62.46	12.46	12.46
TF	-22.57	-31.57	-48.50	-48.50
TE	-28.58	-67.69	-88.74	-88.74
ACTUAL PX	-41.18	.01	-41.23	-41.23
ACTUAL PY	.01	-41.27	-41.19	-41.19

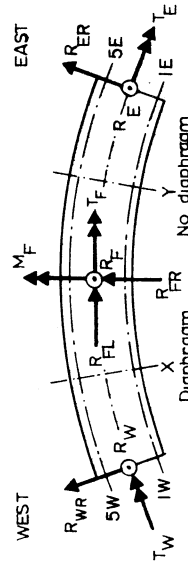
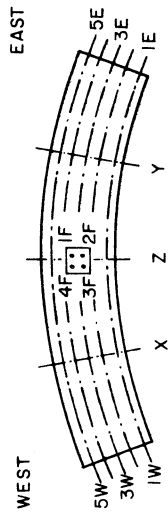
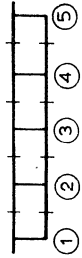
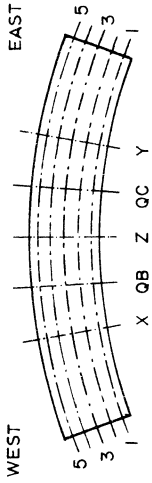


TABLE 22B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR VEHICLE LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.



DEFLECTION AT POINT	IC		3C		IC+3C	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X	.428		-.119		.366	
2X	.399		-.145		.313	
3X	.364		-.172		.258	
4X	.330		-.192		.202	
5X	.302		-.211		.152	
1QB	.329		-.087		.280	
2QB	.277		-.114		.202	
3QB	.223		-.136		.128	
4QB	.181		-.168		.065	
5QB	.159		-.194		.007	
1Z	.071		.078		.149	
2Z	.034		.036		.071	
4Z	-.023		-.024		-.047	
5Z	-.050		-.054		-.105	
1QC	-.070		.387		.277	
2QC	-.096		.341		.208	
3QC	-.118		.246		.095	
4QC	-.144		.192		.012	
5QC	-.173		.159		-.041	
1Y	-.105		.560		.406	
2Y	-.125		.510		.341	
3Y	-.145		.393		.213	
4Y	-.161		.325		.117	
5Y	-.189		.299		.065	
LOAD PX	-41.2		-0.		-41.2	
LOAD PY	-0.		-41.2		-41.1	
ACTUAL PX	-41.2		.0		-41.3	
ACTUAL PY	.0		-41.3		-41.2	

TABLE 22C

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR VEHICLE LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.



TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

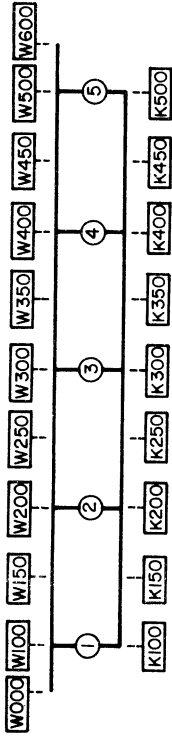
GAGE TYPE	GAGE LOC.	IC		3C		IC+3C	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	-100	-100	34	69	-91	-91
K	K100	-164	-160	69	67	-163	-157
K	K150	-109	-105	24	15	-89	-86
K	K200	-133	-139	40	40	-121	-128
K	K250	-94	-93	23	25	-71	-69
K	K300	-124	-122	34	34	-111	-108
K	K350	-103	-103	28	30	-91	-88
K	K400	-123	-124	38	39	-108	-111
K	K450	-101	-112	25	31	-90	-102
K	K500	-96	-96	36	36	-84	-83
K	K600	-66	-66	23	23	-58	-58
W	W100	356	361	-67	-69	329	311
W	W150	276	264	-63	-53	249	219
W	W200	341	334	-73	-71	301	303
W	W250	301	264	-51	-55	265	233
W	W300	328	326	-85	-85	276	274
W	W350	266	256	-69	-76	226	212
W	W400	288	282	-88	-90	233	229
W	W450	308	260	-62	-70	285	163
W	W500	309	301	-109	-109	226	227
LOAD	PX (KIPS)	-41.2	-0.	-0.	-67	-41.2	-41.2
LOAD	PY (KIPS)	-0.	-41.2	-41.2	-73	-41.1	-41.1
ACTUAL	PX (KIPS)	-41.2	.0	.0	-51	-41.3	-41.3
ACTUAL	PY (KIPS)	.0	-41.3	-41.3	-85	-41.2	-41.2

TABLE 22D

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR VEHICLE LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	1C		3C		IC+3C	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	165	165	135	135	217	217
W	W100	145	147	148	150	298	303
W	W150	117	131	119	133	237	267
W	W200	139	140	156	155	291	298
W	W250	118	130	94	103	214	207
W	W300	138	143	88	94	230	228
W	W350	88	102	68	78	156	180
W	W400	71	72	82	82	157	160
W	W450	57	69	75	85	134	149
W	W500	44	44	71	72	119	118
W	W600	36	36	71	71	113	113
K	K100	-83	-85	-90	-91	-151	-154
K	K150	-73	-66	-85	-82	-141	-133
K	K200	-57	-57	-83	-79	-132	-129
K	K250	-45	-54	-68	-58	-111	-109
K	K300	-58	-58	-50	-50	-107	-107
K	K350	-51	-51	-50	-50	-101	-102
K	K400	-39	-38	-51	-52	-92	-93
K	K450	-38	-40	-51	-52	-93	-96
K	K500	-41	-40	-51	-50	-94	-93
LOAD	PX (KIPS)	-41.2	-0.	-0.	-0.	-41.2	-41.2
LOAD	PY (KIPS)	-0.	-41.2	-41.2	-41.2	-41.1	-41.1
ACTUAL	PX (KIPS)	-41.2	.0	.0	.0	-41.3	-41.3
ACTUAL	PY (KIPS)	.0	-41.3	-41.3	-41.3	-41.2	-41.2

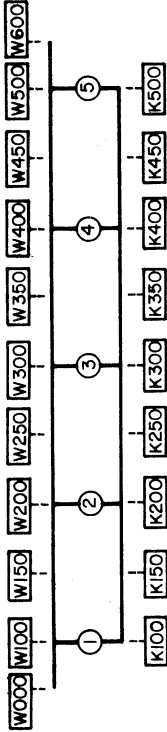
TABLE 22E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR VEHICLE LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

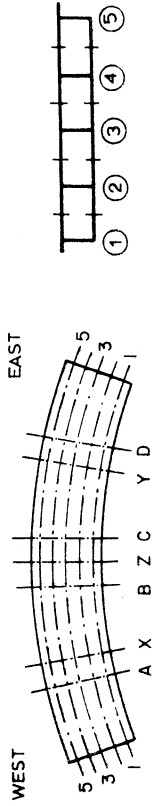


GAGE TYPE	GAGE LOC.	IC		3C		IC+3C	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	122	122	196	196	324	324
W	W100	113	112	171	176	294	296
W	W150	99	100	141	159	243	254
W	W200	135	135	188	186	257	262
W	W250	70	71	138	137	218	227
W	W300	91	91	147	146	249	241
W	W350	59	63	79	85	141	156
W	W400	95	97	68	72	108	121
W	W450	68	69	39	45	115	128
W	W500	74	73	21	20	105	101
W	W600	74	74	4	21	88	88
K	K100	-69	-67	-105	-107	-156	-155
K	K150	-61	-56	-79	-80	-135	-134
K	K200	-60	-59	-83	-80	-143	-145
K	K250	-50	-52	-65	-51	-128	-130
K	K300	-46	-46	-56	-58	-117	-116
K	K350	-58	-55	-29	-31	-99	-99
K	K400	-55	-55	-20	-20	-85	-85
K	K450	-68	-68	-28	-29	-104	-105
K	K500	-60	-59	-32	-32	-99	-98
LOAD	PX (KIPS)	-41.2	-0.	-0.	-107	-41.2	-155
LOAD	PY (KIPS)	-0.	-41.2	-41.2	-80	-41.1	-134
ACTUAL	PX (KIPS)	-41.2	.0	.0	-80	-41.3	-145
ACTUAL	PY (KIPS)	.0	-41.3	-41.3	-51	-41.2	-130



TABLE 22G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
RESULTS FOR VEHICLE LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



NORMALIZED VEHICLE LOAD APPLIED AT

SECTION	GIRDER	IC			3C			1C+3C		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1		26.5	14.9		-4.4	9.9		22.0	15.3
A	2		44.2	24.9		-9.1	20.6		39.1	27.2
A	3		42.3	23.9		-10.9	24.6		35.8	24.9
A	4		39.9	22.5		-12.0	27.2		30.3	21.0
A	5		24.4	13.8		-7.8	17.7		16.7	11.6
A	SUM		177.4			-44.2			144.0	
B	1		-17.6	22.6		-17.1	23.2		-33.8	22.9
B	2		-20.8	26.8		-20.5	27.7		-40.5	27.4
B	3		-21.0	27.0		-14.6	19.8		-33.5	22.7
B	4		-12.3	15.8		-12.4	16.8		-24.7	16.7
B	5		-6.1	7.8		-9.3	12.6		-15.3	10.3
B	SUM		-77.8			-73.9			-147.8	
C	1		-14.6	21.4		-23.4	26.4		-39.1	25.1
C	2		-18.2	26.7		-28.4	31.9		-42.9	27.6
C	3		-12.8	18.8		-21.7	24.5		-36.7	23.6
C	4		-13.3	19.5		-11.8	13.3		-22.6	14.6
C	5		-9.3	13.6		-3.5	3.9		-14.0	9.0
C	SUM		-68.1			-88.8			-155.3	
D	1		-3.8	9.8		36.7	18.4		31.1	20.7
D	2		-8.5	21.9		63.2	31.7		54.6	36.2
D	3		-9.2	23.7		41.7	21.0		30.9	20.5
D	4		-11.4	29.3		36.5	18.3		21.3	14.2
D	5		-5.9	15.2		21.0	10.6		12.7	8.4
D	SUM		-38.8			199.2			150.6	
LOAD	PX (KIPS)		-41.2			-0.			-41.2	
LOAD	PY (KIPS)		-0.			-41.2			-41.1	
ACTUAL	PX (KIPS)		-41.2			.0			-41.3	
ACTUAL	PY (KIPS)		.0			-41.2			-41.2	

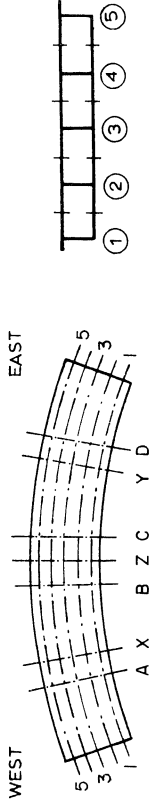
LOAD PX (KIPS)  
LOAD PY (KIPS)  
ACTUAL PX (KIPS)  
ACTUAL PY (KIPS)

TABLE 22H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR VEHICLE LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



NORMALIZED VEHICLE LOAD APPLIED AT

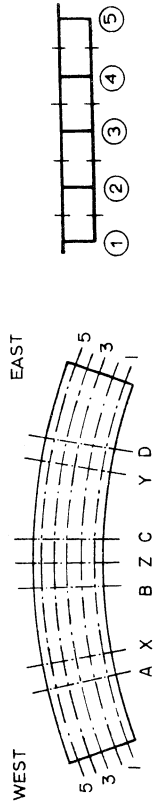
SECTION	GIRDER	1C			3C			1C+3C		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1	37.7	22.0		-16.3	29.7		35.6	23.4	
A	2	36.4	21.3		-9.1	16.6		31.0	20.4	
A	3	33.6	19.6		-9.4	17.2		28.2	18.5	
A	4	37.0	21.6		-11.1	20.1		33.3	21.9	
A	5	26.5	15.5		-9.0	16.3		23.9	15.7	
A	SUM	171.2			-55.0			152.0		
B	1	-13.1	20.1		-14.9	19.6		-24.0	17.7	
B	2	-16.3	24.8		-21.4	28.1		-34.9	25.8	
B	3	-16.5	25.2		-15.7	20.6		-31.8	23.5	
B	4	-12.2	18.6		-15.2	20.0		-27.8	20.6	
B	5	-7.4	11.3		-9.0	11.8		-16.8	12.4	
B	SUM	-65.5			-76.2			-135.2		
C	1	-10.7	14.9		-16.4	25.6		-24.4	16.6	
C	2	-16.2	22.6		-20.3	31.8		-40.5	27.6	
C	3	-15.5	21.6		-14.4	22.5		-35.1	23.9	
C	4	-17.5	24.5		-6.7	10.5		-28.0	19.1	
C	5	-11.6	16.3		-6.1	9.6		-19.0	12.9	
C	SUM	-71.5			-64.0			-147.0		
D	1	-8.5	16.0		45.2	23.0		36.3	25.1	
D	2	-11.9	22.5		48.9	24.8		38.3	26.5	
D	3	-10.5	19.9		38.8	19.7		28.5	19.7	
D	4	-12.4	23.3		35.0	17.8		23.3	16.1	
D	5	-9.7	18.3		28.9	14.7		18.1	12.6	
D	SUM	-52.9			196.9			144.6		
LJAD	PX (KIPS)	-41.2			-0.			-41.2		
LJAD	PY (KIPS)	-0.			-41.2			-41.1		
ACTUAL	PX (KIPS)	-41.2			.0			-41.3		
ACTUAL	PY (KIPS)	.0			-41.3			-41.2		



TABLE 221

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR VEHICLE LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



NORMALIZED VEHICLE LOAD APPLIED AT

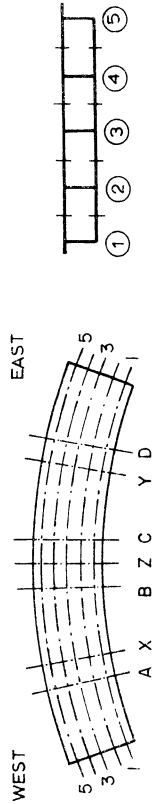
SECTION	GIRDER	1C			3C			1C+3C		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1	31.5	18.0		-9.7	19.8		28.1	19.0	
A	2	40.7	23.3		-9.1	18.6		35.5	24.0	
A	3	38.5	22.0		-10.2	20.9		32.5	22.0	
A	4	38.7	22.1		-11.6	23.7		31.7	21.5	
A	5	25.4	14.5		-8.4	17.0		19.9	13.5	
A	SUM	174.7			-49.0			147.6		
B	1	-15.1	21.3		-15.9	21.1		-28.4	20.1	
B	2	-18.3	25.8		-21.0	27.9		-37.4	26.5	
B	3	-18.5	26.1		-15.2	20.3		-32.6	23.1	
B	4	-12.2	17.2		-13.9	18.6		-26.5	18.8	
B	5	-6.8	9.6		-9.1	12.1		-16.1	11.4	
B	SUM	-71.0			-75.2			-140.9		
C	1	-12.4	17.8		-19.5	26.0		-30.9	20.5	
C	2	-17.1	24.4		-23.9	31.9		-41.6	27.6	
C	3	-14.3	20.4		-17.7	23.5		-35.8	23.8	
C	4	-15.6	22.4		-9.0	12.0		-25.6	17.0	
C	5	-10.6	15.1		-4.9	6.6		-16.8	11.1	
C	SUM	-70.0			-75.1			-150.7		
D	1	-5.9	13.0		40.5	20.5		33.5	22.6	
D	2	-10.0	22.2		56.8	28.7		47.3	32.0	
D	3	-9.8	21.7		40.4	20.4		29.8	20.2	
D	4	-11.8	26.2		35.8	18.1		22.2	15.0	
D	5	-7.6	16.9		24.6	12.4		15.1	10.2	
D	SUM	-45.1			198.2			148.0		
LOAD	PX (KIPS)	-41.2			-0.			-41.2		
LOAD	PY (KIPS)	-0.			-41.2			-41.1		
ACTUAL	PX (KIPS)	-41.2			.0			-41.3		
ACTUAL	PY (KIPS)	.0			-41.3			-41.2		

TABLE 22J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR VEHICLE LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



NORMALIZED VEHICLE LOAD APPLIED AT

SECTION	GIRDER	IC		3C		1C+3C	
		THEORY K-FT	PCT	THEORY K-FT	PCT	THEORY K-FT	PCT
A	1	29.9	17.0	-10.3	20.7	26.6	18.1
A	2	41.9	23.8	-9.1	18.3	36.7	25.0
A	3	40.0	22.7	-10.5	21.1	33.7	22.9
A	4	39.0	22.2	-11.7	23.6	31.3	21.3
A	5	24.9	14.2	-8.1	16.3	18.6	12.7
A	SUM	175.8		-49.7		146.9	
B	1	-16.0	21.5	-16.3	21.8	-30.5	21.2
B	2	-19.5	26.3	-20.8	27.8	-38.8	26.9
B	3	-19.7	26.6	-15.0	20.1	-33.0	22.9
B	4	-12.3	16.5	-13.5	18.0	-25.9	18.0
B	5	-6.7	9.1	-9.2	12.3	-15.9	11.1
B	SUM	-74.1		-74.7		-144.0	
C	1	-13.1	18.9	-20.8	25.3	-34.0	22.1
C	2	-17.6	25.3	-26.0	31.6	-42.0	27.4
C	3	-13.7	19.7	-19.7	23.9	-36.2	23.6
C	4	-14.8	21.3	-10.7	13.0	-24.9	16.2
C	5	-10.3	14.9	-5.1	6.2	-16.5	10.7
C	SUM	-69.5		-82.2		-153.6	
D	1	-5.3	12.4	39.0	19.7	32.5	21.8
D	2	-9.7	22.3	59.3	29.9	50.3	33.7
D	3	-9.6	22.2	40.8	20.6	30.1	20.2
D	4	-11.6	26.9	36.1	18.2	21.9	14.7
D	5	-7.0	16.2	23.1	11.7	14.1	9.5
D	SUM	-43.3		198.2		149.0	
LOAD	PX (KIPS)	-41.2		-0.		-41.2	
LOAD	PY (KIPS)	-0.		-41.2		-41.1	
ACTUAL	PX (KIPS)	-41.2		.0		-41.3	
ACTUAL	PY (KIPS)	.0		-41.3		-41.2	

TABLE 23A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR VEHICLE LOADS APPLIED  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS AFTER 30 KSI COND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED NO RESTRAINT.

REACTION OR LOAD	NORMALIZED VEHICLE LOAD APPLIED AT			
	1C+4C		2C+3C	
	THEORY	EXPERM	THEORY	EXPERM
1E		-4.02		6.65
2E		-.12		6.89
3E		3.15		2.24
4E		4.22		.06
5E		9.61		-2.08
1F		15.71		10.80
2F		13.98		11.03
3F		12.21		18.06
4F		13.70		17.38
1W		7.31		-2.96
2W		5.54		-1.37
3W		2.66		1.10
4W		-.78		6.06
5W		-2.40		10.34
RE		12.84		13.76
RF		55.60		57.27
RW		13.89		13.17
SUMR		82.33		84.20
PX		-41.25		-41.25
PY		-40.49		-42.03
SUMP		-81.68		-83.28
SUMR/SUMP		1.01		1.01
TM		-62.21		87.56
MF		-5.68		20.40
TF		4.83		-1.36
TE		81.30		-62.50
ACTUAL PX		-41.72		-40.59
ACTUAL PY		-40.90		-41.35

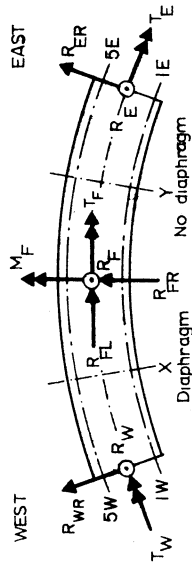
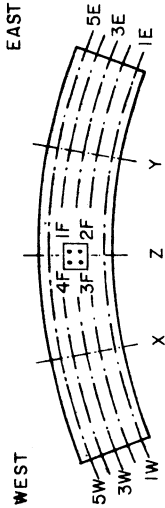
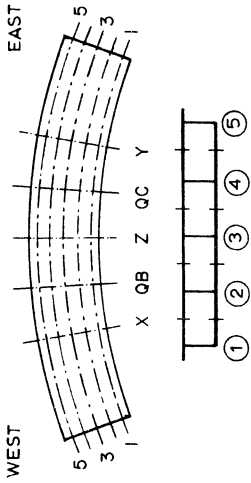


TABLE 23B

SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

RESULTS FOR VEHICLE LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.



NORMALIZED VEHICLE LOAD APPLIED AT

DEFLECTION AT POINT	1C+4C		2C+3C		THEORY		EXPERM		E/T	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM	E/T	E/T
1X	.286		.207		.095		.179			
2X	.252		.259		.122		.148			
3X	.217		.316		.159		.079			
4X	.186		.370		.205		.048			
5X	.160		.424		.241		.037			
1QB	.188		.095		.029		.326			
2QB	.139		.122		.015		.280			
3QB	.099		.159		.009		.195			
4QB	.069		.205		.017		.143			
5QB	.053		.241		.029		.127			
1Z	.022		.029		.029		.326			
2Z	.012		.015		.015		.280			
4Z	.013		.009		.009		.195			
5Z	.025		.017		.017		.143			
1QC	.071		.179		.179		.326			
2QC	.092		.148		.148		.280			
3QC	.139		.079		.079		.195			
4QC	.213		.048		.048		.143			
5QC	.263		.037		.037		.127			
1Y	.157		.326		.326		.326			
2Y	.192		.280		.280		.280			
3Y	.275		.195		.195		.195			
4Y	.386		.143		.143		.143			
5Y	.443		.127		.127		.127			
LOAD PX			-41.2		-41.2		-41.2			
LOAD PY			-40.4		-40.4		-40.4			
ACTUAL PX			-41.7		-41.7		-41.7			
ACTUAL PY			-40.9		-40.9		-40.9			

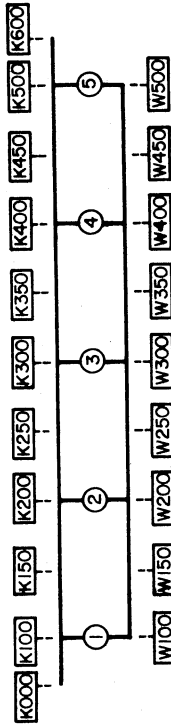
TABLE 23C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR VEHICLE LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



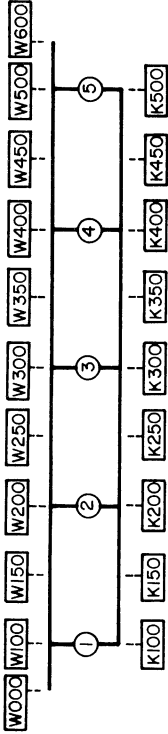
NORMALIZED VEHICLE LOAD APPLIED AT

GAGE TYPE	GAGE LOC.	1C+4C		2C+3C		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000								
K	K100	-91	-144	-79	-138	-79	-132		
K	K150	-88	-106	-80	-77				
K	K200	-72	-73	-104	-112				
K	K250	-94	-92	-84	-86				
K	K300	-80	-80	-119	-122				
K	K350	-93	-75	-93	-88				
K	K400	-75	-69	-167	-161				
K	K450	-69	-49	-119	-127				
K	K500			-149	-151				
K	K600			-49	-93				
W	W100	278	282	265	270				
W	W150	213	208	230	198				
W	W200	264	258	269	258				
W	W250	245	211	227	222				
W	W300	241	239	330	334				
W	W350	196	187	274	288				
W	W400	207	202	407	410				
W	W450	227	190	316	314				
W	W500	211	207	517	513				

LOAD	PX (KIPS)	-41.2
LOAD	PY (KIPS)	-42.0
ACTUAL	PX (KIPS)	-41.7
ACTUAL	PY (KIPS)	-41.3

TABLE 23D

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR VEHICLE LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.



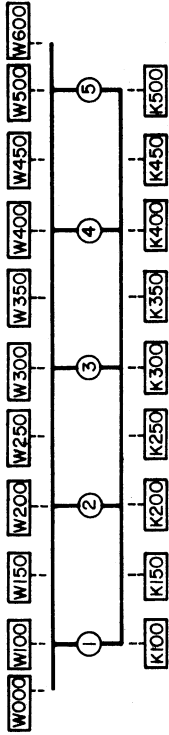
SECTION B  
 TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

NORMALIZED VEHICLE LOAD APPLIED AT  
 2C+3C

GAGE TYPE	GAGE LOC.	1C+4C		2C+3C		*****		*****	
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR
W	W000		293	293		207	207		
W	W100		268	271		230	234		
W	W150		221	240		187	210		
W	W200		268	270		282	278		
W	W250		210	228		222	252		
W	W300		272	274		271	288		
W	W350		196	222		220	253		
W	W400		238	246		259	257		
W	W450		207	244		233	265		
W	W500		192	193		236	241		
W	W600		190	190		257	257		
K	K100		-164	-168		-143	-146		
K	K150		-165	-151		-119	-119		
K	K200		-129	-127		-155	-149		
K	K250		-102	-112		-141	-123		
K	K300		-127	-127		-123	-126		
K	K350		-135	-136		-115	-115		
K	K400		-127	-128		-117	-115		
K	K450		-116	-123		-141	-139		
K	K500		-116	-114		-136	-135		
LOAD	PX (KIPS)		-41.2			-41.2			
LOAD	PY (KIPS)		-40.4			-42.0			
ACTUAL	PX (KIPS)		-41.7			-40.6			
ACTUAL	PY (KIPS)		-40.9			-41.3			

TABLE 23E

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR VEHICLE LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.



SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

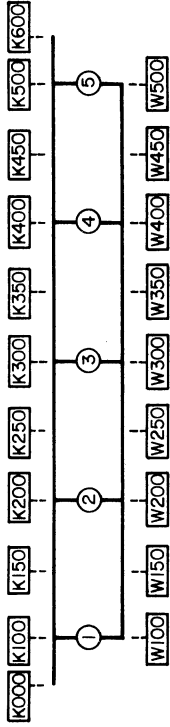
NORMALIZED VEHICLE LOAD APPLIED AT

GAGE TYPE	GAGE LOC.	IC+4C		2C+3C		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	172	172	304	304				
W	W100	174	171	273	280				
W	W150	161	162	232	257				
W	W200	267	268	305	307				
W	W250	190	190	222	231				
W	W300	295	299	275	272				
W	W350	194	214	176	191				
W	W400	319	321	259	269				
W	W450	218	222	184	198				
W	W500	273	273	191	186				
W	W600	287	287	177	177				
K	K100	-133	-133	-166	-166				
K	K150	-105	-94	-141	-150				
K	K200	-109	-106	-150	-153				
K	K250	-110	-124	-141	-140				
K	K300	-120	-118	-134	-133				
K	K350	-170	-164	-120	-119				
K	K400	-131	-138	-112	-110				
K	K450	-125	-138	-154	-149				
K	K500	-167	-163	-123	-121				
LOAD	PX (KIPS)	-41.2	-41.2	-41.2	-41.2				
LOAD	PY (KIPS)	-40.4	-40.4	-42.0	-42.0				
ACTUAL	PX (KIPS)	-41.7	-41.7	-40.6	-40.6				
ACTUAL	PY (KIPS)	-40.9	-40.9	-41.3	-41.3				

TABLE 23F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR VEHICLE LOADS APPLIED AFTER 30 KSI COND. LOADING. SIMPLY SUPPORTED NO RESTRAINT.



SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

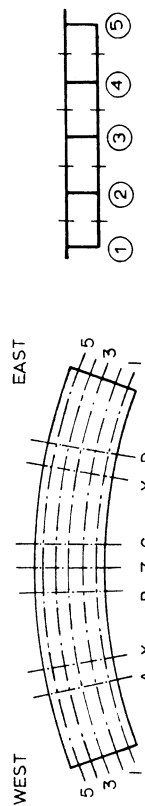
NORMALIZED VEHICLE LOAD APPLIED AT

GAGE TYPE	GAGE LOC.	IC+4C		2C+3C		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	-29	-29	-64	-140				
K	K100	-54	-56	-140	-144				
K	K150	-102	-98	-153	-149				
K	K200	-89	-86	-152	-146				
K	K250	-91	-101	-76	-87				
K	K300	-99	-103	-98	-105				
K	K350	-124	-138	-98	-100				
K	K400	-112	-108	-69	-65				
K	K450	-167	-148	-94	-84				
K	K500	-131	-132	-62	-61				
K	K600	-61	-131	-19	-62				
W	W100	158	160	384	386				
W	W150	197	183	359	335				
W	W200	217	213	414	406				
W	W250	216	206	262	247				
W	W300	246	247	225	227				
W	W350	286	272	176	175				
W	W400	369	356	185	182				
W	W450	305	301	149	147				
W	W500	330	345	181	184				
LOAD	PX (KIPS)	-41.2		-41.2					
LOAD	PY (KIPS)	-40.4		-42.0					
ACTUAL	PX (KIPS)	-41.7		-40.6					
ACTUAL	PY (KIPS)	-40.9		-41.3					



TABLE 23G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
RESULTS FOR VEHICLE LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



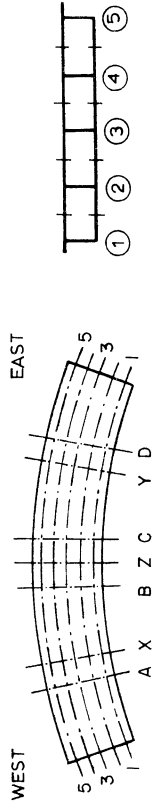
SECTION	GIRDER	1C+4C		2C+3C		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	20.6	15.5	19.6	10.6	19.6	10.6	19.6	10.6
A	2	34.5	26.0	34.1	18.4	34.1	18.4	34.1	18.4
A	3	31.6	23.8	42.4	22.9	42.4	22.9	42.4	22.9
A	4	28.8	21.7	52.5	28.4	52.5	28.4	52.5	28.4
A	5	17.2	13.0	36.4	19.7	36.4	19.7	36.4	19.7
A	SUM	132.8		185.1		185.1		185.1	
B	1	-31.8	18.5	-26.4	14.7	-26.4	14.7	-26.4	14.7
B	2	-38.2	22.2	-38.3	21.4	-38.3	21.4	-38.3	21.4
B	3	-39.6	23.0	-43.6	24.3	-43.6	24.3	-43.6	24.3
B	4	-36.5	21.2	-39.9	22.3	-39.9	22.3	-39.9	22.3
B	5	-25.9	15.1	-31.1	17.3	-31.1	17.3	-31.1	17.3
B	SUM	-172.1		-179.2		-179.2		-179.2	
C	1	-21.5	12.1	-37.3	19.9	-37.3	19.9	-37.3	19.9
C	2	-36.4	20.5	-46.3	24.7	-46.3	24.7	-46.3	24.7
C	3	-41.1	23.2	-40.0	21.3	-40.0	21.3	-40.0	21.3
C	4	-44.4	25.0	-38.8	20.7	-38.8	20.7	-38.8	20.7
C	5	-34.0	19.2	-25.0	13.4	-25.0	13.4	-25.0	13.4
C	SUM	-177.4		-187.4		-187.4		-187.4	
D	1	13.6	9.3	28.8	20.0	28.8	20.0	28.8	20.0
D	2	28.5	19.5	49.3	34.2	49.3	34.2	49.3	34.2
D	3	32.4	22.2	28.7	20.0	28.7	20.0	28.7	20.0
D	4	45.5	31.2	23.7	16.5	23.7	16.5	23.7	16.5
D	5	25.8	17.7	13.4	9.3	13.4	9.3	13.4	9.3
D	SUM	145.8		143.9		143.9		143.9	
LOAD	PX (KIPS)	-41.2		-41.2		-41.2		-41.2	
LOAD	PY (KIPS)	-40.4		-40.4		-40.4		-40.4	
ACTUAL	PX (KIPS)	-41.7		-40.6		-40.6		-40.6	
ACTUAL	PY (KIPS)	-40.9		-41.3		-41.3		-41.3	

TABLE 23H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR VEHICLE LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.

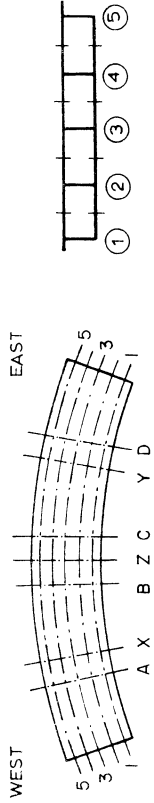


NORMALIZED VEHICLE LOAD APPLIED AT  
2C+3C

SECTION	GIRDER	1C+4C		2C+3C		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	32.9	24.1	30.4	18.1	30.4	18.1	30.4	18.1
A	2	29.4	21.5	29.6	17.6	29.6	17.6	29.6	17.6
A	3	26.0	19.1	31.1	18.5	31.1	18.5	31.1	18.5
A	4	28.6	21.0	40.8	24.3	40.8	24.3	40.8	24.3
A	5	19.6	14.3	36.0	21.4	36.0	21.4	36.0	21.4
A	SUM	136.6		167.9		167.9		167.9	
B	1	-27.8	17.5	-22.5	14.6	-22.5	14.6	-22.5	14.6
B	2	-36.6	23.0	-38.3	24.8	-38.3	24.8	-38.3	24.8
B	3	-37.4	23.5	-36.2	23.4	-36.2	23.4	-36.2	23.4
B	4	-37.3	23.4	-34.3	22.2	-34.3	22.2	-34.3	22.2
B	5	-20.1	12.6	-23.4	15.1	-23.4	15.1	-23.4	15.1
B	SUM	-159.2		-154.7		-154.7		-154.7	
C	1	-20.5	13.0	-27.3	16.1	-27.3	16.1	-27.3	16.1
C	2	-30.0	18.9	-43.2	25.5	-43.2	25.5	-43.2	25.5
C	3	-40.1	25.3	-40.2	23.7	-40.2	23.7	-40.2	23.7
C	4	-41.8	26.3	-35.0	20.6	-35.0	20.6	-35.0	20.6
C	5	-26.2	16.5	-24.0	14.2	-24.0	14.2	-24.0	14.2
C	SUM	-158.6		-169.7		-169.7		-169.7	
D	1	16.1	11.2	36.5	26.2	36.5	26.2	36.5	26.2
D	2	26.5	18.4	35.7	25.6	35.7	25.6	35.7	25.6
D	3	31.8	22.0	27.6	19.8	27.6	19.8	27.6	19.8
D	4	35.0	24.2	22.3	16.0	22.3	16.0	22.3	16.0
D	5	34.9	24.2	17.2	12.4	17.2	12.4	17.2	12.4
D	SUM	144.3		139.3		139.3		139.3	
LOAD	PX (KIPS)	-41.2		-41.2		-41.2		-41.2	
LOAD	PY (KIPS)	-40.4		-40.4		-40.4		-40.4	
ACTUAL	PX (KIPS)	-41.7		-40.6		-40.6		-40.6	
ACTUAL	PY (KIPS)	-40.9		-41.3		-41.3		-41.3	

TABLE 231

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )  
 MOMENTS ABOUT ENTIRE CROSS SECTION N.A.  
 RESULTS FOR VEHICLE LOADS APPLIED  
 AFTER 30 KSI COND. LOADING.  
 SIMPLY SUPPORTED NO RESTRAINT.



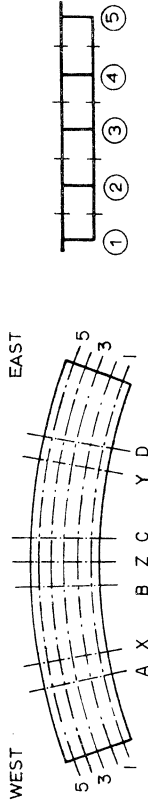
SECTION	GIRDER	1C+4C		2C+3C		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	26.1	19.4	24.4	13.8	24.4	13.8	24.4	13.8
	2	32.3	24.0	32.1	18.1	32.1	18.1	32.1	18.1
	3	29.1	21.7	37.3	21.0	37.3	21.0	37.3	21.0
	4	28.7	21.4	47.3	26.7	47.3	26.7	47.3	26.7
	5	18.3	13.6	36.2	20.4	36.2	20.4	36.2	20.4
	SUM	134.5		177.5		177.5		177.5	
B	1	-29.6	17.9	-24.2	14.6	-24.2	14.6	-24.2	14.6
	2	-37.3	22.6	-38.3	23.1	-38.3	23.1	-38.3	23.1
	3	-38.4	23.3	-39.5	23.8	-39.5	23.8	-39.5	23.8
	4	-37.0	22.4	-36.8	22.2	-36.8	22.2	-36.8	22.2
	5	-22.7	13.8	-26.8	16.2	-26.8	16.2	-26.8	16.2
	SUM	-165.0		-165.7		-165.7		-165.7	
C	1	-21.0	12.5	-31.7	17.9	-31.7	17.9	-31.7	17.9
	2	-32.9	19.7	-44.6	25.1	-44.6	25.1	-44.6	25.1
	3	-40.6	24.3	-40.1	22.6	-40.1	22.6	-40.1	22.6
	4	-43.0	25.7	-36.7	20.7	-36.7	20.7	-36.7	20.7
	5	-29.7	17.8	-24.5	13.8	-24.5	13.8	-24.5	13.8
	SUM	-167.1		-177.6		-177.6		-177.6	
D	1	14.7	10.2	32.3	22.7	32.3	22.7	32.3	22.7
	2	27.6	19.0	43.2	30.5	43.2	30.5	43.2	30.5
	3	32.2	22.1	28.2	19.9	28.2	19.9	28.2	19.9
	4	40.8	28.1	23.1	16.3	23.1	16.3	23.1	16.3
	5	29.9	20.6	15.1	10.6	15.1	10.6	15.1	10.6
	SUM	145.2		141.9		141.9		141.9	
LOAD	PX (KIPS)	-41.2		-41.2		-41.2		-41.2	
LOAD	PY (KIPS)	-40.4		-40.4		-40.4		-40.4	
ACTUAL	PX (KIPS)	-41.7		-40.6		-40.6		-40.6	
ACTUAL	PY (KIPS)	-40.9		-41.3		-41.3		-41.3	

TABLE 23J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR VEHICLE LOADS APPLIED  
AFTER 30 KSI COND. LOADING.  
SIMPLY SUPPORTED NO RESTRAINT.



SECTION	GIRDER	1C+4C		2C+3C		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
	A	24.6	18.4	23.2	12.8	23.2	12.8		
	A	33.0	24.6	32.8	18.1	32.8	18.1		
	A	30.1	22.4	39.3	21.8	39.3	21.8		
	A	28.7	21.4	49.2	27.2	49.2	27.2		
	A	17.8	13.3	36.3	20.1	36.3	20.1		
	A	134.3		180.8		180.8			
	B	-30.3	18.1	-24.9	14.6	-24.9	14.6		
	B	-37.7	22.5	-38.3	22.4	-38.3	22.4		
	B	-38.9	23.2	-41.3	24.2	-41.3	24.2		
	B	-36.8	22.0	-38.2	22.3	-38.2	22.3		
	B	-23.8	14.2	-28.3	16.6	-28.3	16.6		
	B	-167.4		-171.0		-171.0			
	C	-21.1	12.3	-33.5	18.5	-33.5	18.5		
	C	-34.6	20.2	-45.3	25.0	-45.3	25.0		
	C	-40.8	23.9	-40.0	22.1	-40.0	22.1		
	C	-43.6	25.5	-37.7	20.8	-37.7	20.8		
	C	-31.1	18.2	-24.6	13.6	-24.6	13.6		
	C	-171.2		-181.2		-181.2			
	D	14.3	9.8	30.9	21.7	30.9	21.7		
	D	27.9	19.1	45.7	32.0	45.7	32.0		
	D	32.2	22.1	28.4	19.9	28.4	19.9		
	D	43.1	29.5	23.4	16.4	23.4	16.4		
	D	28.3	19.4	14.3	10.0	14.3	10.0		
	D	145.8		142.6		142.6			
LOAD	PX (KIPS)	-41.2		-41.2		-41.2			
LOAD	PY (KIPS)	-40.4		-42.0		-42.0			
ACTUAL	PX (KIPS)	-41.7		-40.6		-40.6			
ACTUAL	PY (KIPS)	-40.9		-41.3		-41.3			

LOAD PX (KIPS)  
LOAD PY (KIPS)  
ACTUAL PX (KIPS)  
ACTUAL PY (KIPS)

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR 24 KSI, 30 KSI, 40 KSI  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS CONDITIONING LOAD STRESS LEVELS  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS

REACTION OR LOAD	CONDITIONING LOAD STRESS LEVEL					
	24 KSI		30 KSI		40 KSI	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	3.30	1.27	3.30	.76	3.30	2.14
2E	5.70	8.68	5.70	7.81	5.70	7.24
3E	4.90	6.23	4.90	7.50	4.90	5.93
4E	6.45	2.22	6.45	2.92	6.45	2.86
5E	10.44	11.79	10.44	10.09	10.44	10.91
1F	34.46	35.30	34.46	33.72	34.46	35.05
2F	34.77	31.56	34.77	32.35	34.77	33.60
3F	34.75	34.53	34.75	35.99	34.75	33.80
4F	34.45	38.04	34.45	36.64	34.45	33.96
1W	3.07	4.40	3.07	4.03	3.07	5.63
2W	5.78	2.19	5.78	4.10	5.78	1.79
3W	5.16	7.86	5.16	5.21	5.16	5.23
4W	6.60	6.20	6.60	8.17	6.60	7.04
5W	10.18	10.55	10.18	10.03	10.18	10.28
RE	30.79	30.19	30.79	29.08	30.79	29.08
PF	138.43	139.43	138.43	138.70	138.43	136.41
PW	30.79	31.20	30.79	31.54	30.79	29.97
SUMR	200.01	200.82	200.01	199.32	200.01	195.46
PX	-100.00	-100.00	-100.00	-100.00	-100.00	-100.00
PY	-100.00	-97.76	-100.00	-96.28	-100.00	-99.97
SUMP	-200.00	-197.76	-200.00	-196.28	-200.00	-199.97
SUMR/SUMP	1.00	1.02	1.00	1.02	1.00	.98
TW	38.70	41.96	38.70	41.35	38.70	37.44
MF	-.04	8.57	-.04	9.84	-.04	-1.34
TF	-.91	10.88	-.91	3.04	-.91	2.42
TE	38.67	37.51	38.67	35.43	38.67	33.86
ACTUAL PX		-7.74		-11.47		-17.57
ACTUAL PY		-7.57		-11.00		-17.57

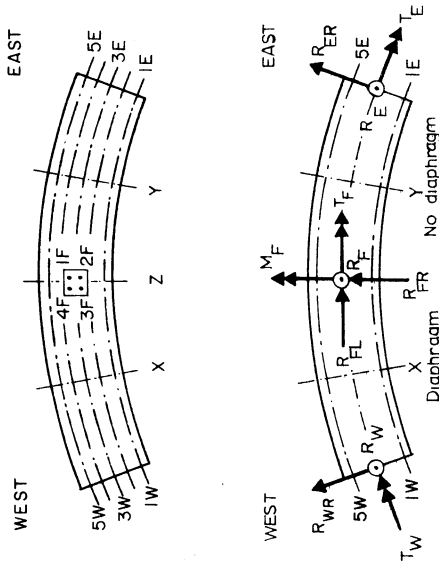
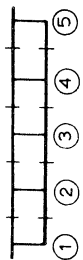
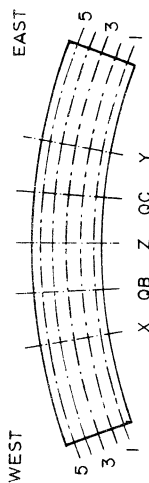


TABLE 24B

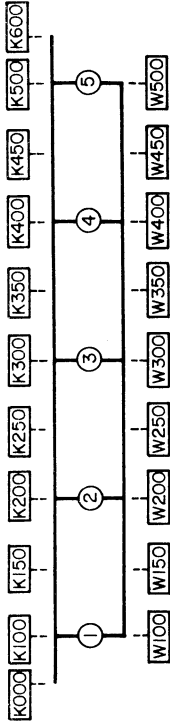
SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR 24 KSI, 30 KSI, 40 KSI  
 CONDITIONING LOAD STRESS LEVELS  
 SIMPLY SUPPORTED, NO RESTRAINTS



DEFLECTION AT POINT	24 KSI			30 KSI			40 KSI		
	THEORY	EXPERM	E/T	THEORY	EXPERM	E/T	THEORY	EXPERM	E/T
1X	.476	.623	1.31	.476	.694	1.46	.476	.736	1.55
2X	.491	.654	1.33	.491	.729	1.48	.491	.778	1.59
3X	.511	.691	1.35	.511	.766	1.50	.511	.820	1.61
4X	.537	.718	1.34	.537	.795	1.48	.537	.862	1.60
5X	.569	.746	1.31	.569	.825	1.45	.569	.912	1.60
1QB	.226	.298	1.31	.226	.336	1.49	.226	.345	1.53
2QB	.226	.309	1.37	.226	.337	1.49	.226	.353	1.56
3QB	.230	.312	1.36	.230	.347	1.51	.230	.360	1.56
4QB	.246	.329	1.34	.246	.367	1.49	.246	.389	1.58
5QB	.267	.343	1.29	.267	.372	1.39	.267	.409	1.53
1Z	.030	.048	1.58	.030	.061	2.00	.030	.066	2.17
2Z	.016	.025	1.60	.016	.026	1.69	.016	.036	2.26
4Z	.014	.023	1.66	.014	.026	1.81	.014	.024	1.71
5Z	.027	.044	1.65	.027	.047	1.76	.027	.054	2.02
1QC	.230	.291	1.26	.230	.321	1.39	.230	.376	1.63
2QC	.228	.290	1.28	.228	.318	1.40	.228	.370	1.62
3QC	.230	.284	1.24	.230	.315	1.37	.230	.366	1.59
4QC	.245	.312	1.27	.245	.339	1.38	.245	.396	1.61
5QC	.267	.331	1.24	.267	.350	1.31	.267	.424	1.59
1Y	.486	.630	1.30	.486	.685	1.41	.486	.809	1.67
2Y	.493	.621	1.26	.493	.680	1.38	.493	.797	1.62
3Y	.509	.643	1.26	.509	.702	1.38	.509	.814	1.60
4Y	.534	.678	1.27	.534	.734	1.37	.534	.862	1.61
5Y	.567	.713	1.26	.567	.777	1.37	.567	.924	1.63
LOAD PX	-100.0	-100.0		-100.0	-100.0		-100.0	-100.0	
LOAD PY	-100.0	-97.8		-100.0	-96.3		-100.0	-100.0	
ACTUAL PX		-7.7			-11.5			-17.6	
ACTUAL PY		-7.6			-11.1			-17.6	

TABLE 24C

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR 24 KSI, 30 KSI, 40 KSI  
 CONDITIONING LOAD STRESS LEVELS  
 SIMPLY SUPPORTED, NO RESTRAINTS



SECTION A

TENSION = +      K = CONCRETE STRAIN METERS  
 COMPRESSION = -      W = WELDABLE STRAIN GAGES

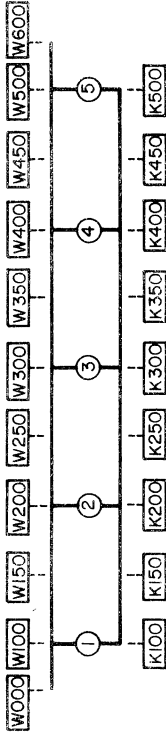
GAGE TYPE	GAGE LOC.	24 KSI			30 KSI			40 KSI		
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
K	K000	-269	-218	-218	-269	-221	-221	-269	-232	-232
K	K100	-228	-342	-334	-228	-354	-346	-228	-379	-368
K	K150	-200	-254	-257	-200	-266	-270	-200	-275	-253
K	K200	-207	-301	-314	-200	-309	-323	-200	-289	-299
K	K250	-207	-246	-248	-207	-254	-256	-207	-254	-252
K	K300	-197	-301	-297	-207	-309	-304	-207	-297	-295
K	K350	-197	-260	-264	-197	-278	-278	-197	-264	-266
K	K400	-216	-316	-318	-216	-324	-326	-216	-311	-310
K	K450	-245	-258	-282	-245	-272	-295	-245	-257	-279
K	K500	-245	-277	-279	-245	-285	-287	-245	-269	-273
K	K600	-245	-178	-178	-245	-182	-182	-245	-182	-182
W	W100	880	870	833	880	878	839	880	840	816
W	W150	766	632	493	766	688	550	766	710	610
W	W200	808	788	769	808	804	789	808	759	749
W	W250	752	644	572	752	693	628	752	711	669
W	W300	814	788	770	808	826	799	808	830	810
W	W350	882	640	601	752	677	625	752	696	676
W	W400	882	718	733	814	751	770	814	777	788
W	W450	882	651	617	814	701	672	814	730	711
W	W500	882	895	882	814	910	899	814	894	896
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-97.8	-96.3	-100.0	-96.3	-96.3	-100.0	-100.0	-100.0
ACTUAL	PX (KIPS)		-7.7	-7.7		-11.5	-11.5		-17.6	-17.6
ACTUAL	PY (KIPS)		-7.6	-7.6		-11.1	-11.1		-17.6	-17.6

TABLE 24D

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR 24 KSI, 30 KSI, 40 KSI  
 CONDITIONING LOAD STRESS LEVELS  
 SIMPLY SUPPORTED, NO RESTRAINTS

SECTION B

TENSION + + K = CONCRETE STRAIN METERS  
 COMPRESSION - - W = WELDABLE STRAIN GAGES

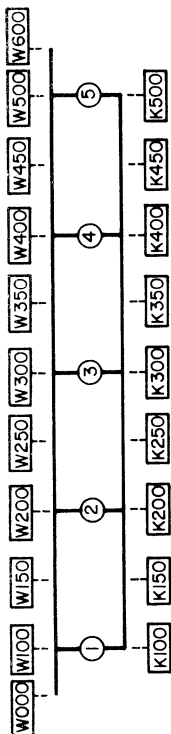


CONDITIONING LOAD STRESS LEVEL

GAGE TYPE	GAGE LOC.	24 KSI		30 KSI		40 KSI		MEASR	ADJUST
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR		
W	W000	675	387	675	442	675	442	550	550
W	W100	625	628	625	645	625	655	652	662
W	W150	507	507	532	532	532	601	561	628
W	W200	532	664	532	707	532	719	708	722
W	W250	571	560	600	600	600	579	625	656
W	W300	526	673	526	712	526	715	754	761
W	W350	539	608	564	646	533	651	615	708
W	W400	533	620	637	651	533	651	662	679
W	W450	567	578	592	599	611	599	619	666
W	W500	611	529	552	536	611	536	604	596
W	W600	624	537	624	578	624	578	621	621
K	K100	-285	-375	-285	-376	-285	-382	-385	-396
K	K150	-393	-377	-248	-395	-248	-378	-403	-375
K	K200	-248	-378	-248	-385	-248	-377	-398	-383
K	K250	-368	-357	-217	-368	-217	-356	-379	-364
K	K300	-217	-375	-217	-374	-217	-377	-386	-391
K	K350	-361	-364	-249	-385	-249	-378	-374	-375
K	K400	-330	-331	-274	-340	-249	-339	-346	-345
K	K450	-337	-343	-274	-351	-274	-355	-361	-364
K	K500	-311	-308	-274	-318	-274	-315	-334	-331
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0
LOAD	PV (KIPS)	-100.0	-97.8	-100.0	-96.3	-100.0	-100.0	-100.0	-100.0
ACTUAL	PX (KIPS)	-7.7	-7.6	-11.5	-11.5	-17.6	-17.6	-17.6	-17.6
ACTUAL	PV (KIPS)	-7.6	-7.6	-11.1	-11.1	-17.6	-17.6	-17.6	-17.6



SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR 24 KSI, 30 KSI, 40 KSI  
 CONDITIONING LOAD STRESS LEVELS  
 SIMPLY SUPPORTED, NO RESTRAINTS



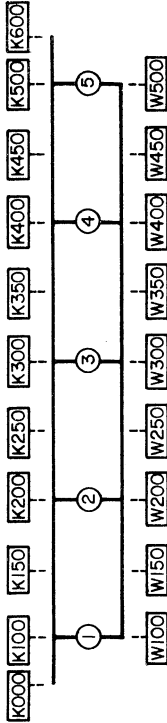
SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	24 KSI		30 KSI		40 KSI	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	680	544	680	641	680	688
W	W100	629	553	629	598	629	658
W	W150	533	497	533	535	533	577
W	W200	552	607	533	586	533	741
W	W250	552	546	526	576	587	615
W	W300	732	717	526	781	526	804
W	W350	498	536	532	575	532	604
W	W400	607	633	532	611	532	722
W	W450	497	523	609	527	609	585
W	W500	540	532	621	572	621	649
W	W600	544	544	621	577	621	627
K	K100	-287	-372	-287	-379	-287	-393
K	K150	-339	-332	-343	-335	-341	-343
K	K200	-248	-375	-248	-373	-248	-376
K	K250	-376	-399	-366	-399	-360	-399
K	K300	-216	-383	-369	-379	-358	-369
K	K350	-424	-408	-384	-412	-377	-405
K	K400	-248	-335	-425	-342	-411	-342
K	K450	-381	-377	-340	-385	-334	-391
K	K500	-273	-332	-386	-339	-381	-357
K	K550	-343	-329	-343	-339	-273	-364
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-97.8	-100.0	-96.3	-100.0	-100.0
ACTUAL	PX (KIPS)	-7.7	-7.7	-11.5	-11.5	-17.6	-17.6
ACTUAL	PY (KIPS)	-7.6	-7.6	-11.1	-11.1	-17.6	-17.6

TABLE 24F

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR 24 KSI, 30 KSI, 40 KSI  
 CONDITIONING LOAD STRESS LEVELS  
 SIMPLY SUPPORTED, NO RESTRAINTS



SECTION D

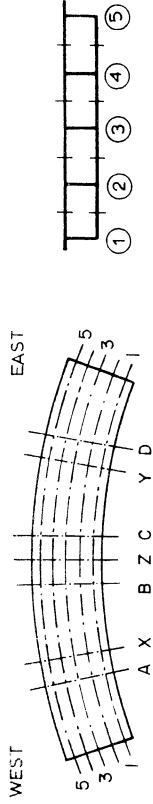
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	24 KSI		30 KSI		40 KSI	
		THEORY	MEASR ADJUST	THEORY	MEASR ADJUST	THEORY	MEASR ADJUST
K	K000	-241	-148	-241	-144	-241	-171
K	K100	-204	-237	-204	-236	-204	-243
K	K150	-177	-367	-177	-346	-177	-321
K	K200	-183	-290	-183	-290	-183	-288
K	K250	-173	-265	-173	-264	-173	-293
K	K300	-190	-271	-190	-274	-190	-280
K	K350	-216	-320	-216	-331	-216	-337
K	K400	889	-274	889	-259	889	-282
K	K450	771	-345	771	-347	771	-346
K	K500	806	-372	806	-300	806	-284
K	K600	746	-296	746	-137	746	-153
W	W100	889	571	889	609	889	672
W	W150	771	646	771	698	771	755
W	W200	806	778	806	791	806	804
W	W250	746	696	746	708	746	738
W	W300	808	611	808	669	808	700
W	W350	655	607	655	711	655	828
W	W400	808	640	808	646	808	816
W	W450	688	808	688	822	688	855
W	W500	718	655	718	800	718	877
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-97.8	-100.0	-96.3	-100.0	-100.0
ACTUAL	PX (KIPS)		-7.7		-11.5		-17.6
ACTUAL	PY (KIPS)		-7.6		-11.1		-17.6

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR 24 KSI, 30 KSI, 40 KSI  
CONDITIONING LOAD STRESS LEVELS  
SIMPLY SUPPORTED, NO RESTRAINTS



CONDITIONING LOAD STRESS LEVEL

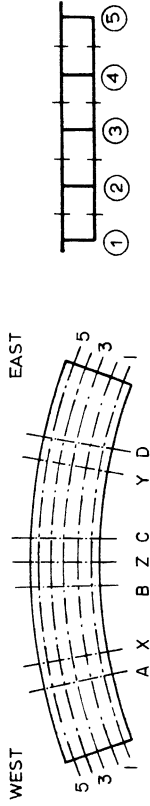
SECTION	GIRDER	24 KSI			30 KSI			40 KSI					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	76.9	17.0	59.0	13.7	76.9	17.0	59.1	13.5	76.9	17.0	55.5	13.4
A	2	102.4	22.7	99.3	23.0	102.4	22.7	101.1	23.2	102.4	22.7	94.3	22.7
A	3	100.2	22.2	101.7	23.6	100.2	22.2	102.7	23.5	100.2	22.2	98.8	23.8
A	4	100.2	22.2	102.9	23.8	100.2	22.2	104.7	24.0	100.2	22.2	101.4	24.4
A	5	72.2	16.0	68.5	15.9	72.2	16.0	68.6	15.7	72.2	16.0	64.8	15.6
A	SUM	451.8		431.4		451.8		436.2		451.8		414.8	
B	1	-80.4	16.5	-73.7	16.3	-80.4	16.5	-72.5	16.4	-80.4	16.5	-78.6	16.0
B	2	-110.1	22.5	-99.6	22.0	-110.1	22.5	-98.1	22.2	-110.1	22.5	-106.4	21.7
B	3	-110.7	22.6	-108.0	23.9	-110.7	22.6	-105.5	23.9	-110.7	22.6	-119.3	24.3
B	4	-109.8	22.5	-99.5	22.0	-109.8	22.5	-97.4	22.0	-109.8	22.5	-108.4	22.1
B	5	-77.8	15.9	-70.8	15.7	-77.8	15.9	-68.5	15.5	-77.8	15.9	-78.7	16.0
B	SUM	-488.7		-451.6		-488.7		-442.0		-488.7		-491.5	
C	1	-80.8	16.5	-73.2	16.2	-80.8	16.5	-78.2	15.8	-80.8	16.5	-86.6	16.7
C	2	-110.3	22.6	-97.9	21.7	-110.3	22.6	-97.6	21.0	-110.3	22.6	-114.1	22.0
C	3	-110.6	22.6	-107.4	23.8	-110.6	22.6	-113.2	24.3	-110.6	22.6	-120.7	23.3
C	4	-109.5	22.4	-100.1	22.2	-109.5	22.4	-99.9	21.5	-109.5	22.4	-113.1	21.8
C	5	-77.5	15.9	-72.9	16.1	-77.5	15.9	-76.7	16.5	-77.5	15.9	-84.6	16.3
C	SUM	-488.7		-451.5		-488.7		-465.6		-488.7		-519.0	
D	1	77.7	17.2	52.3	12.5	77.7	17.2	51.8	12.8	77.7	17.2	53.9	13.3
D	2	103.0	22.8	108.8	25.9	103.0	22.8	102.9	25.4	103.0	22.8	99.7	24.7
D	3	100.0	22.1	90.5	21.6	100.0	22.1	91.4	22.6	100.0	22.1	94.4	23.4
D	4	99.5	22.0	109.3	26.0	99.5	22.0	102.8	25.4	99.5	22.0	103.0	25.5
D	5	71.7	15.9	58.9	14.0	71.7	15.9	55.7	13.8	71.7	15.9	53.3	13.2
D	SUM	451.8		419.7		451.8		404.6		451.8		404.1	
LJAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0		-100.0		-100.0	
LOAD	PY (KIPS)	-100.0		-97.8		-100.0		-96.3		-100.0		-100.0	
ACTUAL	PX (KIPS)	-7.7		-7.7		-11.5		-11.5		-17.6		-17.6	
ACTUAL	PY (KIPS)	-7.6		-7.6		-11.1		-11.1		-17.6		-17.6	

TABLE 24H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR 24 KSI, 30 KSI, 40 KSI  
CONDITIONING LOAD STRESS LEVELS  
SIMPLY SUPPORTED, NO RESTRAINTS

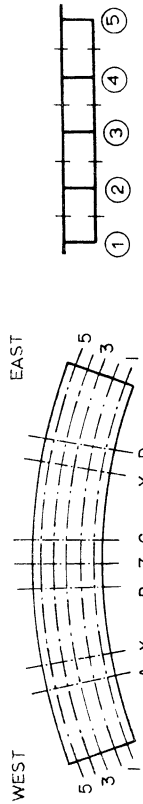


SECTION	GIRDER	24 KSI			30 KSI			40 KSI					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	76.9	17.0	83.8	19.4	76.9	17.0	85.0	19.5	76.9	17.0	87.1	21.0
A	2	102.4	22.7	90.1	20.9	102.4	22.7	91.0	20.9	102.4	22.7	83.9	20.2
A	3	100.2	22.2	87.6	20.3	100.2	22.2	88.3	20.3	100.2	22.2	84.1	20.3
A	4	100.2	22.2	95.9	22.2	100.2	22.2	97.1	22.3	100.2	22.2	90.1	21.7
A	5	72.2	16.0	73.9	17.1	72.2	16.0	74.8	17.1	72.2	16.0	69.9	16.9
A	SUM	451.8		431.3		451.8		436.3		451.8		415.1	
B	1	-80.4	16.5	-66.5	14.7	-80.4	16.5	-64.6	14.6	-80.4	16.5	-72.0	14.6
B	2	-110.1	22.5	-110.6	24.5	-110.1	22.5	-106.3	24.0	-110.1	22.5	-117.6	23.9
B	3	-110.7	22.6	-115.5	25.6	-110.7	22.6	-112.6	25.5	-110.7	22.6	-125.5	25.5
B	4	-109.8	22.5	-101.9	22.6	-109.8	22.5	-101.7	23.0	-109.8	22.5	-112.3	22.8
B	5	-77.8	15.9	-57.1	12.6	-77.8	15.9	-56.8	12.9	-77.8	15.9	-64.2	13.1
B	SUM	-488.7		-451.6		-488.7		-442.0		-488.7		-491.5	
C	1	-80.8	16.5	-60.5	13.4	-80.8	16.5	-62.2	13.4	-80.8	16.5	-70.5	13.6
C	2	-110.3	22.6	-107.0	23.7	-110.3	22.6	-109.5	23.5	-110.3	22.6	-121.8	23.4
C	3	-110.6	22.6	-118.9	26.3	-110.6	22.6	-121.2	26.0	-110.6	22.6	-133.2	25.6
C	4	-109.5	22.4	-104.9	23.2	-109.5	22.4	-109.9	23.6	-109.5	22.4	-121.4	23.4
C	5	-77.5	15.9	-60.4	13.4	-77.5	15.9	-62.8	13.5	-77.5	15.9	-72.6	14.0
C	SUM	-488.7		-451.6		-488.7		-465.6		-488.7		-519.4	
D	1	77.7	17.2	67.6	16.1	77.7	17.2	63.9	15.8	77.7	17.2	65.6	16.2
D	2	103.0	22.8	89.4	21.3	103.0	22.8	85.0	21.0	103.0	22.8	87.8	21.7
D	3	100.0	22.1	89.8	21.4	100.0	22.1	86.3	21.3	100.0	22.1	91.4	22.6
D	4	99.5	22.0	88.6	21.1	99.5	22.0	87.8	21.7	99.5	22.0	88.0	21.8
D	5	71.7	15.9	84.2	20.1	71.7	15.9	81.7	20.2	71.7	15.9	71.3	17.6
D	SUM	451.8		419.7		451.8		404.7		451.8		404.1	
LOAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0		-100.0		-100.0	
LOAD	PY (KIPS)	-100.0		-97.8		-100.0		-96.3		-100.0		-100.0	
ACTUAL	PX (KIPS)			-7.7				-11.5				-17.6	
ACTUAL	PY (KIPS)			-7.6				-11.1				-17.6	

TABLE 24

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR 24 KSI, 30 KSI, 40 KSI  
CONDITIONING LOAD STRESS LEVELS  
SIMPLY SUPPORTED, NO RESTRAINTS



CONDITIONING LOAD STRESS LEVEL

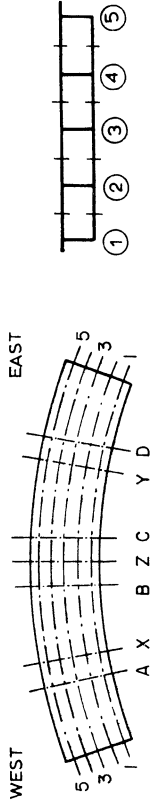
SECTION	GIRDER	24 KSI			30 KSI			40 KSI					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	76.9	17.0	70.1	16.2	76.9	17.0	70.7	16.2	76.9	17.0	69.6	16.8
A	2	102.4	22.7	95.2	22.1	102.4	22.7	96.6	22.1	102.4	22.7	89.7	21.6
A	3	100.2	22.2	95.4	22.1	100.2	22.2	96.3	22.1	100.2	22.2	92.3	22.2
A	4	100.2	22.2	99.8	23.1	100.2	22.2	101.4	23.2	100.2	22.2	96.4	23.2
A	5	72.2	16.0	70.9	16.4	72.2	16.0	71.4	16.4	72.2	16.0	67.1	16.2
A	SUM	451.8		431.5		451.8		436.3		451.8		415.1	
B	1	-80.4	16.5	-69.7	15.4	-80.4	16.5	-68.1	15.4	-80.4	16.5	-75.0	15.2
B	2	-110.1	22.5	-105.7	23.4	-110.1	22.5	-102.7	23.2	-110.1	22.5	-112.6	22.9
B	3	-110.7	22.6	-112.2	24.8	-110.7	22.6	-109.5	24.8	-110.7	22.6	-122.8	25.0
B	4	-109.8	22.5	-100.9	22.3	-109.8	22.5	-99.8	22.6	-109.8	22.5	-110.6	22.5
B	5	-77.8	15.9	-63.2	14.0	-77.8	15.9	-62.1	14.0	-77.8	15.9	-70.7	14.4
B	SUM	-488.7		-451.7		-488.7		-442.1		-488.7		-491.7	
C	1	-80.8	16.5	-66.2	14.6	-80.8	16.5	-69.3	14.9	-80.8	16.5	-77.7	15.0
C	2	-110.3	22.6	-102.9	22.8	-110.3	22.6	-104.2	22.4	-110.3	22.6	-118.4	22.8
C	3	-110.6	22.6	-113.8	25.2	-110.6	22.6	-117.7	25.3	-110.6	22.6	-127.6	24.6
C	4	-109.5	22.4	-102.8	22.8	-109.5	22.4	-105.5	22.6	-109.5	22.4	-117.8	22.7
C	5	-77.5	15.9	-66.0	14.6	-77.5	15.9	-69.0	14.8	-77.5	15.9	-78.0	15.0
C	SUM	-488.7		-451.7		-488.7		-465.7		-488.7		-519.4	
D	1	77.7	17.2	59.2	14.1	77.7	17.2	57.2	14.1	77.7	17.2	59.1	14.6
D	2	103.0	22.8	100.2	23.9	103.0	22.8	95.0	23.5	103.0	22.8	94.4	23.4
D	3	100.0	22.1	90.2	21.5	100.0	22.1	89.1	22.0	100.0	22.1	93.1	23.0
D	4	99.5	22.0	100.1	23.8	99.5	22.0	96.1	23.7	99.5	22.0	96.3	23.8
D	5	71.7	15.9	70.2	16.7	71.7	15.9	67.3	16.6	71.7	15.9	61.3	15.2
D	SUM	451.8		419.8		451.8		404.8		451.8		404.2	
LOAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0		-100.0		-100.0	
LOAD	PY (KIPS)	-100.0		-97.8		-100.0		-96.3		-100.0		-100.0	
ACTUAL	PX (KIPS)			-7.7				-11.5				-17.6	
ACTUAL	PY (KIPS)			-7.6				-11.1				-17.6	

TABLE 24J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR 24 KSI, 30 KSI, 40 KSI  
CONDITIONING LOAD STRESS LEVELS  
SIMPLY SUPPORTED, NO RESTRAINTS



SECTION	GIRDER	24 KSI						30 KSI						40 KSI					
		THEORY		EXPERIMENTAL		THEORY		EXPERIMENTAL		THEORY		EXPERIMENTAL		THEORY		EXPERIMENTAL			
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT		
A	1	76.9	17.0	66.1	15.3	76.9	17.0	66.7	15.3	76.9	17.0	65.3	15.7	76.9	17.0	65.3	15.7		
A	2	102.4	22.7	96.6	22.4	102.4	22.7	98.2	22.5	102.4	22.7	98.2	22.5	102.4	22.7	91.4	22.0		
A	3	100.2	22.2	97.8	22.7	100.2	22.2	98.7	22.6	100.2	22.2	98.7	22.6	100.2	22.2	94.9	22.8		
A	4	100.2	22.2	100.8	23.4	100.2	22.2	102.5	23.5	100.2	22.2	102.5	23.5	100.2	22.2	98.2	23.6		
A	5	72.2	16.0	69.8	16.2	72.2	16.0	70.1	16.1	72.2	16.0	70.1	16.1	72.2	16.0	66.0	15.9		
A	SUM	451.8		431.1		451.8		436.1		451.8		436.1		451.8		415.8			
B	1	-80.4	16.5	-71.0	15.7	-80.4	16.5	-69.6	15.8	-80.4	16.5	-69.6	15.8	-80.4	16.5	-76.1	15.5		
B	2	-110.1	22.5	-103.5	22.9	-110.1	22.5	-100.9	22.9	-110.1	22.5	-100.9	22.9	-110.1	22.5	-110.3	22.5		
B	3	-110.7	22.6	-110.7	24.5	-110.7	22.6	-108.0	24.5	-110.7	22.6	-108.0	24.5	-110.7	22.6	-121.4	24.7		
B	4	-109.8	22.5	-100.4	22.2	-109.8	22.5	-98.9	22.4	-109.8	22.5	-98.9	22.4	-109.8	22.5	-109.7	22.3		
B	5	-77.8	15.9	-65.7	14.6	-77.8	15.9	-64.2	14.5	-77.8	15.9	-64.2	14.5	-77.8	15.9	-73.6	15.0		
B	SUM	-488.7		-451.3		-488.7		-441.5		-488.7		-441.5		-488.7		-491.1			
C	1	-80.8	16.5	-68.1	15.1	-80.8	16.5	-72.0	15.5	-80.8	16.5	-72.0	15.5	-80.8	16.5	-80.6	15.6		
C	2	-110.3	22.6	-101.3	22.5	-110.3	22.6	-102.2	22.0	-110.3	22.6	-102.2	22.0	-110.3	22.6	-116.7	22.5		
C	3	-110.6	22.6	-111.4	24.7	-110.6	22.6	-115.8	24.9	-110.6	22.6	-115.8	24.9	-110.6	22.6	-124.6	24.1		
C	4	-109.5	22.4	-101.8	22.6	-109.5	22.4	-103.5	22.3	-109.5	22.4	-103.5	22.3	-109.5	22.4	-115.8	22.4		
C	5	-77.5	15.9	-68.1	15.1	-77.5	15.9	-71.5	15.4	-77.5	15.9	-71.5	15.4	-77.5	15.9	-80.3	15.5		
C	SUM	-488.7		-450.7		-488.7		-465.0		-488.7		-465.0		-488.7		-518.0			
D	1	77.7	17.2	56.8	13.5	77.7	17.2	55.2	13.6	77.7	17.2	55.2	13.6	77.7	17.2	57.0	14.1		
D	2	103.0	22.8	103.4	24.6	103.0	22.8	98.1	24.2	103.0	22.8	98.1	24.2	103.0	22.8	96.5	23.8		
D	3	100.0	22.1	90.3	21.4	100.0	22.1	89.9	22.2	100.0	22.1	89.9	22.2	100.0	22.1	93.6	23.1		
D	4	99.5	22.0	104.1	24.7	99.5	22.0	99.0	24.4	99.5	22.0	99.0	24.4	99.5	22.0	99.4	24.5		
D	5	71.7	15.9	66.3	15.8	71.7	15.9	63.3	15.6	71.7	15.9	63.3	15.6	71.7	15.9	58.4	14.4		
D	SUM	451.8		421.0		451.8		405.6		451.8		405.6		451.8		404.9			
LJAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0		-100.0		-100.0		-100.0		-100.0			
LJAD	PY (KIPS)	-100.0		-97.8		-100.0		-96.3		-100.0		-96.3		-100.0		-100.0			
ACTUAL	PX (KIPS)	-7.7		-7.7		-7.7		-11.5		-7.7		-11.5		-7.7		-17.6			
ACTUAL	PY (KIPS)	-7.6		-7.6		-7.6		-11.1		-7.6		-11.1		-7.6		-17.6			

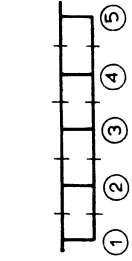


TABLE 25A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR 50 KSI, 60 KSI  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS CONDITIONING LOAD STRESS LEVELS  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS

REACTION OR LOAD	50 KSI		60 KSI		CONDITIONING LOAD STRESS LEVEL	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	3.30	-0.77	3.30	1.29		
2E	5.70	12.90	5.70	11.12		
3E	4.90	5.15	4.90	3.60		
4E	6.45	2.76	6.45	1.39		
5E	10.44	10.19	10.44	11.80		
1F	34.46	37.88	34.46	35.26		
2F	34.77	37.24	34.77	35.00		
3F	34.75	35.88	34.75	35.86		
4F	34.45	33.86	34.45	33.07		
1W	3.07	6.20	3.07	7.59		
2W	5.78	2.34	5.78	.41		
3W	5.16	4.92	5.16	2.13		
4W	6.60	6.55	6.60	13.39		
5W	10.18	11.84	10.18	6.54		
PE	30.79	30.23	30.79	29.20		
RF	138.43	144.86	138.43	139.19		
RW	30.79	31.85	30.79	30.06		
SUMR	200.01	206.94	200.01	198.45		
PX	-100.00	-100.00	-100.00	-100.00		
PY	-100.00	-107.39	-100.00	-102.84		
SUMP	-200.00	-207.39	-200.00	-202.84		
SUMR/SUMP	1.00	1.00	1.00	.98		
TW	38.70	39.85	38.70	27.99		
ME	-0.04	-8.05	-0.04	-2.00		
TF	-0.91	-2.08	-0.91	-3.80		
TE	38.67	30.31	38.67	29.05		
ACTUAL PX		-22.50		-28.94		
ACTUAL PY		-24.16		-29.76		

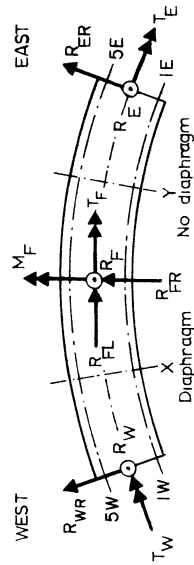
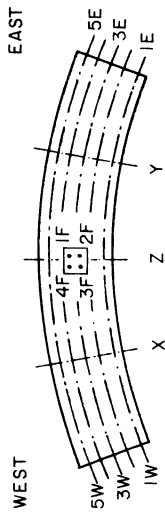
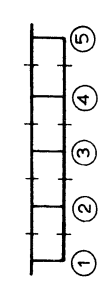
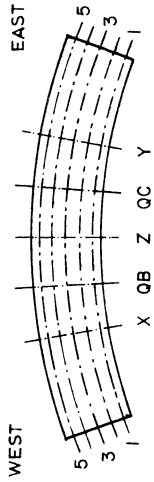


TABLE 25B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR 50 KSI, 60 KSI  
 CONDITIONING LOAD STRESS LEVELS  
 SIMPLY SUPPORTED, NO RESTRAINTS



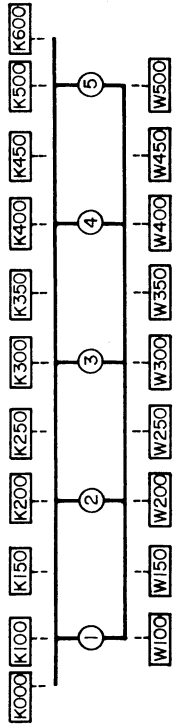
DEFLECTION AT POINT	50 KSI			60 KSI			CONDITIONING LOAD STRESS LEVEL		
	THEORY	EXPERM	E/T	THEORY	EXPERM	E/T	THEORY	EXPERM	E/T
1X	.476	.865	1.82	.476	.869	1.83	.476	.869	1.83
2X	.491	.911	1.86	.491	.909	1.85	.491	.909	1.85
3X	.511	.961	1.88	.511	.951	1.86	.511	.951	1.86
4X	.537	1.012	1.88	.537	.995	1.85	.537	.995	1.85
5X	.569	1.072	1.88	.569	1.045	1.84	.569	1.045	1.84
1QB	.226	.407	1.80	.226	.415	1.83	.226	.415	1.83
2QB	.226	.417	1.85	.226	.416	1.84	.226	.416	1.84
3QB	.230	.422	1.83	.230	.416	1.81	.230	.416	1.81
4QB	.246	.454	1.84	.246	.444	1.80	.246	.444	1.80
5QB	.267	.470	1.76	.267	.454	1.70	.267	.454	1.70
1Z	.030	.086	2.82	.030	.092	3.04	.030	.092	3.04
2Z	.016	.044	2.81	.016	.042	2.70	.016	.042	2.70
4Z	.014	.033	2.31	.014	.017	1.22	.014	.017	1.22
5Z	.027	.062	2.30	.027	.063	2.34	.027	.063	2.34
1QC	.230	.444	1.93	.230	.455	1.97	.230	.455	1.97
2QC	.228	.438	1.93	.228	.447	1.97	.228	.447	1.97
3QC	.230	.425	1.85	.230	.428	1.86	.230	.428	1.86
4QC	.245	.463	1.89	.245	.470	1.91	.245	.470	1.91
5QC	.267	.492	1.84	.267	.503	1.88	.267	.503	1.88
1Y	.486	.954	1.96	.486	.976	2.01	.486	.976	2.01
2Y	.493	.944	1.91	.493	.965	1.96	.493	.965	1.96
3Y	.509	.961	1.89	.509	.948	1.86	.509	.948	1.86
4Y	.534	1.008	1.89	.534	1.035	1.94	.534	1.035	1.94
5Y	.567	1.089	1.92	.567	1.120	1.98	.567	1.120	1.98
LOAD PX	-100.0	-100.0		-100.0	-100.0		-100.0	-100.0	
LOAD PY	-100.0	-107.4		-100.0	-102.8		-100.0	-102.8	
ACTUAL PX		-22.5			-28.9			-28.9	
ACTUAL PY		-24.2			-29.8			-29.8	



TABLE 25C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR 50 KSI, 60 KSI  
CONDITIONING LOAD STRESS LEVELS  
SIMPLY SUPPORTED, NO RESTRAINTS



SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	50 KSI		60 KSI		THEORY		MEASR		ADJUST	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	ADJUST	ADJUST		
K	K000	-269	-253	-269	-251	-269	-251	-269	-251	-269	-251
K	K100	-228	-401	-228	-377	-228	-377	-228	-377	-228	-366
K	K150	-200	-298	-200	-284	-200	-284	-200	-284	-200	-264
K	K200	-200	-311	-200	-293	-200	-293	-200	-293	-200	-302
K	K250	-207	-278	-207	-267	-207	-267	-207	-267	-207	-264
K	K300	-197	-315	-197	-297	-197	-297	-197	-297	-197	-295
K	K350	-216	-292	-216	-273	-216	-273	-216	-273	-216	-272
K	K400	-245	-332	-245	-314	-245	-314	-245	-314	-245	-312
K	K450	880	-283	880	-265	880	-265	880	-265	880	-285
K	K500	792	-294	766	-275	766	-275	766	-275	766	-278
K	K600	766	-200	766	-198	766	-198	766	-198	766	-198
W	W100	880	919	880	884	880	884	880	884	880	888
W	W150	766	792	766	779	766	779	766	779	766	742
W	W200	808	818	808	775	808	775	808	775	808	772
W	W250	752	789	752	773	752	773	752	773	752	718
W	W300	814	921	814	896	814	896	814	896	814	879
W	W350	880	777	880	754	880	754	880	754	880	780
W	W400	766	876	766	845	766	845	766	845	766	849
W	W450	808	812	808	788	808	788	808	788	808	769
W	W500	752	977	752	985	752	985	752	985	752	983
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-107.4	-100.0	-102.8	-100.0	-102.8	-100.0	-102.8	-100.0	-102.8
ACTUAL	PX (KIPS)	-22.5	-24.2	-22.5	-28.9	-22.5	-28.9	-22.5	-28.9	-22.5	-28.9
ACTUAL	PY (KIPS)	-24.2	-24.2	-24.2	-29.8	-24.2	-29.8	-24.2	-29.8	-24.2	-29.8

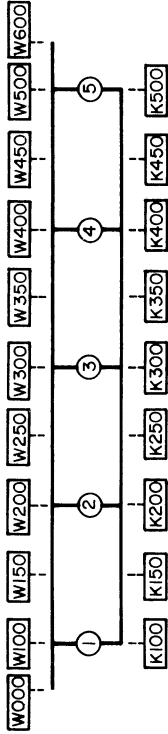
TABLE 25D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR 50 KSI, 60 KSI  
CONDITIONING LOAD STRESS LEVELS  
SIMPLY SUPPORTED, NO RESTRAINTS

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
COMPRESSION = - W = WELDABLE STRAIN GAGES

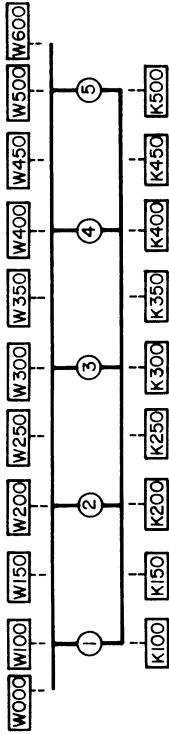


GAGE TYPE	GAGE LOC.	50 KSI			60 KSI			CONDITIONING LOAD STRESS LEVEL		
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
W	W000	675	634	634	675	704	704	675	704	704
W	W100	625	710	722	625	683	694	625	683	694
W	W150	532	615	690	532	599	675	532	599	675
W	W200	532	779	791	532	763	768	532	763	768
W	W250	688	688	738	666	666	746	666	666	746
W	W300	526	839	850	526	812	834	526	812	834
W	W350	686	794	794	666	666	769	666	666	769
W	W400	533	690	708	533	665	677	533	665	677
W	W450	611	664	726	611	637	719	611	637	719
W	W500	624	664	661	624	648	654	624	648	654
W	W600	624	681	681	624	666	666	624	666	666
K	K100	-285	-420	-433	-285	-424	-439	-285	-424	-439
K	K150	-458	-458	-419	-458	-528	-466	-458	-528	-466
K	K200	-248	-429	-411	-248	-420	-398	-248	-420	-398
K	K250	-408	-395	-395	-408	-393	-390	-408	-393	-390
K	K300	-217	-418	-421	-217	-414	-419	-217	-414	-419
K	K350	-406	-401	-401	-406	-392	-393	-406	-392	-393
K	K400	-249	-376	-376	-249	-367	-367	-249	-367	-367
K	K450	-405	-405	-404	-405	-401	-402	-405	-401	-402
K	K500	-274	-370	-367	-274	-366	-363	-274	-366	-363
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-107.4	-102.8	-100.0	-102.8	-102.8	-100.0	-102.8	-102.8
ACTUAL	PX (KIPS)	-22.5	-24.2	-28.9	-22.5	-28.9	-28.9	-22.5	-28.9	-28.9
ACTUAL	PY (KIPS)	-24.2	-24.2	-29.8	-24.2	-29.8	-29.8	-24.2	-29.8	-29.8

TABLE 25E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR 50 KSI, 60 KSI  
CONDITIONING LOAD STRESS LEVELS  
SIMPLY SUPPORTED, NO RESTRAINTS



SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	50 KSI		60 KSI		THEORY		MEASR		ADJUST	
		THEORY	MEASR	THEORY	MEASR	ADJUST	ADJUST	ADJUST	ADJUST	ADJUST	ADJUST
W	W000	680	765	680	743	680	743	680	743	680	743
W	W100	629	715	629	684	629	684	629	684	629	684
W	W150	590	619	590	607	590	607	590	607	590	607
W	W200	533	818	533	880	533	880	533	880	533	880
W	W250	628	669	628	643	628	643	628	643	628	643
W	W300	526	891	526	868	526	868	526	868	526	868
W	W350	532	578	532	554	532	554	532	554	532	554
W	W400	609	784	609	807	609	807	609	807	609	807
W	W450	621	610	621	640	621	640	621	640	621	640
W	W500	729	729	729	723	729	707	729	707	729	706
W	W600	705	705	705	692	705	692	705	692	705	692
K	K100	-287	-436	-287	-428	-287	-447	-287	-447	-287	-442
K	K150	-248	-370	-248	-366	-248	-374	-248	-361	-248	-361
K	K200	-216	-381	-216	-398	-216	-370	-216	-385	-216	-385
K	K250	-248	-384	-248	-433	-248	-383	-248	-433	-248	-433
K	K300	-216	-407	-216	-397	-216	-397	-216	-387	-216	-387
K	K350	-248	-441	-248	-437	-248	-428	-248	-429	-248	-429
K	K400	-273	-362	-273	-370	-273	-351	-273	-361	-273	-361
K	K450	-418	-418	-418	-427	-418	-410	-418	-421	-418	-421
K	K500	-401	-401	-401	-394	-401	-404	-401	-396	-401	-396
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-100.0	-100.0	-107.4	-100.0	-102.8	-100.0	-102.8	-100.0	-102.8
ACTUAL	PX (KIPS)	-22.5	-22.5	-22.5	-28.9	-22.5	-28.9	-22.5	-28.9	-22.5	-28.9
ACTUAL	PY (KIPS)	-24.2	-24.2	-24.2	-29.8	-24.2	-29.8	-24.2	-29.8	-24.2	-29.8

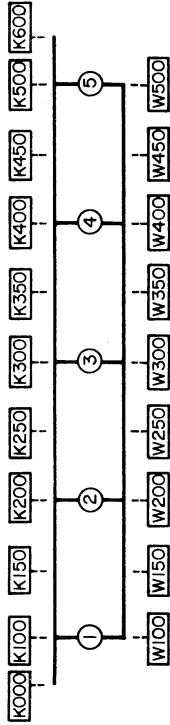
TABLE 25F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR 50 KSI, 60 KSI  
CONDITIONING LOAD STRESS LEVELS  
SIMPLY SUPPORTED, NO RESTRAINTS

SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
COMPRESSION = - W = WELDABLE STRAIN GAGES



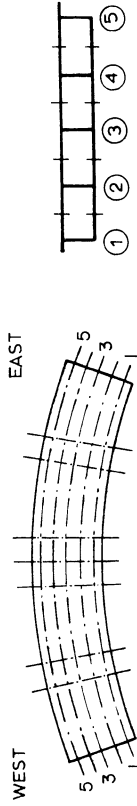
GAGE TYPE	GAGE LOC.	50 KSI			60 KSI			CONDITIONING LOAD STRESS LEVEL		
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
K	K000	-241	-184	-184	-241	-194	-194			
K	K100	-204	-257	-262	-204	-244	-250			
K	K150		-345	-344		-323	-324			
K	K200	-177	-310	-312	-177	-294	-296			
K	K250		-311	-346		-304	-331			
K	K300	-183	-300	-313	-183	-282	-295			
K	K350		-368	-394		-347	-374			
K	K400	-173	-304	-290	-173	-291	-277			
K	K450		-366	-354		-333	-328			
K	K500	-190	-302	-304	-190	-278	-281			
K	K600	-216	-174	-174	-216	-182	-182			
W	W100	889	774	792	889	770	780			
W	W150		834	835		823	825			
W	W200	771	882	877	771	856	852			
W	W250		811	771		782	756			
W	W300	806	923	911	806	876	870			
W	W350		801	761		785	749			
W	W400	746	962	937	746	940	915			
W	W450		815	819		809	813			
W	W500	808	717	758	808	719	756			
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0			
LOAD	PY (KIPS)	-100.0	-107.4		-100.0	-102.8				
ACTUAL	PX (KIPS)		-22.5			-28.9				
ACTUAL	PY (KIPS)		-24.2			-29.8				

TABLE 25G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR 50 KSI,60 KSI  
CONDITIONING LOAD STRESS LEVELS  
SIMPLY SUPPORTED, NO RESTRAINTS



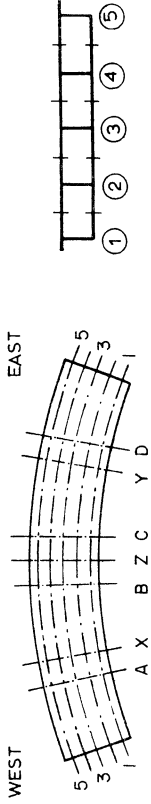
SECTION	GIRDER	50 KSI				60 KSI				CONDITIONING LOAD STRESS LEVEL			
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
A	1	76.9	17.0	59.7	13.5	76.9	17.0	58.2	14.0				
A	2	102.4	22.7	99.7	22.6	102.4	22.7	93.1	22.4				
A	3	100.2	22.2	105.2	23.8	100.2	22.2	98.9	23.8				
A	4	100.2	22.2	108.7	24.6	100.2	22.2	100.7	24.3				
A	5	72.2	16.0	58.0	15.4	72.2	16.0	64.2	15.5				
A	SUM	451.8		441.2		451.8		415.1					
B	1	-80.4	16.5	-69.1	16.0	-80.4	16.5	-79.0	16.0				
B	2	-110.1	22.5	-93.9	21.7	-110.1	22.5	-107.2	21.8				
B	3	-110.7	22.6	-107.1	24.8	-110.7	22.6	-122.2	24.8				
B	4	-109.8	22.5	-93.3	21.6	-109.8	22.5	-104.6	21.2				
B	5	-77.8	15.9	-69.3	16.0	-77.8	15.9	-79.7	16.2				
B	SUM	-488.7		-432.7		-488.7		-492.5					
C	1	-80.8	16.5	-97.0	16.4	-80.8	16.5	-88.6	15.9				
C	2	-110.3	22.6	-129.7	21.9	-110.3	22.6	-126.2	22.6				
C	3	-110.6	22.6	-137.4	23.2	-110.6	22.6	-126.3	22.6				
C	4	-109.5	22.4	-129.1	21.8	-109.5	22.4	-126.0	22.6				
C	5	-77.5	15.9	-97.9	16.6	-77.5	15.9	-90.8	16.3				
C	SUM	-488.7		-591.1		-488.7		-557.9					
D	1	77.7	17.2	56.8	13.6	77.7	17.2	55.5	13.7				
D	2	103.0	22.8	102.7	24.5	103.0	22.8	99.2	24.5				
D	3	100.0	22.1	98.5	23.5	100.0	22.1	94.0	23.2				
D	4	99.5	22.0	106.1	25.4	99.5	22.0	103.0	25.4				
D	5	71.7	15.9	54.1	12.9	71.7	15.9	53.5	13.2				
D	SUM	451.8		418.3		451.8		405.2					
LJAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0					
LJAD	PY (KIPS)	-100.0		-107.4		-100.0		-102.8					
ACTUAL	PX (KIPS)	-22.5		-22.5		-28.9		-28.9					
ACTUAL	PY (KIPS)	-24.2		-24.2		-29.8		-29.8					

TABLE 25H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR 50 KSI, 60 KSI  
CONDITIONING LOAD STRESS LEVELS  
SIMPLY SUPPORTED, NO RESTRAINTS



SECTION	GIRDER	50 KSI			60 KSI			CONDITIONING LOAD STRESS LEVEL		
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT
A	1	76.9	17.0	91.7	20.8	76.9	17.0	86.6	20.9	
A	2	102.4	22.7	89.7	20.3	102.4	22.7	85.0	20.5	
A	3	100.2	22.2	88.7	20.1	100.2	22.2	83.7	20.2	
A	4	100.2	22.2	95.4	21.6	100.2	22.2	89.3	21.5	
A	5	72.2	16.0	75.6	17.1	72.2	16.0	70.5	17.0	
A	SUM	451.8		441.1		451.8		415.1		
B	1	-80.4	16.5	-64.2	14.9	-80.4	16.5	-77.0	15.9	
B	2	-110.1	22.5	-102.9	23.8	-110.1	22.5	-116.0	24.0	
B	3	-110.7	22.6	-108.2	25.1	-110.7	22.6	-119.3	24.7	
B	4	-109.8	22.5	-98.9	22.9	-109.8	22.5	-107.9	22.3	
B	5	-77.8	15.9	-57.4	13.3	-77.8	15.9	-63.2	13.1	
B	SUM	-488.7		-431.7		-488.7		-483.4		
C	1	-80.8	16.5	-81.6	13.8	-80.8	16.5	-80.2	14.4	
C	2	-110.3	22.6	-136.4	23.1	-110.3	22.6	-126.7	22.7	
C	3	-110.6	22.6	-151.1	25.6	-110.6	22.6	-142.3	25.5	
C	4	-109.5	22.4	-138.5	23.4	-109.5	22.4	-128.4	23.0	
C	5	-77.5	15.9	-83.7	14.2	-77.5	15.9	-80.2	14.4	
C	SUM	-488.7		-591.2		-488.7		-557.7		
D	1	77.7	17.2	67.2	16.0	77.7	17.2	65.8	16.2	
D	2	103.0	22.8	91.4	21.8	103.0	22.8	88.5	21.8	
D	3	100.0	22.1	95.2	22.7	100.0	22.1	92.2	22.7	
D	4	99.5	22.0	91.9	21.9	99.5	22.0	88.4	21.8	
D	5	71.7	15.9	74.1	17.7	71.7	15.9	70.5	17.4	
D	SUM	451.8		419.8		451.8		405.4		
LOAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0		
LOAD	PY (KIPS)	-100.0		-107.4		-100.0		-102.8		
ACTUAL	PX (KIPS)			-22.5				-28.9		
ACTUAL	PY (KIPS)			-24.2				-29.8		

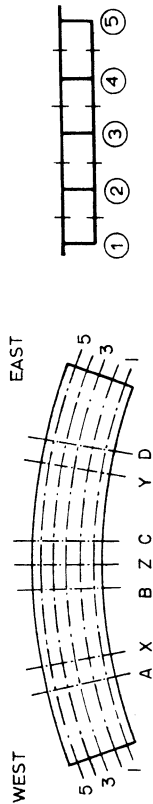
\*\*\*\*\*  
THEORY PCT K-FT PCT  
\*\*\*\*\*  
EXPERIMENTAL PCT K-FT PCT  
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TABLE 251

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR 50 KSI, 60 KSI  
CONDITIONING LOAD STRESS LEVELS  
SIMPLY SUPPORTED, NO RESTRAINTS

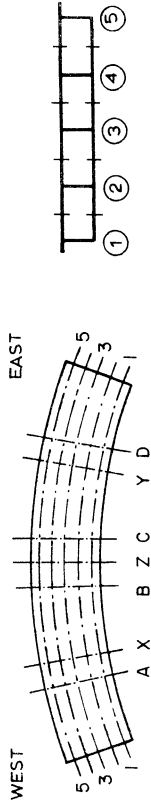


SECTION	GIRDER	50 KSI		60 KSI		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	76.9	17.0	74.0	16.8	76.9	17.0	70.9	17.1
A	2	102.4	22.7	95.3	21.6	102.4	22.7	89.5	21.6
A	3	100.2	22.2	97.9	22.2	100.2	22.2	92.2	22.2
A	4	100.2	22.2	102.8	23.3	100.2	22.2	95.7	23.0
A	5	72.2	16.0	71.4	16.2	72.2	16.0	67.1	16.1
A	SUM	451.8		441.3		451.8		415.2	
B	1	-80.4	16.5	-66.4	15.4	-80.4	16.5	-77.9	16.0
B	2	-110.1	22.5	-98.9	22.9	-110.1	22.5	-112.1	23.0
B	3	-110.7	22.6	-107.7	24.9	-110.7	22.6	-120.6	24.7
B	4	-109.8	22.5	-96.4	22.3	-109.8	22.5	-106.4	21.8
B	5	-77.8	15.9	-62.7	14.5	-77.8	15.9	-70.6	14.5
B	SUM	-488.7		-432.2		-488.7		-487.6	
C	1	-80.8	16.5	-88.5	15.0	-80.8	16.5	-83.9	15.0
C	2	-110.3	22.6	-133.4	22.6	-110.3	22.6	-126.5	22.7
C	3	-110.6	22.6	-145.0	24.5	-110.6	22.6	-135.2	24.2
C	4	-109.5	22.4	-134.4	22.7	-109.5	22.4	-127.4	22.8
C	5	-77.5	15.9	-90.1	15.2	-77.5	15.9	-84.9	15.2
C	SUM	-488.7		-591.4		-488.7		-558.0	
D	1	77.7	17.2	61.5	14.7	77.7	17.2	60.1	14.8
D	2	103.0	22.8	97.7	23.3	103.0	22.8	94.5	23.3
D	3	100.0	22.1	97.0	23.2	100.0	22.1	93.2	23.0
D	4	99.5	22.0	99.8	23.8	99.5	22.0	96.5	23.8
D	5	71.7	15.9	63.1	15.0	71.7	15.9	61.1	15.1
D	SUM	451.8		419.1		451.8		405.4	
LOAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0	
LOAD	PY (KIPS)	-100.0		-107.4		-100.0		-102.8	
ACTUAL	PX (KIPS)			-22.5				-28.9	
ACTUAL	PY (KIPS)			-24.2				-29.8	

\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

TABLE 25J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.



RESULTS FOR 50 KSI, 60 KSI  
CONDITIONING LOAD STRESS LEVELS  
SIMPLY SUPPORTED, NO RESTRAINTS

SECTION	GIRDER	50 KSI			60 KSI			THEORY			EXPERIMENTAL		
		K-FT	PCT	PCT	K-FT	PCT	PCT	K-FT	PCT	PCT	K-FT	PCT	PCT
A	1	76.9	17.0	69.4	15.7	76.9	17.0	66.5	16.0	76.9	17.0	66.5	16.0
A	2	102.4	22.7	96.9	21.9	102.4	22.7	90.8	21.8	102.4	22.7	90.8	21.8
A	3	100.2	22.2	101.0	22.8	100.2	22.2	95.1	22.9	100.2	22.2	95.1	22.9
A	4	100.2	22.2	105.1	23.8	100.2	22.2	97.7	23.5	100.2	22.2	97.7	23.5
A	5	72.2	16.0	69.8	15.8	72.2	16.0	65.6	15.8	72.2	16.0	65.6	15.8
A	SUM	451.8		442.0		451.8		415.7		451.8		415.7	
B	1	-80.4	16.5	-67.3	15.6	-80.4	16.5	-78.2	16.0	-80.4	16.5	-78.2	16.0
B	2	-110.1	22.5	-97.0	22.4	-110.1	22.5	-110.2	22.5	-110.1	22.5	-110.2	22.5
B	3	-110.7	22.6	-107.5	24.9	-110.7	22.6	-121.2	24.8	-110.7	22.6	-121.2	24.8
B	4	-109.8	22.5	-95.2	22.0	-109.8	22.5	-105.7	21.6	-109.8	22.5	-105.7	21.6
B	5	-77.8	15.9	-65.1	15.1	-77.8	15.9	-73.8	15.1	-77.8	15.9	-73.8	15.1
B	SUM	-488.7		-432.0		-488.7		-489.1		-488.7		-489.1	
C	1	-80.8	16.5	-91.2	15.5	-80.8	16.5	-85.3	15.3	-80.8	16.5	-85.3	15.3
C	2	-110.3	22.6	-131.9	22.4	-110.3	22.6	-126.4	22.7	-110.3	22.6	-126.4	22.7
C	3	-110.6	22.6	-141.6	24.0	-110.6	22.6	-131.2	23.6	-110.6	22.6	-131.2	23.6
C	4	-109.5	22.4	-132.1	22.4	-109.5	22.4	-126.7	22.8	-109.5	22.4	-126.7	22.8
C	5	-77.5	15.9	-92.9	15.8	-77.5	15.9	-87.0	15.6	-77.5	15.9	-87.0	15.6
C	SUM	-488.7		-589.7		-488.7		-556.6		-488.7		-556.6	
D	1	77.7	17.2	59.4	14.2	77.7	17.2	58.0	14.3	77.7	17.2	58.0	14.3
D	2	103.0	22.8	99.7	23.8	103.0	22.8	96.5	23.8	103.0	22.8	96.5	23.8
D	3	100.0	22.1	97.7	23.3	100.0	22.1	93.6	23.1	100.0	22.1	93.6	23.1
D	4	99.5	22.0	102.8	24.5	99.5	22.0	99.6	24.6	99.5	22.0	99.6	24.6
D	5	71.7	15.9	59.9	14.3	71.7	15.9	58.1	14.3	71.7	15.9	58.1	14.3
D	SUM	451.8		419.4		451.8		405.7		451.8		405.7	
LOAD	PX (KIPS)	-100.0		-100.0		-100.0		-100.0		-100.0		-100.0	
LOAD	PY (KIPS)	-100.0		-107.4		-100.0		-102.8		-100.0		-102.8	
ACTUAL	PX (KIPS)	-22.5		-22.5		-22.5		-28.9		-22.5		-28.9	
ACTUAL	PY (KIPS)	-24.2		-24.2		-24.2		-29.8		-24.2		-29.8	



TABLE 26A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 24 KSI COND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	NORMALIZED POINT LOADS APPLIED AT					
	(1-X)		(1-Y)		(1-X)+(1-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	8.07	6.70	41.39	25.26	49.45	31.72
2E	.05	1.56	9.57	24.61	9.62	25.95
3E	-1.31	-1.41	-4.42	7.89	-1.73	5.71
4E	-2.91	-3.49	-1.17	-9.03	-4.08	-10.60
5E	-9.62	-10.65	-8.32	-8.93	-17.94	-18.14
1F	-16.14	4.36	20.53	2.28	4.39	11.60
2F	11.60	29.10	48.71	28.42	60.32	52.53
3F	48.40	29.97	11.88	30.93	60.28	53.01
4F	20.66	4.83	-16.30	5.97	4.35	12.61
1W	37.19	30.47	8.03	7.49	45.23	36.54
2W	11.88	17.69	.12	3.58	11.99	20.85
3W	3.59	9.56	-1.36	-2.69	2.23	8.65
4W	.87	.04	-3.03	-3.69	-2.16	-2.23
5W	-12.33	-16.08	-9.62	-11.12	-21.95	-27.04
RE	-5.72	-7.29	41.05	39.80	35.32	34.64
RF	64.53	68.26	64.82	67.60	129.34	129.75
RW	41.20	41.58	-5.86	-6.43	35.34	36.77
SUMR	100.01	102.65	100.01	100.97	200.00	201.16
PX	-100.00	-100.00	0.	0.	-100.00	-100.00
PY	0.	-.01	-100.00	-100.00	-100.00	-98.68
SUMP	-100.00	-100.01	-100.00	-100.00	-200.00	-198.68
SUMR/SUMP	1.00	1.03	1.00	1.01	1.00	1.01
TW	-283.15	-284.95	-98.93	-114.47	-382.10	-386.55
MF	110.40	2.01	-110.50	9.30	-.11	2.24
TF	-83.22	-74.82	-84.56	-76.65	-167.78	-121.99
TE	-98.64	-102.27	-283.43	-262.49	-382.02	-350.61
ACTUAL PX		-12.66		0.		-12.86
ACTUAL PY		-.01		-12.75		-12.69

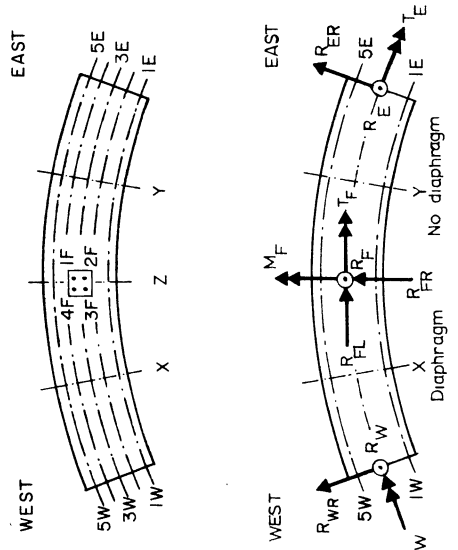
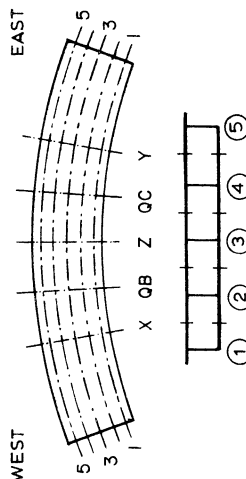


TABLE 26B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 24 KSI CONCD. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



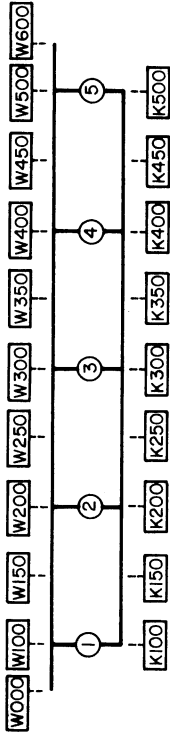
DEFLECTION AT POINT	(1-X)		(1-Y)		NORMALIZED POINT LOADS APPLIED AT (1-X)+(1-Y)	
	THEORY	EXPERM E/T	THEORY	EXPERM E/T	THEORY	EXPERM E/T
1X	.942	1.109	1.18	.86	.789	.920
2X	.806	.953	1.18	.88	.608	.724
3X	.692	.803	1.16	.90	.450	.537
4X	.605	.709	1.17	.90	.316	.404
5X	.535	.615	1.15	.91	.198	.259
1QB	.625	.708	1.13	.83	.536	.604
2QB	.512	.574	1.12	.85	.361	.421
3QB	.407	.454	1.11	.86	.201	.250
4QB	.329	.353	1.07	.93	.063	.100
5QB	.261	.284	1.09	.97	-.067	-.044
1Z	.150	.164	1.03	.173	.324	.338
2Z	.078	.070	.89	.081	.158	.141
4Z	-.063	-.054	.87	-.058	.126	-.113
5Z	-.129	-.135	1.05	-.132	-.257	-.266
1QC	-.087	-.065	.74	.682	.595	.694
2QC	-.148	-.140	.94	.529	.381	.452
3QC	-.203	-.203	1.00	.398	.195	.228
4QC	-.263	-.254	.97	.314	.050	.075
5QC	-.325	-.288	.89	.255	-.070	-.052
1Y	-.153	-.131	.86	1.101	.948	1.237
2Y	-.197	-.171	.87	.825	.629	.772
3Y	-.239	-.204	.85	.658	.419	.481
4Y	-.283	-.264	.93	.559	.276	.351
5Y	-.329	-.317	.96	.504	.175	.211
LOAD PX	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD PY	0.	-0	-100.0	-100.0	-98.7	-98.7
ACTUAL PX	-12.7	-12.7	0.	0.	-12.9	-12.9
ACTUAL PY	-0	-0	-12.7	-12.7	-12.7	-12.7



TABLE 26D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 24 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.



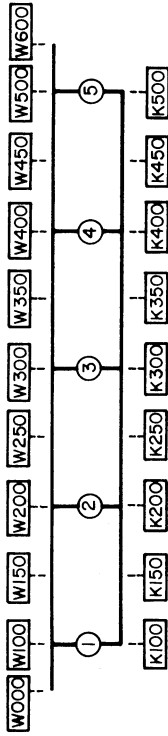
SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	184	375	473	311	658	639
W	W100	189	381	427	353	616	701
W	W150	309	346	291	284	476	597
W	W200	185	332	291	295	405	607
W	W250	323	345	207	217	475	511
W	W300	256	370	149	173	405	536
W	W350	251	293	222	155	370	418
W	W400	147	208	209	172	301	351
W	W450	130	173	298	208	428	349
W	W500	114	135	315	160	430	275
W	W600	125	125	125	151	259	259
K	K100	-91	-195	-197	-193	-289	-330
K	K150	-248	-227	-141	-160	-364	-344
K	K200	-82	-166	-174	-167	-224	-307
K	K250	-208	-232	-118	-97	-308	-311
K	K300	-100	-226	-66	-86	-166	-297
K	K350	-197	-199	-101	-103	-292	-293
K	K400	-66	-150	-105	-128	-172	-276
K	K450	-118	-134	-140	-145	-252	-267
K	K500	-58	-126	-129	-154	-187	-258
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	-0	-100.0	-100.0	-98.7	-98.7
ACTUAL	PX (KIPS)	-12.7	-12.7	0.	0.	-12.9	-12.9
ACTUAL	PY (KIPS)	-0	-0	-12.7	-12.7	-12.7	-12.7

TABLE 26E

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 24 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION C

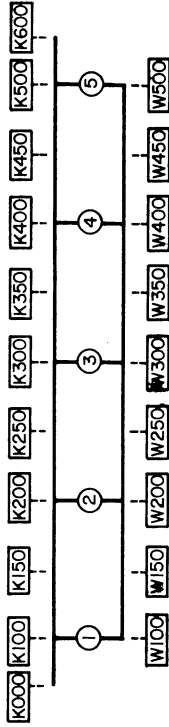
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)		MEASR	ADJUST	THEORY	MEASR	ADJUST
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR					
W	W000	425	262	302	471	728	679	679	679	728	679	679
W	W100	387	266	279	441	666	665	665	676	666	665	676
W	W150	234	233	203	350	484	540	540	588	484	682	679
W	W200	280	332	203	392	300	464	464	456	300	464	456
W	W250	190	177	241	294	396	519	519	512	294	519	512
W	W300	154	231	241	304	353	318	318	327	304	335	350
W	W350	231	156	121	184	400	254	254	273	184	228	222
W	W400	231	198	121	140	388	205	205	205	140	205	205
W	W450	304	172	95	90					95	61	61
W	W500	326	180	62	61					62	36	36
W	W600		192		36							
K	K100	-178	-171	-137	-297	-315	-381	-381	-389	-137	-312	-312
K	K150		-154		-220		-271	-271	-347		-220	-220
K	K200	-134	-145	-95	-209	-229	-324	-324	-334	-95	-212	-212
K	K250		-119		-205		-191	-191	-318		-205	-205
K	K300	-67	-100	-95	-186	-163	-279	-279	-274	-95	-183	-183
K	K350		-139		-146		-146	-146	-266		-146	-146
K	K400	-110	-141	-52	-113	-163	-243	-243	-239	-52	-110	-110
K	K450		-167		-142		-138	-138	-300		-142	-142
K	K500	-133	-168	-37	-125	-171	-276	-276	-274	-37	-124	-124
LOAD	PX (KIPS)	-100.0	-100.0	0.0	0.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	0.0	-0.0	-100.0	-100.0	-100.0	-98.7	-98.7	-98.7	-100.0	-100.0	-100.0
ACTUAL	PX (KIPS)		-12.7		0.0		-12.9	-12.9	-12.9		0.0	0.0
ACTUAL	PY (KIPS)		-0.0		-12.7		-12.7	-12.7	-12.7		-12.7	-12.7

TABLE 26F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 24 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

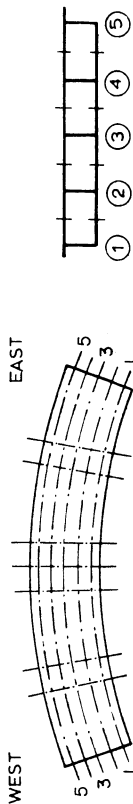
GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	51	36	-407	-239	-355	-170
K	K100	43	56	-331	-410	-287	-326
K	K150	109	107	-631	-550	-73	-413
K	K200	37	62	-252	-488	-215	-414
K	K250	38	56	-206	-326	-168	-314
K	K300	37	55	-170	-324	-133	-272
K	K350	47	71	-266	-393	-137	-314
K	K400	50	52	-179	-379	-137	-316
K	K450	35	35	-201	-274	-153	-234
K	K500	15	35	-95	-274	-79	-234
K	K600	36	58	-407	-410	-355	-170
W	W100	-42	-38	1480	818	1297	634
W	W150	-80	-73	1081	1085	888	924
W	W200	-93	-94	1147	1096	983	922
W	W250	-90	-80	930	797	684	654
W	W300	-77	-74	930	559	753	492
W	W350	-123	-120	715	554	552	443
W	W400	-134	-130	696	675	501	492
W	W450	-111	-113	696	518	390	368
W	W500	-87	-95	696	651	519	528

LOAD	PX (KIPS)	PY (KIPS)
LOAD	-100.0	-100.0
LOAD	0.	0.
LOAD	-100.0	-100.0
LOAD	0.	0.
LOAD	-100.0	-100.0

ACTUAL	PX (KIPS)	PY (KIPS)
ACTUAL	-12.7	-12.7
ACTUAL	0.	0.
ACTUAL	-12.7	-12.7
ACTUAL	0.	0.
ACTUAL	-12.7	-12.7

**TABLE 26G**  
**DISTRIBUTION OF MOMENTS TO EACH GIRDER**  
**( KIP-FT AND PERCENTAGE )**  
**MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH**

RESULTS FOR POINT LOADS  
 APPLIED AFTER 24 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

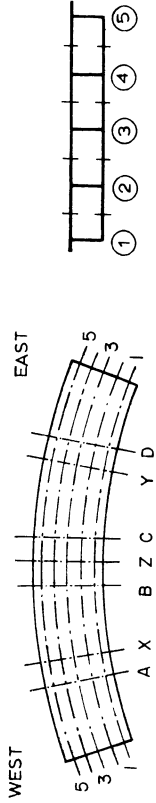


SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	116.1	81.5	17.3	-16.1	-3.7	6.7	100.0	21.8	72.0	18.9
A	2	139.9	124.0	26.3	-21.8	-12.1	22.2	118.0	25.8	105.4	27.6
A	3	119.5	108.9	23.0	-22.1	-12.5	22.8	97.4	21.3	85.7	22.5
A	4	107.1	99.1	21.0	-22.7	-16.2	29.6	84.4	18.4	76.2	20.0
A	5	74.6	58.9	12.5	-16.8	-10.3	18.8	57.8	12.6	42.0	11.0
A	SUM	557.1	472.4		-99.4	-54.8		457.7		381.3	
B	1	-27.6	-45.3	21.9	-56.6	-39.4	25.0	-80.1	20.0	-80.5	23.8
B	2	-42.4	-52.7	25.4	-63.5	-41.0	26.0	-100.5	25.0	-88.1	26.0
B	3	-53.3	-56.1	27.0	-39.7	-29.8	18.9	-87.6	21.8	-79.7	23.6
B	4	-34.5	-34.7	16.8	-48.1	-26.5	16.8	-78.4	19.5	-55.1	16.3
B	5	-18.8	-18.5	8.9	-38.6	-20.8	13.2	-54.7	13.6	-35.0	10.3
B	SUM	-176.6	-207.3		-246.6	-157.4		-401.3		-338.3	
C	1	-47.2	-33.5	20.5	-39.5	-59.8	29.9	-86.7	21.5	-87.1	25.3
C	2	-55.4	-43.9	26.9	-48.2	-63.2	31.5	-103.4	25.7	-100.6	29.2
C	3	-36.9	-32.7	20.0	-50.8	-45.9	22.9	-86.4	21.5	-74.6	21.6
C	4	-45.8	-30.4	18.6	-28.7	-24.7	12.3	-75.0	18.6	-53.7	15.6
C	5	-36.4	-23.0	14.0	-13.2	-6.7	3.4	-50.8	12.6	-28.9	8.4
C	SUM	-221.7	-163.4		-180.5	-200.3		-402.4		-344.9	
D	1	-16.4	-3.4	6.5	126.4	76.7	18.0	110.0	24.1	62.5	17.9
D	2	-21.8	-11.9	22.7	148.9	141.0	33.0	127.0	27.8	121.8	34.9
D	3	-21.6	-11.1	21.3	115.7	80.2	18.8	94.1	20.6	67.6	19.4
D	4	-21.6	-17.7	33.8	97.4	82.9	19.4	75.8	16.6	61.7	17.7
D	5	-15.9	-8.3	15.8	65.6	46.2	10.8	49.7	10.9	35.5	10.2
D	SUM	-97.3	-52.3		553.9	427.0		456.6		349.2	
LOAD	PX (KIPS)	-100.0	-100.0		0.	0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.	-0		-100.0	0.		-100.0		-98.7	
ACTUAL	PX (KIPS)		-12.7			0.				-12.9	
ACTUAL	PY (KIPS)		-0			-12.7				-12.7	

**TABLE 26H**  
**DISTRIBUTION OF MOMENTS TO EACH GIRDER**  
**( KIP-FT AND PERCENTAGE )**

**MOMENTS ABOUT TENSION FLANGE STEEL**

**RESULTS FOR POINT LOADS**  
**APPLIED AFTER 24 KSI COND. LOADING.**  
**SIMPLY SUPPORTED, NO RESTRAINTS.**

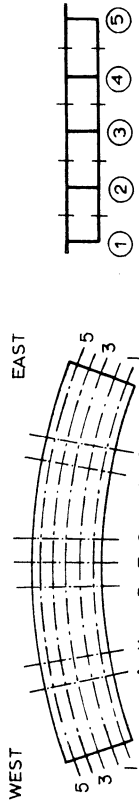


SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)		
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT
A	1	116.1	20.8	135.0	-16.1	16.2	-19.4	100.0	21.8	114.0
A	2	139.9	25.1	120.2	-21.8	22.0	-15.6	118.0	25.8	99.4
A	3	119.5	21.4	98.9	-22.1	22.2	-12.3	97.4	21.3	82.1
A	4	107.1	19.2	109.0	-22.7	22.8	-10.3	84.4	18.4	93.6
A	5	74.6	13.4	76.0	-16.8	16.9	-8.9	57.8	12.6	65.9
A	SUM	557.1		539.2	-99.4		-66.4	457.7		455.0
B	1	-27.6	15.6	-34.8	-56.6	22.9	-28.7	-80.1	20.0	-53.7
B	2	-42.4	24.0	-56.1	-63.5	25.8	-40.6	-100.5	25.0	-88.1
B	3	-53.3	30.2	-66.0	-39.7	16.1	-26.2	-87.6	21.8	-88.3
B	4	-34.5	19.6	-45.4	-48.1	19.5	-36.9	-78.4	19.5	-80.1
B	5	-18.8	10.6	-22.2	-38.6	15.7	-26.6	-54.7	13.6	-45.9
B	SUM	-176.6		-224.5	-246.6		-159.1	-401.3		-356.1
C	1	-47.2	21.3	-25.1	-39.5	21.9	-50.5	-86.7	21.5	-61.3
C	2	-55.4	25.0	-39.1	-48.2	26.7	-62.7	-103.4	25.7	-93.2
C	3	-36.9	16.7	-33.7	-50.8	28.2	-53.3	-86.4	21.5	-84.6
C	4	-45.8	20.6	-42.7	-28.7	15.9	-36.7	-75.0	18.6	-75.9
C	5	-36.4	16.4	-30.2	-13.2	7.3	-25.5	-50.8	12.6	-53.4
C	SUM	-221.7		-170.9	-180.5		-228.6	-402.4		-368.4
D	1	-16.4	16.8	-19.4	126.4	22.8	106.5	110.0	24.1	82.0
D	2	-21.8	22.4	-20.6	148.9	26.9	132.8	127.0	27.8	108.2
D	3	-21.6	22.2	-17.5	115.7	20.9	99.8	94.1	20.6	83.1
D	4	-21.6	22.2	-15.1	97.4	17.6	87.7	75.8	16.6	74.6
D	5	-15.9	16.3	-10.1	65.6	11.8	76.2	49.7	10.9	66.2
D	SUM	-97.3		-82.7	553.9		502.9	456.6		414.1
LOAD	PX (KIPS)	-100.0		-100.0	0.		0.	-100.0		-100.0
LOAD	PY (KIPS)	0.		-0	-100.0		-100.0	-100.0		-98.7
ACTUAL	PX (KIPS)			-12.7	0.		0.	-12.9		-12.9
ACTUAL	PY (KIPS)			-0	-12.7		-12.7	-12.7		-12.7



**TABLE 261**  
**DISTRIBUTION OF MOMENTS TO EACH GIRDER**  
**( KIP-FT AND PERCENTAGE )**

**MOMENTS ABOUT ENTIRE GRCS SECTION N.A.**  
**RESULTS FOR POINT LOADS**  
**APPLIED AFTER 24 KSI CCND. LOADING.**  
**SIMPLY SUPPORTED, NO RESTRAINTS.**



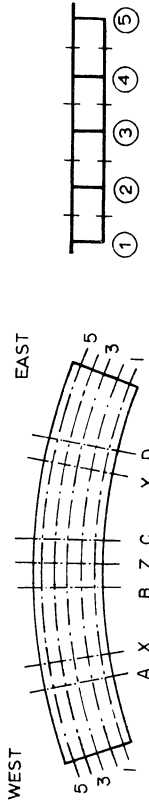
SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	116.1	105.4	21.0	-16.1	-10.7	16.2	100.0	21.8	90.8	21.9
A	2	139.9	122.4	24.4	-21.8	-13.7	22.0	118.0	25.8	102.8	24.8
A	3	119.5	104.5	20.8	-22.1	-12.4	20.7	97.4	21.3	84.1	20.3
A	4	107.1	103.5	20.6	-22.7	-13.6	22.6	84.4	18.4	84.0	20.3
A	5	74.6	66.6	13.3	-16.8	-9.6	16.1	57.8	12.6	52.7	12.7
A	SUM	557.1	502.4		-99.4	-60.0		457.7		414.3	
B	1	-27.6	-39.5	18.2	-56.6	-33.5	22.9	-80.1	20.0	-65.7	18.9
B	2	-42.4	-54.6	25.2	-63.5	-40.8	25.8	-100.5	25.0	-88.1	25.3
B	3	-53.3	-61.6	28.4	-39.7	-27.8	17.6	-87.6	21.8	-84.5	24.3
B	4	-34.5	-40.7	18.7	-48.1	-32.3	20.4	-78.4	19.5	-68.9	19.8
B	5	-18.8	-20.6	9.5	-38.6	-24.0	15.2	-54.7	13.6	-41.0	11.8
B	SUM	-176.6	-216.9		-246.6	-158.4		-401.3		-348.3	
C	1	-47.2	-28.8	17.2	-39.5	-54.7	25.3	-86.7	21.5	-72.8	20.3
C	2	-55.4	-41.3	24.6	-48.2	-62.9	29.1	-103.4	25.7	-96.6	27.0
C	3	-36.9	-33.3	19.9	-50.8	-50.0	23.1	-86.4	21.5	-80.1	22.4
C	4	-45.8	-37.2	22.2	-28.7	-31.3	14.5	-75.0	18.6	-66.0	18.4
C	5	-36.4	-27.0	16.1	-13.2	-17.1	7.9	-50.8	12.6	-42.5	11.9
C	SUM	-221.7	-167.6		-180.5	-216.0		-402.4		-358.0	
D	1	-16.4	-10.5	16.0	126.4	90.0	22.8	110.0	24.1	71.2	18.8
D	2	-21.8	-15.8	23.9	148.9	137.4	29.8	127.0	27.8	115.8	30.6
D	3	-21.6	-14.0	21.2	115.7	89.0	19.3	94.1	20.6	74.5	19.7
D	4	-21.6	-16.5	25.1	97.4	85.1	18.5	75.8	16.6	67.5	17.8
D	5	-15.9	-9.1	13.8	65.6	59.6	12.9	49.7	10.9	49.2	13.0
D	SUM	-97.3	-65.9		553.9	461.1		456.6		378.3	
LOAD	PX (KIPS)	-100.0	-100.0		0.	0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.	-0		-100.0	-100.0		-100.0		-98.7	
ACTUAL	PX (KIPS)		-12.7			0.				-12.9	
ACTUAL	PY (KIPS)		-0			-12.7				-12.7	

TABLE 26J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.A.

RESULTS FGR POINT LOADS  
APPLIED AFTER 24 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	116.1	20.8	99.1	20.1	-16.1	16.2	-13.4	20.9	100.0	21.8	85.6	21.1
A	2	139.9	25.1	122.8	24.9	-21.8	22.0	-13.5	21.1	118.0	25.8	103.5	25.5
A	3	119.5	21.4	105.8	21.4	-22.1	22.2	-12.4	19.4	97.4	21.3	84.5	20.9
A	4	107.1	19.2	102.4	20.8	-22.7	22.8	-14.6	22.9	84.4	18.4	82.5	20.4
A	5	74.6	13.4	63.5	12.9	-16.8	16.9	-10.0	15.6	57.8	12.6	49.2	12.1
A	SUM	557.1		493.7		-99.4		-63.9		457.7		405.2	
B	1	-27.6	15.6	-41.7	19.4	-56.6	22.9	-35.6	22.3	-80.1	20.0	-71.9	20.6
B	2	-42.4	24.0	-53.8	25.0	-63.5	25.8	-40.8	25.6	-100.5	25.0	-88.1	25.2
B	3	-53.3	30.2	-59.8	27.8	-39.7	16.1	-28.7	17.9	-87.6	21.8	-82.8	23.7
B	4	-34.5	19.6	-39.2	18.3	-48.1	19.5	-31.0	19.4	-78.4	19.5	-66.1	18.9
B	5	18.8	10.6	-20.3	9.5	-38.6	15.7	-23.6	14.8	-54.7	13.6	-40.3	11.5
B	SUM	-176.6		-214.8		-246.6		-159.8		-401.3		-349.1	
C	1	-47.2	21.3	-30.2	18.0	-39.5	21.9	-56.1	25.9	-86.7	21.5	-77.7	21.6
C	2	-55.4	25.0	-42.4	25.3	-48.2	26.7	-63.0	29.1	-103.4	25.7	-98.2	27.3
C	3	-36.9	16.7	-33.0	19.7	-50.8	28.2	-48.7	22.5	-86.4	21.5	-78.1	21.7
C	4	-45.8	20.6	-35.5	21.2	-28.7	15.5	-29.8	13.7	-75.0	18.6	-62.7	17.5
C	5	-36.4	16.4	-26.4	15.8	-13.2	7.3	-19.2	8.9	-50.8	12.6	-42.4	11.8
C	SUM	-221.7		-167.6		-180.5		-216.8		-402.4		-359.1	
D	1	-16.4	16.8	-12.9	19.1	126.4	22.8	86.2	19.1	110.0	24.1	68.9	18.6
D	2	-21.8	22.4	-15.2	22.4	148.9	26.9	138.4	30.7	127.0	27.8	117.6	31.8
D	3	-21.6	22.2	-13.9	20.4	115.7	20.9	87.3	19.3	94.1	20.6	73.1	19.8
D	4	-21.6	22.2	-17.0	25.1	97.4	17.6	84.2	18.7	75.8	16.6	65.6	17.7
D	5	-15.9	16.3	-8.8	12.9	65.6	11.8	55.0	12.2	49.7	10.9	44.9	12.1
D	SUM	-97.3		-67.8		553.9		451.2		456.6		370.1	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		-0		-100.0		-100.0		-100.0		-98.7	
ACTUAL	PX (KIPS)			-12.7				0.				-12.9	
ACTUAL	PY (KIPS)			-0				-12.7				-12.7	

TABLE 27A  
SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 24 KSI COND. LOADING.  
TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	NORMALIZED POINT LOADS APPLIED AT			
	(3-X)		(3-Y)	
	THEORY	EXPERM	THEORY	EXPERM
1E	-0.07	1.58	-2.53	-1.15
2E	-1.42	-3.62	8.65	13.64
3E	-1.32	-1.57	15.17	8.18
4E	-1.78	.04	9.25	-1.56
5E	-3.27	-4.57	8.15	17.80
1F	-3.10	10.02	37.97	38.19
2F	-3.02	7.61	38.15	39.08
3F	37.65	25.70	-3.40	-4.24
4F	37.57	26.71	-3.58	-2.19
1W	.98	6.30	-.08	.20
2W	8.09	1.02	-1.37	.20
3W	9.08	10.04	-1.35	-3.38
4W	9.17	7.78	-1.83	-1.49
5W	11.45	14.78	-3.22	-3.71
RE	-7.86	-8.14	38.69	36.91
RF	69.10	70.04	69.16	70.84
RW	38.77	39.92	-7.85	-8.18
SUMR	100.01	101.82	100.00	99.57
PX	-100.00	-100.00	0.	0.
PY	0.	0.	-100.00	-100.00
SUMP	-100.00	-100.00	-100.00	-100.00
SUMR/SUMP	1.00	1.02	1.00	1.00
TW	56.66	61.03	-17.34	-24.47
MF	122.04	52.17	-124.65	-125.55
TF	-.24	5.13	-.54	1.74
TE	-17.39	-22.23	56.50	58.40
ACTUAL PX		-12.78		0.
ACTUAL PY		0.		-12.74

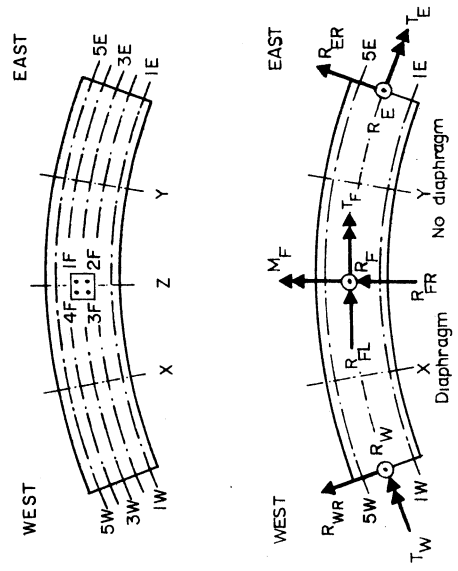
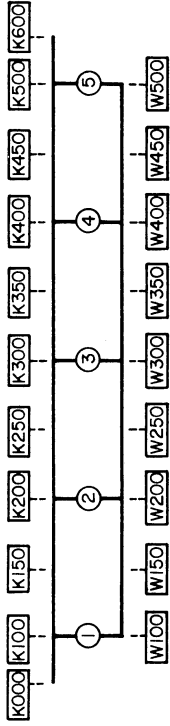




TABLE 27C

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 24 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	-314	-241	68	73	-245	-213
K	K100	-277	-473	59	150	-218	-422
K	K150	-292	-303	50	66	-201	-243
K	K200	-251	-402	52	103	-216	-353
K	K250	-289	-300	50	60	-208	-242
K	K300	-268	-387	52	93	-199	-343
K	K350	-249	-330	50	73	-208	-291
K	K400	-266	-404	58	97	-208	-357
K	K450	-289	-299	65	67	-223	-265
K	K500	-289	-338	65	90	-223	-299
K	K600	-289	-208	65	56	-223	-190
W	W100	1044	973	-217	-222	826	853
W	W150	969	617	-196	-169	772	657
W	W200	1048	889	-211	-222	836	831
W	W250	958	684	-196	-178	762	675
W	W300	982	933	-210	-221	771	804
W	W350	956	797	-210	-188	762	684
W	W400	731	873	-210	-218	771	763
W	W450	940	725	-210	-183	771	676
W	W500	765	994	-210	-253	771	846
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-96.6
ACTUAL	PX (KIPS)	-12.8	-12.8	0.	0.	-12.8	-12.8
ACTUAL	PY (KIPS)	0.	0.	-12.7	-12.7	-12.7	-12.4

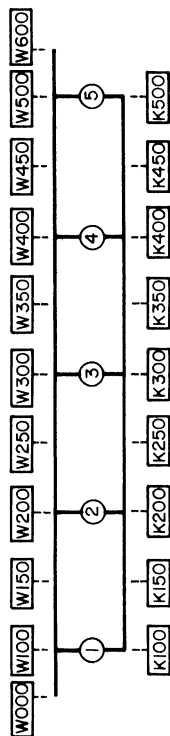
TABLE 27D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 24 KSI CJND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
W	W000	194	260	260	448	279	642
W	W100	196	284	287	399	307	596
W	W150	222	235	270	314	278	530
W	W200	222	326	324	287	290	623
W	W250	335	332	371	228	240	586
W	W300	226	402	428	214	267	684
W	W350	226	313	364	308	247	588
W	W400	201	313	311	381	272	581
W	W450	186	268	305	408	261	578
W	W500	186	243	246	381	247	490
W	W600	186	243	243	408	259	492
K	K100	-90	-170	-171	-180	-192	-344
K	K150	-99	-183	-175	-149	-207	-352
K	K200	-99	-207	-204	-149	-178	-363
K	K250	-133	-237	-236	-92	-168	-358
K	K300	-102	-245	-248	-145	-167	-370
K	K350	-92	-214	-216	-168	-180	-359
K	K400	-92	-167	-167	-168	-185	-329
K	K450	-92	-159	-166	-168	-171	-328
K	K500	-92	-153	-151	-168	-160	-299
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-96.6
ACTUAL	PX (KIPS)	-12.8	-12.8	0.	0.	-12.8	-12.8
ACTUAL	PY (KIPS)	0.	0.	-12.7	-12.7	-12.4	-12.4

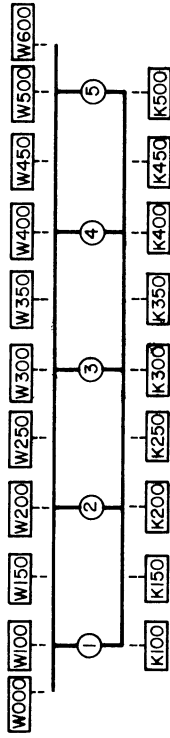
TABLE 27E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 24 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)		
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	ADJUST
W	W000	451	251	185	207	636	483	483
W	W100	403	250	187	215	591	487	487
W	W150		226		218		453	474
W	W200	309	306	232	375	541	704	705
W	W250		211		351		567	540
W	W300	204	252	368	476	572	756	745
W	W350		192		304		504	528
W	W400	309	267	226	297	535	632	658
W	W450		231		218		459	485
W	W500	393	253	178	207	571	481	472
W	W600	421	264	159	213	580	492	492
K	K100	-182	-189	-87	-146	-269	-346	-342
K	K150		-172		-149		-332	-314
K	K200	-147	-175	-103	-189	-250	-389	-396
K	K250		-153		-243		-423	-453
K	K300	-88	-138	-145	-290	-234	-453	-452
K	K350		-165		-258		-456	-438
K	K400	-146	-167	-100	-167	-247	-351	-345
K	K450		-218		-169		-399	-390
K	K500	-174	-179	-80	-129	-255	-516	-313
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0	
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-96.6	
ACTUAL	PX (KIPS)		-12.8		0.		-12.8	
ACTUAL	PY (KIPS)		0.		-12.7		-12.4	

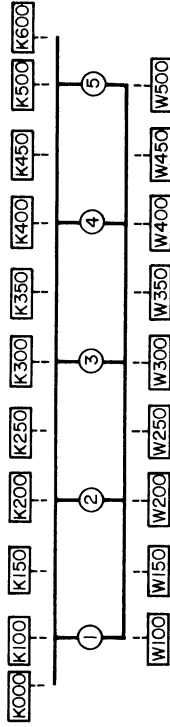
TABLE 27F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 24 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS APPLIED AT

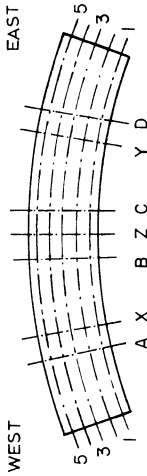
GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
K	K000	62	34	-278	-153	-215	-116
K	K100	53	60	-241	-291	-187	-214
K	K150		112		-552		-368
K	K200	45	83	-231	-407	-186	-296
K	K250		65		-350		-276
K	K300	46	69	-238	-352	-192	-262
K	K350		98		-501		-362
K	K400	44	79	-225	-395	-181	-255
K	K450		116		-603		-386
K	K500	50	82	-226	-427	-176	-298
K	K600	57	28	-250	-138	-193	-295
W	W100	-224	-104	1042	651	818	454
W	W150		-141		846		548
W	W200	-199	-170	994	1037	794	695
W	W250		-157		945		614
W	W300	-211	-135	1049	851	837	582
W	W350		-150		791		542
W	W400	-192	-190	958	1034	766	711
W	W450		-156		805		540
W	W500	-206	-162	955	934	749	662
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-96.6
ACTUAL	PX (KIPS)		-12.8		0.		-12.8
ACTUAL	PY (KIPS)		0.		-12.7		-12.4



TABLE 27G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR POINT LOADS  
APPLIED AFTER 24 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT

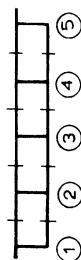
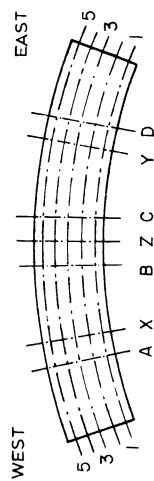
SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1	92.9	67.0	16.3	-19.5	-14.8	16.7	73.4	59.9	16.2
A	2	129.6	111.8	22.8	-26.1	-26.5	22.4	103.5	99.1	22.9
A	3	130.4	120.3	22.9	-25.8	-28.7	22.2	104.6	105.0	23.1
A	4	127.8	119.7	22.5	-26.0	-29.5	22.3	101.8	104.2	22.5
A	5	88.4	174.7	15.5	-19.0	-18.5	16.3	69.4	63.5	15.3
A	SUM	569.0	493.6		-116.3	-118.1		452.7	431.8	
B	1	-27.5	-33.3	12.5	-48.8	-35.3	18.4	-77.0	-66.9	15.9
B	2	-48.2	-48.9	22.0	-61.5	-41.2	23.2	-109.9	-88.9	22.7
B	3	-66.7	-63.8	30.4	-48.3	-40.4	18.3	-113.8	-101.4	23.5
B	4	-49.2	-49.8	22.6	-60.0	-41.0	22.7	-109.2	-88.9	22.5
B	5	-27.9	-32.7	12.7	-46.1	-32.7	17.4	-74.5	-63.9	15.4
B	SUM	-219.6	-228.5		-264.8	-190.4		-484.4	-410.0	
C	1	-49.2	-32.3	18.6	-26.8	-28.2	12.0	-76.4	-63.0	15.7
C	2	-60.9	-43.2	23.0	-50.2	-54.1	22.4	-110.5	-99.4	22.8
C	3	-46.9	-37.2	17.7	-72.3	-64.9	32.3	-116.8	-104.2	24.1
C	4	-60.4	-41.5	22.8	-49.2	-49.7	22.0	-109.0	-96.8	22.4
C	5	-47.5	-32.8	17.9	-25.2	-28.8	11.3	-73.0	-63.6	15.0
C	SUM	-265.0	-187.1		-223.7	-225.8		-485.8	-427.0	
D	1	-20.0	-9.1	17.2	92.3	57.0	16.2	72.3	38.7	16.0
D	2	-26.5	-21.3	22.7	132.1	130.7	23.2	105.6	89.8	23.3
D	3	-25.8	-18.5	22.2	131.1	112.7	23.0	105.3	76.8	23.3
D	4	-25.6	-23.5	22.0	127.5	126.4	22.4	102.0	87.5	22.5
D	5	-18.6	-12.7	16.0	85.8	68.7	15.1	67.2	47.2	14.8
D	SUM	-116.4	-85.1		568.7	495.6		452.3	340.0	
LOAD	PX (KIPS)	-100.0	-100.0		0.	0.		-100.0	-100.0	
LOAD	PY (KIPS)	0.	0.		-100.0	0.		-100.0	-96.6	
ACTUAL	PX (KIPS)	0.	-12.8		0.	0.		-12.8	-12.8	
ACTUAL	PY (KIPS)	0.	0.		-12.7	-12.7		-12.7	-12.4	

TABLE 27H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 24 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



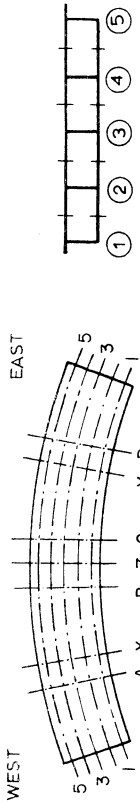
NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	92.9	16.3	103.6	19.5	-19.5	16.7	-35.3	26.2	73.4	16.2	90.7	19.4
A	2	129.6	22.8	111.9	21.1	-26.1	22.4	-24.3	18.0	103.5	22.9	96.7	20.7
A	3	130.4	22.9	107.2	20.2	-25.8	22.2	-24.4	18.1	104.6	23.1	93.1	19.9
A	4	127.8	22.5	120.2	22.7	-26.0	22.3	-28.5	21.1	101.8	22.5	107.6	23.1
A	5	88.4	15.5	87.4	16.5	-19.0	16.3	-22.4	16.6	69.4	15.3	78.4	16.8
A	SUM	569.0		530.3		-115.3		-135.1		452.7		466.5	
B	1	-27.5	12.5	-28.2	12.1	-48.8	18.4	-33.5	15.6	-77.0	15.9	-57.5	14.0
B	2	-48.2	22.0	-57.6	24.8	-61.5	23.2	-51.7	24.1	-109.9	22.7	-100.2	24.4
B	3	-66.7	30.4	-70.7	30.4	-48.3	18.3	-50.7	23.6	-113.8	23.5	-107.1	26.1
B	4	-49.2	22.4	-49.7	21.4	-60.0	22.7	-51.3	23.9	-109.2	22.5	-94.2	22.9
B	5	-27.9	12.7	-26.0	11.2	-46.1	17.4	-27.4	12.8	-74.5	15.4	-51.7	12.6
B	SUM	-219.6		-232.3		-264.8		-214.6		-484.4		-410.7	
C	1	-49.2	18.6	-30.5	14.7	-26.8	12.0	-23.2	9.7	-76.4	15.7	-55.6	11.8
C	2	-60.9	23.0	-49.2	23.7	-50.2	22.4	-54.1	22.6	-110.5	22.8	-110.1	23.4
C	3	-46.9	17.7	-44.2	21.3	-72.3	32.3	-84.2	35.2	-116.8	24.1	-136.9	29.1
C	4	-60.4	22.8	-50.2	24.1	-49.2	22.0	-53.2	22.2	-109.0	22.4	-108.1	23.0
C	5	-47.5	17.9	-33.7	16.2	-25.2	11.3	-24.8	10.3	-73.0	15.0	-59.8	12.7
C	SUM	-265.0		-207.7		-223.7		-239.5		-485.8		-470.5	
D	1	-20.0	17.2	-18.2	15.7	92.3	16.2	84.7	14.9	72.3	16.0	61.9	15.4
D	2	-26.5	22.7	-24.5	21.2	132.1	23.2	119.1	21.0	105.6	23.3	86.1	21.4
D	3	-25.8	22.2	-23.0	19.9	131.1	23.0	117.3	20.6	105.3	23.3	82.3	20.5
D	4	-25.6	22.0	-25.8	22.3	127.5	22.4	127.3	22.4	102.0	22.5	88.8	22.1
D	5	-18.6	16.0	-24.0	20.8	85.8	15.1	119.9	21.1	67.2	14.8	85.1	20.7
D	SUM	-116.4		-115.5		568.7		568.3		452.3		402.1	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-96.6	
ACTUAL	PX (KIPS)			-12.8		0.		0.				-12.8	
ACTUAL	PY (KIPS)			0.		-12.7		-12.7				-12.4	

TABLE 21  
DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 24 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



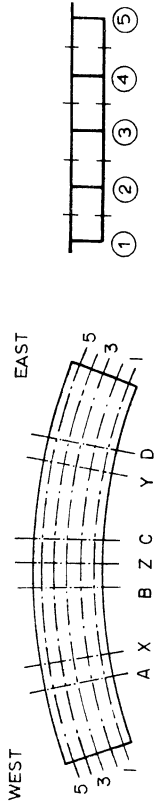
SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)				
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT		
A	1	92.9	83.4	16.3	-19.5	-24.0	16.7	-24.0	73.4	16.2	73.7	16.5
A	2	129.6	111.9	21.9	-26.1	-25.6	22.4	-25.6	103.5	22.9	98.1	21.9
A	3	130.4	114.5	22.4	-25.8	-26.8	22.2	-26.8	104.6	23.1	99.7	22.3
A	4	127.8	120.0	23.5	-26.0	-29.1	22.3	-29.1	101.8	22.5	105.8	23.6
A	5	88.4	80.4	15.8	-19.0	-20.3	16.3	-20.3	69.4	15.3	70.2	15.7
A	SUM	569.0	510.1		-116.3	-125.7		-125.7	452.7		447.4	
B	1	-27.5	-30.5	13.2	-48.8	-34.3	18.4	-34.3	-77.0	15.9	-61.7	15.0
B	2	-48.2	-53.7	23.3	-61.5	-47.0	23.2	-47.0	-109.9	22.7	-95.2	23.2
B	3	-66.7	-67.6	29.3	-48.3	-46.1	18.3	-46.1	-113.8	23.5	-104.6	25.5
B	4	-49.2	-49.8	21.6	-60.0	-46.7	22.9	-46.7	-109.2	22.5	-91.8	22.4
B	5	-27.9	-29.0	12.6	-46.1	-29.8	14.6	-29.8	-74.5	15.4	-57.1	13.9
B	SUM	-219.6	-230.7		-264.8	-203.9		-203.9	-484.4		-410.5	
C	1	-49.2	-31.3	15.8	-26.8	-25.5	12.0	-25.5	-76.4	15.7	-58.9	13.1
C	2	-60.9	-46.5	23.4	-50.2	-54.1	23.2	-54.1	-110.5	22.8	-105.3	23.3
C	3	-46.9	-41.1	20.7	-72.3	-75.6	32.4	-75.6	-116.8	24.1	-122.4	27.1
C	4	-60.4	-46.3	23.3	-49.2	-51.7	22.1	-51.7	-109.0	22.4	-103.1	22.8
C	5	-47.5	-33.3	16.8	-25.2	-26.6	11.4	-26.6	-73.0	15.0	-61.5	13.6
C	SUM	-265.0	-198.6		-223.7	-233.4		-233.4	-485.8		-451.2	
D	1	-20.0	-13.2	13.4	92.3	69.4	16.2	69.4	72.3	16.0	49.0	13.3
D	2	-26.5	-22.7	23.0	132.1	125.6	23.2	125.6	105.6	23.3	88.2	24.0
D	3	-25.8	-20.5	20.8	131.1	114.8	21.7	114.8	105.3	23.3	79.3	21.6
D	4	-25.6	-24.5	24.8	127.5	126.8	24.0	126.8	102.0	22.5	88.1	24.0
D	5	-18.6	-17.8	18.0	85.8	91.6	17.3	91.6	67.2	14.8	63.2	17.2
D	SUM	-116.4	-98.7		568.7	528.2		528.2	452.3		367.8	
LOAD	PX (KIPS)	-100.0	0.		0.	0.		0.	-100.0		-100.0	
LOAD	PY (KIPS)	0.	0.		-100.0	-100.0		-100.0	-100.0		-96.6	
ACTUAL	PX (KIPS)		-12.8			0.					-12.8	
ACTUAL	PY (KIPS)		0.			-12.7					-12.4	

TABLE 27J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 24 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	92.9	16.3	78.7	15.6	-19.5	16.7	-22.9	18.4	73.4	16.2	69.7	15.8
A	2	129.6	22.8	111.9	22.2	-26.1	22.4	-25.8	20.6	103.5	22.9	98.3	22.2
A	3	130.4	22.9	116.5	23.1	-25.8	22.2	-27.5	22.0	104.6	23.1	101.5	22.9
A	4	127.8	22.5	119.9	23.7	-26.0	22.3	-29.2	23.4	101.8	22.5	105.4	23.8
A	5	88.4	15.5	77.9	15.4	-19.0	16.3	-19.5	15.6	69.4	15.3	67.4	15.2
A	SUM	569.0		504.9		-116.3		-124.9		452.7		442.4	
B	1	-27.5	12.5	-31.4	13.7	-48.8	18.4	-34.6	17.3	-77.0	15.9	-63.4	15.5
B	2	-48.2	22.0	-52.3	22.7	-61.5	23.2	-45.2	22.6	-109.9	22.7	-93.1	22.7
B	3	-66.7	30.4	-66.3	28.8	-48.3	18.3	-44.4	22.2	-113.8	23.5	-103.4	25.2
B	4	-49.2	22.4	-49.8	21.7	-60.0	22.7	-45.2	22.6	-109.2	22.5	-90.8	22.1
B	5	-27.9	12.7	-30.2	13.1	-46.1	17.4	-30.6	15.3	-74.5	15.4	-59.3	14.5
B	SUM	-219.6		-230.0		-264.8		-199.8		-484.4		-409.9	
C	1	-49.2	18.6	-31.6	16.2	-26.8	12.0	-26.2	11.4	-76.4	15.7	-60.0	13.6
C	2	-60.9	23.0	-45.4	23.3	-50.2	22.4	-54.1	23.4	-110.5	22.8	-103.2	23.3
C	3	-46.9	17.7	-39.7	20.4	-72.3	32.3	-72.3	31.3	-116.8	24.1	-116.6	26.3
C	4	-60.4	22.8	-44.7	23.0	-49.2	22.0	-50.9	22.1	-109.0	22.4	-100.7	22.8
C	5	-47.5	17.9	-33.2	17.0	-25.2	11.3	-27.3	11.8	-73.0	15.0	-62.1	14.0
C	SUM	-265.0		-194.6		-223.7		-230.8		-485.8		-442.5	
D	1	-20.0	17.2	-12.4	13.0	92.3	16.2	65.5	12.6	72.3	16.0	46.1	12.8
D	2	-26.5	22.7	-22.4	23.4	132.1	23.2	127.4	24.6	105.6	23.3	88.7	24.7
D	3	-25.8	22.2	-20.1	21.0	131.1	23.0	114.1	22.0	105.3	23.3	78.5	21.8
D	4	-25.6	22.0	-24.1	25.3	127.5	22.4	126.5	24.4	102.0	22.5	87.9	24.4
D	5	-18.6	16.0	-16.5	17.3	85.8	15.1	84.6	16.3	67.2	14.8	58.3	16.2
D	SUM	-116.4		-95.4		568.7		518.3		452.3		359.5	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-96.6	
ACTUAL	PX (KIPS)			-12.8				0.				-12.8	
ACTUAL	PY (KIPS)			0.				-12.7				-12.4	

TABLE 28A  
SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR PJINT LOADS  
MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 24 KSI CCND. LOADING.  
TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	(5-X)		(5-Y)		(5-X)+(5-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	-8.14	-3.82	-23.25	-21.67	-31.35	-25.74
2E	-2.93	-8.84	-1.70	-3.45	-4.63	-10.97
3E	-1.37	-1.57	2.03	7.86	.67	4.68
4E	-.71	4.86	12.87	10.04	12.16	13.94
5E	2.95	-.76	46.35	43.78	49.30	45.59
1F	10.14	10.00	53.96	48.21	64.05	70.84
2F	-17.30	-14.74	26.17	16.98	8.87	15.36
3F	26.89	29.33	-17.04	-13.26	9.84	3.94
4F	54.33	51.42	10.75	19.09	65.07	59.55
1W	-26.90	-17.22	-8.12	-6.44	-35.03	-24.10
2W	.30	-15.82	-2.90	-3.78	-2.60	-18.75
3W	5.47	8.30	-1.39	-3.46	4.08	3.82
4W	14.38	16.14	-.72	-.59	13.66	16.86
5W	42.90	44.81	3.00	4.23	45.91	50.72
RE	-10.20	-10.13	36.30	36.56	26.11	27.50
RF	74.05	76.01	73.83	71.02	147.88	149.69
RW	36.15	36.21	-10.13	-10.04	26.02	28.55
SUMR	100.00	102.09	100.00	97.54	200.01	205.74
PX	-100.00	-100.00	0.	.01	-100.00	-100.00
PY	0.	.01	-100.00	-100.00	-100.00	-101.44
SUMP	-100.00	-99.99	-100.00	-99.99	-200.00	-201.44
SUMR/SUMP	1.00	1.02	1.00	.98	1.00	1.02
TW	395.40	401.42	62.83	63.11	458.34	476.63
MF	132.56	128.23	-129.62	-89.04	2.94	-34.07
TF	82.32	70.24	83.37	95.37	165.69	166.63
TE	62.78	50.99	395.63	371.96	458.42	431.14
ACTUAL PX		-12.73		.01		-12.47
ACTUAL PY		.01		-12.53		-12.65

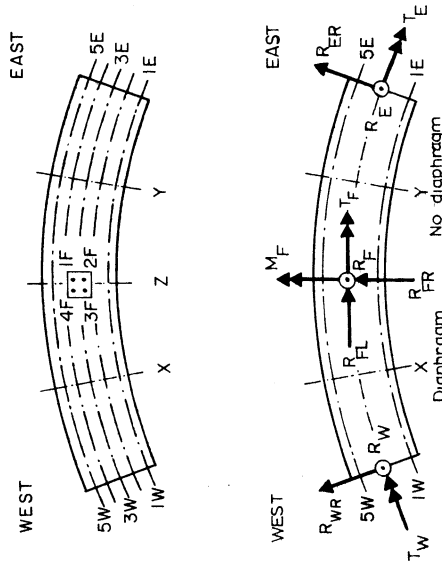
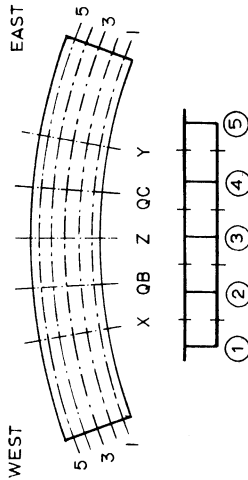


TABLE 28B  
SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

RESULTS FOR POINT LOADS  
APPLIED AFTER 24 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



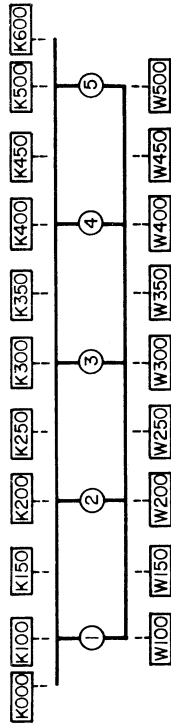
DEFLECTION AT POINT	(5-X)		(5-Y)		NORMALIZED POINT LOADS APPLIED AT		(5-X)+(5-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X	.535	.729	-0.329	-0.370	1.12	1.12	.205	.276
2X	.673	.914	-0.306	-0.355	1.16	1.16	.367	.463
3X	.831	1.115	-0.284	-0.355	1.25	1.25	.547	.665
4X	1.019	1.330	-0.264	-0.314	1.19	1.19	.755	.904
5X	1.234	1.555	-0.246	-0.299	1.21	1.21	.988	1.163
1QB	.267	.382	-0.326	-0.346	1.06	1.06	-0.059	-0.048
2QB	.372	.507	-0.283	-0.318	1.12	1.12	.089	.130
3QB	.489	.633	-0.241	-0.264	1.10	1.10	.248	.299
4QB	.636	.783	-0.207	-0.217	1.05	1.05	.429	.490
5QB	.791	.937	-0.166	-0.192	1.16	1.16	.624	.691
1Z	-.127	-.104	-.126	-.123	.98	.98	-0.253	-0.237
2Z	-.061	-.044	-.061	-.050	.82	.82	-0.123	-0.104
4Z	.078	.071	.079	.094	1.19	1.19	.157	.163
5Z	.158	.167	.162	.198	1.22	1.22	.321	.377
1QC	-.331	-.390	.255	.318	1.25	1.25	-0.077	-0.030
2QC	-.287	-.345	.348	.431	1.24	1.24	.061	.124
3QC	-.244	-.300	.468	.553	1.18	1.18	.224	.297
4QC	-.209	-.255	.638	.764	1.20	1.20	.430	.533
5QC	-.168	-.210	.829	1.010	1.22	1.22	.661	.801
1Y	-.337	-.413	.504	.627	1.24	1.24	.168	.267
2Y	-.311	-.407	.614	.755	1.23	1.23	.303	.422
3Y	-.238	-.372	.773	.949	1.23	1.23	.486	.633
4Y	-.266	-.376	1.009	1.279	1.27	1.27	.743	1.010
5Y	-.246	-.336	1.361	1.715	1.26	1.26	1.116	1.402
LOAD PX	-100.0	-100.0	0.	0.			-100.0	-100.0
LOAD PY	0.	0.	-100.0	-100.0			-100.0	-101.4
ACTUAL PX			-12.7	0.			-12.5	-12.5
ACTUAL PY			0.	-12.5			-12.6	-12.6

TABLE 28C  
SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
APPLIED AFTER 24 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)	
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
K	K000	-303	-267	-267	83	56	-192
K	K100	-250	-465	-446	71	150	-317
K	K150		-284	-295		61	-209
K	K200	-228	-387	-417	60	106	-294
K	K250		-307	-326		51	-255
K	K300	-262	-394	-395	61	103	-283
K	K350		-355	-384		79	-282
K	K400	-280	-488	-488	58	106	-361
K	K450		-373	-419		75	-287
K	K500	-335	-485	-490	67	98	-376
K	K600	-412	-300	-300	75	61	-222
W	W100	928	925	941	-265	-251	613
W	W150		729	593		-157	476
W	W200	862	931	879	-236	-244	623
W	W250		728	683		-197	478
W	W300	1033	1006	1017	-250	-226	756
W	W350		836	915		-183	698
W	W400	1091	1036	1060	-228	-224	810
W	W450		866	901		-191	675
W	W500	1315	1419	1414	-243	-224	1205
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	0.	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-101.4
ACTUAL	PX (KIPS)		-12.7	0.		0.	-12.5
ACTUAL	PY (KIPS)		0.	-12.5		-12.5	-12.6

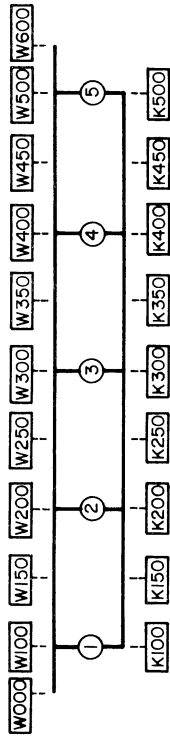
TABLE 28D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 24 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS APPLIED AT

GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	252	214	499	274	751	504
W	W100	245	259	443	292	688	569
W	W150	249	241	325	274	574	532
W	W200	382	343	232	270	615	654
W	W250	303	403	389	234	692	667
W	W300	318	488	526	296	845	798
W	W350	309	443	564	286	873	757
W	W400	-110	454	-195	340	-306	670
W	W450	-113	450	-155	393	-268	810
W	W500	-153	426	-102	347	-255	881
W	W600	-139	431	-187	341	-326	762
K	K100	-147	-225	-236	-185	-384	768
K	K150	-170	-174	-241	-242	-462	-468
K	K200	-253	-243	-275	-257	-457	-443
K	K250	-249	-226	-204	-201	-461	-448
K	K300	-245	-252	-180	-179	-440	-417
K	K350	-218	-218	-187	-184	-443	-448
K	K400	-187	-182	-215	-217	-435	-437
K	K450	-255	-244	-227	-234	-404	-405
K	K500	-243	-244	-194	-210	-430	-432
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-101.4
ACTUAL	PX (KIPS)	-12.7	-12.7	0.	0.	-12.5	-12.5
ACTUAL	PY (KIPS)	0.	0.	-12.5	-12.5	-12.6	-12.6

LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-101.4
ACTUAL	PX (KIPS)	-12.7	-12.7	0.	0.	-12.5	-12.5
ACTUAL	PY (KIPS)	0.	0.	-12.5	-12.5	-12.6	-12.6



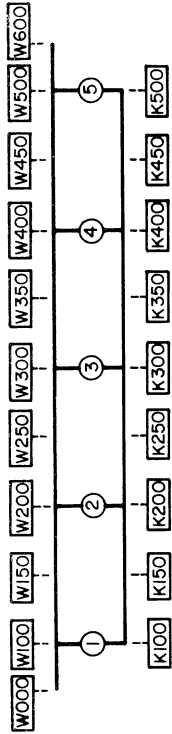
TABLE 38E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 24 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

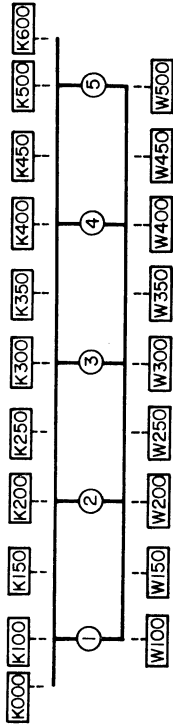


GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)			
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST		
W	W000	511	272	272	199	139	711	431	431
W	W100	451	269	274	209	155	661	449	448
W	W150		244	264		159		433	448
W	W200	338	323	324	217	360	555	689	689
W	W250		256	251		281		550	526
W	W300	240	312	308	357	480	598	794	788
W	W350		251	266		320		602	643
W	W400	388	373	392	310	478	698	899	915
W	W450		331	352		358		697	706
W	W500	510	368	357	376	430	886	795	792
W	W600	545	374	374	383	463	929	836	836
K	K100	-200	-239	-238	-89	-214	-290	-437	-433
K	K150		-215	-222		-187		-385	-362
K	K200	-161	-224	-231	-97	-196	-259	-407	-415
K	K250		-205	-210		-220		-402	-438
K	K300	-105	-188	-187	-144	-248	-249	-418	-405
K	K350		-205	-195		-373		-549	-520
K	K400	-185	-214	-206	-145	-231	-331	-417	-427
K	K450		-303	-285		-150		-429	-442
K	K500	-228	-217	-215	-177	-270	-405	-440	-435
LOAD	PX (KIPS)	-100.0	-100.0		0.			-100.0	-100.0
LOAD	PY (KIPS)	0.	0.		-100.0	-100.0		-100.0	-101.4
ACTUAL	PX (KIPS)		-12.7		0.				-12.5
ACTUAL	PY (KIPS)		0.		-12.5				-12.6

TABLE 28F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 24 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

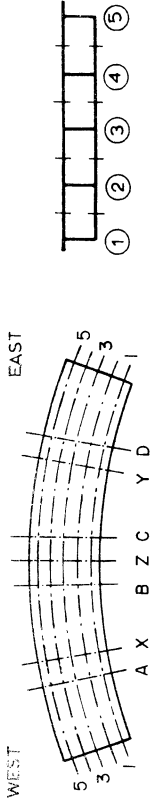


SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)		MEASR	ADJUST	THEORY	MEASR	ADJUST
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR					
K	K000	75	34	-243	-136	-167	-100					
K	K100	64	69	-205	-238	-141	-180					
K	K150		124	-190	-468	-135	-381					
K	K200	54	108	-226	-345	-171	-270					
K	K250		79	-226	-319	-171	-252					
K	K300	55	95	-226	-379	-171	-304					
K	K350		142	-264	-514	-212	-421					
K	K400	52	117	-318	-474	-259	-612					
K	K450		186	-379	-718	-312	-843					
K	K500	59	130	-379	-531	-312	-443					
K	K600	67	41	-379	-209	-312	-159					
W	W100	-271	-168	829	496	558	376					394
W	W150		-209		645		535					477
W	W200	-240	-252	806	780	566	616					593
W	W250		-232		739		594					563
W	W300	-252	-190	1015	713	762	566					579
W	W350		-187		888		781					749
W	W400	-226	-252	1187	1353	960	1193					1131
W	W450		-211		1134		978					997
W	W500	-242	-249	1386	744	1143	537					630
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0					
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-101.4					
ACTUAL	PX (KIPS)		-12.7		0.		-12.5					
ACTUAL	PY (KIPS)		0.		-12.5		-12.6					

TABLE 100  
DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )



MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR POINT LOADS  
APPLIED AFTER 24 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

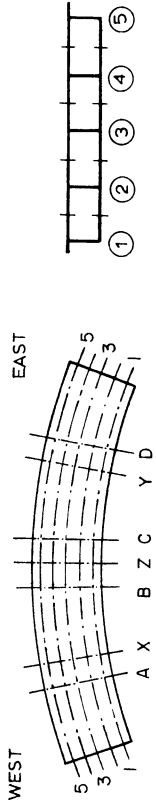
SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)				
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT		
A	1	83.4	64.5	11.7	-23.6	17.2	-15.9	13.4	59.8	13.4	45.1	10.9
A	2	115.8	109.8	20.0	-31.3	22.7	-26.7	24.1	84.5	19.0	80.1	19.3
A	3	126.6	130.8	23.8	-30.5	22.2	-29.2	24.5	96.0	21.6	97.2	23.4
A	4	143.1	144.0	26.2	-30.3	22.0	-28.7	24.1	112.8	25.4	109.2	26.3
A	5	113.2	101.2	18.4	-22.0	16.0	-16.6	13.9	91.3	20.5	83.1	20.0
A	SUM	582.1	550.4		-137.8		-119.1		444.4		414.6	
B	1	-33.3	-28.0	10.2	-54.0	17.1	-33.2	15.7	-87.5	14.9	-63.3	12.6
B	2	-54.8	-49.8	18.1	-65.8	20.8	-38.6	18.2	-120.3	20.5	-93.6	18.6
B	3	-77.2	-73.4	26.8	-54.7	17.3	-43.7	20.6	-130.4	22.2	-120.7	24.0
B	4	-65.5	-69.6	25.4	-77.6	24.5	-51.1	24.1	-142.7	24.3	-125.2	24.9
B	5	-42.9	-53.6	19.5	-64.2	20.3	-45.2	21.3	-107.2	18.2	-100.1	19.9
B	SUM	-273.7	-274.4		-316.3		-211.9		-588.1		-502.9	
C	1	-55.2	-35.0	14.8	-28.0	10.4	-16.7	6.8	-83.5	14.3	-55.7	11.1
C	2	-68.0	-47.7	20.2	-48.5	18.1	-44.7	18.2	-116.3	19.9	-95.5	19.1
C	3	-56.1	-46.8	19.8	-73.3	27.3	-62.6	25.5	-127.8	21.9	-113.0	22.6
C	4	-76.9	-59.0	24.9	-68.5	25.5	-67.2	27.4	-144.5	24.7	-132.6	26.5
C	5	-62.3	-48.1	20.4	-50.4	18.8	-54.3	22.1	-112.2	19.2	-103.3	20.7
C	SUM	-318.5	-236.6		-268.8		-245.6		-584.3		-500.1	
D	1	-24.1	-15.2	12.4	76.3	13.1	43.1	9.0	52.2	11.7	33.7	8.5
D	2	-31.8	-32.5	26.4	108.9	18.7	98.2	20.6	77.1	17.3	77.9	19.7
D	3	-30.7	-26.9	21.5	125.0	21.4	97.7	20.5	94.2	21.2	79.9	20.2
D	4	-30.2	-30.5	25.1	152.7	26.2	164.0	34.5	122.5	27.5	144.1	36.4
D	5	-21.9	-17.9	14.5	120.6	20.7	73.0	15.3	98.7	22.2	59.9	15.1
D	SUM	-138.7	-122.9		583.5		475.9		444.7		395.5	
LOAD	PX (KIPS)	-100.0	-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.	0.		-100.0		-100.0		-100.0		-101.4	
ACTUAL	PX (KIPS)	-12.7	-12.7		0.		0.		0.		-12.5	
ACTUAL	PY (KIPS)	0.	0.		-12.5		-12.5		-12.5		-12.6	

TABLE 28H:

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 24 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT  
(5-Y)

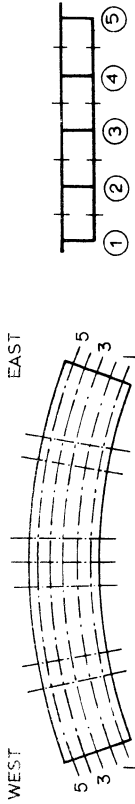
SECTION	GIRDER	(5-X)		(5-Y)		(5-X)+(5-Y)			
		THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT		
A	1	83.4	14.3	103.0	17.6	19.8	13.4	74.1	17.4
A	2	115.8	19.9	112.0	19.1	-31.3	22.7	84.5	19.0
A	3	126.6	21.7	113.9	19.4	-30.5	22.2	96.0	21.6
A	4	143.1	24.6	138.8	23.7	-30.3	22.0	112.8	25.4
A	5	113.2	19.5	118.7	20.2	-22.0	16.0	91.3	20.5
A	SUM	582.1		596.5		-137.8		444.4	
B	1	-33.3	12.2	-34.3	13.1	-54.0	17.1	-87.5	14.9
B	2	-54.8	20.0	-62.1	23.7	-65.8	20.8	-120.3	20.5
B	3	-77.2	28.2	-69.3	26.4	-54.7	17.3	-130.4	22.2
B	4	-65.5	23.9	-56.0	21.3	-77.6	24.5	-142.7	24.3
B	5	-42.9	15.7	-40.6	15.5	-64.2	20.3	-107.2	18.2
B	SUM	-273.7		-262.3		-316.3		-588.1	
C	1	-55.2	17.3	-40.8	15.0	-28.0	10.4	-83.5	14.3
C	2	-68.0	21.4	-65.1	24.0	-48.5	18.1	-116.3	19.9
C	3	-56.1	17.6	-58.7	21.7	-73.3	27.3	-127.8	21.9
C	4	-76.9	24.2	-63.9	23.6	-68.5	25.5	-144.5	24.7
C	5	-62.3	19.5	-42.6	15.7	-50.4	18.8	-112.2	19.2
C	SUM	-318.5		-271.0		-268.8		-584.3	
D	1	-24.1	17.4	-19.3	12.1	76.3	13.1	52.2	11.7
D	2	-31.8	22.9	-30.1	18.9	108.9	18.7	77.1	17.3
D	3	-30.7	22.2	-30.7	19.3	125.0	21.4	94.2	21.2
D	4	-30.2	21.8	-40.1	25.2	152.7	26.2	122.5	27.5
D	5	-21.9	15.8	-38.8	24.4	120.6	20.7	98.7	22.2
D	SUM	-138.7		-159.0		583.5		444.7	
LOAD	PX (KIPS)	-100.0		-100.0		0.		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0	
ACTUAL	PX (KIPS)			-12.7		0.		-12.5	
ACTUAL	PY (KIPS)			0.		-12.5		-12.6	

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DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 24 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



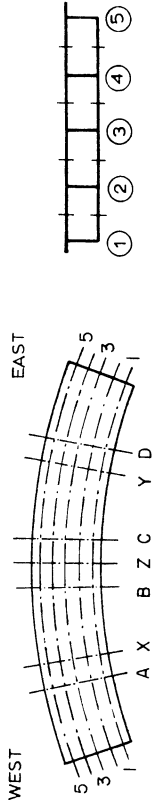
NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1	83.4	81.7	14.4	-23.6	-24.6	17.2	-23.6	13.4	58.1
A	2	115.8	110.8	19.6	-31.3	-27.1	22.7	-31.3	19.0	80.7
A	3	126.6	123.3	21.8	-30.5	-26.7	22.2	-30.5	21.6	91.3
A	4	143.1	141.7	25.0	-30.3	-28.8	22.0	-30.3	25.4	105.0
A	5	113.2	109.1	19.2	-22.0	-20.2	16.0	-22.0	20.5	84.9
A	SUM	582.1	566.6		-137.8	-127.5		-137.8	444.4	420.0
B	1	-33.3	-31.5	11.8	-54.0	-39.0	17.1	-54.0	14.9	-71.9
B	2	-54.8	-56.6	21.2	-65.8	-50.7	21.4	-65.8	20.5	-110.5
B	3	-77.2	-71.2	26.6	-54.7	-50.9	21.5	-54.7	22.2	-125.2
B	4	-65.5	-62.0	23.2	-77.6	-58.4	24.5	-77.6	24.3	-120.3
B	5	-42.9	-46.4	17.3	-64.2	-37.4	20.3	-64.2	18.2	-81.7
B	SUM	-273.7	-267.7		-316.3	-236.4		-316.3	-588.1	-509.5
C	1	-55.2	-38.2	14.9	-28.0	-26.4	10.4	-28.0	14.3	-64.4
C	2	-68.0	-57.3	22.4	-48.5	-50.5	18.1	-48.5	19.9	-106.7
C	3	-56.1	-53.4	20.9	-73.3	-73.4	27.3	-73.3	21.9	-124.2
C	4	-76.9	-61.7	24.1	-68.5	-70.8	25.5	-68.5	24.7	-130.1
C	5	-62.3	-45.1	17.6	-50.4	-44.8	18.8	-50.4	19.2	-86.2
C	SUM	-318.5	-255.7		-268.8	-265.9		-268.8	-584.3	-511.7
D	1	-24.1	-17.0	12.2	76.3	55.8	13.1	76.3	11.7	44.1
D	2	-31.8	-31.4	22.6	108.9	100.6	18.7	108.9	17.3	79.4
D	3	-30.7	-28.4	20.4	125.0	107.8	20.0	125.0	21.2	88.0
D	4	-30.2	-35.0	25.2	152.7	161.9	30.0	152.7	27.5	140.2
D	5	-21.9	-27.2	19.6	120.6	113.0	21.0	120.6	22.2	93.7
D	SUM	-138.7	-139.0		583.5	539.0		583.5	444.7	445.2
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	0.		0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	0.	-100.0	-100.0		-100.0	-101.4	-101.4
ACTUAL	PX (KIPS)		-12.7	0.		0.			-12.5	-12.5
ACTUAL	PY (KIPS)		0.	0.		-12.5			-12.6	-12.6

TABLE 28J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 24 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT  
(5-Y)

SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1	83.4	76.9	13.7	-23.6	-23.0	17.2	59.8	55.0	13.4
A	2	115.8	110.5	19.7	-31.3	-27.5	22.7	84.5	80.6	19.0
A	3	126.6	126.1	22.5	-30.5	-27.5	22.2	96.0	93.6	21.6
A	4	143.1	142.4	25.4	-30.3	-28.8	22.0	112.8	106.3	25.4
A	5	113.2	105.7	18.8	-22.0	-19.1	16.0	91.3	84.1	20.5
A	SUM	582.1	561.7		-137.8	-126.0		444.4	419.5	
B	1	-33.3	-30.9	11.4	-54.0	-38.0	17.1	-87.5	-70.3	14.9
B	2	-54.8	-54.9	20.2	-65.8	-47.9	20.8	-120.3	-106.0	20.7
B	3	-77.2	-72.1	26.5	-54.7	-48.7	17.3	-130.4	-123.6	24.2
B	4	-65.5	-65.7	24.1	-77.6	-56.5	24.4	-142.7	-122.2	23.9
B	5	-42.9	-48.8	17.9	-64.2	-40.4	20.3	-107.2	-88.7	17.4
B	SUM	-273.7	-272.4		-316.3	-231.4		-588.1	-510.8	
C	1	-55.2	-37.7	15.0	-28.0	-26.8	10.4	-83.5	-63.4	14.3
C	2	-68.0	-54.9	21.9	-48.5	-48.3	18.1	-116.3	-103.1	19.9
C	3	-56.1	-51.3	20.5	-73.3	-69.1	27.3	-127.8	-119.8	23.5
C	4	-76.9	-60.7	24.2	-68.5	-69.4	25.5	-144.5	-131.2	25.7
C	5	-62.3	-46.0	18.4	-50.4	-47.8	18.8	-112.2	-92.3	18.1
C	SUM	-318.5	-250.6		-268.8	-261.5		-584.3	-509.9	
D	1	-24.1	-16.4	12.1	76.3	52.2	13.1	52.2	41.1	11.7
D	2	-31.8	-31.8	23.6	108.9	99.8	18.7	77.1	78.9	17.3
D	3	-30.7	-27.9	20.7	125.0	105.6	21.4	94.2	86.3	21.2
D	4	-30.2	-33.8	25.1	152.7	162.7	26.2	122.5	141.8	27.5
D	5	-21.9	-25.0	18.6	120.6	108.6	20.7	98.7	91.4	22.2
D	SUM	-138.7	-134.8		583.5	528.9		444.7	439.5	
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	0.		-100.0	-100.0	
LOAD	PY (KIPS)	0.	0.	0.	-100.0	-100.0		-100.0	-101.4	
ACTUAL	PX (KIPS)		-12.7	0.	0.	0.			-12.5	
ACTUAL	PY (KIPS)		0.	0.	-12.5	-12.5			-12.6	

TABLE 2.28A  
SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 24 KSI COND. LOADING.  
TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

NORMALIZED POINT LOADS APPLIED AT

REACTION OR LOAD	(1-X)+(5-Y)		THEORY EXPERM		THEORY EXPERM	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	-15.18	-14.50				
2E	-1.65	-3.33				
3E	.72	6.40				
4E	9.96	8.60				
5E	36.73	34.45				
1F	37.82	42.65				
2F	37.77	31.49				
3F	31.36	25.69				
4F	31.41	36.42				
1W	29.07	23.73				
2W	8.98	13.22				
3W	2.20	8.55				
4W	.15	.62				
5W	-9.33	-13.67				
RE	30.58	31.62				
RF	138.36	136.25				
RW	31.07	32.45				
SUMR	200.01	200.32				
PX	-100.00	-100.00				
PY	-100.00	-99.60				
SUMP	-200.00	-199.60				
SUMR/SUMP	1.00	1.00				
TW	-220.32	-224.87				
MF	-19.22	-18.04				
TF	.15	32.83				
TE	296.99	282.58				
ACTUAL PX						-12.78
ACTUAL PY						-12.73

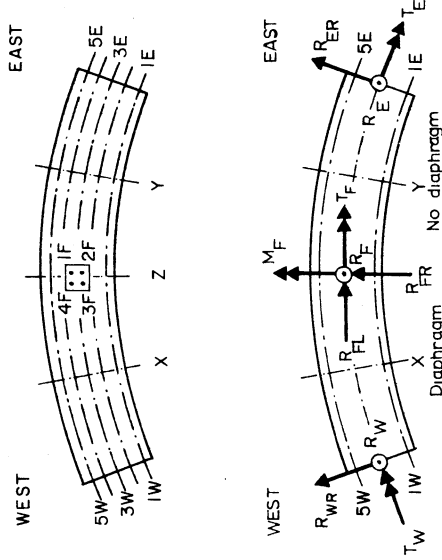






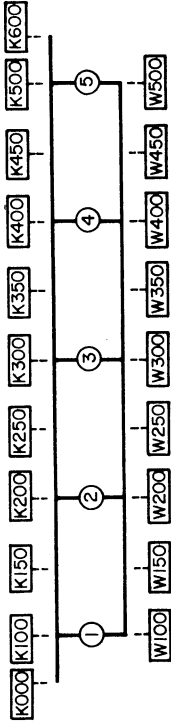
TABLE 29C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 24 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS APPLIED AT

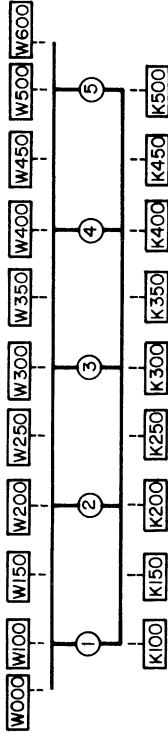
GAGE TYPE	GAGE LOC.	((1-X)+(5-Y))		*****		*****		*****		
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
K	K000	-347	-268	-268						
K	K100	-269	-513	-499						
K	K150		-276	-288						
K	K200	-211	-366	-386						
K	K250		-202	-203						
K	K300	-183	-297	-289						
K	K350		-226	-222						
K	K400	-152	-265	-277						
K	K450		-188	-234						
K	K500	-159	-201	-199						
K	K600	-186	-139	-139						
W	W100	1100	962	963						
W	W150		595	552						
W	W200	823	794	771						
W	W250		620	510						
W	W300	720	642	641						
W	W350		512	483						
W	W400	568	552	539						
W	W450		501	440						
W	W500	573	574	567						

LOAD	PX (KIPS)	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-99.6
ACTUAL	PX (KIPS)	-12.8	
ACTUAL	PY (KIPS)	-12.7	

TABLE 29D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 24 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

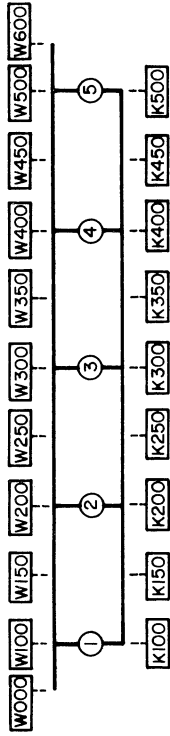
NORMALIZED POINT LOADS APPLIED AT

GAGE TYPE	GAGE LOC.	(1-X)+(5-Y)		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	ADJUST	ADJUST	MEASR	ADJUST
W	W000	684	602	602			
W	W100	632	625	629			
W	W150		523	579			
W	W200	510	579	590			
W	W250		511	537			
W	W300	488	629	643			
W	W350		475	547			
W	W400	536	532	536			
W	W450		479	557			
W	W500	657	456	462			
W	W600	678	455	455			
K	K100	-287	-385	-388			
K	K150		-469	-436			
K	K200	-238	-333	-334			
K	K250		-350	-372			
K	K300	-202	-372	-368			
K	K350		-376	-380			
K	K400	-253	-345	-355			
K	K450		-278	-307			
K	K500	-295	-282	-274			
LOAD	PX (KIPS)	-100.0	-100.0	-100.0			
LOAD	PY (KIPS)	-100.0	-99.6				
ACTUAL	PX (KIPS)		-12.8				
ACTUAL	PY (KIPS)		-12.7				

TABLE 29E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 24 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

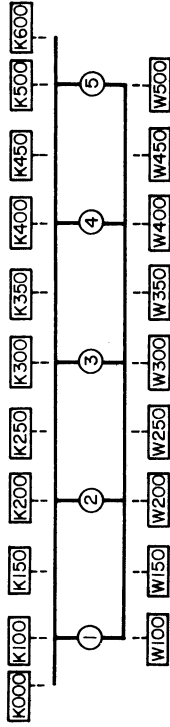
NORMALIZED POINT LOADS APPLIED AT

GAGE TYPE	GAGE LOC.	(1-X)+(5-Y)		MEASR		ADJUST		THEORY		MEASR		ADJUST	
		THEORY	MEASR	THEORY	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST		
W	W000	624	409	409	409								
W	W100	596	434	423	379								
W	W150		385	379	660								
W	W200	498	659	427	682								
W	W250		456	427	682								
W	W300	512	682	488	673								
W	W350		464	488	673								
W	W400	541	673	503	585								
W	W450		513	585	621								
W	W500	680	580	621									
W	W600	709	621										
K	K100	-267	-358	-350									
K	K150		-318	-272									
K	K200	-232	-327	-333									
K	K250		-329	-381									
K	K300	-211	-345	-330									
K	K350		-496	-467									
K	K400	-256	-355	-373									
K	K450		-302	-335									
K	K500	-310	-393	-387									

LOAD	PX (KIPS)	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-99.6
ACTUAL	PX (KIPS)	-12.8	
ACTUAL	PY (KIPS)	-12.7	

TABLE 29F

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 24 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

NORMALIZED POINT LOADS APPLIED AT

GAGE TYPE	GAGE LOC.	(1-X) + (5-Y)		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
K	K000	-191	-91	-172	-91		
K	K100	-161	-172	-330	-175		
K	K150	-152	-330	-264	-305		
K	K200	-237	-264	-301	-257		
K	K250	-187	-237	-413	-264		
K	K300	-227	-301	-403	-312		
K	K350	-275	-413	-615	-440		
K	K400	-330	-403	-461	-399		
K	K450		-615	-173	-634		
K	K500		-461		-466		
K	K600		-173		-461		
W	W100	646	374	646	388		
W	W150		475		447		
W	W200	642	610	589	591		
W	W250		589		556		
W	W300	837	553	711	568		
W	W350		711		704		
W	W400	1024	1137	931	1078		
W	W450		931		944		
W	W500	1209	515		609		

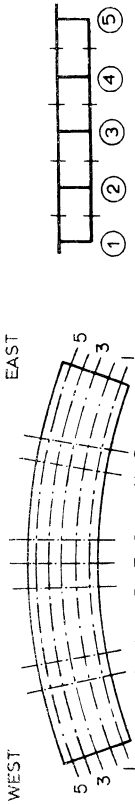
LOAD	PX (KIPS)	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-99.6
ACTUAL	PX (KIPS)		-12.8
ACTUAL	PY (KIPS)		-12.7

TABLE 29C

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR POINT LOADS  
APPLIED AFTER 24 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT

\*\*\*\*\*  
THEORY PCT  
K-FT  
\*\*\*\*\*  
EXPERIMENTAL  
K-FT PCT  
\*\*\*\*\*

\*\*\*\*\*  
THEORY PCT  
K-FT  
\*\*\*\*\*  
EXPERIMENTAL  
K-FT PCT  
\*\*\*\*\*

(1-X)+(5-Y)  
\*\*\*\*\*  
THEORY PCT  
K-FT  
\*\*\*\*\*  
EXPERIMENTAL  
K-FT PCT  
\*\*\*\*\*

SECTION	GIRDER	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
A	1	92.4	22.0	63.3	17.8
A	2	108.5	25.9	94.5	26.6
A	3	88.9	21.2	81.1	22.8
A	4	76.8	18.3	72.8	20.5
A	5	52.6	12.5	43.5	12.2
A	SUM	419.3		355.2	
B	1	-80.8	16.6	-73.5	18.5
B	2	-106.4	21.9	-86.7	21.8
B	3	-105.0	21.6	-94.0	23.7
B	4	-111.4	22.9	-82.3	20.7
B	5	-83.2	17.1	-60.9	15.3
B	SUM	-486.9		-397.5	
C	1	-76.1	15.6	-50.9	12.7
C	2	-104.4	21.3	-85.4	21.4
C	3	-109.0	22.3	-92.6	23.2
C	4	-113.5	23.2	-95.9	24.0
C	5	-86.5	17.7	-74.4	18.6
C	SUM	-489.5		-399.2	
D	1	59.9	12.3	32.3	8.5
D	2	87.1	17.9	76.3	20.1
D	3	103.4	21.3	77.5	20.4
D	4	131.1	27.0	136.5	36.0
D	5	104.7	21.5	56.5	14.9
D	SUM	486.2		379.2	

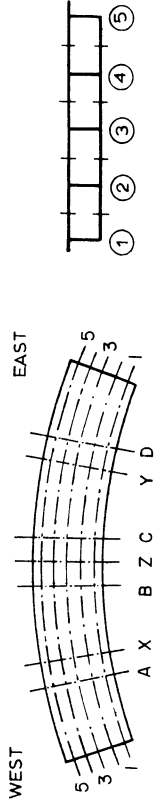
LOAD	PX (KIPS)	-100.0
LOAD	PY (KIPS)	-99.6
ACTUAL	PX (KIPS)	-12.8
ACTUAL	PY (KIPS)	-12.7

TABLE 29H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 24 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	(1-X)+(5-Y)		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	92.4	22.0	111.9	26.8		
A	2	108.5	25.9	95.7	22.9		
A	3	88.9	21.2	75.5	18.1		
A	4	76.8	18.3	80.1	19.2		
A	5	52.6	12.5	54.6	13.1		
A	SUM	419.3		417.8			
B	1	-80.8	16.6	-69.3	16.1		
B	2	-106.4	21.9	-104.2	24.2		
B	3	-105.0	21.6	-110.4	25.7		
B	4	-111.4	22.9	-99.2	23.1		
B	5	-83.2	17.1	-47.0	10.9		
B	SUM	-486.9		-430.0			
C	1	-76.1	15.6	-54.7	12.7		
C	2	-104.4	21.3	-91.9	21.3		
C	3	-109.0	22.3	-113.8	26.3		
C	4	-113.5	23.2	-110.8	25.6		
C	5	-86.5	17.7	-61.1	14.1		
C	SUM	-489.5		-432.3			
D	1	59.9	12.3	50.3	10.2		
D	2	87.1	17.9	76.0	15.4		
D	3	103.4	21.3	94.6	19.2		
D	4	131.1	27.0	131.9	26.8		
D	5	104.7	21.5	139.0	28.3		
D	SUM	486.2		491.9			
LOAD	PX (KIPS)	-100.0		-100.0			
LOAD	PY (KIPS)	-100.0		-99.6			
ACTUAL	PX (KIPS)			-12.8			
ACTUAL	PY (KIPS)			-12.7			

\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT

\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT

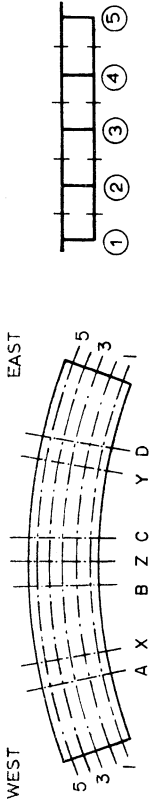
\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT

\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT

TABLE 28  
DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 24 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



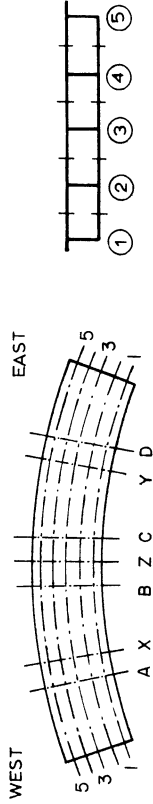
NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	(1-X)+(5-Y)		THEORY		EXPERIMENTAL		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	92.4	22.0	85.0	22.2						
A	2	108.5	25.9	95.1	24.8						
A	3	88.9	21.2	78.6	20.5						
A	4	76.8	18.3	76.1	19.9						
A	5	52.6	12.5	48.5	12.6						
A	SUM	419.3		383.2							
B	1	-80.8	16.6	-71.2	17.1						
B	2	-106.4	21.9	-96.4	23.2						
B	3	-105.0	21.6	-103.1	24.8						
B	4	-111.4	22.9	-91.7	22.1						
B	5	-83.2	17.1	-53.2	12.8						
B	SUM	-486.9		-415.6							
C	1	-76.1	15.6	-53.0	12.7						
C	2	-104.4	21.3	-89.0	21.3						
C	3	-109.0	22.3	-104.4	25.0						
C	4	-113.5	23.2	-104.2	24.9						
C	5	-86.5	17.7	-67.0	16.1						
C	SUM	-489.5		-417.6							
D	1	59.9	12.3	40.4	9.4						
D	2	87.1	17.9	76.2	17.7						
D	3	103.4	21.3	85.2	19.8						
D	4	131.1	27.0	134.5	31.3						
D	5	104.7	21.5	93.4	21.7						
D	SUM	486.2		429.6							
LOAD	PX (KIPS)	-100.0		-100.0							
LOAD	PY (KIPS)	-100.0		-99.6							
ACTUAL	PX (KIPS)			-12.8							
ACTUAL	PY (KIPS)			-12.7							

**TABLE 29J**  
 DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
 APPLIED AFTER 24 KSI CGND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	THEORY		EXPERIMENTAL		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
***** (1-X)+(5-Y) *****									
A	1	92.4	22.0	79.9	21.3				
A	2	108.5	25.9	94.9	25.3				
A	3	88.9	21.2	79.3	21.1				
A	4	76.8	18.3	75.3	20.0				
A	5	52.6	12.5	46.4	12.3				
A	SUM	419.3		375.8					
B	1	-80.8	16.6	-71.9	17.5				
B	2	-106.4	21.9	-93.0	22.7				
B	3	-105.0	21.6	-100.0	24.4				
B	4	-111.4	22.9	-89.1	21.7				
B	5	-83.2	17.1	-55.7	13.6				
B	SUM	-486.9		-409.7					
C	1	-76.1	15.6	-52.6	12.8				
C	2	-104.4	21.3	-37.6	21.4				
C	3	-109.0	22.3	-99.5	24.3				
C	4	-113.5	23.2	-101.2	24.7				
C	5	-86.5	17.7	-69.1	16.9				
C	SUM	-489.5		-410.0					
D	1	59.9	12.3	37.9	8.9				
D	2	87.1	17.9	76.2	17.9				
D	3	103.4	21.3	83.6	19.6				
D	4	131.1	27.0	135.3	31.8				
D	5	104.7	21.5	92.3	21.7				
D	SUM	486.2		425.3					
LOAD	PX (KIPS)								
LOAD	PY (KIPS)	-100.0		-100.0					
ACTUAL	PX (KIPS)								
ACTUAL	PY (KIPS)								

LOAD PX (KIPS) -100.0  
 LOAD PY (KIPS) -100.0  
 ACTUAL PX (KIPS) -12.8  
 ACTUAL PY (KIPS) -12.7



TABLE 30A  
SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 40 KSI COND. LOADING.  
TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	NORMALIZED POINT LOADS APPLIED AT			
	(1-X)		(1-Y)	
	THEORY	EXPERM	THEORY	EXPERM
1E	8.07	6.97	41.39	23.25
2E	.05	1.29	9.57	25.03
3E	-1.31	-2.81	-.42	7.46
4E	-2.91	-4.22	-1.17	-2.39
5E	-9.62	-8.04	-8.32	-14.35
1F	-16.14	3.11	20.53	.26
2F	11.60	30.28	48.71	36.67
3F	48.40	31.49	11.88	31.94
4F	20.66	3.31	-16.30	-3.11
1W	37.19	30.14	8.03	6.96
2W	11.88	18.20	.12	2.64
3W	3.59	7.82	-1.36	-.02
4W	.87	1.43	-3.03	-6.20
5W	-12.33	-15.86	-9.62	-10.66
RE	-5.72	-6.81	41.05	39.00
RF	64.53	68.19	54.82	65.76
RW	41.20	41.73	-5.86	-7.28
SUMR	100.01	103.11	100.01	97.48
PX	-100.00	-100.00	0.	.01
PY	0.	.04	-100.00	-100.00
SUMP	-100.00	-99.96	-100.00	-99.99
SUMR/SUMP	1.00	1.03	1.00	.97
TW	-283.15	-279.85	-98.93	-113.41
MF	110.40	2.12	-110.50	-12.15
TF	-83.22	-83.02	-84.56	-107.19
TE	-98.64	-91.42	-283.43	-264.03
ACTUAL PX		-19.33		.02
ACTUAL PY		.01		-19.27

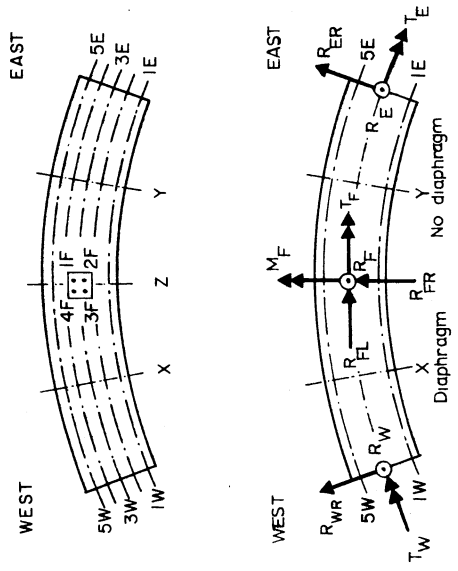
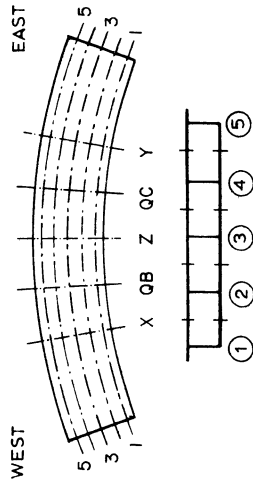


TABLE 30B

SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

RESULTS FOR POINT LOADS APPLIED AFTER 40 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

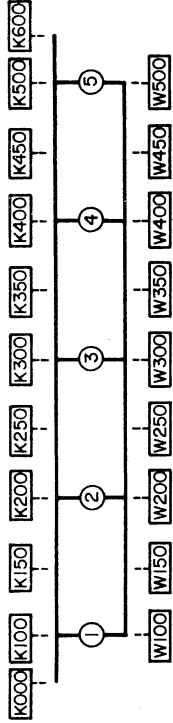


DEFLECTION AT POINT	(1-X)		(1-Y)		(1-X)+(1-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X	.942	1.524	-0.153	-0.145	.789	1.338
2X	.806	1.269	-0.198	-0.210	.608	1.016
3X	.692	1.041	-0.243	-0.283	.450	.712
4X	.605	.835	-0.289	-0.344	.316	.449
5X	.535	.658	-0.337	-0.407	.198	.198
1QB	.625	.985	-0.090	-0.083	.536	.895
2QB	.512	.779	-0.151	-0.169	.361	.586
3QB	.407	.571	-0.206	-0.250	.201	.315
4QB	.329	.412	-0.266	-0.334	.063	.054
5QB	.261	.282	-0.328	-0.421	-0.067	-0.185
1Z	.160	.252	.165	.261	.324	.535
2Z	.078	.119	.080	.125	.158	.255
4Z	-0.063	-0.095	-0.063	-0.069	-0.126	-0.198
5Z	-0.129	-0.203	-0.128	-0.195	-0.257	-0.420
1QC	-0.087	-0.090	.682	1.107	.595	1.083
2QC	-0.148	-0.184	.529	.807	.381	.656
3QC	-0.203	-0.260	.398	.539	.195	.274
4QC	-0.263	-0.345	.314	.365	.050	-0.003
5QC	-0.325	-0.435	.255	.238	-0.070	-0.215
1Y	-0.153	-0.159	1.101	2.000	.948	1.918
2Y	-0.197	-0.230	.825	1.299	.629	1.105
3Y	-0.239	-0.299	.658	.862	.419	.563
4Y	-0.283	-0.359	.559	.655	.276	.284
5Y	-0.329	-0.412	.504	.564	.175	.082
LOAD PX	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD PY	0.	0.	-100.0	-100.0	-100.0	-99.4
ACTUAL PX	0.	0.	0.	0.	0.	-19.3
ACTUAL PY	0.	0.	-19.3	-19.3	-19.1	-19.1

TABLE 30C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 40 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION A

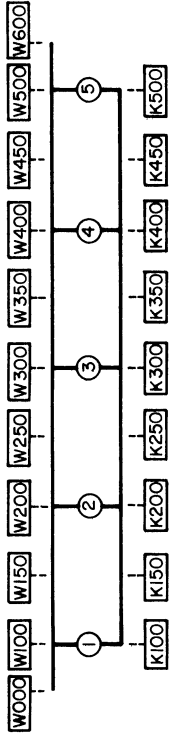
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	-431	-443	56	59	-374	-396
K	K100	-341	-916	48	116	-292	-860
K	K150		-416		52		-354
K	K200	-271	-510	42	67	-229	-458
K	K250		-258		50		-200
K	K300	-245	-425	44	52	-201	-376
K	K350		-330		33		-292
K	K400	-211	-380	44	53	-167	-329
K	K450		-260		27		-222
K	K500	-227	-275	51	42	-176	-235
K	K600	-261	-197	58	24	-203	-177
W	W100	1365	1334	-178	-40	1187	1252
W	W150		1053		-65		981
W	W200	1059	1059	-164	-76	895	939
W	W250		972		-36		864
W	W300	970	919	-181	-109	789	760
W	W350		768		-93		650
W	W400	796	733	-171	-145	625	578
W	W450		976		-29		896
W	W500	816	719	-187	-194	628	519
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-99.4
ACTUAL	PX (KIPS)		-19.3		0.		-19.3
ACTUAL	PY (KIPS)		0.		-19.3		-19.1

TABLE 300

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 40 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



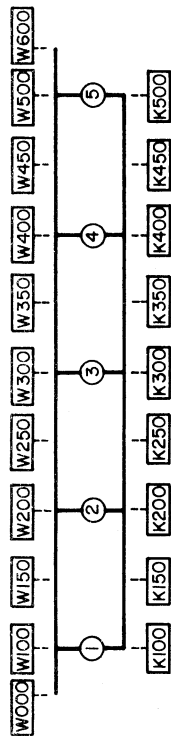
SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
W	W000	184	554	554	473	350	921
W	W100	189	451	457	427	353	846
W	W150	411	450	450	298	336	778
W	W200	185	406	418	291	364	768
W	W250	350	406	406	230	258	642
W	W300	256	422	426	149	199	597
W	W350	306	338	338	147	187	475
W	W400	147	183	184	222	170	344
W	W450	157	153	153	298	200	353
W	W500	130	112	112	298	178	254
W	W600	114	81	81	315	162	219
K	K100	-91	-242	-235	-197	-183	-409
K	K150	-335	-319	-319	-141	-153	-451
K	K200	-82	-149	-149	-174	-182	-330
K	K250	-133	-150	-150	-202	-202	-293
K	K300	-100	-221	-230	-66	-94	-306
K	K350	-198	-198	-200	-105	-112	-297
K	K400	-66	-149	-150	-105	-132	-271
K	K450	-115	-115	-130	-129	-150	-268
K	K500	-58	-124	-120	-129	-155	-262
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	0.	0.	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-99.4
ACTUAL	PX (KIPS)	-19.3	-19.3	0.	0.	0.	-19.3
ACTUAL	PY (KIPS)	0.	0.	-15.3	-15.3	-15.3	-19.1

TABLE 30E

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 40 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION C

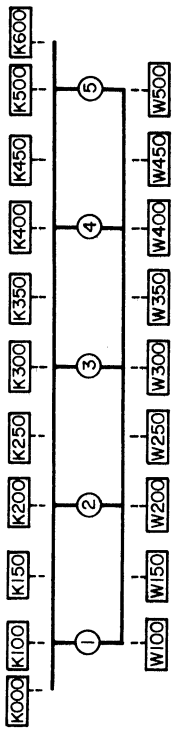
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)			
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST		
W	W000	425	329	329	302	715	728	1109	1109
W	W100	387	311	308	279	612	666	979	1000
W	W150		271	274	203	464	484	737	823
W	W200	280	406	404		520		916	910
W	W250		192	189		350		527	556
W	W300	154	206	211	241	364	396	585	586
W	W350		144	160		205		325	357
W	W400	231	223	227	121	154	353	363	380
W	W450		166	166		101		235	254
W	W500	304	185	184	95	51	400	203	196
W	W600	326	186	186	62	0	388	136	136
K	K100	-178	-173	-169	-137	-360	-315	-531	-511
K	K150		-150	-128		-319		-460	-462
K	K200	-134	-143	-141	-95	-189	-229	-323	-334
K	K250		-106	-115		-195		-292	-278
K	K300	-67	-100	-101	-95	-174	-163	-256	-254
K	K350		-139	-135		-107		-225	-229
K	K400	-110	-146	-148	-52	-90	-163	-218	-220
K	K450		-179	-181		-134		-299	-298
K	K500	-133	-178	-175	-37	-129	-171	-294	-291
LOAD	PX (KIPS)	-100.0	-100.0		0.	.0	-100.0	-100.0	
LOAD	PY (KIPS)	0.	0.		-100.0	-100.0		-99.4	
ACTUAL	PX (KIPS)		-19.3		.0	.0		-19.3	
ACTUAL	PY (KIPS)		0.		-19.3	-19.1			

TABLE 30F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 40 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

NORMALIZED POINT LOADS APPLIED AT

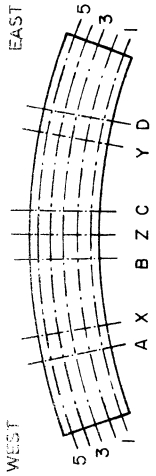
GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	51	43	-407	-297	-355	-269
K	K100	43	56	-331	-447	-287	-403
K	K150	129	128	-252	-555	-215	-497
K	K200	37	74	-252	-481	-215	-428
K	K250	74	72	-206	-346	-168	-288
K	K300	38	57	-206	-342	-168	-293
K	K350	83	92	-170	-397	-133	-340
K	K400	37	56	-170	-278	-133	-225
K	K450	55	55	-179	-387	-137	-317
K	K500	42	35	-201	-268	-153	-218
K	K600	48	14	-201	-91	-153	-72
W	W100	-183	-55	1480	570	1297	918
W	W150	-164	-64	1147	1359	983	1286
W	W200	-177	-98	930	1213	753	1104
W	W250	-163	-91	715	874	552	788
W	W300	-176	-120	696	789	519	606
W	W350	-183	-150	613	564	428	436
W	W400	-176	-185	620	624	403	403
W	W450	-176	-112	498	498	343	322
W	W500	-176	-95	620	613	468	468

LOAD PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-99.4

ACTUAL PX (KIPS)	-19.3	0.	-19.3	0.	-19.3	-19.1
ACTUAL PY (KIPS)	0.	0.	-19.3	-19.3	-19.3	-19.1

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
RESULTS FOR POINT LOADS  
APPLIED AFTER 40 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



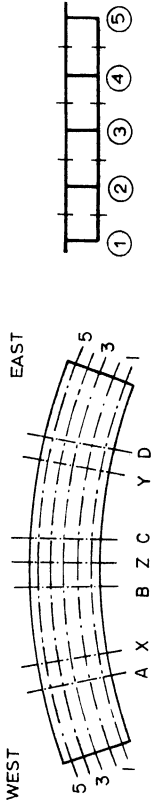
NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	116.1	95.9	20.8	-16.1	16.2	-0.9	100.0	21.8	90.6	21.0
A	2	139.9	144.8	25.1	-21.8	22.0	-9.1	118.0	25.8	130.7	30.3
A	3	119.5	121.7	23.9	-22.1	22.2	-13.3	97.4	21.3	101.8	23.5
A	4	107.1	95.4	19.2	-22.7	22.8	-19.3	84.4	18.4	73.2	16.9
A	5	74.6	51.8	13.4	-16.8	16.5	-14.3	57.8	12.6	35.8	8.3
A	SUM	557.1	509.6		-99.4		-56.8	457.7		432.1	
B	1	-27.6	-58.2	15.6	-56.6	22.9	-42.8	-80.1	20.0	-103.0	25.7
B	2	-42.4	-65.9	24.0	-63.5	25.8	-50.0	-100.5	25.0	-113.6	28.4
B	3	-53.3	-64.4	30.2	-39.7	16.1	-34.1	-87.6	21.8	-93.0	23.2
B	4	-34.5	-33.1	14.1	-48.1	19.5	-27.5	-78.4	19.5	-58.3	14.6
B	5	-18.8	-13.7	5.8	-38.6	15.7	-21.7	-54.7	13.6	-32.7	8.2
B	SUM	-176.6	-235.4		-246.6		-176.2	-401.3		-400.6	
C	1	-47.2	-39.7	21.3	-39.5	21.9	-86.1	-86.7	21.5	-130.2	30.2
C	2	-55.4	-52.3	29.4	-48.2	26.7	-85.4	-103.4	25.7	-135.1	31.3
C	3	-36.9	-31.4	17.7	-50.8	28.2	-56.4	-86.4	21.5	-86.4	20.0
C	4	-45.8	-31.8	17.9	-28.7	15.9	-27.0	-75.0	18.6	-56.6	13.1
C	5	-36.4	-22.4	12.6	-13.2	7.3	-5.9	-50.8	12.6	-23.4	5.4
C	SUM	-221.7	-177.5		-180.5		-260.9	-402.4		-431.7	
D	1	-16.4	-3.4	5.3	126.4	22.8	98.6	110.0	24.1	95.3	23.1
D	2	-21.8	-12.0	18.9	148.9	26.9	165.1	127.0	27.8	154.5	37.5
D	3	-21.6	-16.2	25.5	115.7	20.9	97.5	94.1	20.6	78.7	19.1
D	4	-21.6	-23.1	36.3	97.4	17.6	78.3	75.8	16.6	52.5	12.7
D	5	-15.9	-8.9	14.0	65.6	11.8	43.9	49.7	10.9	31.3	7.6
D	SUM	-97.3	-63.7		553.9		483.4	456.6		412.4	
LOAD	PX (KIPS)	-100.0	-100.0		0.		.0	-100.0		-100.0	
LOAD	PY (KIPS)	0.	.0		-100.0		.0	-100.0		-99.4	
ACTUAL	PX (KIPS)		-19.3							-19.3	
ACTUAL	PY (KIPS)		.0							-19.1	

**TABLE 30H**  
**DISTRIBUTION OF MOMENTS TO EACH GIRDER**  
**( KIP-FT AND PERCENTAGE )**

**MOMENTS ABOUT TENSION FLANGE STEEL**

**RESULTS FOR POINT LOADS**  
**APPLIED AFTER 40 KSI CCND. LOADING.**  
**SIMPLY SUPPORTED, NO RESTRAINTS.**



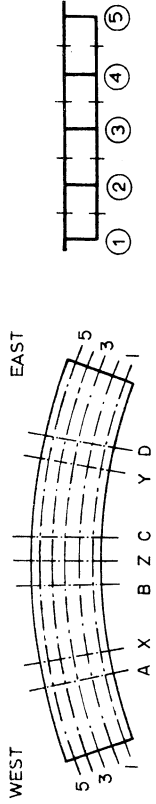
**NORMALIZED POINT LOADS APPLIED AT**

SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)					
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT			
A	1	116.1	20.8	219.1	34.0	-16.1	16.2	-30.7	34.3	100.0	21.8	202.4	36.2
A	2	139.9	25.1	126.0	19.6	-21.8	22.0	-22.0	24.5	118.0	25.8	107.7	19.3
A	3	119.5	21.4	106.3	16.5	-22.1	22.2	-15.2	17.0	97.4	21.3	89.7	16.0
A	4	107.1	19.2	115.5	17.9	-22.7	22.8	-12.4	13.8	84.4	18.4	94.0	16.8
A	5	74.6	13.4	76.7	11.9	-16.8	16.9	-9.3	10.3	57.8	12.6	65.1	11.6
A	SUM	557.1		643.6		-99.4		-89.6		457.7		558.9	
B	1	-27.6	15.6	-47.9	20.5	-56.6	22.9	-27.8	17.0	-80.1	20.0	-72.1	18.4
B	2	-42.4	24.0	-54.3	23.3	-63.5	25.8	-40.4	24.7	-100.5	25.0	-99.5	25.3
B	3	-53.3	30.2	-61.5	26.4	-39.7	16.1	-28.2	17.2	-87.6	21.8	-90.5	23.0
B	4	-34.5	19.6	-46.8	20.1	-48.1	19.5	-39.6	24.2	-78.4	19.5	-82.2	20.9
B	5	-18.8	10.6	-22.7	9.7	-38.6	15.7	-27.6	16.8	-54.7	13.6	-48.5	12.4
B	SUM	-176.6		-233.3		-246.6		-163.7		-401.3		-392.8	
C	1	-47.2	21.3	-25.3	14.4	-39.5	21.9	-59.3	25.3	-86.7	21.5	-83.2	21.5
C	2	-55.4	25.0	-35.9	20.5	-48.2	26.7	-69.3	29.5	-103.4	25.7	-98.9	25.5
C	3	-36.9	16.7	-34.5	19.7	-50.8	28.2	-48.6	20.7	-86.4	21.5	-76.0	19.6
C	4	-45.8	20.6	-46.3	26.4	-28.7	15.9	-30.7	13.1	-75.0	18.6	-71.3	18.4
C	5	-36.4	16.4	-33.3	19.0	-13.2	7.3	-26.8	11.4	-50.8	12.6	-58.1	15.0
C	SUM	-221.7		-175.3		-180.5		-234.7		-402.4		-387.6	
D	1	-16.4	16.8	-21.7	22.2	126.4	22.8	114.2	21.6	110.0	24.1	101.6	22.8
D	2	-21.8	22.4	-25.8	26.5	148.9	26.9	135.8	25.7	127.0	27.8	109.6	24.6
D	3	-21.6	22.2	-21.5	22.1	115.7	20.9	109.0	20.6	94.1	20.6	89.4	20.1
D	4	-21.6	22.2	-18.2	18.7	97.4	17.6	92.7	17.5	75.8	16.6	80.4	18.1
D	5	-15.9	16.3	-10.2	10.5	65.6	11.8	77.1	14.6	49.7	10.9	64.4	14.5
D	SUM	-97.3		-97.4		553.9		528.8		456.6		445.4	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-99.4	
ACTUAL	PX (KIPS)			-19.3				0.				-19.3	
ACTUAL	PY (KIPS)			0.				-19.3				-19.1	



TABLE 301  
DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT ENTIRE GROSS SECTION N.A.  
RESULTS FOR POINT LOADS  
APPLIED AFTER 40 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



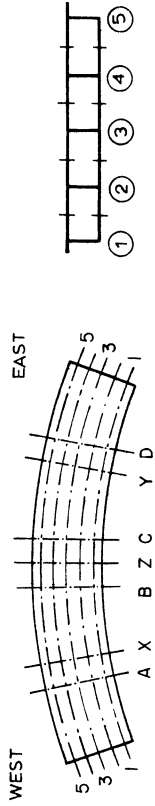
SECTION	GIRDER	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT	THEORY K-FT	EXPERIMENTAL PCT
A	1	116.1	20.8	-16.1	16.2	100.0	21.8
A	2	139.9	25.1	-21.8	22.0	118.0	25.8
A	3	119.5	21.4	-22.1	22.2	97.4	21.3
A	4	107.1	19.2	-22.7	22.8	84.4	18.4
A	5	74.6	13.4	-16.8	16.9	57.8	12.6
A	SUM	557.1		-99.4		457.7	
B	1	-27.6	15.6	-56.6	22.9	-80.1	20.0
B	2	-42.4	24.0	-63.5	25.8	-100.5	25.0
B	3	-53.3	30.2	-39.7	16.1	-87.6	21.8
B	4	-34.5	19.6	-48.1	19.5	-78.4	19.5
B	5	-18.8	10.6	-38.6	15.7	-54.7	13.6
B	SUM	-176.6		-246.6		-401.3	
C	1	-47.2	21.3	-39.5	21.9	-86.7	21.5
C	2	-55.4	25.0	-48.2	26.7	-103.4	25.7
C	3	-36.9	16.7	-50.8	28.2	-86.4	21.5
C	4	-45.8	20.6	-28.7	15.9	-75.0	18.6
C	5	-36.4	16.4	-13.2	7.3	-50.8	12.6
C	SUM	-221.7		-180.5		-402.4	
D	1	-16.4	16.8	126.4	22.8	110.0	24.1
D	2	-21.8	22.4	148.9	26.9	127.0	27.8
D	3	-21.6	22.2	115.7	20.9	94.1	20.6
D	4	-21.6	22.2	97.4	17.6	75.8	16.6
D	5	-15.9	16.3	65.6	11.8	49.7	10.9
D	SUM	-97.3		553.9		456.6	
LOAD	PX (KIPS)	-100.0		0.		-100.0	
LOAD	PY (KIPS)	0.		-100.0		-100.0	
ACTUAL	PX (KIPS)						
ACTUAL	PY (KIPS)						

TABLE 30J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 40 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)					
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT			
A	1	116.1	20.8	144.6	25.8	-16.1	16.2	-23.5	28.2	100.0	21.8	134.8	28.0
A	2	139.9	25.1	138.4	24.7	-21.8	22.0	-15.2	18.2	118.0	25.8	122.8	25.5
A	3	119.5	21.4	116.9	20.8	-22.1	22.2	-13.9	16.7	97.4	21.3	97.8	20.3
A	4	107.1	19.2	102.5	18.3	-22.7	22.8	-17.5	21.0	84.4	18.4	80.9	16.8
A	5	74.6	13.4	58.6	10.4	-16.8	16.9	-13.3	16.0	57.8	12.6	45.1	9.4
A	SUM	557.1		561.0		-99.4		-83.5		457.7		481.4	
B	1	-27.6	15.6	-54.7	22.9	-56.6	22.9	-37.7	21.7	-80.1	20.0	-92.9	23.0
B	2	-42.4	24.0	-62.9	26.3	-63.5	25.8	-46.9	26.9	-100.5	25.0	-109.4	27.1
B	3	-53.3	30.2	-63.4	26.6	-39.7	16.1	-32.2	18.5	-87.6	21.8	-92.2	22.8
B	4	-34.5	19.6	-39.3	16.5	-48.1	19.5	-32.9	18.9	-78.4	19.5	-68.7	17.0
B	5	-18.8	10.6	-18.4	7.7	-38.6	15.7	-24.5	14.0	-54.7	13.6	-40.7	10.1
B	SUM	-176.6		-238.6		-246.6		-174.1		-401.3		-403.8	
C	1	-47.2	21.3	-34.6	19.2	-39.5	21.9	-76.7	29.4	-86.7	21.5	-114.3	26.6
C	2	-55.4	25.0	-48.0	26.7	-48.2	26.7	-80.8	31.0	-103.4	25.7	-125.4	29.2
C	3	-36.9	16.7	-32.4	18.0	-50.8	28.2	-54.0	20.7	-86.4	21.5	-83.3	19.4
C	4	-45.8	20.6	-37.5	20.8	-28.7	15.9	-28.4	10.9	-75.0	18.6	-62.0	14.4
C	5	-36.4	16.4	-27.7	15.4	-13.2	7.3	-21.0	8.1	-50.8	12.6	-44.1	10.3
C	SUM	-221.7		-180.2		-180.5		-260.8		-402.4		-429.1	
D	1	-16.4	16.8	-13.1	16.4	126.4	22.8	103.4	20.8	110.0	24.1	97.2	22.8
D	2	-21.8	22.4	-17.6	22.0	148.9	26.9	156.5	31.5	127.0	27.8	142.1	33.4
D	3	-21.6	22.2	-18.0	22.6	115.7	20.9	101.1	20.3	94.1	20.6	82.3	19.4
D	4	-21.6	22.2	-22.0	27.5	97.4	17.6	82.5	16.6	75.8	16.6	62.2	14.6
D	5	-15.9	16.3	-9.3	11.6	65.6	11.8	53.9	10.8	49.7	10.9	41.7	9.8
D	SUM	-97.3		-80.0		553.9		497.4		456.6		425.4	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LJAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-99.4	
ACTUAL	PX (KIPS)	0.		-19.3		0.		0.		-19.3		-19.3	
ACTUAL	PY (KIPS)	0.		0.		-19.3		-19.3		-19.3		-19.1	

TABLE 30A  
SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 40 KSI CCND. LOADING.  
TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	NORMALIZED POINT LOADS APPLIED AT			
	(3-X)		(3-Y)	
	THEORY	EXPERM	THEORY	EXPERM
1E	-0.07	2.96	-2.53	-3.02
2E	-1.42	-3.43	8.65	12.99
3E	-1.32	-3.85	15.17	11.24
4E	-1.78	-3.36	9.25	3.70
5E	-3.27	-2.85	8.15	11.96
1F	-3.10	3.76	37.97	47.50
2F	-3.02	-2.61	38.15	49.52
3F	37.65	32.63	-3.40	-14.33
4F	37.57	36.28	-3.58	-12.37
1W	.98	8.83	-0.08	2.77
2W	8.09	1.84	-1.37	-2.19
3W	9.08	2.22	-1.35	-2.0
4W	9.17	10.58	-1.83	-7.30
5W	11.45	17.22	-3.22	.64
RE	-7.86	-7.53	38.69	36.87
RF	69.10	70.06	69.16	70.32
RW	38.77	40.69	-7.85	-6.28
SUMR	100.01	103.22	100.00	100.91
PX	-100.00	-100.00	0.	0.
PY	0.	.01	-100.00	-100.00
SUMP	-100.00	-99.99	-100.00	-100.00
SUMR/SUMP	1.00	1.03	1.00	1.01
TW	56.66	65.66	-17.34	-24.11
MF	122.04	101.64	-124.65	-185.58
TF	-0.24	15.03	-0.54	-0.09
TF	-17.39	-22.00	56.50	53.18
ACTUAL PX		-19.20		0.
ACTUAL PY		.01		-19.34

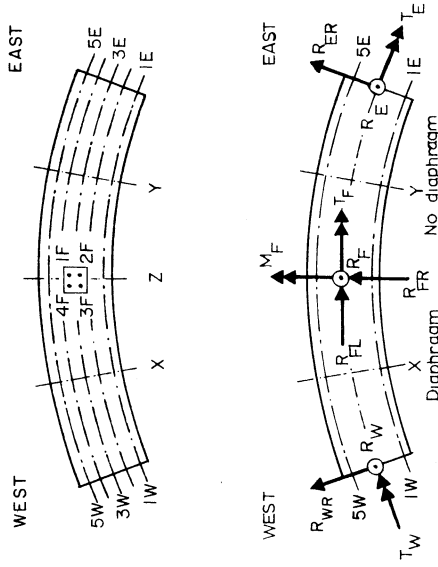
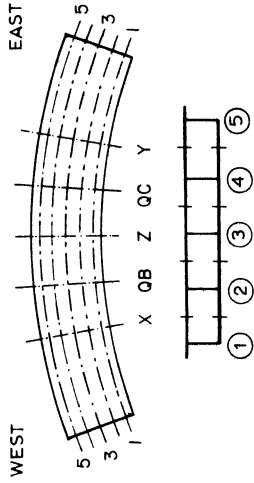


TABLE 31B

SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

RESULTS FOR POINT LOADS  
APPLIED AFTER 40 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



DEFLECTION AT POINT	(3-X)		(3-Y)		(3-X)+(3-Y)	
	THEORY	EXPERM E/T	THEORY	EXPERM E/T	THEORY	EXPERM E/T
1X	.692	1.078 1.56	-.239	-.477 2.00	.453	.833 1.84
2X	.740	1.205 1.63	-.249	-.534 2.14	.491	.923 1.88
3X	.793	1.306 1.65	-.260	-.570 2.19	.532	.998 1.88
4X	.809	1.344 1.66	-.273	-.576 2.11	.536	1.016 1.90
5X	.831	1.374 1.65	-.288	-.605 2.11	.544	1.035 1.90
1QB	.421	.645 1.53	-.207	-.405 1.95	.214	.396 1.85
2QB	.441	.685 1.55	-.215	-.419 1.95	.225	.425 1.89
3QB	.460	.722 1.57	-.222	-.450 2.03	.238	.460 1.93
4QB	.481	.741 1.54	-.235	-.455 1.94	.246	.462 1.88
5QB	.500	.805 1.61	-.245	-.491 2.00	.255	.475 1.86
1Z	.013	.018 1.34	.011	.012 1.08	.024	.054 2.23
2Z	.007	.016 2.18	.007	.013 1.98	.014	.032 2.37
4Z	.007	.002 .24	.006	.004 .73	.012	.005 .37
5Z	.012	.021 1.74	.009	.024 2.64	.022	.035 1.63
1QC	-.208	-.341 1.64	.408	.683 1.67	.200	.229 1.15
2QC	-.216	-.357 1.65	.442	.760 1.72	.226	.293 1.30
3QC	-.221	-.363 1.64	.489	.900 1.84	.267	.381 1.43
4QC	-.234	-.392 1.68	.476	.841 1.77	.243	.300 1.24
5QC	-.244	-.400 1.64	.479	.837 1.75	.235	.260 1.10
1Y	-.243	-.392 1.62	.658	1.063 1.62	.415	.526 1.27
2Y	-.251	-.421 1.68	.735	1.250 1.70	.484	.643 1.33
3Y	-.260	-.449 1.72	.894	1.666 1.86	.634	.991 1.56
4Y	-.272	-.465 1.71	.793	1.370 1.73	.521	.705 1.35
5Y	-.284	-.482 1.70	.773	1.289 1.67	.489	.619 1.27
LOAD PX	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD PY	0.	0.	-100.0	-100.0	-100.0	-97.9
ACTUAL PX			0.	0.		-19.4
ACTUAL PY			-19.3	-19.3		-19.0

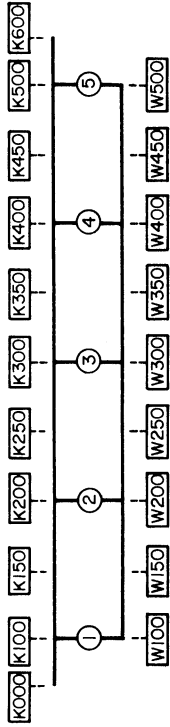
TABLE 31C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 40 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

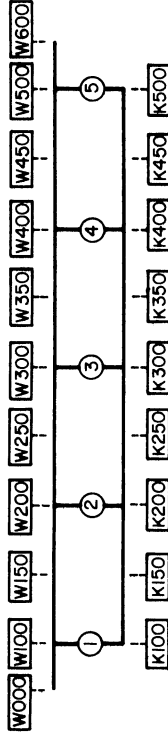


GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)		
		THEORY	MEASR ADJUST	THEORY	MEASR ADJUST	THEORY	MEASR ADJUST	
K	K000	-314	-322	68	125	-245	-299	-654
K	K100	-277	-689	59	272	-218	-654	-650
K	K150		-363		81		-300	-353
K	K200	-251	-449	50	154	-201	-414	-429
K	K250		-298		60		-239	-246
K	K300	-268	-438	52	128	-216	-394	-393
K	K350		-363		96		-322	-321
K	K400	-249	-456	50	134	-199	-407	-422
K	K450		-325		89		-287	-356
K	K500	-266	-373	58	134	-208	-345	-342
K	K600	-289	-245	65	90	-223	-227	-227
W	W100	1044	965	-217	-259	826	871	879
W	W150		844		-225		769	698
W	W200	969	945	-196	-253	772	838	818
W	W250		855		-223		774	749
W	W300	1048	1105	-211	-295	836	963	963
W	W350		913		-239		805	832
W	W400	958	1015	-196	-281	762	886	878
W	W450		957		-246		866	799
W	W500	982	1101	-210	-309	771	926	932
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0	
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-97.9	
ACTUAL	PX (KIPS)		-19.2		0.		-19.4	
ACTUAL	PY (KIPS)		0.		-19.3		-19.0	

TABLE 31D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 40 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION B

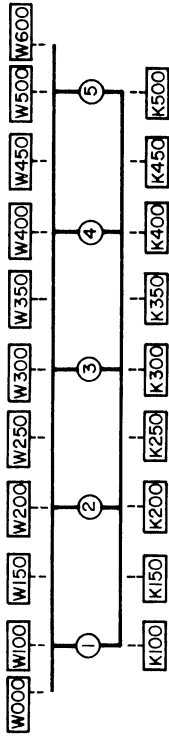
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

NORMALIZED POINT LOADS APPLIED AT

GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
W	W000	194	295	295	448	319	642
W	W100	196	266	271	399	288	596
W	W150	222	255	297	314	286	550
W	W200	335	373	371	314	317	711
W	W250	380	380	449	214	252	650
W	W300	226	487	516	308	266	773
W	W350	382	382	455	381	269	656
W	W400	201	324	329	408	293	662
W	W450	186	316	373	381	290	620
W	W500	309	310	314	408	295	608
W	W600	309	309	309	408	280	610
K	K100	-90	-158	-163	-180	-192	-271
K	K150	-99	-147	-142	-149	-257	-340
K	K200	-133	-207	-201	-149	-192	-374
K	K250	-102	-240	-230	-92	-207	-393
K	K300	-177	-249	-255	-145	-209	-421
K	K350	-180	-219	-220	-168	-213	-400
K	K400	-165	-177	-174	-168	-203	-357
K	K450	-165	-180	-181	-168	-187	-357
K	K500	-165	-165	-163	-168	-171	-324
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	0.	0.	-100.0
LOAD	PY (KIPS)	0.	0.	0.	-100.0	-100.0	-97.9
ACTUAL	PX (KIPS)	-19.2	-19.2	-19.2	C.	C.	-19.4
ACTUAL	PY (KIPS)	0.	0.	0.	-19.3	-19.3	-19.0

**TABLE 31E**  
SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
APPLIED AFTER 40 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



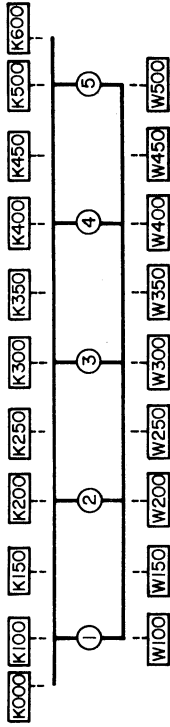
TENSION = + K = CONCRETE STRAIN METERS  
COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	451	328	185	246	636	634
W	W100	403	295	187	232	591	576
W	W150	261	280	232	250	541	539
W	W200	309	367	232	457	541	862
W	W250	222	227	440	427	572	669
W	W300	204	254	368	578	572	886
W	W350	200	223	226	366	601	652
W	W400	309	343	226	367	535	775
W	W450	268	280	255	272	555	584
W	W500	393	298	178	251	571	609
W	W600	421	288	159	250	580	593
K	K100	-182	-195	-87	-105	-269	-329
K	K150	-191	-187	-103	-93	-250	-304
K	K200	-147	-189	-103	-172	-382	-380
K	K250	-174	-176	-145	-228	-435	-466
K	K300	-88	-171	-100	-346	-234	-537
K	K350	-146	-187	-100	-258	-247	-475
K	K400	-174	-185	-80	-157	-255	-358
K	K450	-266	-253	-106	-175	-439	-427
K	K500	-196	-194	-106	-106	-325	-320
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-97.9	-97.9
ACTUAL	PX (KIPS)	-19.2	0.	0.	0.	-19.4	-19.4
ACTUAL	PY (KIPS)	0.	-19.3	-19.3	-19.3	-19.0	-19.0

TABLE 31F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 40 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION D

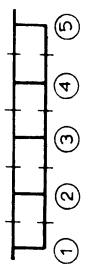
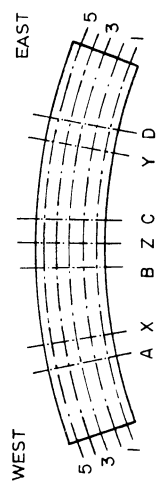
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)		MEASR	ADJUST
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR		
K	K000	62	46	-278	-149	-215	-107	-107	-107
K	K100	53	66	-241	-264	-187	-187	-187	-196
K	K150		151		-532		-363		-354
K	K200	45	113	-231	-465	-186	-331	-331	-326
K	K250		95		-439		-313		-337
K	K300	46	95	-238	-397	-192	-276	-276	-279
K	K350		155		-644		-453		-388
K	K400	44	129	-225	-472	-181	-315	-315	-295
K	K450		189		-689		-440		-423
K	K500	50	129	-226	-465	-176	-318	-318	-319
K	K600	57	38	-250	-158	-193	-112	-112	-318
W	W100	-224	-152	1042	741	818	498	498	506
W	W150		-192		952		642		595
W	W200	-199	-217	994	1107	794	769	769	766
W	W250		-199		1100		789		731
W	W300	-211	-248	1049	1426	837	995	995	964
W	W350		-203		1025		694		673
W	W400	-192	-269	958	1181	766	795	795	798
W	W450		-207		896		604		604
W	W500	-206	-224	955	968	749	702	702	715
LOAD	PX (KIPS)	-100.0	-100.0	0.	C.	-100.0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	0.	.0	-100.0	-100.0	-100.0	-97.9	-97.9	-97.9
ACTUAL	PX (KIPS)		-19.2		G.		-19.4		-19.4
ACTUAL	PY (KIPS)		.0		-19.3		-19.0		-19.0



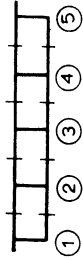
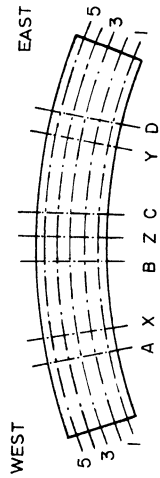
**TABLE 31G**  
 DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 40 KSI CCND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	(3-X)			(3-Y)			(3-X) + (3-Y)			
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	
A	1	92.9	16.3	68.5	12.1	-19.5	16.7	73.4	16.2	61.7	12.3
A	2	129.6	22.8	124.9	22.0	-26.1	22.4	103.5	22.9	112.2	22.4
A	3	130.4	22.9	144.0	25.4	-25.8	22.2	104.6	23.1	126.8	25.4
A	4	127.8	22.5	142.5	25.1	-26.0	22.3	101.8	22.5	124.7	24.9
A	5	88.4	15.5	87.3	15.4	-19.0	16.3	69.4	15.3	74.6	14.9
A	SUM	569.0		567.2		-116.3		452.7		500.0	
B	1	-27.5	12.5	-34.4	12.7	-48.8	18.4	-77.0	15.9	-74.4	15.0
B	2	-48.2	22.0	-57.3	21.2	-61.5	23.2	-109.9	22.7	-106.8	21.5
B	3	-66.7	30.4	-78.9	29.2	-48.3	18.3	-113.8	23.5	-125.8	25.3
B	4	-49.2	22.4	-58.3	21.6	-60.0	22.7	-109.2	22.5	-109.5	22.0
B	5	-27.9	12.7	-41.6	15.4	-46.1	17.4	-74.5	15.4	-80.7	16.2
B	SUM	-219.6		-270.4		-264.8		-484.4		-497.2	
C	1	-49.2	18.6	-39.6	18.2	-26.8	12.0	-76.4	15.7	-77.8	14.8
C	2	-60.9	23.0	-51.1	23.4	-50.2	22.4	-110.5	22.8	-122.8	23.3
C	3	-46.9	17.7	-39.0	17.9	-72.3	32.3	-116.8	24.1	-127.4	24.2
C	4	-60.4	22.8	-50.5	23.1	-49.2	22.0	-109.0	22.4	-118.5	22.5
C	5	-47.5	17.9	-37.9	17.4	-25.2	11.3	-73.0	15.0	-79.3	15.1
C	SUM	-265.0		-218.1		-223.7		-485.8		-525.8	
D	1	-20.0	17.2	-12.8	10.8	92.3	16.2	72.3	16.0	43.2	10.6
D	2	-26.5	22.7	-27.3	23.1	132.1	23.2	105.6	23.3	99.0	24.3
D	3	-25.8	22.2	-29.1	24.6	131.1	23.0	105.3	23.3	113.9	28.0
D	4	-25.6	22.0	-32.3	27.3	127.5	22.4	102.0	22.5	99.2	24.4
D	5	-18.6	16.0	-16.7	14.2	85.8	15.1	67.2	14.8	51.7	12.7
D	SUM	-116.4		-118.3		568.7		452.3		407.0	
LOAD	PX (KIPS)	-100.0		-100.0		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-57.9	
ACTUAL	PX (KIPS)	0.		-19.2		0.		-19.4		-19.4	
ACTUAL	PY (KIPS)	0.		0.		-19.3		-19.0		-19.0	

**TABLE 31H**  
**DISTRIBUTION OF MOMENTS TO EACH GIRDER**  
**( KIP-FT AND PERCENTAGE )**

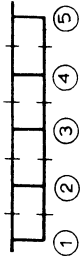
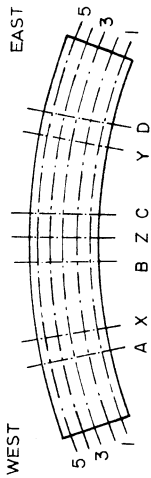


MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
 APPLIED AFTER 40 KSI CCND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1	92.9	183.8	16.3	-19.5	-62.5	16.7	73.4	172.6	16.2
A	2	129.6	125.8	22.8	-26.1	-30.7	22.4	103.5	112.1	22.9
A	3	130.4	118.0	22.9	-25.8	-30.9	22.2	104.6	102.6	23.1
A	4	127.8	134.3	22.5	-26.0	-36.3	22.3	101.8	121.5	22.5
A	5	88.4	98.4	15.5	-19.0	-33.4	16.3	69.4	91.2	15.3
A	SUM	569.0	660.2		-116.3	-193.8		452.7	599.9	
B	1	-27.5	-25.5	12.5	-48.8	-37.3	18.4	-77.0	-59.4	15.9
B	2	-48.2	-55.0	22.0	-61.5	-57.1	23.2	-109.9	-105.6	22.7
B	3	-66.7	-72.6	30.4	-48.3	-65.5	18.3	-113.8	-124.2	23.5
B	4	-49.2	-53.7	22.4	-60.0	-60.3	22.7	-109.2	-106.1	22.5
B	5	-27.9	-28.7	12.7	-46.1	-30.3	17.4	-74.5	-56.7	15.4
B	SUM	-219.6	-235.5		-264.8	-250.5		-484.4	-452.0	
C	1	-49.2	-32.5	18.6	-26.8	-14.2	12.0	-76.4	-52.3	15.7
C	2	-60.9	-54.5	23.0	-50.2	-46.6	22.4	-110.5	-108.3	22.8
C	3	-46.9	-55.6	17.7	-72.3	-97.0	32.3	-116.8	-158.5	24.1
C	4	-60.4	-60.3	22.8	-49.2	-52.7	22.0	-109.0	-117.5	22.4
C	5	-47.5	-40.0	17.9	-25.2	-22.4	11.3	-73.0	-64.0	15.0
C	SUM	-265.0	-242.8		-223.7	-232.9		-485.8	-500.7	
D	1	-20.0	-23.3	17.2	92.3	82.2	16.2	72.3	57.5	16.0
D	2	-26.5	-35.6	22.7	132.1	140.3	23.2	105.6	96.4	23.3
D	3	-25.8	-34.4	22.2	131.1	135.6	23.0	105.3	88.4	23.3
D	4	-25.6	-43.6	22.0	127.5	153.6	22.4	102.0	100.4	22.5
D	5	-18.6	-42.0	16.0	85.8	136.3	15.1	67.2	90.7	14.8
D	SUM	-116.4	-179.0		568.7	648.0		452.3	433.4	
LOAD	PX (KIPS)	-100.0	-100.0		0.	0.		-100.0	-100.0	
LOAD	PY (KIPS)	0.	0.		-100.0	-100.0		-100.0	-97.9	
ACTUAL	PX (KIPS)	0.	-19.2		0.	0.		-19.4	-19.4	
ACTUAL	PY (KIPS)	0.	0.		-19.3	-19.3		-19.0	-19.0	

**TABLE 311**  
 DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )  
 MOMENTS ABOUT ENTIRE GRCS SECTION N.A.



RESULTS FOR POINT LOADS  
 APPLIED AFTER 40 KSI CCND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

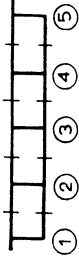
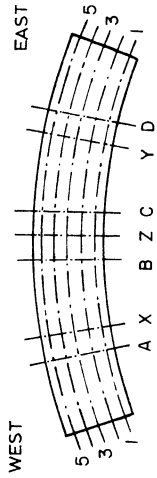
SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1	92.9	120.0	19.7	-19.5	-37.1	21.9	73.4	111.2	20.4
A	2	129.6	125.4	20.6	-26.1	-32.0	18.9	103.5	112.2	20.6
A	3	130.4	132.4	21.7	-25.8	-34.7	20.5	104.6	116.0	21.3
A	4	127.8	138.9	22.8	-26.0	-37.6	22.2	101.8	123.3	22.6
A	5	88.4	92.3	15.2	-19.0	-28.0	16.5	69.4	82.1	15.1
A	SUM	569.0	608.9		-116.3	-169.4		452.7	544.7	
B	1	-27.5	-29.5	11.7	-48.8	-37.2	15.9	-77.0	-66.1	14.0
B	2	-48.2	-56.0	22.3	-61.5	-52.8	22.5	-109.9	-106.2	22.5
B	3	-66.7	-75.4	30.0	-48.3	-56.3	24.0	-113.8	-124.9	26.4
B	4	-49.2	-55.8	22.2	-60.0	-54.6	23.3	-109.2	-107.7	22.8
B	5	-27.9	-34.5	13.7	-46.1	-33.7	14.4	-74.5	-67.4	14.3
B	SUM	-219.6	-251.2		-264.8	-234.6		-484.4	-472.3	
C	1	-49.2	-35.7	15.4	-26.8	-22.2	8.8	-76.4	-63.7	12.4
C	2	-60.9	-53.0	22.9	-50.2	-55.5	22.0	-110.5	-114.8	22.4
C	3	-46.9	-48.2	20.8	-72.3	-90.4	35.8	-116.8	-144.7	28.3
C	4	-60.4	-55.9	24.1	-49.2	-56.3	22.3	-109.0	-118.0	23.0
C	5	-47.5	-39.0	16.8	-25.2	-27.9	11.0	-73.0	-70.9	13.8
C	SUM	-265.0	-231.9		-223.7	-252.2		-485.8	-512.0	
D	1	-20.0	-17.5	12.0	92.3	72.3	11.7	72.3	49.6	11.8
D	2	-26.5	-31.0	21.3	132.1	141.7	23.0	105.6	97.9	23.4
D	3	-25.8	-31.5	21.6	131.1	150.7	24.5	105.3	102.6	24.5
D	4	-25.6	-37.4	25.7	127.5	149.6	24.3	102.0	99.7	23.8
D	5	-18.6	-28.0	19.3	85.8	101.6	16.5	67.2	69.1	16.5
D	SUM	-116.4	-145.4		568.7	615.9		452.3	418.9	
LOAD	PX (KIPS)	-100.0	-100.0		0.	0.		-100.0	-100.0	
LOAD	PY (KIPS)	0.	0.		-100.0	-100.0		-100.0	-100.0	
ACTUAL	PX (KIPS)	-19.2	-19.2		0.	0.		-19.4	-19.4	
ACTUAL	PY (KIPS)	0.	0.		-19.3	-19.3		-19.0	-19.0	

TABLE 31J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 40 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT  
(3-Y)

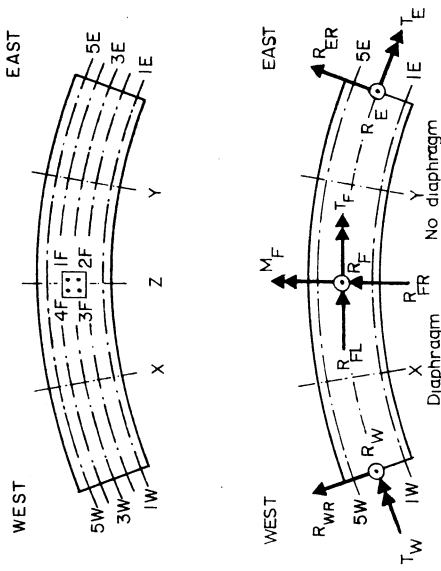
SECTION	GIRDER	THEORY		EXPERIMENTAL		THEORY		EXPERIMENTAL					
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT				
		(3-X)		(3-Y)		(3-X)		(3-Y)					
A	1	92.9	16.3	116.1	19.1	-19.5	16.7	-39.6	23.1	73.4	16.2	108.8	20.0
A	2	129.6	22.8	125.2	20.6	-26.1	22.4	-32.1	18.7	103.5	22.9	112.2	20.6
A	3	130.4	22.9	136.6	22.5	-25.8	22.2	-35.6	20.7	104.6	23.1	119.8	22.0
A	4	127.8	22.5	139.9	23.0	-26.0	22.3	-37.9	22.0	101.8	22.5	123.7	22.8
A	5	88.4	15.5	90.1	14.8	-19.0	16.3	-26.6	15.5	69.4	15.3	79.1	14.6
A	SUM	569.0		607.9		-116.3		-171.9		452.7		543.5	
B	1	-27.5	12.5	-31.0	12.0	-48.8	18.4	-37.2	16.2	-77.0	15.9	-68.8	14.3
B	2	-48.2	22.0	-56.5	21.9	-61.5	23.2	-50.9	22.2	-109.9	22.7	-106.4	22.1
B	3	-66.7	30.4	-76.8	29.7	-48.3	18.3	-53.9	23.5	-113.8	23.5	-125.2	26.0
B	4	-49.2	22.4	-56.7	22.0	-60.0	22.7	-52.7	22.9	-109.2	22.5	-108.3	22.5
B	5	-27.9	12.7	-37.2	14.4	-46.1	17.4	-35.1	15.3	-74.5	15.4	-72.4	15.1
B	SUM	-219.6		-258.2		-264.8		-229.7		-484.4		-481.2	
C	1	-49.2	18.6	-36.9	16.2	-26.8	12.0	-26.6	10.1	-76.4	15.7	-68.7	13.3
C	2	-60.9	23.0	-52.3	23.0	-50.2	22.4	-61.0	23.1	-110.5	22.8	-118.3	22.8
C	3	-46.9	17.7	-45.7	20.1	-72.3	32.3	-87.7	33.2	-116.8	24.1	-139.1	26.8
C	4	-60.4	22.8	-53.8	23.7	-49.2	22.0	-58.3	22.0	-109.0	22.4	-118.2	22.8
C	5	-47.5	17.9	-38.7	17.0	-25.2	11.3	-30.9	11.7	-73.0	15.0	-74.0	14.3
C	SUM	-265.0		-227.4		-223.7		-264.6		-485.8		-518.3	
D	1	-20.0	17.2	-16.1	11.6	92.3	16.2	69.2	11.3	72.3	16.0	47.2	11.3
D	2	-26.5	22.7	-30.1	21.7	132.1	23.2	142.0	23.3	105.6	23.3	98.2	23.6
D	3	-25.8	22.2	-30.6	22.1	131.1	23.0	156.5	25.7	105.3	23.3	108.2	26.0
D	4	-25.6	22.0	-35.8	25.8	127.5	22.4	148.3	24.3	102.0	22.5	99.5	23.9
D	5	-18.6	16.0	-26.2	18.9	85.8	15.1	93.5	15.3	67.2	14.8	63.7	15.3
D	SUM	-116.4		-138.9		568.7		609.4		452.3		416.9	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-97.9	
ACTUAL	PX (KIPS)			-19.2				0.				-19.4	
ACTUAL	PY (KIPS)			0.				-19.3				-19.0	

LOAD PX (KIPS)  
LOAD PY (KIPS)  
ACTUAL PX (KIPS)  
ACTUAL PY (KIPS)

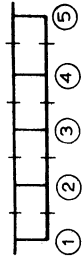
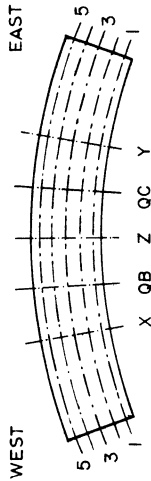
TABLE 32A  
SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 40 KSI COND. LOADING.  
TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	NORMALIZED POINT LOADS APPLIED AT			
	(5-X)		(5-Y)	
	THEORY	EXPERM	THEORY	EXPERM
1E	-8.14	-7.75	-23.25	-20.70
2E	-2.93	-7.53	-1.70	-6.63
3E	-1.37	-5.22	2.03	9.16
4E	-7.1	2.10	12.87	12.76
5E	2.95	.96	46.35	41.59
1F	10.14	1.20	53.96	50.77
2F	-17.30	-28.78	26.17	13.54
3F	26.89	38.49	-17.04	-14.42
4F	54.33	64.53	10.75	23.48
1W	-26.90	-16.33	-8.12	-4.55
2W	.30	-11.16	-2.90	-4.71
3W	5.47	-3.12	-1.39	-.69
4W	14.38	22.53	-.72	-3.62
5W	42.90	45.56	3.00	4.49
RE	-10.20	-10.44	36.30	36.18
RF	74.05	75.44	73.83	73.37
RW	36.15	37.48	-10.13	-9.08
SUMR	100.00	102.48	100.00	100.47
PX	-100.00	-100.00	0.	0.
PY	0.	0.	-100.00	-100.00
SUMP	-100.00	-100.00	-100.00	-100.00
SUMR/SUMP	1.00	1.02	1.00	1.00
TW	395.40	405.15	62.83	49.32
MF	132.56	195.90	-129.62	-82.87
TF	82.32	84.03	83.37	112.69
TE	62.78	33.58	395.63	370.42
ACTUAL PX		-19.22		0.
ACTUAL PY		0.		-19.36



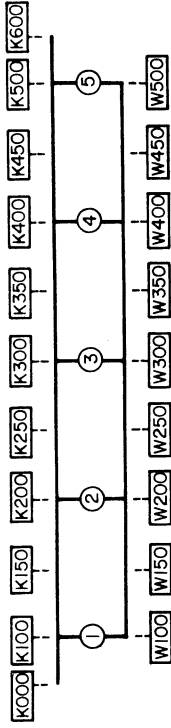
**TABLE 32B**  
 SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 40 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



DEFLECTION AT PCINT	(5-X)		(5-Y)		(5-X)+(5-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X	.535	.876	1.64	1.64	1.52	1.35
2X	.673	1.191	1.77	1.77	1.63	1.62
3X	.831	1.518	1.83	1.83	1.68	1.72
4X	1.019	1.855	1.82	1.82	1.66	1.75
5X	1.234	2.237	1.81	1.81	1.66	1.76
1QB	.267	.442	1.66	1.66	1.53	1.30
2QB	.372	.645	1.73	1.73	1.56	1.50
3QB	.489	.856	1.75	1.75	1.59	1.72
4QB	.636	1.117	1.76	1.76	1.53	1.68
5QB	.791	1.368	1.73	1.73	1.59	1.68
1Z	-.127	-.179	1.41	1.41	1.51	1.46
2Z	-.061	-.083	1.35	1.35	1.66	1.49
4Z	.078	.113	1.46	1.46	1.44	1.42
5Z	.158	.230	1.45	1.45	1.68	1.61
1QC	-.331	-.577	1.74	1.74	1.30	2.47
2QC	-.287	-.522	1.82	1.82	1.37	.40
3QC	-.244	-.470	1.93	1.93	1.56	1.47
4QC	-.209	-.427	2.05	2.05	1.65	1.66
5QC	-.168	-.366	2.18	2.18	1.71	1.75
1Y	-.337	-.613	1.82	1.82	1.32	.79
2Y	-.311	-.597	1.92	1.92	1.39	1.16
3Y	-.288	-.580	2.02	2.02	1.49	1.44
4Y	-.266	-.541	2.03	2.03	1.64	1.65
5Y	-.246	-.512	2.08	2.08	1.81	1.91
LOAD PX	-100.0	-100.0	0.0	0.0	-100.0	-100.0
LOAD PY	0.0	0.0	-100.0	-100.0	-100.0	-102.0
ACTUAL PX	0.0	-19.2	0.0	0.0	-19.0	-19.0
ACTUAL PY	0.0	0.0	-19.4	-19.4	-10.4	-10.4

TABLE 32C

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 40 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	-303	-349	83	88	-219	-258
K	K100	-250	-670	71	214	-178	-464
K	K150	-346	-400	60	73	-246	-289
K	K200	-228	-427	60	137	-167	-293
K	K250	-307	-329	52	50	-240	-264
K	K300	-262	-446	61	125	-200	-320
K	K350	-383	-407	90	84	-274	-302
K	K400	-280	-552	58	131	-222	-426
K	K450	-400	-478	78	86	-289	-350
K	K500	-335	-543	67	127	-268	-427
K	K600	-412	-354	75	88	-337	-279
W	W100	928	875	-265	-283	663	536
W	W150	862	850	-236	-198	626	594
W	W200	1033	933	-250	-270	782	617
W	W250	1091	701	-228	-271	862	371
W	W300	1315	1137	-243	-280	1071	778
W	W350	883	1019	-243	-219	1001	750
W	W400	1657	1306	-286	-243	1284	1012
W	W450	886	883	-265	-286	560	1153
W	W500	732	1587	-243	-252	1314	1314
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-102.0
ACTUAL	PX (KIPS)	-19.2	-19.2	0.	0.	-19.0	-19.0
ACTUAL	PY (KIPS)	0.	0.	-19.4	-19.4	-10.4	-10.4

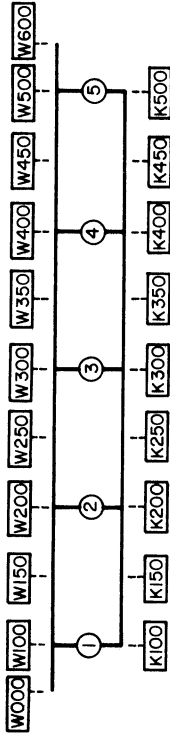
TABLE 32D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 40 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

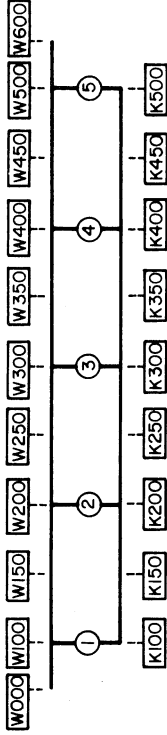


GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)		MEASR	ADJUST
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR		
W	W000	252	171	499	317	751	504	504	504
W	W100	245	196	443	278	688	495	504	504
W	W150	249	196	325	286	574	471	530	530
W	W200	382	396	325	273	574	684	680	680
W	W250	382	434	232	241	615	663	744	744
W	W300	303	567	232	289	615	858	897	897
W	W350	318	480	389	331	692	806	939	939
W	W400	309	514	526	403	845	962	975	975
W	W450	318	491	526	421	845	936	1082	1082
W	W500	309	550	564	407	873	973	987	987
W	W600	309	590	564	384	873	1007	1007	1007
K	K100	-110	-186	-195	-249	-306	-437	-453	-453
K	K150	-113	-107	-155	-316	-268	-435	-401	-401
K	K200	-153	-251	-102	-194	-255	-461	-434	-434
K	K250	-139	-315	-187	-179	-326	-513	-448	-448
K	K300	-147	-230	-236	-198	-384	-449	-451	-451
K	K350	-147	-206	-236	-242	-384	-460	-461	-461
K	K400	-147	-206	-236	-250	-384	-461	-460	-460
K	K450	-147	-305	-236	-217	-384	-527	-518	-518
K	K500	-147	-264	-236	-218	-384	-481	-479	-479
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-102.0	-102.0	-102.0
ACTUAL	PX (KIPS)	-19.2	-19.2	0.	0.	-19.0	-19.0	-19.0	-19.0
ACTUAL	PY (KIPS)	0.	0.	-15.4	-15.4	-10.4	-10.4	-10.4	-10.4



TABLE 32E

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 40 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



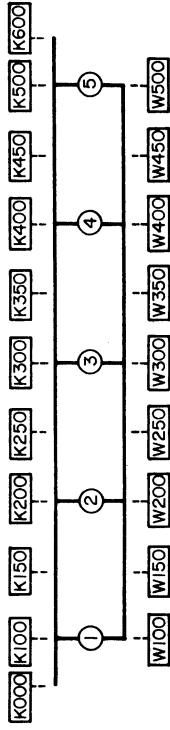
SECTION C

TENSION = +      K = CONCRETE STRAIN METERS  
 COMPRESSION = -      W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	511	355	199	98	711	474
W	W100	451	314	209	134	661	465
W	W150		285		144		439
W	W200	338	379	217	385	555	775
W	W250		275		330		574
W	W300	240	329	357	529	598	881
W	W350		276		389		691
W	W400	388	495	310	626	698	1161
W	W450		395		480		888
W	W500	510	436	376	665	886	1150
W	W600	545	419	383	712	929	1175
K	K100	-200	-247	-89	-208	-290	-447
K	K150		-244		-159		-393
K	K200	-161	-241	-57	-164	-259	-390
K	K250		-234		-176		-381
K	K300	-105	-231	-144	-201	-249	-412
K	K350		-238		-210		-407
K	K400	-185	-236	-145	-364	-331	-579
K	K450		-377		-244		-465
K	K500	-228	-235	-177	-82	-405	-445
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-102.0
ACTUAL	PX (KIPS)		-19.2		0.		-19.0
ACTUAL	PY (KIPS)		0.		-19.4		-10.4

TABLE 32F

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 40 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION D

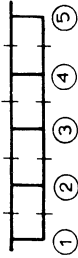
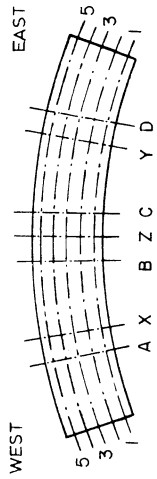
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)			
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST		
K	K000	75	52	52	-243	-122	-167	-85	-85
K	K100	64	83	87	-205	-201	-141	-137	-147
K	K150		167	160	-190	-407	-135	-312	-313
K	K200	54	141	136	-341	-329	-171	-249	-235
K	K250		115	126	-337	-383	-171	-248	-274
K	K300	55	129	139	-226	-372	-212	-283	-298
K	K350		204	206	-264	-544	-212	-427	-481
K	K400	52	181	168	-318	-528	-259	-429	-428
K	K450		277	301	-379	-773	-312	-625	-687
K	K500	59	200	209	-379	-559	-312	-464	-479
K	K600	67	62	200	-379	-229	-312	-181	-464
W	W100	-271	-228	-229	829	515	558	329	337
W	W150		-296	-286		646		412	364
W	W200	-240	-315	-311	806	727	566	476	473
W	W250		-293	-271		725		488	452
W	W300	-252	-338	-334	1015	976	762	728	731
W	W350		-227	-234		1121		940	851
W	W400	-226	-335	-335	1187	1582	960	1366	1296
W	W450		-271	-262		1393		1232	1083
W	W500	-242	-343	-347	1386	516	1143	269	294
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	0.	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-100.0	-102.0	-102.0
ACTUAL	PX (KIPS)		-19.2	0.	0.	0.	-19.0	-19.0	-19.0
ACTUAL	PY (KIPS)		0.	-15.4	-15.4	-15.4	-10.4	-10.4	-10.4

TABLE 32G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE)  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR POINT LOADS  
APPLIED AFTER 40 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT

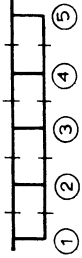
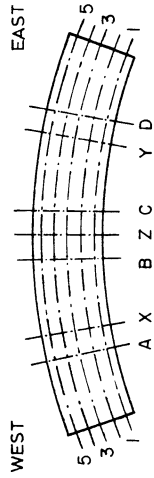
SECTION	GIRDER	(5-X)			(5-Y)			(5-X) + (5-Y)					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	83.4	14.3	63.2	9.8	-23.6	17.2	-18.2	12.8	59.8	13.4	40.7	8.1
A	2	115.8	19.9	122.2	19.0	-31.3	22.7	-33.8	23.8	84.5	19.0	90.9	18.0
A	3	126.6	21.7	153.3	23.8	-30.5	22.2	-35.9	25.3	96.0	21.6	113.0	22.4
A	4	143.1	24.6	183.8	28.5	-30.3	22.0	-33.5	23.6	112.8	25.4	152.2	30.1
A	5	113.2	19.5	122.1	18.9	-22.0	16.0	-20.5	14.5	91.3	20.5	108.0	21.4
A	SUM	582.1		644.5		-137.8		-142.0		444.4		504.8	
B	1	-33.3	12.2	-22.9	6.9	-54.0	17.1	-35.0	14.5	-87.5	14.9	-59.0	10.2
B	2	-54.8	20.0	-55.5	16.8	-65.8	20.8	-42.4	17.6	-120.3	20.5	-99.3	17.1
B	3	-77.2	28.2	-94.0	28.4	-54.7	17.3	-46.9	19.4	-130.4	22.2	-140.7	24.3
B	4	-65.5	23.9	-86.9	26.3	-77.6	24.5	-63.9	26.5	-142.7	24.3	-153.9	26.5
B	5	-42.9	15.7	-71.3	21.6	-64.2	20.3	-53.1	22.0	-107.2	18.2	-127.5	22.0
B	SUM	-273.7		-330.6		-316.3		-241.4		-588.1		-580.3	
C	1	-55.2	17.3	-44.7	15.8	-28.0	10.4	-10.8	3.5	-83.5	14.3	-57.4	9.5
C	2	-68.0	21.4	-56.9	20.1	-48.5	18.1	-48.0	15.8	-116.3	19.9	-105.0	17.5
C	3	-56.1	17.6	-51.5	18.2	-73.3	27.3	-76.3	25.1	-127.8	21.9	-129.7	21.6
C	4	-76.9	24.2	-73.9	26.0	-68.5	25.5	-89.2	29.3	-144.5	24.7	-166.5	27.7
C	5	-62.3	19.5	-56.7	20.0	-50.4	18.8	-80.1	26.3	-112.2	19.2	-142.6	23.7
C	SUM	-318.5		-283.7		-268.8		-304.4		-584.3		-601.2	
D	1	-24.1	17.4	-20.4	12.4	76.3	13.1	44.1	8.6	52.2	11.7	27.4	7.1
D	2	-31.8	22.9	-41.2	25.1	108.9	18.7	93.7	18.3	77.1	17.3	60.0	15.5
D	3	-30.7	22.2	-39.2	24.0	125.0	21.4	121.6	23.8	94.2	21.2	91.5	23.7
D	4	-30.2	21.8	-39.8	24.3	152.7	26.2	190.9	37.4	122.5	27.5	164.4	42.5
D	5	-21.9	15.8	-23.2	14.2	120.6	20.7	60.7	11.9	98.7	22.2	43.4	11.2
D	SUM	-138.7		-163.8		583.5		511.0		444.7		386.7	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-102.0	
ACTUAL	PX (KIPS)	0.		-19.2		0.		0.		-19.0		-19.0	
ACTUAL	PY (KIPS)	0.		0.		-19.4		-19.4		-10.4		-10.4	

TABLE 32H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 40 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

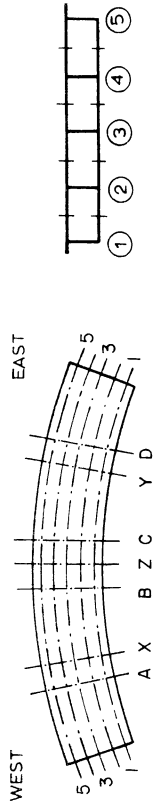


NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)				
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT		
A	1	83.4	161.5	22.9	-23.6	-54.4	17.2	-31.3	59.8	13.4	115.9	22.1
A	2	115.8	125.3	17.8	-31.3	-32.4	22.7	-65.8	84.5	19.0	91.7	17.5
A	3	126.6	126.1	17.9	-30.5	-27.7	15.4	-70.0	96.0	21.6	96.1	18.3
A	4	143.1	153.6	21.8	-30.3	-34.2	19.0	-61.4	112.8	25.4	114.2	21.7
A	5	113.2	138.4	19.6	-22.0	-31.7	17.6	-42.9	91.3	20.5	107.4	20.4
A	SUM	582.1	704.9		-137.8	-180.4		-273.7	444.4		525.4	
B	1	-33.3	-27.5	10.1	-54.0	-50.3	17.1	-77.2	-87.5	14.9	-77.1	13.9
B	2	-54.8	-66.9	24.6	-65.8	-64.9	22.5	-77.2	-120.3	20.5	-124.7	22.4
B	3	-77.2	-70.0	25.8	-54.7	-62.9	21.8	-70.0	-130.4	22.2	-136.6	24.6
B	4	-65.5	-61.4	22.6	-77.6	-73.2	25.4	-61.4	-142.7	24.3	-135.4	24.3
B	5	-42.9	-45.9	16.9	-64.2	-36.9	12.8	-42.9	-107.2	18.2	-82.6	14.8
B	SUM	-273.7	-271.7		-316.3	-288.1		-273.7	-588.1		-556.4	
C	1	-55.2	-43.4	13.7	-28.0	-34.0	13.0	-43.4	-83.5	14.3	-75.1	13.2
C	2	-68.0	-73.5	23.1	-48.5	-44.7	17.1	-73.5	-116.3	19.9	-112.8	19.9
C	3	-56.1	-73.6	23.2	-73.3	-73.9	28.3	-73.6	-127.8	21.9	-137.9	24.3
C	4	-76.9	-76.5	24.1	-68.5	-67.2	25.7	-76.5	-144.5	24.7	-148.2	26.1
C	5	-62.3	-50.6	15.9	-50.4	-41.7	15.9	-50.6	-112.2	19.2	-93.4	16.5
C	SUM	-318.5	-317.6		-268.8	-261.5		-317.6	-584.3		-567.4	
D	1	-24.1	-26.0	11.1	76.3	64.6	9.9	-26.0	52.2	11.7	48.3	9.3
D	2	-31.8	-39.8	16.9	108.9	104.0	16.0	-39.8	77.1	17.3	77.0	14.8
D	3	-30.7	-43.2	18.4	125.0	124.9	19.2	-43.2	94.2	21.2	96.1	18.5
D	4	-30.2	-62.6	26.6	152.7	175.9	27.1	-62.6	122.5	27.5	144.1	27.7
D	5	-21.9	-63.6	27.0	120.6	181.0	27.8	-63.6	98.7	22.2	154.9	29.8
D	SUM	-138.7	-235.3		583.5	650.4		-235.3	444.7		520.5	
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	0.		-100.0	-100.0		-100.0	
LOAD	PY (KIPS)	0.	0.	0.	-100.0	-100.0		0.	-100.0		-102.0	
ACTUAL	PX (KIPS)	0.	-19.2	0.	0.	0.		-19.2	-19.0		-19.0	
ACTUAL	PY (KIPS)	0.	0.	0.	-19.4	-19.4		0.	-10.4		-10.4	

TABLE 3.32  
 DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )  
 MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
 APPLIED AFTER 40 KSI CCND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

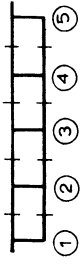
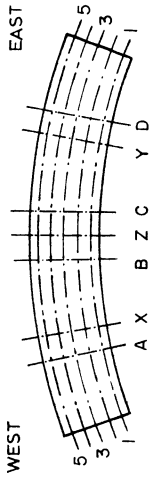


SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	83.4	14.3	107.1	15.9	-23.6	17.2	-34.3	21.6	59.8	13.4	74.3	14.4
A	2	115.8	19.9	123.6	18.4	-31.3	22.7	-33.2	20.9	84.5	19.0	91.3	17.8
A	3	126.6	21.7	141.2	21.0	-30.5	22.2	-32.2	20.3	96.0	21.6	105.5	20.5
A	4	143.1	24.6	170.4	25.4	-30.3	22.0	-33.8	21.3	112.8	25.4	135.2	26.3
A	5	113.2	19.5	129.4	19.3	-22.0	16.0	-25.5	16.0	91.3	20.5	107.8	21.0
A	SUM	582.1		671.6		-137.8		-159.2		444.4		514.1	
B	1	-33.3	12.2	-25.4	8.5	-54.0	17.1	-43.5	16.3	-87.5	14.9	-69.0	12.2
B	2	-54.8	20.0	-61.8	20.8	-65.8	20.8	-54.9	20.5	-120.3	20.5	-113.4	20.0
B	3	-77.2	28.2	-80.7	27.1	-54.7	17.3	-55.8	20.9	-130.4	22.2	-138.5	24.4
B	4	-65.5	23.9	-72.8	24.4	-77.6	24.5	-69.1	25.8	-142.7	24.3	-143.7	25.3
B	5	-42.9	15.7	-57.2	19.2	-64.2	20.3	-44.1	16.5	-107.2	18.2	-102.6	18.1
B	SUM	-273.7		-298.1		-316.3		-267.3		-588.1		-567.2	
C	1	-55.2	17.3	-44.0	14.5	-28.0	10.4	-23.7	8.4	-83.5	14.3	-67.2	11.5
C	2	-68.0	21.4	-66.1	21.8	-48.5	18.1	-46.2	16.5	-116.3	19.9	-109.4	18.8
C	3	-56.1	17.6	-63.8	21.1	-73.3	27.3	-75.0	26.7	-127.8	21.9	-134.3	23.0
C	4	-76.9	24.2	-75.3	24.9	-68.5	25.5	-77.0	27.4	-144.5	24.7	-156.4	26.8
C	5	-62.3	19.5	-53.3	17.6	-50.4	18.8	-58.8	20.9	-112.2	19.2	-115.4	19.8
C	SUM	-318.5		-302.6		-268.8		-280.7		-584.3		-582.7	
D	1	-24.1	17.4	-22.9	11.7	76.3	13.1	53.2	9.3	52.2	11.7	36.7	8.2
D	2	-31.8	22.9	-40.6	20.7	108.9	18.7	98.3	17.1	77.1	17.3	67.6	15.1
D	3	-30.7	22.2	-41.0	21.0	125.0	21.4	123.1	21.5	94.2	21.2	93.6	21.0
D	4	-30.2	21.8	-50.0	25.5	152.7	26.2	184.3	32.1	122.5	27.5	155.4	34.8
D	5	-21.9	15.8	-41.2	21.1	120.6	20.7	114.4	20.0	98.7	22.2	93.2	20.9
D	SUM	-138.7		-195.8		583.5		573.4		444.7		446.5	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-102.0	
ACTUAL	PX (KIPS)			-19.2		0.		0.		-19.0		-19.0	
ACTUAL	PY (KIPS)			0.		-10.4		-10.4		-10.4		-10.4	

TABEL 32J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE)  
MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 40 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	(5-X)		(5-Y)		(5-X)+(5-Y)	
		THEORY K-FT	PCT	THEORY K-FT	PCT	THEORY K-FT	PCT
A	1	83.4	14.3	105.3	15.6	188.7	19.9
A	2	115.8	19.9	123.2	18.2	239.0	28.1
A	3	126.6	21.7	145.6	21.6	272.2	33.3
A	4	143.1	24.6	175.1	25.9	318.2	39.5
A	5	113.2	19.5	126.2	18.7	239.4	28.2
A	SUM	582.1		675.5		1257.6	
B	1	-33.3	12.2	-25.1	8.0	-58.4	20.2
B	2	-54.8	20.0	-60.1	19.0	-114.9	49.0
B	3	-77.2	28.2	-87.5	27.7	-164.7	65.9
B	4	-65.5	23.9	-79.9	25.3	-145.4	59.2
B	5	-42.9	15.7	-63.1	20.0	-106.0	45.7
B	SUM	-273.7		-315.7		-589.4	
C	1	-55.2	17.3	-44.2	14.8	-99.4	32.1
C	2	-68.0	21.4	-63.5	21.3	-131.5	42.7
C	3	-56.1	17.6	-60.7	20.4	-116.8	38.0
C	4	-76.9	24.2	-74.7	25.1	-151.6	49.3
C	5	-62.3	19.5	-54.5	18.3	-116.8	36.8
C	SUM	-318.5		-297.5		-616.0	
D	1	-24.1	17.4	-21.9	11.6	-46.0	29.0
D	2	-31.8	22.9	-40.8	21.6	-72.6	43.2
D	3	-30.7	22.2	-40.4	21.4	-71.1	42.8
D	4	-30.2	21.8	-47.4	25.1	-77.6	42.9
D	5	-21.9	15.8	-38.4	20.3	-60.3	36.1
D	SUM	-138.7		-189.0		-327.7	
LOAD	PX (KIPS)	-100.0		-100.0		-200.0	
LOAD	PY (KIPS)	0.		0.		0.	
ACTUAL	PX (KIPS)			-19.2		-19.2	
ACTUAL	PY (KIPS)			0.		0.	

LOAD	PX (KIPS)	PY (KIPS)	(5-X)		(5-Y)		(5-X)+(5-Y)	
			THEORY K-FT	PCT	THEORY K-FT	PCT	THEORY K-FT	PCT
EXPERIMENTAL			59.8	13.4	-33.6	21.2	26.2	20.6
EXPERIMENTAL			84.5	19.0	-33.3	21.0	51.2	17.4
EXPERIMENTAL			96.0	21.6	-33.4	21.1	62.6	20.6
EXPERIMENTAL			112.8	25.4	-33.8	21.3	79.0	26.9
EXPERIMENTAL			91.3	20.5	-24.3	15.4	67.0	20.6
EXPERIMENTAL			444.4		-158.5		285.9	
EXPERIMENTAL			-87.5	14.9	-42.1	16.1	-129.6	11.7
EXPERIMENTAL			-120.3	20.5	-51.6	19.7	-171.9	18.9
EXPERIMENTAL			-130.4	22.2	-53.5	20.4	-183.9	24.2
EXPERIMENTAL			-142.7	24.3	-67.4	25.7	-210.1	25.7
EXPERIMENTAL			-107.2	18.2	-47.5	18.1	-154.7	19.6
EXPERIMENTAL			-588.1		-262.2		-850.3	
EXPERIMENTAL			-83.5	14.3	-25.5	8.6	-109.0	11.1
EXPERIMENTAL			-116.3	19.9	-47.1	15.9	-163.4	18.2
EXPERIMENTAL			-127.8	21.9	-75.7	25.5	-203.5	22.3
EXPERIMENTAL			-144.5	24.7	-82.8	27.9	-227.3	27.2
EXPERIMENTAL			-112.2	19.2	-66.0	22.2	-178.2	21.2
EXPERIMENTAL			-584.3		-297.0		-881.3	
EXPERIMENTAL			52.2	11.7	50.0	8.6	102.2	7.3
EXPERIMENTAL			77.1	17.3	96.9	16.7	174.0	14.1
EXPERIMENTAL			94.2	21.2	122.6	21.2	216.8	20.0
EXPERIMENTAL			122.5	27.5	187.1	32.3	309.6	34.3
EXPERIMENTAL			98.7	22.2	122.5	21.2	221.2	24.2
EXPERIMENTAL			444.7		579.1		1023.8	
EXPERIMENTAL			-100.0		0.		-100.0	
EXPERIMENTAL			-100.0		-100.0		-200.0	
EXPERIMENTAL					0.		0.	
EXPERIMENTAL					-19.4		-19.4	

TABLE 33A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 40 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

NORMALIZED POINT LOADS APPLIED AT  
 (1-X)+(5-Y)

REACTION OR LOAD	*****		*****		*****	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	-15.18	-15.26				
2E	-1.65	-2.97				
3E	.72	6.89				
4E	9.96	12.29				
5E	36.73	29.50				
1F	37.82	43.42				
2F	37.77	27.95				
3F	31.36	25.34				
4F	31.41	40.08				
1W	29.07	27.53				
2W	8.98	12.05				
3W	2.20	4.63				
4W	.15	.34				
5W	-9.33	-11.49				
RE	30.58	30.45				
RF	138.36	136.79				
RW	31.07	33.06				
SUMR	200.01	200.30				
PX	-100.00	-100.00				
PY	-100.00	-97.64				
SUMP	-200.00	-157.64				
SUMR/SUMP	1.00	1.01				
1W	-220.32	-230.92				
MF	-19.22	-8.93				
1F	.15	45.32				
TF	296.99	265.59				
ACTION REACTION						
REACTION						

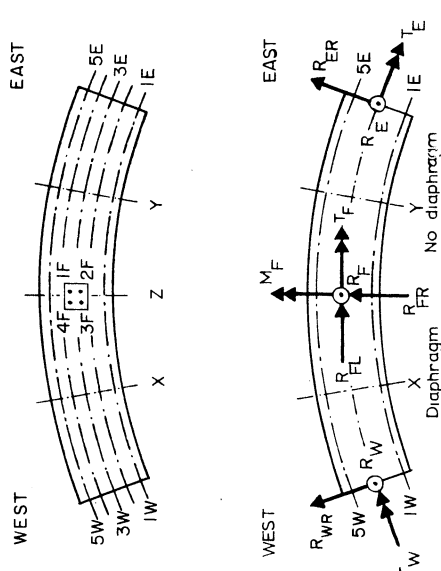
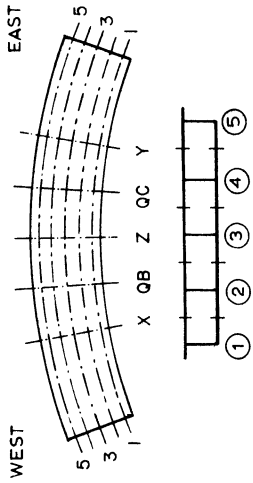


TABLE 33B

SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

RESULTS FOR POINT LOADS  
 APPLIED AFTER 40 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT

DEFLECTION AT POINT	(1-X)+(5-Y)		THEORY EXPERM		E/T		THEORY EXPERM		E/T	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X	.613	1.046	1.71							
2X	.500	.821	1.64							
3X	.408	.633	1.55							
4X	.340	.472	1.39							
5X	.289	.352	1.22							
1QB	.300	.500	1.67							
2QB	.230	.368	1.60							
3QB	.166	.255	1.53							
4QB	.122	.144	1.17							
5QB	.094	.102	1.08							
1Z	.034	.027	.81							
2Z	.016	.023	1.42							
4Z	.016	.050	3.04							
5Z	.033	.095	2.84							
1QC	.167	.136	.82							
2QC	.200	.223	1.12							
3QC	.265	.395	1.49							
4QC	.375	.634	1.69							
5QC	.504	.921	1.83							
1Y	.351	.364	1.04							
2Y	.417	.488	1.17							
3Y	.535	.748	1.40							
4Y	.726	1.185	1.63							
5Y	1.032	1.955	1.89							
LOAD										
PX	-100.0		-100.0							
PY	-100.0		-97.6							
ACTUAL										
PX			-19.4							
PY			-19.0							



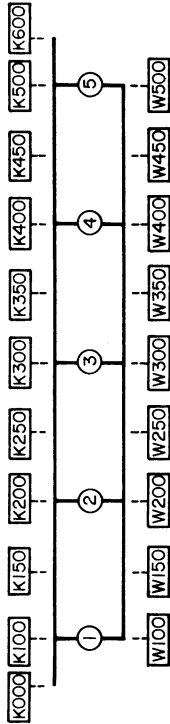
TABLE 33C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 40 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



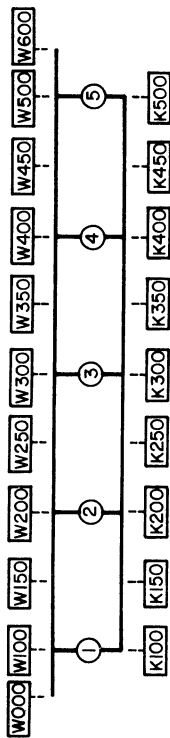
NORMALIZED POINT LOADS APPLIED AT

GAGE TYPE	GAGE LOC.	(1-X) + (5-Y)		THEORY MEASR ADJUST		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	ADJUST	ADJUST	ADJUST	ADJUST	ADJUST	ADJUST
K	K000	-347	-395	-833	-833				
K	K100	-269	-833	-799	-799				
K	K150	-211	-344	-289	-289				
K	K200	-199	-433	-461	-461				
K	K250	-183	-199	-198	-198				
K	K300	-152	-338	-333	-333				
K	K350	-159	-249	-239	-239				
K	K400	-186	-286	-285	-285				
K	K450	-159	-175	-189	-189				
K	K500	-186	-193	-197	-197				
K	K600	-186	-144	-144	-144				
W	W100	1100	1095	1110	1110				
W	W150	823	841	827	827				
W	W200	720	839	820	820				
W	W250	568	750	650	650				
W	W300	573	705	701	701				
W	W350	573	576	537	537				
W	W400	573	534	525	525				
W	W450	573	712	366	366				
W	W500	573	541	540	540				
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0				
LOAD	PY (KIPS)	-97.6	-97.6	-97.6	-97.6				
ACTUAL	PX (KIPS)	-19.4	-19.4	-19.4	-19.4				
ACTUAL	PY (KIPS)	-19.0	-19.0	-19.0	-19.0				

TABLE 33D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 40 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

NORMALIZED POINT LOADS APPLIED AT

GAGE TYPE	GAGE LOC.	(1-X)+(5-Y)		*****		*****		*****	
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR

W	W000	684	833	833						
W	W100	632	706	714						
W	W150		665	717						
W	W200	510	666	683						
W	W250		573	610						
W	W300	488	700	694						
W	W350		609	665						
W	W400	536	597	620						
W	W450		563	647						
W	W500	657	512	507						
W	W600	678	461	461						

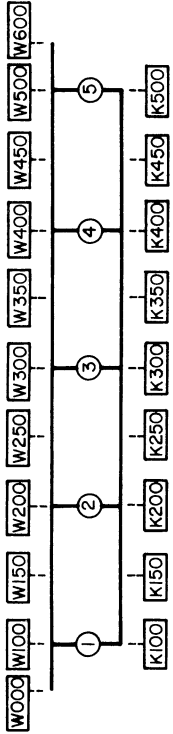
K	K100	-287	-458	-445						
K	K150		-622	-596						
K	K200	-238	-319	-329						
K	K250		-290	-328						
K	K300	-202	-382	-382						
K	K350		-410	-415						
K	K400	-253	-378	-389						
K	K450		-309	-343						
K	K500	-295	-324	-314						

LOAD	PX (KIPS)	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-97.6
ACTUAL	PX (KIPS)		-19.4
ACTUAL	PY (KIPS)		-19.0

TABLE 33E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 40 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

NORMALIZED POINT LOADS APPLIED AT

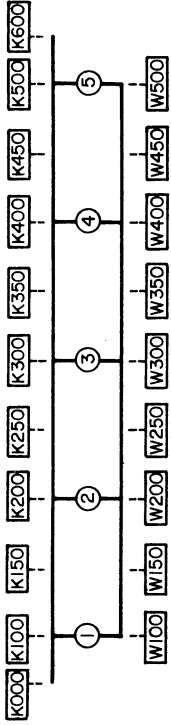
GAGE TYPE	GAGE LOC.	(1-X)+(5-Y)		THEORY		MEASR		ADJUST		THEORY		MEASR		ADJUST	
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST		
W	W000														
W	W100	624	428		428										
W	W150	596	441		427										
W	W200	498	413		402										
W	W250		770		766										
W	W300	512	532		508										
W	W350		753		777										
W	W400	541	545		605										
W	W450		875		868										
W	W500	680	657		642										
W	W600	709	865		869										
			917		917										
K	K100														
K	K150	-267	-362		-357										
K	K200		-297		-252										
K	K250	-232	-299		-290										
K	K300		-288		-331										
K	K350	-211	-315		-308										
K	K400		-506		-486										
K	K450	-256	-386		-398										
K	K500		-247		-271										
K		-310	-544		-556										

LOAD	PX (KIPS)	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-97.6
ACTUAL	PX (KIPS)	-19.4	
ACTUAL	PY (KIPS)	-19.0	

TABLE 33F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 40 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION D

TENSION = +      K = CONCRETE STRAIN METERS  
 COMPRESSION = -      W = WELDABLE STRAIN GAGES

NORMALIZED POINT LOADS APPLIED AT

(1-X)+(5-Y)  
 \*\*\*\*\*  
 THEORY      MEASR      ADJUST      \*\*\*\*\*  
 \*\*\*\*\*  
 THEORY      MEASR      ADJUST      \*\*\*\*\*  
 \*\*\*\*\*  
 THEORY      MEASR      ADJUST      \*\*\*\*\*  
 \*\*\*\*\*

GAGE TYPE	GAGE LOC.	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
K	K000	-191	-68	-68			
K	K100	-161	-121	-128			
K	K150	-152	-258	-252			
K	K200	-187	-248	-243			
K	K250	-187	-233	-281			
K	K300	-227	-296	-308			
K	K350	-227	-450	-485			
K	K400	-275	-454	-449			
K	K450	-330	-694	-749			
K	K500		-527	-541			
K	K600		-208	-527			
W	W100	646	368	375			
W	W150	642	454	423			
W	W200	837	515	511			
W	W250	1024	543	507			
W	W300	1209	773	776			
W	W350		853	814			
W	W400		1400	1343			
W	W450		1229	1079			
W	W500		331	356			

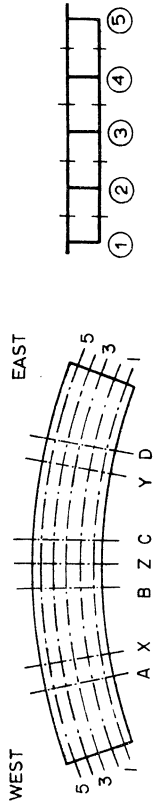
LOAD	PX (KIPS)	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-97.6
ACTUAL	PX (KIPS)	-19.4	-19.4
ACTUAL	PY (KIPS)	-19.0	-19.0



**TABLE 33H**  
**DISTRIBUTION OF MOMENTS TO EACH GIRDER**  
**( KIP-FT AND PERCENTAGE )**

**MOMENTS ABOUT TENSION FLANGE STEEL**

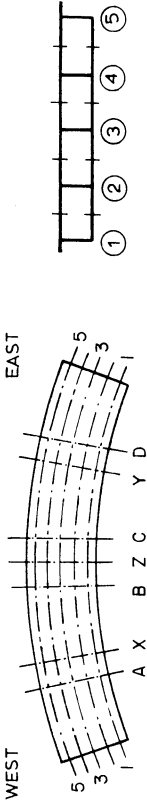
**RESULTS FOR POINT LOADS**  
**APPLIED AFTER 40 KSI COND. LOADING.**  
**SIMPLY SUPPORTED, NO RESTRAINTS.**



**NORMALIZED POINT LOADS APPLIED AT**

SECTION	GIRDER	(1-X)+(5-Y)		THEORY		EXPERIMENTAL		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	92.4	22.0	198.2	38.2						
A	2	108.5	25.9	105.7	20.4						
A	3	88.9	21.2	83.8	16.1						
A	4	76.8	18.3	79.8	15.4						
A	5	52.6	12.5	51.5	9.9						
A	SUM	419.3		519.0							
B	1	-80.8	16.6	-91.9	18.8						
B	2	-106.4	21.9	-114.9	23.5						
B	3	-105.0	21.6	-114.6	23.4						
B	4	-111.4	22.9	-112.4	23.0						
B	5	-83.2	17.1	-55.5	11.3						
B	SUM	-486.9		-489.3							
C	1	-76.1	15.6	-55.7	13.0						
C	2	-104.4	21.3	-80.4	18.8						
C	3	-109.0	22.3	-109.9	25.7						
C	4	-113.5	23.2	-110.2	25.7						
C	5	-86.5	17.7	-72.0	16.8						
C	SUM	-489.5		-428.3							
D	1	59.9	12.3	38.6	7.2						
D	2	87.1	17.9	73.3	13.7						
D	3	103.4	21.3	97.6	18.3						
D	4	131.1	27.0	151.6	28.4						
D	5	104.7	21.5	172.1	32.3						
D	SUM	486.2		533.3							
LOAD	PX (KIPS)			-100.0							
LOAD	PY (KIPS)			-100.0							
ACTUAL	PX (KIPS)			-19.4							
ACTUAL	PY (KIPS)			-19.0							

**TABLE 331**  
 DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE)  
 MOMENTS ABOUT ENTIRE GROSS SECTION N.A.



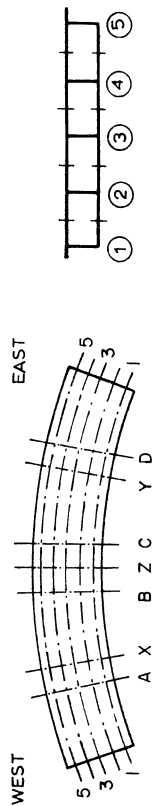
RESULTS FOR PCINT LOADS  
 APPLIED AFTER 40 KSI CCND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION	GIRDER	THEORY		EXPERIMENTAL		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
***** (1-X)+(5-Y) *****									
A	1	92.4	22.0	131.1	29.2				
A	2	108.5	25.9	110.3	24.6				
A	3	88.9	21.2	88.8	19.8				
A	4	76.8	18.3	74.5	16.6				
A	5	52.6	12.5	44.5	9.9				
A	SUM	419.3		449.0					
B	1	-80.8	16.6	-90.9	19.0				
B	2	-106.4	21.9	-109.7	22.9				
B	3	-105.0	21.6	-111.1	23.2				
B	4	-111.4	22.9	-105.9	22.1				
B	5	-83.2	17.1	-50.8	12.7				
B	SUM	-486.9		-478.4					
C	1	-76.1	15.6	-54.0	11.9				
C	2	-104.4	21.3	-98.9	19.5				
C	3	-109.0	22.3	-110.0	24.1				
C	4	-113.5	23.2	-116.0	25.5				
C	5	-86.5	17.7	-86.7	19.0				
C	SUM	-489.5		-455.6					
D	1	59.9	12.3	34.8	7.5				
D	2	87.1	17.9	69.7	15.1				
D	3	103.4	21.3	96.2	20.8				
D	4	131.1	27.0	159.6	34.5				
D	5	104.7	21.5	101.8	22.0				
D	SUM	486.2		462.1					
LOAD	PX (KIPS)	-100.0		-100.0					
LOAD	PY (KIPS)	-100.0		-97.6					
ACTUAL	PX (KIPS)			-19.4					
ACTUAL	PY (KIPS)			-19.0					

**TABLE 33J**  
 DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE)

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
 APPLIED AFTER 40 KSI CCND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	(1-X)+(5-Y)		THEORY		EXPERIMENTAL		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	92.4	22.0	127.7	28.7						
A	2	108.5	25.9	111.0	25.0						
A	3	88.9	21.2	89.8	20.2						
A	4	76.8	18.3	73.5	16.6						
A	5	52.6	12.5	42.2	9.5						
A	SUM	419.3		444.2							
B	1	-80.8	16.6	-90.4	19.1						
B	2	-106.4	21.9	-106.9	22.6						
B	3	-105.0	21.6	-109.5	23.1						
B	4	-111.4	22.9	-103.5	21.9						
B	5	-83.2	17.1	-62.8	13.3						
B	SUM	-486.9		-473.1							
C	1	-76.1	15.6	-53.6	11.4						
C	2	-104.4	21.3	-94.1	20.1						
C	3	-109.0	22.3	-110.0	23.5						
C	4	-113.5	23.2	-119.1	25.4						
C	5	-86.5	17.7	-92.1	19.6						
C	SUM	-489.5		-469.0							
D	1	59.9	12.3	33.5	6.9						
D	2	87.1	17.9	68.9	14.3						
D	3	103.4	21.3	95.8	19.9						
D	4	131.1	27.0	162.3	33.7						
D	5	104.7	21.5	121.7	25.2						
D	SUM	486.2		482.1							
LOAD	PX (KIPS)	-100.0		-100.0							
LOAD	PY (KIPS)	-100.0		-97.6							
ACTUAL	PX (KIPS)	-100.0		-19.4							
ACTUAL	PY (KIPS)	-100.0		-19.0							



TABLE 34A  
SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 50 KSI COND. LOADING.  
TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	(1-X)		(1-Y)		NORMALIZED POINT LOADS APPLIED AT		(1-X)+(1-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	8.07	7.31	41.39	13.53	49.45	22.35	49.45	22.35
2E	.05	-.59	9.57	34.61	9.62	30.05	9.62	30.05
3E	-1.31	-1.09	-.42	6.29	-1.73	4.06	-1.73	4.06
4E	-2.91	-7.36	-1.17	-4.14	-4.08	-5.14	-4.08	-5.14
5E	-9.62	-5.56	-8.32	-12.72	-17.94	-18.51	-17.94	-18.51
1F	-16.14	5.73	20.53	2.44	4.39	7.27	4.39	7.27
2F	11.60	29.22	48.71	35.67	60.32	56.15	60.32	56.15
3F	48.40	28.16	11.88	31.15	60.28	56.27	60.28	56.27
4F	20.66	3.30	-16.30	-.99	4.35	6.54	4.35	6.54
1W	37.19	33.71	8.03	6.20	45.23	37.70	45.23	37.70
2W	11.88	11.80	.12	2.38	11.99	15.75	11.99	15.75
3W	3.59	7.36	-1.36	-1.83	2.23	7.02	2.23	7.02
4W	.87	1.38	-3.03	-1.40	-2.16	-.27	-2.16	-.27
5W	-12.33	-11.62	-9.62	-12.56	-21.95	-22.27	-21.95	-22.27
RE	-5.72	-7.29	41.05	37.57	35.32	32.81	35.32	32.81
RF	64.53	66.41	64.82	68.27	129.34	126.23	129.34	126.23
RW	41.20	42.63	-5.86	-7.21	35.34	37.93	35.34	37.93
SUMR	100.01	101.75	100.01	98.63	200.00	196.97	200.00	196.97
PX	-100.00	-100.00	0.	-.02	-100.00	-100.00	-100.00	-100.00
PY	0.	.01	-100.00	-100.00	-100.00	-93.78	-100.00	-93.78
SUMP	-100.00	-99.99	-100.00	-100.02	-200.00	-193.78	-200.00	-193.78
SUMR/SUMP	1.00	1.02	1.00	.99	1.00	1.02	1.00	1.02
TW	-283.15	-260.07	-98.93	-106.26	-382.10	-349.81	-382.10	-349.81
MF	110.40	-5.23	-110.50	-11.92	-.11	-.92	-.11	-.92
TF	-83.22	-72.52	-84.56	-98.05	-167.78	-147.91	-167.78	-147.91
TE	-98.64	-83.64	-283.43	-234.78	-382.02	-300.80	-382.02	-300.80
ACTUAL PX		-19.37		0.		-19.43		-19.43
ACTUAL PY		0.		-19.28		-18.22		-18.22

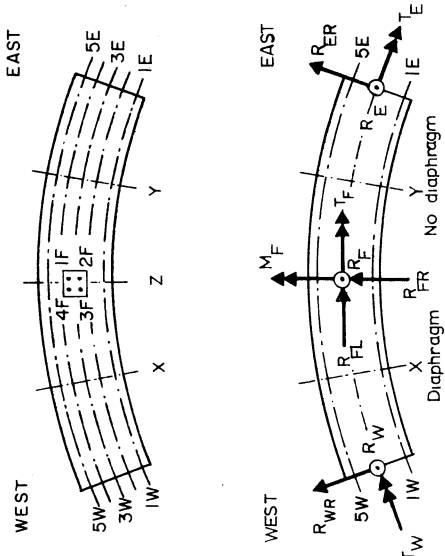




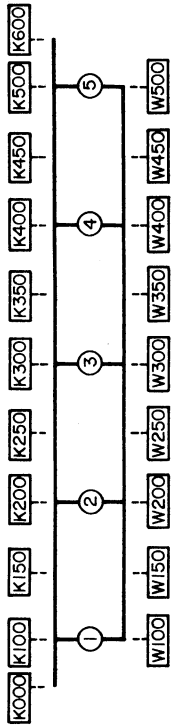
TABLE 34C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 50 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



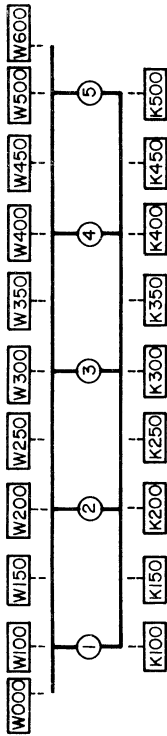
NORMALIZED POINT LOADS APPLIED AT

GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)			
		THEORY	ADJUST	MEASR	ADJUST	THEORY	MEASR	ADJUST	
K	K000	-431	-500	-1066	56	74	-374	-444	-973
K	K100	-341	-1066	-1020	48	130	-292	-973	-933
K	K150		-412	-352		41		-344	-293
K	K200	-271	-562	-601	42	77	-229	-498	-532
K	K250		-254	-244		61		-203	-185
K	K300	-245	-448	-437	44	57	-201	-398	-384
K	K350		-342	-322		35		-306	-279
K	K400	-211	-390	-390	44	57	-167	-344	-346
K	K450		-256	-275		35		-227	-241
K	K500	-227	-279	-284	51	43	-176	-251	-255
K	K600	-261	-203	-203	58	30	-203	-188	-188
W	W100	1365	1312	1319	-178	-36	1187	1253	1259
W	W150		1122	1109		-61		1059	1060
W	W200	1059	1012	994	-164	-80	895	910	892
W	W250		1006	881		-23		912	788
W	W300	970	881	875	-181	-107	789	734	730
W	W350		779	723		-98		662	597
W	W400	796	715	702	-171	-138	625	549	534
W	W450		979	500		-25		894	364
W	W500	816	703	705	-187	-178	628	505	509
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	0.	-0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	0.	0	0	-100.0	-100.0	-100.0	-93.8	-93.8
ACTUAL	PX (KIPS)		-19.4		0.			-19.4	
ACTUAL	PY (KIPS)		0.		-19.3			-18.2	

TABLE 34D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 50 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION B

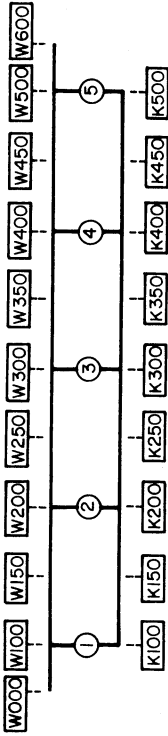
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	184	565	473	366	658	896
W	W100	189	446	427	371	616	797
W	W150	185	441	291	378	476	705
W	W200	185	420	291	419	476	761
W	W250	256	369	149	248	405	553
W	W300	147	416	222	182	370	552
W	W350	130	321	298	152	428	472
W	W400	114	168	315	193	430	298
W	W450	97	143	298	177	428	226
W	W500	114	93	315	169	430	227
W	W600	66	66	169	169	190	190
K	K100	-91	-249	-197	-211	-289	-419
K	K150	-82	-376	-141	-175	-224	-515
K	K200	-100	-156	-66	-196	-166	-323
K	K250	-66	-147	-105	-87	-172	-292
K	K300	-66	-227	-129	-94	-187	-307
K	K350	-66	-201	-105	-113	-172	-300
K	K400	-58	-151	-129	-136	-187	-273
K	K450	-58	-111	-129	-157	-187	-255
K	K500	-58	-121	-129	-161	-187	-268
LOAD	PX (KIPS)	-100.0	-100.0	0.	-0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-93.8
ACTUAL	PX (KIPS)	-19.4	-19.4	C.	-19.4	-19.4	-19.4
ACTUAL	PY (KIPS)	0.	0.	-19.3	-19.3	-18.2	-18.2

TABLE 34E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 50 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	425	343	302	796	728	1085
W	W100	387	315	279	654	666	935
W	W150		268		482		699
W	W200	280	381	203	535	484	856
W	W250		175		359		490
W	W300	154	168	241	364	396	533
W	W350		115		218		541
W	W400	231	196	121	168	353	337
W	W450		156		99		352
W	W500	304	177	95	40	400	243
W	W600	326	183	62	-16	388	179
K	K100	-178	-191	-137	-402	-315	-530
K	K150		-155		-363		-449
K	K200	-134	-146	-95	-194	-229	-325
K	K250		-104		-214		-289
K	K300	-67	-97	-95	-188	-163	-265
K	K350		-131		-101		-227
K	K400	-110	-144	-52	-88	-163	-224
K	K450		-179		-137		-302
K	K500	-133	-180	-37	-133	-171	-296
LOAD	PX (KIPS)	-100.0	-100.0	0.	-0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-93.8
ACTUAL	PX (KIPS)		-19.4		0.		-19.4
ACTUAL	PY (KIPS)		0.		-19.3		-18.2

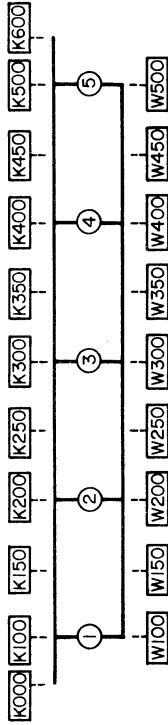
TABLE 34F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 50 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

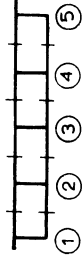
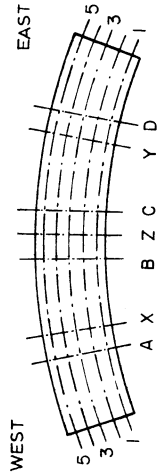
SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	51	47	-407	-297	-355	-245
K	K100	43	59	-331	-457	-287	-371
K	K150	140	138	-252	-635	-215	-500
K	K200	37	78	-206	-528	-168	-433
K	K250	76	76	-206	-367	-168	-284
K	K300	38	59	-170	-365	-133	-290
K	K350	37	92	-179	-453	-137	-356
K	K400	42	61	-201	-302	-153	-233
K	K450	58	58	-179	-406	-137	-310
K	K500	48	36	-201	-267	-153	-202
K	K600	15	36	-201	-87	-153	-67
W	W100	-183	-61	1480	1045	1297	854
W	W150	-164	-59	1147	1480	983	1254
W	W200	-177	-94	930	1240	753	991
W	W250	-119	-85	715	921	552	744
W	W300	-163	-119	696	813	519	582
W	W350	-176	-129	696	611	519	432
W	W400		-187	696	646	519	382
W	W450		-113	696	519	519	339
W	W500		-95	696	659	519	459
LOAD	PX (KIPS)	-100.0	-100.0	0.	-0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-93.8
ACTUAL	PX (KIPS)	-19.4	-19.4	0.	0.	-19.4	-19.4
ACTUAL	PY (KIPS)	0.	0.	-19.3	-19.3	-18.2	-18.2

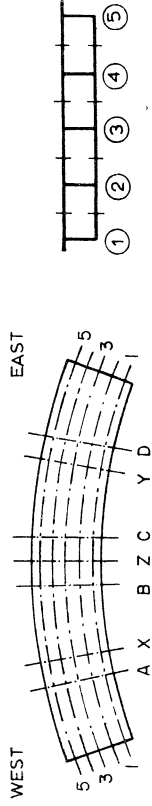
**TABLE 34G**  
 DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )



MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 50 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	116.1	20.8	95.0	18.8	-16.1	16.2	100.0	21.8	91.9	21.1
A	2	139.9	25.1	145.5	28.7	-21.8	22.0	118.0	25.8	133.3	30.7
A	3	119.5	21.4	119.9	23.7	-22.1	22.2	97.4	21.3	101.5	23.3
A	4	107.1	19.2	94.6	18.7	-22.7	22.8	84.4	18.4	72.1	16.6
A	5	74.6	13.4	51.2	10.1	-16.8	16.9	57.8	12.6	36.1	8.3
A	SUM	557.1		506.2		-99.4		457.7		434.9	
B	1	-27.6	15.6	-58.9	24.8	-56.6	22.9	-80.1	20.0	-100.7	26.2
B	2	-42.4	24.0	-68.4	28.7	-63.5	25.8	-100.5	25.0	-113.9	29.7
B	3	-53.3	30.2	-65.5	27.5	-39.7	16.1	-87.6	21.8	-90.0	23.4
B	4	-34.5	19.6	-33.1	13.9	-48.1	19.5	-78.4	19.5	-51.7	13.5
B	5	-18.8	10.6	-12.0	5.0	-38.6	15.7	-54.7	13.6	-27.6	7.2
B	SUM	-176.6		-237.9		-246.6		-401.3		-384.0	
C	1	-47.2	21.3	-40.5	24.2	-39.5	21.9	-86.7	21.5	-122.8	30.3
C	2	-55.4	25.0	-49.9	29.8	-48.2	26.7	-103.4	25.7	-127.2	31.4
C	3	-36.9	16.7	-27.1	16.2	-50.8	28.2	-86.4	21.5	-80.9	20.0
C	4	-45.8	20.6	-28.5	17.0	-28.7	15.9	-75.0	18.5	-52.9	13.1
C	5	-36.4	16.4	-21.3	12.7	-13.2	7.3	-50.8	12.6	-21.1	5.2
C	SUM	-221.7		-157.3		-180.5		-402.4		-404.9	
D	1	-16.4	16.8	-3.4	5.6	126.4	22.8	110.0	24.1	90.4	23.0
D	2	-21.8	22.4	-11.1	18.2	148.9	26.9	127.0	27.8	143.9	36.6
D	3	-21.6	22.2	-15.6	25.4	115.7	20.9	94.1	20.6	76.2	19.4
D	4	-21.6	22.2	-22.4	36.6	97.4	17.6	75.8	16.6	51.2	13.0
D	5	-15.9	16.3	-8.7	14.2	65.6	11.8	49.7	10.9	31.3	8.0
D	SUM	-57.3		-61.2		553.9		456.6		392.9	
LOAD	PX (KIPS)	-100.0		-100.0		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-93.8	
ACTUAL	PX (KIPS)			-19.4		0.				-19.4	
ACTUAL	PY (KIPS)			0.		-19.3				-18.2	

TABLE 3A  
DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )



MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 50 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	116.1	20.8	257.4	37.0	-16.1	16.2	-32.4	34.0	100.0	21.8	231.6	37.7
A	2	139.9	25.1	137.6	19.8	-21.8	22.0	-21.2	22.2	118.0	25.8	116.1	18.9
A	3	119.5	21.4	111.7	16.1	-22.1	22.2	-17.1	18.0	97.4	21.3	95.2	15.5
A	4	107.1	19.2	112.3	16.1	-22.7	22.8	-14.2	14.9	84.4	18.4	100.3	16.3
A	5	74.6	13.4	76.6	11.0	-16.8	16.9	-10.5	11.0	57.8	12.6	70.4	11.5
A	SUM	557.1		695.6		-99.4		-95.4		457.7		613.5	
B	1	-27.6	15.6	-51.9	21.4	-56.6	22.9	-32.6	18.8	-80.1	20.0	-77.4	19.1
B	2	-42.4	24.0	-58.0	23.9	-63.5	25.8	-43.3	24.9	-100.5	25.0	-103.1	25.5
B	3	-53.3	30.2	-62.9	26.0	-39.7	16.1	-28.3	16.2	-87.6	21.8	-91.4	22.6
B	4	-34.5	19.6	-47.2	19.5	-48.1	19.5	-41.0	23.6	-78.4	19.5	-84.0	20.8
B	5	-18.8	10.6	-22.4	9.2	-38.6	15.7	-28.8	16.5	-54.7	13.6	-48.9	12.1
B	SUM	-176.6		-242.3		-246.6		-174.0		-401.3		-404.7	
C	1	-47.2	21.3	-27.9	15.7	-39.5	21.9	-66.0	26.6	-86.7	21.5	-85.1	21.6
C	2	-55.4	25.0	-36.7	20.6	-48.2	26.7	-72.9	29.4	-103.4	25.7	-97.7	24.8
C	3	-36.9	16.7	-33.9	19.0	-50.8	28.2	-51.5	20.8	-86.4	21.5	-79.6	20.2
C	4	-45.8	20.6	-45.9	25.7	-28.7	15.9	-29.9	12.0	-75.0	18.6	-72.6	18.4
C	5	-36.4	16.4	-33.9	19.0	-13.2	7.3	-28.0	11.3	-50.8	12.6	-59.6	15.1
C	SUM	-221.7		-178.3		-180.5		-248.3		-402.4		-394.6	
D	1	-16.4	16.8	-23.1	22.2	126.4	22.8	121.7	21.8	110.0	24.1	96.8	21.9
D	2	-21.8	22.4	-27.8	26.7	148.9	26.9	140.5	25.1	127.0	27.8	111.4	25.2
D	3	-21.6	22.2	-22.8	21.9	115.7	20.9	115.7	20.7	94.1	20.6	90.6	20.5
D	4	-21.6	22.2	-19.7	19.0	97.4	17.6	102.9	18.4	75.8	16.6	82.9	18.7
D	5	-15.9	16.3	-10.7	10.3	65.6	11.8	78.4	14.0	49.7	10.9	60.9	13.8
D	SUM	-97.3		-104.1		553.9		559.2		456.6		442.6	
LOAD	PX (KIPS)	-100.0		-100.0		0.		-100.0		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-93.8	
ACTUAL	PX (KIPS)	0.		-19.4		0.		0.		0.		-19.4	
ACTUAL	PY (KIPS)	0.		0.		-19.3		-19.3		-19.3		-18.2	

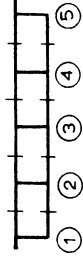
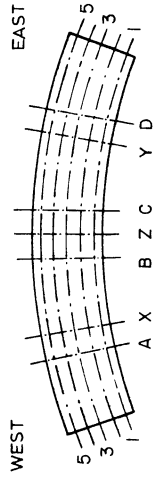


TABEL 341

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 50 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT

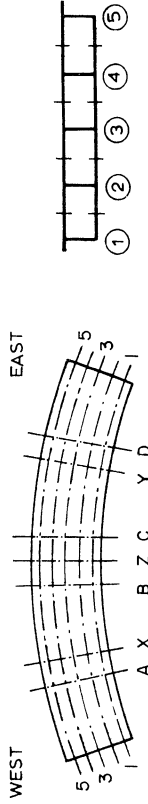
SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)					
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT			
A	1	116.1	20.8	167.5	28.3	-16.1	16.2	-14.3	19.9	100.0	21.8	154.3	30.0
A	2	139.9	25.1	142.0	24.0	-21.8	22.0	-14.4	19.9	118.0	25.8	125.7	24.4
A	3	119.5	21.4	116.3	19.7	-22.1	22.2	-14.6	20.3	97.4	21.3	98.7	19.2
A	4	107.1	19.2	102.6	17.4	-22.7	22.8	-16.7	23.2	84.4	18.4	84.7	16.5
A	5	74.6	13.4	62.5	10.6	-16.8	16.9	-12.1	16.7	57.8	12.6	51.4	10.0
A	SUM	557.1		590.9		-99.4		-72.1		457.7		514.7	
B	1	-27.6	15.6	-55.1	22.9	-56.6	22.9	-38.5	21.4	-80.1	20.0	-87.8	22.2
B	2	-42.4	24.0	-62.6	26.1	-63.5	25.8	-48.9	27.4	-100.5	25.0	-107.9	27.3
B	3	-53.3	30.2	-54.1	26.7	-39.7	16.1	-31.1	17.4	-87.6	21.8	-90.8	23.0
B	4	-34.5	19.6	-40.9	17.0	-48.1	19.5	-34.8	19.5	-78.4	19.5	-69.6	17.6
B	5	-18.8	10.6	-17.7	7.4	-38.6	15.7	-25.7	14.3	-54.7	13.6	-39.4	10.0
B	SUM	-176.6		-240.4		-246.6		-178.9		-401.3		-395.6	
C	1	-47.2	21.3	-33.5	19.3	-39.5	21.9	-76.0	29.7	-86.7	21.5	-102.0	25.5
C	2	-55.4	25.0	-42.6	24.6	-48.2	26.7	-79.1	30.9	-103.4	25.7	-110.9	27.8
C	3	-36.9	16.7	-30.9	17.8	-50.8	28.2	-54.5	21.3	-86.4	21.5	-80.2	20.1
C	4	-45.8	20.6	-38.1	22.0	-28.7	15.9	-29.3	11.4	-75.0	18.6	-63.8	16.0
C	5	-36.4	16.4	-28.3	16.3	-13.2	7.3	-17.3	6.8	-50.8	12.6	-42.4	10.6
C	SUM	-221.7		-173.4		-180.5		-256.2		-402.4		-399.3	
D	1	-16.4	16.8	-12.2	15.2	126.4	22.8	112.8	21.2	110.0	24.1	93.3	22.5
D	2	-21.8	22.4	-18.6	23.1	148.9	26.9	158.6	29.8	127.0	27.8	129.4	31.2
D	3	-21.6	22.2	-18.8	23.4	115.7	20.9	108.3	20.3	94.1	20.6	82.6	19.9
D	4	-21.6	22.2	-21.2	26.4	97.4	17.6	91.4	17.2	75.8	16.6	65.4	15.7
D	5	-15.9	16.3	-9.6	11.9	65.6	11.8	61.0	11.5	49.7	10.9	44.5	10.7
D	SUM	-97.3		-80.4		553.9		532.1		456.6		415.2	
LOAD	PX (KIPS)	-100.0		-100.0		0.		-0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-93.8	
ACTUAL	PX (KIPS)	0.		-19.4		0.		0.		-19.4		-19.4	
ACTUAL	PY (KIPS)	0.		0.		-19.3		-19.3		-18.2		-18.2	

TABLE 34J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 50 KSI CGND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)		
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT
A	1	116.1	20.8	165.8	16.1	16.2	-25.8	100.0	21.8	151.4
A	2	139.9	25.1	142.5	-21.8	22.0	-14.8	118.0	25.8	126.9
A	3	119.5	21.4	117.2	-22.1	22.2	-14.2	97.4	21.3	99.3
A	4	107.1	19.2	100.9	-22.7	22.8	-17.4	84.4	18.4	83.2
A	5	74.6	13.4	58.5	-16.8	16.9	-12.8	57.8	12.6	47.5
A	SUM	557.1		585.0	-99.4		-84.9	457.7		508.3
B	1	-27.6	15.6	-56.5	-56.6	22.9	-40.7	-80.1	20.0	-92.9
B	2	-42.4	24.0	-65.6	-63.5	25.8	-52.0	-100.5	25.0	-110.7
B	3	-53.3	30.2	-64.6	-39.7	16.1	-32.6	-87.6	21.8	-90.5
B	4	-34.5	19.6	-39.6	-48.1	19.5	-33.5	-78.4	19.5	-67.2
B	5	-18.8	10.6	-17.8	-38.6	15.7	-25.1	-54.7	13.6	-39.0
B	SUM	-176.6		-244.1	-246.6		-183.8	-401.3		-400.2
C	1	-47.2	21.3	-35.7	-39.5	21.9	-80.3	-86.7	21.5	-109.3
C	2	-55.4	25.0	-46.2	-48.2	26.7	-82.7	-103.4	25.7	-119.1
C	3	-36.9	16.7	-29.6	-50.8	28.2	-56.1	-86.4	21.5	-80.5
C	4	-45.8	20.6	-35.8	-28.7	15.9	-28.9	-75.0	18.6	-60.6
C	5	-36.4	16.4	-27.6	-13.2	7.3	-22.6	-50.8	12.6	-45.0
C	SUM	-221.7		-175.0	-180.5		-270.6	-402.4		-414.5
D	1	-16.4	16.8	-13.6	126.4	22.8	110.4	110.0	24.1	92.3
D	2	-21.8	22.4	-18.3	148.9	26.9	163.5	127.0	27.8	134.2
D	3	-21.6	22.2	-18.1	115.7	20.9	106.6	94.1	20.6	81.2
D	4	-21.6	22.2	-21.7	97.4	17.6	88.4	75.8	16.6	62.8
D	5	-15.9	16.3	-9.2	65.6	11.8	56.0	49.7	10.9	40.2
D	SUM	-97.3		-81.0	553.9		524.9	456.6		410.7
LOAD	PX (KIPS)	-100.0		-100.0	0.		-0.	-100.0		-100.0
LOAD	PY (KIPS)	0.		0.	-100.0		-100.0	-100.0		-93.8
ACTUAL	PX (KIPS)	0.		-19.4	0.		0.	-19.4		-19.4
ACTUAL	PY (KIPS)	0.		0.	-19.3		-19.3	-18.2		-18.2

**TABLE 35A**  
SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 50 KSI COND. LOADING.  
TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	NORMALIZED POINT LOADS APPLIED AT					
	(3-X)		(3-Y)		(3-X)+(3-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	-0.07	5.58	-2.53	-9.78	-2.60	-3.04
2E	-1.42	-7.76	8.65	25.54	7.23	14.00
3E	-1.32	-0.98	15.17	7.49	13.86	5.51
4E	-1.78	-3.96	9.25	2.65	7.47	8.72
5E	-3.27	-0.33	8.15	11.03	4.88	5.43
1F	-3.10	10.70	37.97	45.05	34.87	31.80
2F	-3.02	3.07	38.15	49.66	35.13	27.88
3F	37.65	25.76	-3.40	-11.14	34.26	39.34
4F	37.57	30.39	-3.58	-12.59	34.00	40.78
1W	.98	9.13	-.08	-.59	.90	7.47
2W	8.09	-1.45	-1.37	-.70	6.72	.50
3W	9.08	7.92	-1.35	.23	7.73	6.61
4W	9.17	7.28	-1.83	-1.26	7.34	3.65
5W	11.45	18.04	-3.22	-5.25	8.23	13.37
RE	-7.86	-7.45	38.69	36.93	30.84	30.62
RF	69.10	69.92	69.16	70.98	138.26	139.80
RW	38.77	40.92	-7.85	-7.57	30.92	31.60
SUMR	100.01	103.39	100.00	100.34	200.02	202.02
PX	-100.00	-100.00	0.	.01	-100.00	-100.00
PY	0.	.02	-100.00	-100.00	-100.00	-99.01
SUMP	-100.00	-99.98	-100.00	-99.99	-200.00	-199.01
SUMR/SUMP	1.00	1.03	1.00	1.00	1.00	1.02
TW	56.66	68.31	-17.34	-25.42	39.31	38.46
MF	122.04	63.57	-124.65	-177.66	-2.60	30.66
TF	-.24	18.39	-.54	-9.09	-.78	8.04
TE	-17.39	-20.63	56.50	48.19	39.11	30.00
ACTUAL PX		-19.27		.01		-19.44
ACTUAL PY		0.		-19.32		-19.25

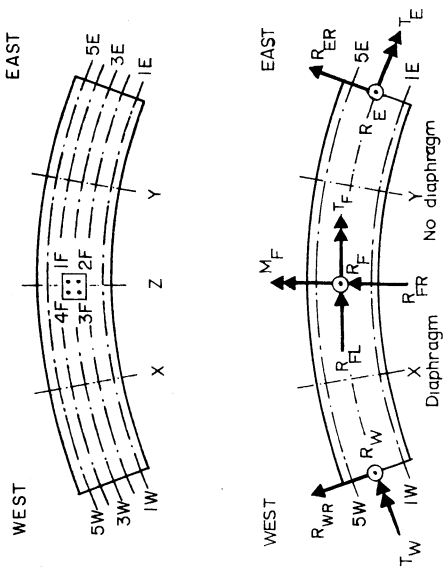
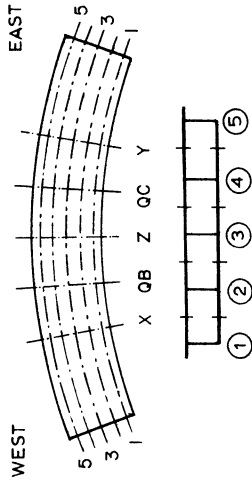


TABLE 35B

SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

RESULTS FOR POINT LOADS  
APPLIED AFTER 50 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



DEFLECTION AT POINT	(3-X)		(3-Y)		(3-X)+(3-Y)		E/T
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM	
1X	.692	1.121	-239	-446	.453	.848	1.87
2X	.740	1.250	-249	-475	.491	.952	1.94
3X	.793	1.370	-260	-501	.532	1.025	1.92
4X	.809	1.396	-273	-542	.536	1.045	1.95
5X	.831	1.423	-288	-567	.544	1.056	1.94
1QB	.421	.669	-207	-378	.214	.405	1.89
2QB	.441	.707	-215	-401	.225	.442	1.96
3QB	.460	.741	-222	-408	.238	.454	1.90
4QB	.481	.795	-235	-433	.246	.472	1.92
5QB	.500	.811	-245	-480	.255	.471	1.85
1Z	.013	.022	.011	.026	.024	.059	2.44
2Z	.007	.013	.007	.018	.014	.038	2.78
4Z	.007	.001	.006	.001	.012	.010	.79
5Z	.012	.018	.009	.011	.022	.040	1.86
1QC	-.208	-.327	.408	.689	.200	.276	1.38
2QC	-.216	-.344	.442	.775	.226	.334	1.48
3QC	-.221	-.370	.489	.886	.267	.411	1.54
4QC	-.234	-.391	.476	.840	.243	.348	1.43
5QC	-.244	-.415	.479	.809	.235	.309	1.31
1Y	-.243	-.389	.658	1.096	.415	.581	1.40
2Y	-.251	-.415	.735	1.300	.484	.727	1.50
3Y	-.260	-.430	.894	1.732	.634	1.125	1.78
4Y	-.272	-.446	.793	1.425	.521	.783	1.50
5Y	-.284	-.488	.773	1.328	.489	.706	1.44
LOAD PX	-100.0	-100.0	0.	0.	-100.0	-100.0	
LOAD PY	0.	0.	-100.0	-100.0	-100.0	-99.0	
ACTUAL PX			0.	0.		-19.4	
ACTUAL PY			-19.3	0.		-19.2	

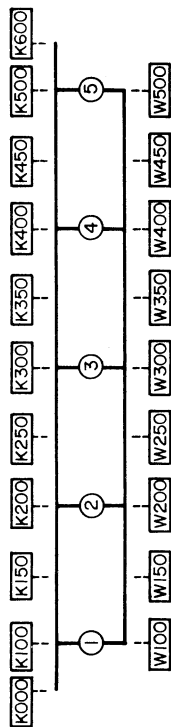
TABLE 3FC

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 50 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



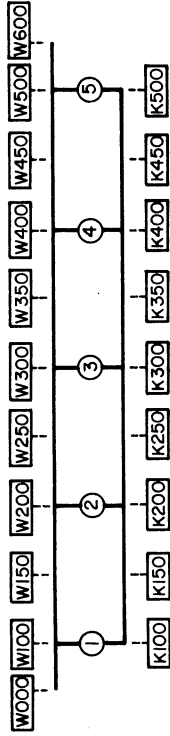
NORMALIZED POINT LOADS APPLIED AT

GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)		
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	
K	K000	-314	-345	68	111	-245	-311	-685
K	K100	-277	-755	59	236	-218	-685	-679
K	K150		-417		80		-290	-361
K	K200	-251	-480	50	143	-201	-434	-453
K	K250		-283		62		-227	-236
K	K300	-268	-441	52	118	-216	-392	-390
K	K350		-373		89		-326	-320
K	K400	-249	-465	50	126	-199	-414	-432
K	K450		-325		77		-281	-364
K	K500	-266	-391	58	121	-208	-357	-353
K	K600	-289	-262	65	86	-223	-243	-243
W	W100	1044	957	-217	-240	826	869	871
W	W150		813		-196		740	677
W	W200	969	910	-196	-231	772	802	793
W	W250		839		-200		747	722
W	W300	1048	1100	-211	-269	836	950	945
W	W350		910		-222		797	816
W	W400	958	1045	-196	-264	762	892	830
W	W450		942		-214		828	771
W	W500	982	1074	-210	-297	771	900	908
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0	
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-99.0	
ACTUAL	PX (KIPS)		-19.3		0.		-19.4	
ACTUAL	PY (KIPS)		0.		-19.3		-19.2	

TABLE 35D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 50 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.



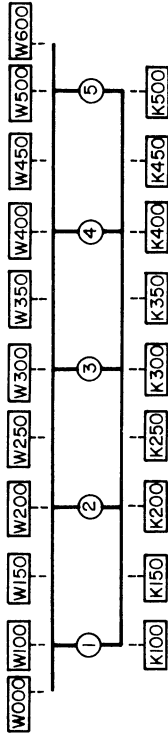
SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)		ADJUST
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	
W	W000	194	302	448	321	642	645	645
W	W100	196	255	399	281	596	573	584
W	W150		265		312		568	643
W	W200	222	418	314	336	536	749	751
W	W250		396		260		658	749
W	W300	335	503	214	253	549	774	804
W	W350		403		277		679	791
W	W400	226	317	308	271	534	614	627
W	W450		311		292		609	701
W	W500	201	313	381	301	582	611	619
W	W600	186	324	408	289	594	619	619
K	K100	-90	-165	-180	-207	-271	-360	-376
K	K150		-160		-293		-422	-375
K	K200	-99	-219	-149	-202	-248	-403	-381
K	K250		-254		-218		-439	-415
K	K300	-133	-272	-92	-215	-225	-440	-445
K	K350		-238		-220		-420	-422
K	K400	-102	-190	-145	-212	-248	-376	-374
K	K450		-193		-199		-381	-382
K	K500	-92	-173	-168	-183	-260	-342	-339
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-99.0	-99.0
ACTUAL	PX (KIPS)		-19.3		0.		-19.4	
ACTUAL	PY (KIPS)		0.		-19.3		-19.2	

TABLE 3FE

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 50 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



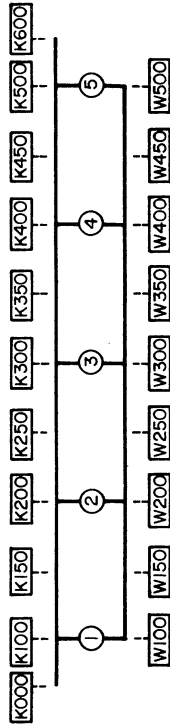
SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
W	W000	451	341	185	284	636	658
W	W100	403	295	187	247	591	575
W	W150	309	257	232	240	541	522
W	W200	204	343	368	431	572	817
W	W250	188	197	226	435	535	661
W	W300	309	212	178	555	571	858
W	W350	393	188	159	352	571	638
W	W400	421	327	288	373	571	778
W	W450	-182	258	272	263	582	582
W	W500	-147	295	288	275	614	603
W	W600	-88	292	292	284	615	615
K	K100	-182	-207	-87	-122	-269	-344
K	K150	-147	-196	-103	-115	-250	-302
K	K200	-88	-137	-145	-180	-234	-379
K	K250	-146	-174	-100	-244	-247	-478
K	K300	-174	-164	-80	-349	-234	-478
K	K350	-174	-181	-100	-261	-247	-548
K	K400	-174	-188	-100	-261	-247	-476
K	K450	-174	-273	-80	-174	-255	-367
K	K500	-174	-203	-80	-122	-255	-435
LOAD	PX (KIPS)	-100.0	-100.0	0.	.0	-100.0	-100.0
LOAD	PY (KIPS)	0.	.0	-100.0	-100.0	-100.0	-99.0
ACTUAL	PX (KIPS)	-19.3	-19.3	0.	.0	-19.4	-19.4
ACTUAL	PY (KIPS)	0.	0.	-19.3	-19.3	-19.2	-19.2

TABLE 35F

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 50 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION D

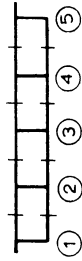
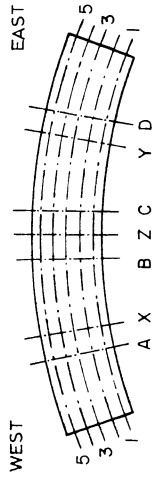
TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	62	47	-278	-158	-215	-117
K	K100	53	68	-241	-275	-187	-200
K	K150	158	154	-231	-579	-186	-412
K	K200	45	116	-238	-494	-192	-362
K	K250	98	114	-225	-428	-181	-315
K	K300	46	93	-226	-393	-176	-284
K	K350	158	164	-250	-690	-193	-511
K	K400	44	134	-226	-498	-176	-350
K	K450	190	175	-250	-678	-193	-495
K	K500	50	129	-157	-474	-120	-341
K	K600	57	40	-137	-157	-120	-341
W	W100	-224	-137	1042	767	818	530
W	W150	-199	-181	994	951	794	663
W	W200	-211	-214	1049	1143	837	814
W	W250	-192	-190	958	1117	766	820
W	W300	-206	-236	955	1373	749	994
W	W350	-100.0	-184	955	1066	749	775
W	W400	0.	-265	955	1178	749	841
W	W450	0.	-200	955	900	749	637
W	W500	0.	-224	955	987	749	725
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-99.0
ACTUAL	PX (KIPS)		-19.3		0.		-19.4
ACTUAL	PY (KIPS)		0.		-19.3		-19.2



**TABLE 35G**  
**DISTRIBUTION OF MOMENTS TO EACH GIRDER**  
**( KIP-FT AND PERCENTAGE )**

**MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH**  
**RESULTS FOR POINT LOADS**  
**APPLIED AFTER 50 KSI COND. LOADING.**  
**SIMPLY SUPPORTED, NO RESTRAINTS.**



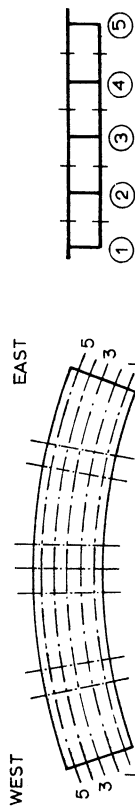
**NORMALIZED POINT LOADS APPLIED AT**

SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	92.9	65.6	11.7	-19.5	16.7	-15.2	73.4	16.2	59.7	12.3
A	2	129.6	121.6	21.8	-26.1	22.4	-29.8	103.5	22.9	107.9	22.2
A	3	130.4	142.6	25.5	-25.8	22.2	-34.2	104.6	23.1	123.8	25.5
A	4	127.8	143.7	25.7	-26.0	22.3	-35.5	101.8	22.5	123.0	25.3
A	5	88.4	85.2	15.2	-19.0	16.3	-22.1	69.4	15.3	71.9	14.8
A	SUM	569.0	558.7		-116.3		-136.9	452.7		486.3	
B	1	-27.5	-34.3	12.3	-48.8	18.4	-37.7	-77.0	15.9	-74.2	14.8
B	2	-48.2	-62.0	22.2	-61.5	23.2	-49.8	-109.9	22.7	-110.9	22.2
B	3	-66.7	-82.3	29.5	-48.3	18.3	-45.1	-113.8	23.5	-127.6	25.5
B	4	-49.2	-58.8	21.0	-60.0	22.7	-45.7	-109.2	22.5	-106.9	21.4
B	5	-27.9	-41.9	15.0	-46.1	17.4	-38.1	-74.5	15.4	-80.3	16.1
B	SUM	-219.6	-279.3		-264.8		-216.4	-484.4		-499.9	
C	1	-49.2	-39.4	18.9	-26.8	12.0	-33.8	-76.4	15.7	-77.5	15.0
C	2	-60.9	-48.2	23.2	-50.2	22.4	-65.1	-110.5	22.8	-118.3	23.0
C	3	-46.9	-35.0	16.8	-72.3	32.3	-80.7	-116.8	24.1	-123.4	23.9
C	4	-60.4	-48.3	23.2	-49.2	22.0	-61.6	-109.0	22.4	-116.3	22.6
C	5	-47.5	-37.2	17.9	-25.2	11.3	-37.4	-73.0	15.0	-80.0	15.5
C	SUM	-265.0	-208.0		-223.7		-278.6	-485.8		-515.5	
D	1	-20.0	-11.7	10.4	92.3	16.2	65.5	72.3	16.0	45.1	10.6
D	2	-26.5	-26.2	23.2	132.1	23.2	145.8	105.6	23.3	103.6	24.2
D	3	-25.8	-27.5	24.3	131.1	23.0	162.3	105.3	23.3	118.4	27.7
D	4	-25.6	-31.0	27.5	127.5	22.4	147.7	102.0	22.5	106.3	24.9
D	5	-18.6	-16.5	14.6	85.8	15.1	74.5	67.2	14.8	53.8	12.6
D	SUM	-116.4	-112.9		568.7		595.8	452.3		427.2	
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.		.0	-100.0		-100.0	
LOAD	PY (KIPS)	0.	0.	0.	-100.0		-100.0	-100.0		-99.0	
ACTUAL	PX (KIPS)	0.	-19.3	0.	0.		.0	-19.4		-19.4	
ACTUAL	PY (KIPS)	0.	0.	0.	-19.3		-19.3	-19.2		-19.2	

TABLE 35H  
DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 50 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

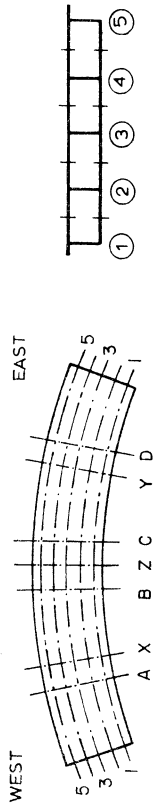


SECTION	GIRDER	(3-X)				(3-Y)				(3-X)+(3-Y)			
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
A	1	92.9	16.3	204.5	29.1	-19.5	16.7	-56.0	30.9	73.4	16.2	183.3	29.3
A	2	129.6	22.8	134.5	19.1	-26.1	22.4	-30.6	16.9	103.5	22.9	118.1	18.8
A	3	130.4	22.9	119.0	16.9	-25.8	22.2	-30.0	16.5	104.6	23.1	102.6	16.4
A	4	127.8	22.5	140.2	19.9	-26.0	22.3	-34.2	18.8	101.8	22.5	125.8	20.1
A	5	88.4	15.5	105.5	15.0	-19.0	16.3	-30.8	17.0	69.4	15.3	96.6	15.4
A	SUM	569.0		703.7		-116.3		-181.5		452.7		626.4	
B	1	-27.5	12.5	-27.4	10.8	-48.8	18.4	-42.9	15.7	-77.0	15.9	-64.7	13.5
B	2	-48.2	22.0	-58.4	23.0	-61.5	23.2	-66.0	24.2	-109.9	22.7	-110.7	23.0
B	3	-66.7	30.4	-79.4	31.3	-48.3	18.3	-68.1	24.9	-113.8	23.5	-131.7	27.4
B	4	-49.2	22.4	-58.2	22.9	-60.0	22.7	-63.7	23.3	-109.2	22.5	-112.9	23.5
B	5	-27.9	12.7	-30.5	12.0	-46.1	17.4	-32.5	11.9	-74.5	15.4	-60.5	12.6
B	SUM	-219.6		-253.9		-264.8		-273.2		-484.4		-480.6	
C	1	-49.2	18.6	-34.4	14.0	-26.8	12.0	-16.9	7.0	-76.4	15.7	-54.0	10.6
C	2	-60.9	23.0	-54.3	22.2	-50.2	22.4	-48.8	20.1	-110.5	22.8	-109.4	21.4
C	3	-46.9	17.7	-54.4	22.2	-72.3	32.3	-99.0	40.8	-116.8	24.1	-162.0	31.7
C	4	-60.4	22.8	-60.6	24.7	-49.2	22.0	-54.2	22.3	-109.0	22.4	-119.8	23.4
C	5	-47.5	17.9	-41.4	16.9	-25.2	11.3	-23.9	9.8	-73.0	15.0	-66.4	13.0
C	SUM	-265.0		-245.1		-223.7		-242.7		-485.8		-511.6	
D	1	-20.0	17.2	-24.3	13.6	92.3	16.2	88.2	13.0	72.3	16.0	63.9	13.4
D	2	-26.5	22.7	-37.0	20.7	132.1	23.2	149.1	21.9	105.6	23.3	105.7	22.1
D	3	-25.8	22.2	-34.5	19.3	131.1	23.0	139.8	20.6	105.3	23.3	94.5	19.8
D	4	-25.6	22.0	-44.9	25.1	127.5	22.4	161.1	23.7	102.0	22.5	114.3	23.9
D	5	-18.6	16.0	-38.1	21.3	85.8	15.1	140.9	20.7	67.2	14.8	99.9	20.9
D	SUM	-116.4		-178.8		568.7		679.1		452.3		478.3	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-99.0	
ACTUAL	PX (KIPS)			-19.3		0.		0.				-19.4	
ACTUAL	PY (KIPS)			0.		-19.3		-19.3				-19.2	

TABLE 351  
DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

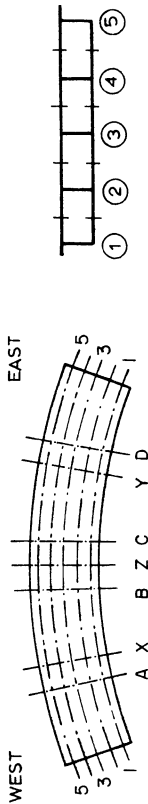
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 50 KSI COND. LOADING-  
SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)				
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT		
A	1	92.9	127.6	20.5	-19.5	16.7	-33.4	21.3	73.4	16.2	114.9	20.9
A	2	129.6	127.4	20.4	-26.1	22.4	-30.2	19.2	103.5	22.9	112.5	20.5
A	3	130.4	132.1	21.2	-25.8	22.2	-32.3	20.6	104.6	23.1	114.4	20.8
A	4	127.8	142.2	22.8	-26.0	22.3	-35.0	22.3	101.8	22.5	124.3	22.6
A	5	88.4	94.3	15.1	-19.0	16.3	-26.0	16.6	69.4	15.3	82.9	15.1
A	SUM	569.0	623.6		-116.3		-156.8		452.7		549.0	
B	1	-27.5	-30.5	11.5	-48.8	18.4	-40.6	16.4	-77.0	15.9	-69.0	14.1
B	2	-48.2	-60.0	22.6	-61.5	23.2	-58.8	23.7	-109.9	22.7	-110.8	22.6
B	3	-66.7	-80.7	30.4	-48.3	18.3	-57.8	23.3	-113.8	23.5	-129.9	26.5
B	4	-49.2	-58.5	22.0	-60.0	22.7	-55.7	22.5	-109.2	22.5	-110.2	22.5
B	5	-27.9	-35.6	13.4	-46.1	17.4	-35.0	14.1	-74.5	15.4	-69.4	14.2
B	SUM	-219.6	-265.3		-264.8		-247.9		-484.4		-489.3	
C	1	-49.2	-36.6	16.0	-26.8	12.0	-24.5	9.5	-76.4	15.7	-64.5	12.6
C	2	-60.9	-51.6	22.6	-50.2	22.4	-56.1	21.7	-110.5	22.8	-113.4	22.1
C	3	-46.9	-45.7	20.0	-72.3	32.3	-90.8	35.1	-116.8	24.1	-144.9	28.2
C	4	-60.4	-55.1	24.1	-49.2	22.0	-57.5	22.2	-109.0	22.4	-118.3	23.0
C	5	-47.5	-39.5	17.3	-25.2	11.3	-29.9	11.6	-73.0	15.0	-72.5	14.1
C	SUM	-265.0	-228.6		-223.7		-258.8		-485.8		-513.5	
D	1	-20.0	-17.3	12.2	92.3	16.2	75.7	11.9	72.3	16.0	53.5	11.9
D	2	-26.5	-31.0	21.8	132.1	23.2	147.3	23.3	105.6	23.3	104.6	23.2
D	3	-25.8	-30.6	21.5	131.1	23.0	152.3	24.1	105.3	23.3	107.7	23.9
D	4	-25.6	-37.2	26.2	127.5	22.4	153.8	24.3	102.0	22.5	109.9	24.4
D	5	-13.6	-26.1	18.4	85.8	15.1	104.1	16.4	67.2	14.8	74.4	16.5
D	SUM	-116.4	-142.3		568.7		633.2		452.3		450.2	
LOAD	PX (KIPS)	-100.0	-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.	0.		-100.0		-100.0		-100.0		-99.0	
ACTUAL	PX (KIPS)	0.	-19.3		0.		0.		0.		-19.4	
ACTUAL	PY (KIPS)	0.	0.		-19.5		-19.5		-19.2		-19.2	

TABLE 35J  
DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )



MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.  
RESULTS FOR POINT LOADS  
APPLIED AFTER 50 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)				
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT		
A	1	92.9	16.3	20.3	-19.5	16.7	-35.1	22.2	73.4	16.2	113.8	20.9
A	2	129.6	22.8	20.3	-26.1	22.4	-30.1	19.1	103.5	22.9	111.6	20.4
A	3	130.4	22.9	21.8	-25.8	22.2	-32.9	20.8	104.6	23.1	117.6	21.5
A	4	127.8	22.5	22.9	-26.0	22.3	-35.1	22.2	101.8	22.5	124.0	22.7
A	5	88.4	15.5	14.6	-19.0	16.3	-24.7	15.6	69.4	15.3	78.8	14.4
A	SUM	569.0	621.8		-116.3		-157.9		452.7		545.8	
B	1	-27.5	12.5	11.7	-48.8	18.4	-39.9	16.6	-77.0	15.9	-70.5	14.3
B	2	-48.2	22.0	22.5	-61.5	23.2	-55.9	23.2	-109.9	22.7	-110.8	22.5
B	3	-66.7	30.4	30.1	-48.3	18.3	-55.5	23.0	-113.8	23.5	-129.0	26.2
B	4	-49.2	22.4	21.7	-60.0	22.7	-53.6	22.3	-109.2	22.5	-109.1	22.1
B	5	-27.9	12.7	14.0	-46.1	17.4	-36.0	15.0	-74.5	15.4	-73.3	14.9
B	SUM	-219.6	-270.1		-264.8		-240.8		-484.4		-492.8	
C	1	-49.2	18.6	16.8	-26.8	12.0	-28.2	10.5	-76.4	15.7	-68.9	13.4
C	2	-60.9	23.0	22.6	-50.2	22.4	-60.4	22.5	-110.5	22.8	-115.5	22.4
C	3	-46.9	17.7	19.5	-72.3	32.3	-87.8	32.6	-116.8	24.1	-138.5	26.9
C	4	-60.4	22.8	23.6	-49.2	22.0	-59.4	22.1	-109.0	22.4	-117.4	22.8
C	5	-47.5	17.9	17.5	-25.2	11.3	-33.2	12.3	-73.0	15.0	-75.1	14.6
C	SUM	-265.0	-222.7		-223.7		-269.0		-485.8		-515.4	
D	1	-20.0	17.2	11.8	92.3	16.2	71.7	11.5	72.3	16.0	50.4	11.3
D	2	-26.5	22.7	22.1	132.1	23.2	146.7	23.6	105.6	23.3	104.3	23.4
D	3	-25.8	22.2	21.8	131.1	23.0	157.0	25.2	105.3	23.3	112.9	25.4
D	4	-25.6	22.0	26.4	127.5	22.4	151.6	24.3	102.0	22.5	108.6	24.4
D	5	-18.6	16.0	17.9	85.8	15.1	95.9	15.4	67.2	14.8	68.4	15.4
D	SUM	-116.4	-135.7		568.7		622.9		452.3		444.6	
LOAD	PX (KIPS)	-100.0			0.				-100.0		-100.0	
LOAD	PY (KIPS)	0.			-100.0				-100.0		-99.0	
ACTUAL	PX (KIPS)										-19.4	
ACTUAL	PY (KIPS)										-19.2	

TABLE 36A  
SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 50 KSI COND. LOADING.  
TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	(5-X)		(5-Y)		(5-X)+(5-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	-8.14	3.41	-23.25	-23.43	-31.39	-25.98
2E	-2.93	-14.14	-1.70	-3.50	-4.63	-9.58
3E	-1.37	-1.53	2.03	7.06	.67	4.19
4E	-7.1	-1.67	12.87	19.53	12.16	20.94
5E	2.95	3.66	46.35	36.06	49.30	36.64
1F	10.14	1.72	53.96	45.92	64.09	84.32
2F	-17.30	-29.96	26.17	8.68	8.87	12.57
3F	26.89	38.92	-17.04	-7.19	9.84	-7.70
4F	54.33	65.61	10.75	29.82	65.07	62.21
1W	-26.90	-16.60	-8.12	-6.64	-35.03	-24.54
2W	.30	-15.14	-2.90	-4.49	-2.60	-15.10
3W	5.47	4.61	-1.39	.19	4.08	5.23
4W	14.38	14.33	-7.2	-1.64	13.66	11.92
5W	42.90	49.11	3.00	.77	45.91	51.59
RE	-10.20	-10.27	36.30	35.72	26.11	26.21
RF	74.05	76.29	73.83	77.23	147.88	151.40
RW	36.15	36.31	-10.13	-11.81	26.02	29.10
SUMR	100.00	102.33	100.00	101.14	200.01	206.71
PX	-100.00	-100.00	0.	.01	-100.00	-100.00
PY	0.	.01	-100.00	-100.00	-100.00	-101.86
SUMP	-100.00	-99.99	-100.00	-99.99	-200.00	-201.86
SUMR/SUMP	1.00	1.02	1.00	1.01	1.00	1.02
TW	395.40	413.95	62.83	45.46	458.34	461.21
MF	132.56	199.15	-129.62	-47.95	2.94	-62.57
TF	82.32	87.55	83.37	111.37	165.69	212.49
TE	62.76	33.37	395.63	365.58	458.42	400.75
ACTUAL PX		-19.16		.02		-19.25
ACTUAL PY		0.		-19.07		-19.60

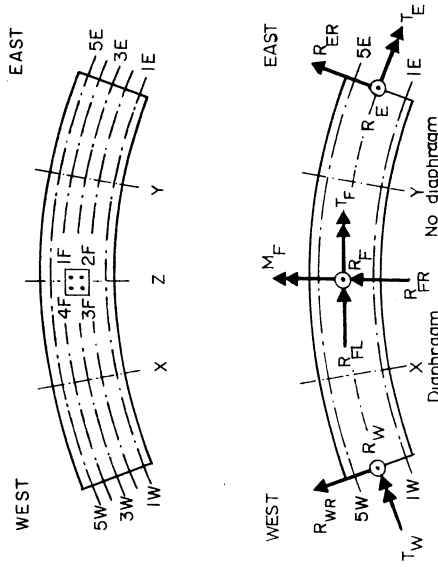
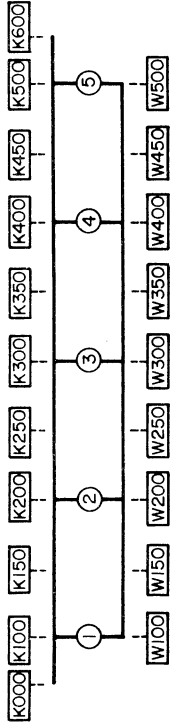




TABLE 36C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 50 KSI COND. LADJING. SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)			
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST		
K	K000	-303	-390	-390	83	104	-219	-258	-258
K	K100	-250	-752	-745	71	217	-178	-465	-460
K	K150	-228	-355	-440	60	71	-167	-230	-285
K	K200	-262	-474	-496	61	139	-200	-293	-308
K	K250	-280	-304	-329	58	60	-222	-221	-247
K	K300	-335	-472	-483	67	117	-268	-308	-323
K	K350	-412	-412	-431	75	82	-337	-272	-295
K	K400	-423	-580	-576	73	122	-421	-410	-408
K	K450	-590	-423	-521	75	73	-280	-280	-296
K	K500	-412	-336	-386	88	114	-272	-421	-419
K	K600	928	877	881	88	88	663	-272	-272
W	W100	877	881	881	-265	-236	471	471	481
W	W150	836	738	738	-236	-170	509	509	422
W	W200	862	931	921	-236	-215	566	566	542
W	W250	665	809	809	-221	-192	290	290	672
W	W300	1033	1182	1193	-250	-263	782	767	769
W	W350	1058	1058	1188	-228	-196	748	748	870
W	W400	1091	1354	1383	-228	-244	862	988	993
W	W450	948	1224	1224	-237	-190	571	571	1216
W	W500	1315	1609	1690	-243	-297	1071	1280	1314
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	0.	0.	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	0.	-100.0	-100.0	-100.0	-100.0	-100.0
ACTUAL	PX (KIPS)	-19.2	-19.2	-19.2	0.	0.	-19.2	-19.2	-19.2
ACTUAL	PY (KIPS)	0.	0.	0.	-19.1	-19.1	-19.1	-19.1	-19.6

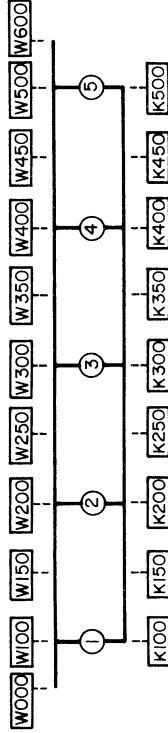
TABLE 36D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 50 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	252	168	499	340	751	513
W	W100	245	178	443	278	688	486
W	W150		181		322		495
W	W200	249	442	325	312	574	748
W	W250		457		221		703
W	W300	382	605	232	268	615	898
W	W350		523		343		872
W	W400	303	520	389	387	692	940
W	W450		509		358		976
W	W500	318	579	526	423	845	1029
W	W600	309	636	564	395	873	1072
K	K100	-110	-193	-195	-250	-306	-456
K	K150		-103		-324		-495
K	K200	-113	-254	-155	-184	-268	-489
K	K250		-326		-171		-551
K	K300	-153	-239	-102	-183	-255	-504
K	K350		-219		-237		-506
K	K400	-139	-224	-187	-253	-326	-496
K	K450		-333		-225		-579
K	K500	-147	-285	-236	-239	-384	-522
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-101.9
ACTUAL	PX (KIPS)		-19.2		0.		-19.2
ACTUAL	PY (KIPS)		0.		-19.1		-19.6



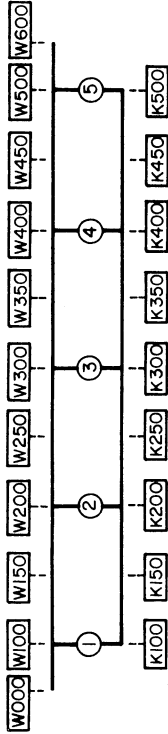
TABLE 36E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
APPLIED AFTER 50 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
COMPRESSION = - W = WELDABLE STRAIN GAGES

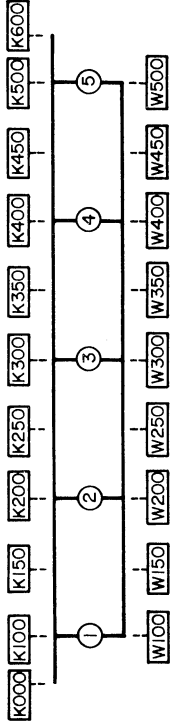


GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)			
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST		
W	W000	511	373	373	199	133	711	496	496
W	W100	451	320	332	209	160	661	470	457
W	W150		280	321		183		435	450
W	W200	338	374	371	217	372	555	749	747
W	W250		263	282		356		588	607
W	W300	240	308	313	357	553	598	895	905
W	W350		272	316		399		675	787
W	W400	388	510	530	310	591	698	1148	1168
W	W450		409	438		511		917	943
W	W500	510	462	449	376	745	886	1211	1206
W	W600	545	448	448	383	831	929	1263	1263
K	K100	-200	-269	-257	-89	-224	-290	-467	-456
K	K150		-262	-267		-155		-396	-365
K	K200	-161	-249	-256	-97	-176	-259	-385	-382
K	K250		-255	-250		-180		-377	-415
K	K300	-105	-249	-250	-144	-220	-249	-405	-401
K	K350		-251	-251		-370		-567	-557
K	K400	-185	-254	-247	-145	-258	-331	-474	-506
K	K450		-407	-373		-71		-434	-504
K	K500	-228	-259	-257	-177	-412	-405	-647	-630
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	0.	0.	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	0.	-100.0	-100.0	-100.0	-101.9	-101.9
ACTUAL	PX (KIPS)	-19.2	-19.2	-19.2	0.	0.	-19.2	-19.2	-19.2
ACTUAL	PY (KIPS)	0.	0.	0.	-19.1	-19.1	-19.6	-19.6	-19.6

TABLE 36F

SUMMARY OF STRAINS (MICRC IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 50 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

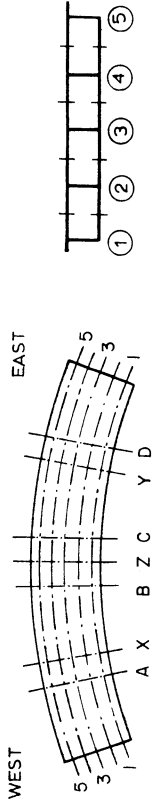
GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)	
		THEORY	MEASR.	THEORY	MEASR.	THEORY	MEASR.
K	K000	75	59	-243	-124	-167	-96
K	K100	64	88	-205	-211	-141	-153
K	K150	181	174	-461	-454	-396	-395
K	K200	54	152	-190	-370	-135	-313
K	K250	120	128	-331	-397	-282	-282
K	K300	55	128	-226	-366	-171	-318
K	K350	216	216	-596	-639	-541	-597
K	K400	52	210	-264	-547	-212	-533
K	K450	284	318	-790	-842	-746	-833
K	K500	59	203	-318	-565	-259	-549
K	K600	67	63	-379	-215	-312	-190
W	W100	-271	-229	829	564	558	422
W	W150	-281	-270	806	626	566	516
W	W200	-302	-299	767	763	621	614
W	W250	-278	-257	750	699	598	554
W	W300	-322	-318	1015	1037	762	920
W	W350	-219	-221	1083	1003	960	924
W	W400	-309	-310	1187	1614	1508	1436
W	W450	-252	-245	1436	1290	1347	1206
W	W500	-314	-319	1386	374	1143	265
LOAD	PX (KIPS)	-100.0	-100.0	0.	0.	-100.0	-100.0
LOAD	PY (KIPS)	0.	0.	-100.0	-100.0	-100.0	-101.9
ACTUAL	PX (KIPS)	-19.2	0.	0.	0.	-19.2	-19.6
ACTUAL	PY (KIPS)	0.	0.	-19.1	-19.1	-19.6	-19.6

TABLE 36G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

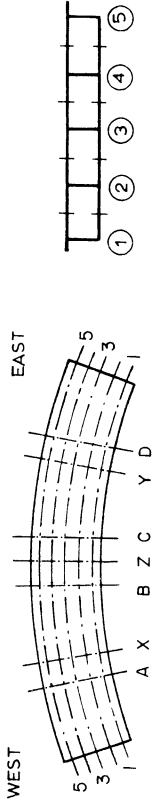
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR POINT LOADS  
APPLIED AFTER 50 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	83.4	14.3	61.1	9.3	-23.6	17.2	-14.4	11.4	59.8	13.4	32.7	6.7
A	2	115.8	19.9	122.6	18.6	-31.3	22.7	-28.0	22.1	84.5	19.0	78.8	16.2
A	3	126.6	21.7	157.6	23.9	-30.5	22.2	-32.4	25.6	96.0	21.6	110.9	22.8
A	4	143.1	24.6	192.1	29.1	-30.3	22.0	-31.0	24.5	112.8	25.4	153.3	31.5
A	5	113.2	19.5	126.6	19.2	-22.0	16.0	-20.6	16.3	91.3	20.5	111.2	22.8
A	SUM	582.1		659.9		-137.8		-126.3		444.4		487.0	
B	1	-33.3	12.2	-21.7	6.3	-54.0	17.1	-36.9	15.2	-87.5	14.9	-59.9	9.8
B	2	-54.8	20.0	-60.3	17.3	-65.8	20.8	-46.7	19.2	-120.3	20.5	-107.1	17.6
B	3	-77.2	28.2	-100.6	28.9	-54.7	17.3	-46.0	18.9	-130.4	22.2	-149.9	24.6
B	4	-65.5	23.9	-90.8	26.1	-77.6	24.5	-61.3	25.2	-142.7	24.3	-158.0	26.0
B	5	-42.9	15.7	-74.5	21.4	-64.2	20.3	-52.2	21.5	-107.2	18.2	-134.3	22.0
B	SUM	-273.7		-348.0		-316.3		-243.0		-588.1		-609.6	
C	1	-55.2	17.3	-44.3	15.5	-28.0	10.4	-14.9	4.5	-83.5	14.3	-57.6	9.3
C	2	-68.0	21.4	-55.7	19.5	-48.5	18.1	-50.4	15.3	-116.3	19.9	-104.5	17.0
C	3	-56.1	17.6	-49.7	17.4	-73.3	27.3	-82.3	25.1	-127.8	21.9	-133.3	21.6
C	4	-76.9	24.2	-76.0	26.6	-68.5	25.5	-90.4	27.5	-144.5	24.7	-169.8	27.6
C	5	-62.3	19.5	-59.7	20.9	-50.4	18.8	-90.3	27.5	-112.2	19.2	-150.9	24.5
C	SUM	-318.5		-285.4		-268.8		-328.3		-584.3		-616.1	
D	1	-24.1	17.4	-19.5	12.7	76.3	13.1	45.3	8.8	52.2	11.7	35.4	7.9
D	2	-31.8	22.9	-39.1	25.5	108.9	18.7	96.0	18.6	77.1	17.3	76.6	17.0
D	3	-30.7	22.2	-37.3	24.3	125.0	21.4	126.1	24.4	94.2	21.2	110.8	24.7
D	4	-30.2	21.8	-36.5	23.8	152.7	26.2	194.3	37.7	122.5	27.5	180.8	40.3
D	5	-21.9	15.8	-21.0	13.7	120.6	20.7	54.4	10.5	98.7	22.2	45.5	10.1
D	SUM	-138.7		-153.5		583.5		516.0		444.7		449.0	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-101.9	
ACTUAL	PX (KIPS)	0.		-19.2		0.		0.		0.		-19.2	
ACTUAL	PY (KIPS)	0.		0.		-19.1		-19.1		0.		-19.6	

**TABLE 36H**  
 DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )



**MOMENTS ABOUT TENSION FLANGE STEEL**

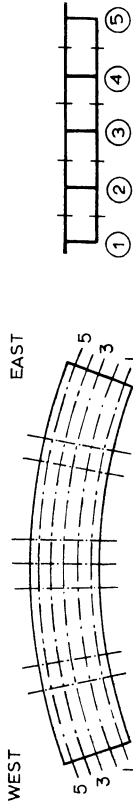
RESULTS FOR POINT LOADS  
 APPLIED AFTER 50 KSI CCND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1	83.4	185.0	23.7	-23.6	-51.7	17.2	59.8	118.4	23.1
A	2	115.8	139.6	17.9	-31.3	-29.0	22.7	84.5	93.0	18.1
A	3	126.6	134.1	17.2	-30.5	-27.0	22.2	96.0	93.8	18.3
A	4	143.1	157.1	21.4	-30.3	-31.8	22.0	112.8	110.2	21.5
A	5	113.2	154.7	19.8	-22.0	-28.5	16.0	91.3	98.1	19.1
A	SUM	582.1	780.4		-137.8	-168.0		444.4	513.4	
B	1	-33.3	-28.6	10.0	-54.0	-50.9	17.1	-87.5	-83.8	13.7
B	2	-54.8	-68.9	24.0	-65.8	-62.6	20.3	-120.3	-155.1	22.2
B	3	-77.2	-72.7	25.4	-54.7	-59.0	20.5	-130.4	-152.4	25.0
B	4	-65.5	-66.6	23.2	-77.6	-74.7	26.0	-142.7	-148.1	24.3
B	5	-42.9	-49.9	17.4	-64.2	-39.8	13.9	-107.2	-90.5	14.8
B	SUM	-273.7	-286.6		-316.3	-287.0		-588.1	-609.9	
C	1	-55.2	-47.2	13.8	-28.0	-35.5	12.1	-83.5	-76.9	13.5
C	2	-68.0	-77.3	22.6	-48.5	-58.2	19.9	-116.3	-111.1	19.5
C	3	-56.1	-80.0	23.4	-73.3	-84.8	29.0	-127.8	-136.1	23.9
C	4	-76.9	-82.4	24.1	-68.5	-59.7	23.8	-144.5	-148.7	26.2
C	5	-62.3	-55.4	16.2	-50.4	-44.1	15.1	-112.2	-95.7	16.8
C	SUM	-318.5	-342.3		-268.8	-292.1		-584.3	-568.5	
D	1	-24.1	-28.4	11.3	76.3	70.3	10.3	52.2	57.1	9.1
D	2	-31.8	-43.1	17.1	108.9	114.0	15.7	77.1	95.4	15.4
D	3	-30.7	-44.2	17.6	125.0	128.0	18.8	94.2	113.7	18.1
D	4	-30.2	-69.0	27.4	152.7	183.6	26.9	122.5	178.5	28.4
D	5	-21.9	-66.8	26.6	120.6	186.6	27.3	98.7	182.2	29.0
D	SUM	-138.7	-251.5		583.5	682.6		444.7	627.9	
LOAD	PX (KIPS)	-100.0	-100.0		0.	0.		-100.0	-100.0	
LOAD	PY (KIPS)	0.	0.		-100.0	-100.0		-100.0	-101.9	
ACTUAL	PX (KIPS)		-19.2			0.			-19.2	
ACTUAL	PY (KIPS)		0.		-19.1	-19.1			-19.6	

TABLE 361

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 50 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



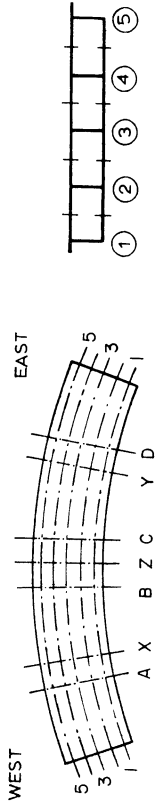
NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	83.4	14.3	116.4	16.3	-23.6	17.2	-31.0	21.4	59.8	13.4	71.0	14.2
A	2	115.8	19.9	130.2	18.2	-31.3	22.7	-28.4	19.6	84.5	19.0	85.2	17.1
A	3	126.6	21.7	147.2	20.6	-30.5	22.2	-30.0	20.7	96.0	21.6	103.3	20.7
A	4	143.1	24.6	181.0	25.3	-30.3	22.0	-31.3	21.6	112.8	25.4	134.1	26.9
A	5	113.2	19.5	139.1	19.5	-22.0	16.3	-24.2	16.7	91.3	20.5	105.4	21.1
A	SUM	582.1		713.9		-137.8		-144.9		444.4		498.9	
B	1	-33.3	12.2	-25.5	8.1	-54.0	17.1	-44.7	16.7	-87.5	14.9	-73.2	12.0
B	2	-54.8	20.0	-65.1	20.7	-65.8	20.8	-55.5	20.8	-120.3	20.5	-122.6	20.1
B	3	-77.2	28.2	-85.2	27.1	-54.7	17.3	-53.2	19.9	-130.4	22.2	-151.3	24.8
B	4	-65.5	23.9	-77.4	24.6	-77.6	24.5	-68.8	25.7	-142.7	24.3	-152.8	25.1
B	5	-42.9	15.7	-60.9	19.4	-64.2	20.3	-45.3	17.0	-107.2	18.2	-110.0	18.0
B	SUM	-273.7		-314.1		-316.3		-267.5		-588.1		-610.0	
C	1	-55.2	17.3	-45.9	14.5	-28.0	10.4	-26.3	8.5	-83.5	14.3	-68.3	11.6
C	2	-68.0	21.4	-67.7	21.3	-48.5	18.1	-54.7	17.7	-116.3	19.9	-108.2	18.3
C	3	-56.1	17.6	-66.5	21.0	-73.3	27.3	-83.7	27.1	-127.8	21.9	-134.9	22.9
C	4	-76.9	24.2	-79.6	25.1	-68.5	25.5	-78.9	25.6	-144.5	24.7	-158.1	26.8
C	5	-62.3	19.5	-57.3	18.1	-50.4	18.8	-64.7	21.0	-112.2	19.2	-120.3	20.4
C	SUM	-318.5		-317.0		-268.8		-308.3		-584.3		-589.9	
D	1	-24.1	17.4	-23.5	11.9	76.3	13.1	56.5	9.6	52.2	11.7	45.1	8.5
D	2	-31.8	22.9	-40.9	20.7	108.9	18.7	104.1	17.6	77.1	17.3	85.4	16.2
D	3	-30.7	22.2	-40.4	20.5	125.0	21.4	127.0	21.5	94.2	21.2	112.1	21.2
D	4	-30.2	21.8	-51.0	25.9	152.7	26.2	189.6	32.1	122.5	27.5	179.8	34.0
D	5	-21.9	15.8	-41.5	21.0	120.6	20.7	113.4	19.2	98.7	22.2	106.6	20.1
D	SUM	-138.7		-197.3		583.5		590.5		444.7		529.0	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		0.		0.	
ACTUAL	PX (KIPS)	-19.2		-19.2		0.		0.		-19.2		-19.2	
ACTUAL	PY (KIPS)	0.		0.		-19.1		-19.1		0.		0.	

**TABLE 36J**  
 DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
 APPLIED AFTER 50 KSI CCND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	(5-X)			(5-Y)			(5-X) + (5-Y)					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	83.4	14.3	117.9	16.5	-23.6	17.2	-32.2	22.2	59.8	13.4	74.6	14.5
A	2	115.8	19.9	128.6	18.0	-31.3	22.7	-28.4	19.5	84.5	19.0	83.9	16.4
A	3	126.6	21.7	150.9	21.1	-30.5	22.2	-30.7	21.1	96.0	21.6	105.9	20.6
A	4	143.1	24.6	184.7	25.8	-30.3	22.0	-31.2	21.5	112.8	25.4	140.8	27.4
A	5	113.2	19.5	134.0	18.7	-22.0	16.0	-22.9	15.7	91.3	20.5	108.1	21.1
A	SUM	582.1		716.0		-137.8		-145.5		444.4		513.2	
B	1	-33.3	12.2	-25.3	7.6	-54.0	17.1	-43.4	16.6	-87.5	14.9	-71.6	11.6
B	2	-54.8	20.0	-63.6	19.1	-65.8	20.8	-52.5	20.1	-120.3	20.5	-117.8	19.2
B	3	-77.2	28.2	-93.2	28.0	-54.7	17.3	-51.3	19.6	-130.4	22.2	-150.7	24.5
B	4	-65.5	23.9	-83.8	25.2	-77.6	24.5	-66.6	25.5	-142.7	24.3	-155.0	25.2
B	5	-42.9	15.7	-66.4	20.0	-64.2	20.3	-47.8	18.3	-107.2	18.2	-119.7	19.5
B	SUM	-273.7		-332.3		-316.3		-261.6		-588.1		-614.9	
C	1	-55.2	17.3	-45.6	14.7	-28.0	10.4	-27.5	8.6	-83.5	14.3	-67.1	11.1
C	2	-68.0	21.4	-64.5	20.8	-48.5	18.1	-52.9	16.5	-116.3	19.9	-106.7	17.7
C	3	-56.1	17.6	-63.2	20.4	-73.3	27.3	-82.9	25.9	-127.8	21.9	-134.2	22.2
C	4	-76.9	24.2	-78.1	25.2	-68.5	25.5	-83.9	26.2	-144.5	24.7	-163.4	27.1
C	5	-62.3	19.5	-58.1	18.8	-50.4	18.8	-73.5	22.9	-112.2	19.2	-131.9	21.9
C	SUM	-318.5		-309.4		-268.8		-320.7		-584.3		-603.4	
D	1	-24.1	17.4	-22.1	11.6	76.3	13.1	52.3	8.6	52.2	11.7	41.3	7.5
D	2	-31.8	22.9	-40.4	21.2	108.9	18.7	101.8	16.8	77.1	17.3	83.0	15.1
D	3	-30.7	22.2	-39.4	20.7	125.0	21.4	126.6	20.9	94.2	21.2	111.6	20.2
D	4	-30.2	21.8	-49.0	25.7	152.7	26.2	191.5	31.7	122.5	27.5	180.2	32.7
D	5	-21.9	15.8	-39.6	20.8	120.6	20.7	132.6	21.9	98.7	22.2	135.1	24.5
D	SUM	-138.7		-190.5		583.5		604.8		444.7		551.3	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	0.		0.		-100.0		-100.0		-100.0		-101.9	
ACTUAL	PX (KIPS)			-19.2		0.		0.				-19.2	
ACTUAL	PY (KIPS)			0.		-19.1		-19.1				-19.6	

TABLE 37A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 50 KSI COND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

NORMALIZED POINT LOADS APPLIED AT  
 (1-X)+(5-Y)  
 \*\*\*\*\*  
 THEORY EXPERM \*\*\*\*\*  
 THEORY EXPERM \*\*\*\*\*  
 THEORY EXPERM

REACTION OR LOAD	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	-15.18	-19.25				
2E	-1.65	1.29				
3F	.72	5.51				
4E	9.96	16.80				
5E	36.73	26.38				
1F	37.82	46.46				
2F	37.77	29.46				
3F	31.36	23.35				
4F	31.41	38.16				
1W	29.07	26.93				
2W	8.98	12.39				
3W	2.20	6.52				
4W	.15	.74				
5W	-9.33	-12.49				
RF	30.58	30.73				
RF	138.36	137.43				
RW	31.07	34.09				
SUMR	200.01	202.25				
PX	-100.00	-100.00				
PY	-100.00	-98.39				
SUMP	-200.00	-198.39				
SUMR/SUMP	1.00	1.02				
TW	-220.32	-232.82				
MF	-19.22	-21.61				
TF	.15	47.71				
TE	296.99	274.71				
ACTUAL PX						-19.39
ACTUAL PY						-19.14

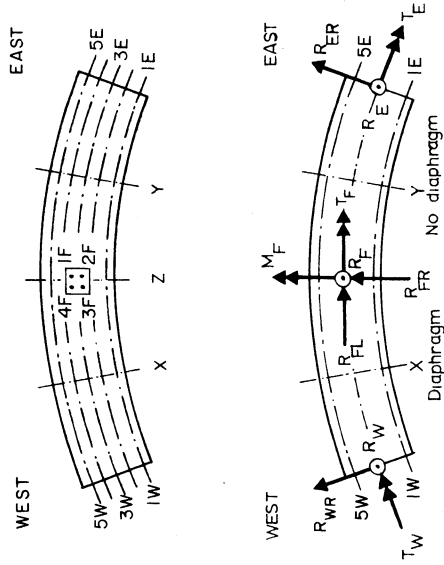
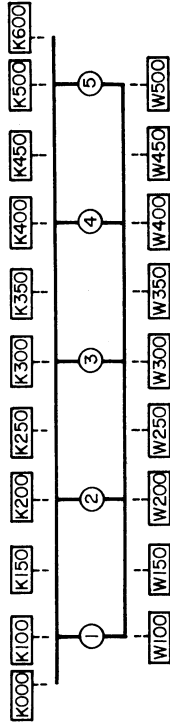






TABLE 37C

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 50 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

NORMALIZED POINT LOADS APPLIED AT

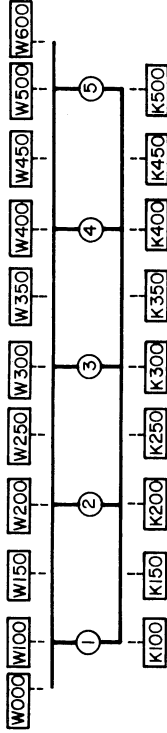
GAGE TYPE	GAGE LOC.	(1-X)+(5-Y)		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	ADJUST	ADJUST	THEORY	ADJUST
K	K000	-347	-440	-930			
K	K100	-269	-930	-891			
K	K150		-334	-285			
K	K200	-211	-468	-502			
K	K250		-202	-196			
K	K300	-183	-359	-352			
K	K350		-259	-247			
K	K400	-152	-299	-299			
K	K450		-177	-192			
K	K500	-159	-201	-204			
K	K600	-186	-157	-157			
*****							
W	W100	1100	1113	1119			
W	W150		912	911			
W	W200	823	833	820			
W	W250		802	713			
W	W300	720	690	687			
W	W350		593	556			
W	W400	568	554	544			
W	W450		737	388			
W	W500	573	547	551			
*****							
LOAD	PX (KIPS)	-100.0	-100.0	-100.0			
LOAD	PY (KIPS)	-100.0	-98.4				
ACTUAL	PX (KIPS)		-19.4				
ACTUAL	PY (KIPS)		-19.1				



TABLE 37E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
APPLIED AFTER 50 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION C

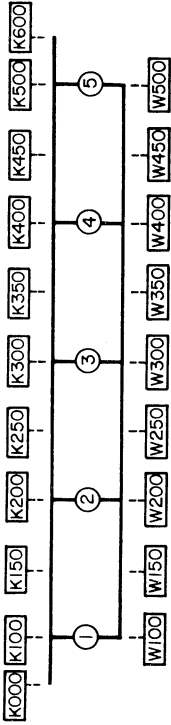
TENSION = + K = CONCRETE STRAIN METERS  
COMPRESSION = - W = WELDABLE STRAIN GAGES

NORMALIZED POINT LOADS APPLIED AT

GAGE TYPE	GAGE LOC.	(1-X) + (5-Y)		THEORY MEASR ADJUST		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	ADJUST	ADJUST	ADJUST	ADJUST	ADJUST	
W	W000	624	459	459					
W	W100	596	469	458					
W	W150		438	431					
W	W200	498	750	743					
W	W250		551	539					
W	W300	512	754	775					
W	W350		533	639					
W	W400	541	834	842					
W	W450		686	683					
W	W500	680	921	922					
W	W600	709	1005	1005					
K	K100	-267	-411	-406					
K	K150		-312	-269					
K	K200	-232	-322	-313					
K	K250		-307	-351					
K	K300	-211	-328	-323					
K	K350		-513	-499					
K	K400	-256	-401	-413					
K	K450		-232	-260					
K	K500	-310	-570	-584					
LOAD	PX (KIPS)	-100.0	-100.0	-100.0					
LOAD	PY (KIPS)	-100.0	-58.4	-58.4					
ACTUAL	PX (KIPS)		-19.4	-19.4					
ACTUAL	PY (KIPS)		-19.1	-19.1					

TABLE 37F

SUMMARY OF STRAINS (MICR IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 50 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION D  
 TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

NORMALIZED POINT LOADS APPLIED AT

GAGE TYPE	GAGE LOC.	(1-X) + (5-Y)		THEORY MEASR ADJUST		THEORY MEASR ADJUST	
		THEORY	MEASR	ADJUST	ADJUST	MEASR	ADJUST
K	K000	-191	-80	-80			
K	K100	-161	-137	-143			
K	K150		-288	-281			
K	K200	-152	-275	-270			
K	K250		-246	-297			
K	K300	-187	-310	-324			
K	K350		-493	-526			
K	K400	-227	-487	-478			
K	K450		-712	-776			
K	K500	-275	-528	-544			
K	K600	-330	-215	-528			
W	W100	646	411	417			
W	W150		493	450			
W	W200	642	568	563			
W	W250		569	527			
W	W300	837	856	860			
W	W350		859	810			
W	W400	1024	1459	1399			
W	W450		1269	1126			
W	W500	1209	243	267			

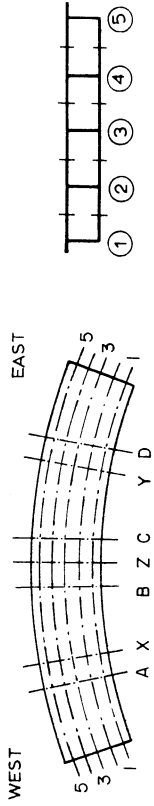
LOAD	PX (KIPS)	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-98.4
ACTUAL	PX (KIPS)	-19.4	
ACTUAL	PY (KIPS)	-19.1	

TABLE 37G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR POINT LOADS  
APPLIED AFTER 50 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT

\*\*\*\*\*  
THEORY K-FT PCT  
\*\*\*\*\*  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

\*\*\*\*\*  
THEORY K-FT PCT  
\*\*\*\*\*  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

(1-X)+(5-Y)  
\*\*\*\*\*  
THEORY K-FT PCT  
\*\*\*\*\*  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

SECTION	GIRDER	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
A	1	92.4	22.0	78.8	19.4
A	2	108.5	25.9	119.2	29.4
A	3	88.9	21.2	94.2	23.2
A	4	76.8	18.3	73.2	18.0
A	5	52.6	12.5	40.2	9.9
A	SUM	419.3		405.6	

B	1	-80.8	16.6	-91.8	19.1
B	2	-106.4	21.9	-109.6	22.8
B	3	-105.0	21.6	-111.3	23.2
B	4	-111.4	22.9	-97.8	20.4
B	5	-83.2	17.1	-59.3	14.4
B	SUM	-486.9		-479.8	

C	1	-76.1	15.6	-55.8	11.0
C	2	-104.4	21.3	-100.8	19.8
C	3	-109.0	22.3	-113.9	22.4
C	4	-113.5	23.2	-125.2	24.6
C	5	-86.5	17.7	-112.8	22.2
C	SUM	-489.5		-508.4	

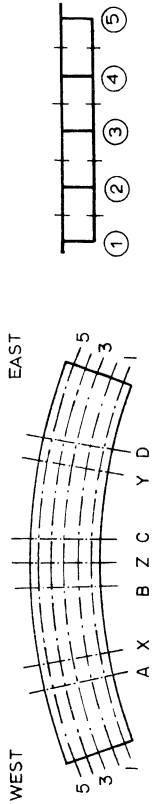
D	1	59.9	12.3	34.4	8.2
D	2	87.1	17.9	71.8	17.1
D	3	103.4	21.3	101.4	24.1
D	4	131.1	27.0	171.5	40.8
D	5	104.7	21.5	41.2	9.8
D	SUM	486.2		420.4	

LOAD	PX (KIPS)	-100.0
LOAD	PY (KIPS)	-100.0
ACTUAL	PX (KIPS)	-98.4
ACTUAL	PY (KIPS)	-19.4
		-19.1

**TABLE 37H**  
 DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
 APPLIED AFTER 50 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

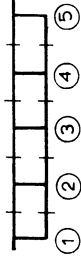
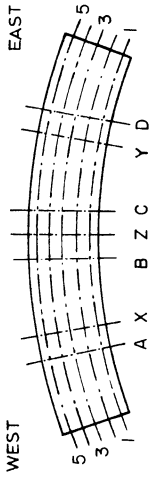


NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	(1-X)+(5-Y)		THEORY		EXPERIMENTAL		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	92.4	22.0	223.3	39.6						
A	2	108.5	25.9	113.2	20.1						
A	3	88.9	21.2	89.1	15.8						
A	4	76.8	18.3	84.2	14.9						
A	5	52.6	12.5	54.5	9.6						
A	SUM	419.3		564.3							
B	1	-80.8	16.6	-98.1	18.9						
B	2	-106.4	21.9	-123.4	23.7						
B	3	-105.0	21.6	-117.1	22.5						
B	4	-111.4	22.9	-120.9	23.3						
B	5	-83.2	17.1	-60.2	11.6						
B	SUM	-486.9		-519.7							
C	1	-76.1	15.6	-62.5	13.9						
C	2	-104.4	21.3	-87.1	19.3						
C	3	-109.0	22.3	-115.1	25.5						
C	4	-113.5	23.2	-112.9	25.0						
C	5	-86.5	17.7	-73.2	16.2						
C	SUM	-489.5		-450.8							
D	1	59.9	12.3	43.4	7.7						
D	2	87.1	17.9	90.5	14.2						
D	3	103.4	21.3	103.5	18.3						
D	4	131.1	27.0	161.2	28.5						
D	5	104.7	21.5	177.3	31.3						
D	SUM	486.2		565.9							
LOAD	PX (KIPS)			-100.0							
LOAD	PY (KIPS)			-100.0							
ACTUAL	PX (KIPS)			-98.4							
ACTUAL	PY (KIPS)			-19.4							

TABLE 371

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.



RESULTS FOR POINT LOADS  
APPLIED AFTER 50 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	(1-X)+(5-Y)		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	92.4	22.0	143.3	30.1		
A	2	108.5	25.9	116.5	24.5		
A	3	88.9	21.2	92.0	19.3		
A	4	76.8	18.3	78.1	16.4		
A	5	52.6	12.5	46.6	9.8		
	SUM	419.3		476.6			
B	1	-80.8	16.6	-95.3	19.0		
B	2	-106.4	21.9	-117.3	23.4		
B	3	-105.0	21.6	-114.6	22.8		
B	4	-111.4	22.9	-110.6	22.0		
B	5	-83.2	17.1	-64.3	12.8		
	SUM	-486.9		-502.1			
C	1	-76.1	15.6	-59.5	12.5		
C	2	-104.4	21.3	-93.2	19.6		
C	3	-109.0	22.3	-114.6	24.0		
C	4	-113.5	23.2	-118.4	24.8		
C	5	-86.5	17.7	-90.9	19.1		
	SUM	-489.5		-476.6			
D	1	59.9	12.3	38.4	7.9		
D	2	87.1	17.9	75.7	15.6		
D	3	103.4	21.3	102.4	21.1		
D	4	131.1	27.0	167.0	34.4		
D	5	104.7	21.5	102.0	21.0		
	SUM	486.2		485.5			
LOAD	PX (KIPS)	-100.0		-100.0			
LOAD	PY (KIPS)	-100.0		-98.4			
ACTUAL	PX (KIPS)			-19.4			
ACTUAL	PY (KIPS)			-19.1			

\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

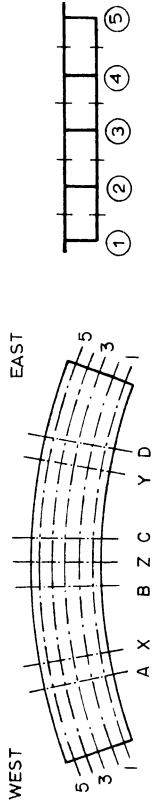
\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

TABLE 37J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE)

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 50 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS APPLIED AT

SECTION	GIRDER	(1-X)+(5-Y)		THEORY		EXPERIMENTAL		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	92.4	22.0	142.9	30.2						
A	2	108.5	25.9	116.9	24.7						
A	3	88.9	21.2	92.5	19.5						
A	4	76.8	18.3	77.1	16.3						
A	5	52.6	12.5	44.1	9.3						
A	SUM	419.3		473.5							
B	1	-80.8	16.6	-94.3	19.1						
B	2	-106.4	21.9	-114.1	23.1						
B	3	-105.0	21.6	-113.4	22.9						
B	4	-111.4	22.9	-107.2	21.7						
B	5	-83.2	17.1	-65.8	13.3						
B	SUM	-486.9		-494.8							
C	1	-76.1	15.6	-58.9	12.1						
C	2	-104.4	21.3	-96.7	19.8						
C	3	-109.0	22.3	-114.2	23.4						
C	4	-113.5	23.2	-121.2	24.8						
C	5	-86.5	17.7	-97.4	19.9						
C	SUM	-489.5		-488.4							
D	1	59.9	12.3	36.7	7.1						
D	2	87.1	17.9	74.6	14.5						
D	3	103.4	21.3	102.0	19.8						
D	4	131.1	27.0	168.9	32.8						
D	5	104.7	21.5	132.5	25.7						
D	SUM	486.2		514.8							
LOAD	PX (KIPS)	-100.0		-100.0							
LOAD	PY (KIPS)	-100.0		-98.4							
ACTUAL	PX (KIPS)			-19.4							
ACTUAL	PY (KIPS)			-19.1							



**TABLE 38 A**  
 SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 60 KSI COND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	(1-X)		(1-Y)		(1-X)+(1-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	8.07	7.11	41.39	16.87	49.45	23.66
2E	.05	.28	9.57	36.22	9.62	33.48
3E	-1.31	-2.27	-4.2	6.36	-1.73	4.42
4E	-2.91	-6.95	-1.17	-11.08	-4.08	-12.57
5E	-9.62	-5.71	-8.32	-8.72	-17.94	-15.08
1F	-16.14	3.06	20.53	1.42	4.39	5.72
2F	11.60	31.54	48.71	40.04	60.32	67.15
3F	48.40	32.61	11.88	32.19	60.23	60.24
4F	20.66	1.04	-16.30	-5.86	4.35	-2.92
1W	37.19	37.26	8.03	5.87	45.23	40.51
2W	11.88	9.63	.12	2.71	11.99	13.55
3W	3.59	.21	-1.36	-2.68	2.23	4.56
4W	.87	11.96	-3.03	-1.60	-2.16	2.65
5W	-12.33	-17.10	-9.62	-11.76	-21.95	-24.30
RE	-5.72	-7.54	41.05	39.65	35.32	34.11
RF	64.53	68.25	64.82	67.79	129.34	130.29
RW	41.20	41.96	-5.86	-7.46	35.34	36.57
SUMR	100.01	102.67	100.01	99.98	200.00	201.37
PX	-100.00	-100.00	0.	.06	-100.00	-100.00
PY	-0.	.11	-100.00	-100.00	-100.00	-98.12
SUMP	-100.00	-99.89	-100.00	-99.94	-200.00	-198.12
SUMR/SUMP	1.00	1.03	1.00	1.00	1.00	1.02
TW	-283.15	-273.73	-98.93	-101.81	-382.10	-361.54
MF	110.40	-1.43	-110.50	-22.69	.11	-23.17
TF	-83.22	-90.07	-84.56	-115.00	-167.78	-187.03
TE	-98.64	-84.57	-283.43	-253.38	-382.02	-318.86
ACTUAL PX		-19.28		.01		-17.58
ACTUAL PY		.02		-19.15		-19.21

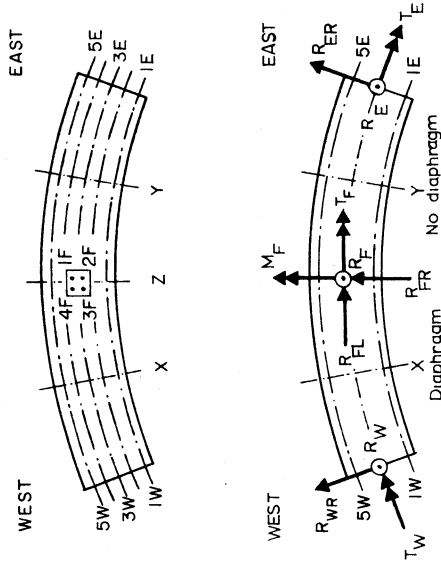
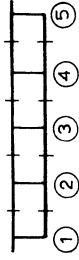
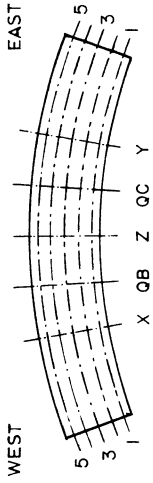


TABLE 38B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI CCND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



DEFLECTION AT POINT	(1-X)		(1-Y)		(1-X)+(1-Y)	
	THEORY	EXPERM E/T	THEORY	EXPERM E/T	THEORY	EXPERM E/T
1X	.942	1.760 1.87	-.153	-.170 1.11	.789	1.586 2.01
2X	.806	1.434 1.78	-.198	-.245 1.24	.608	1.176 1.93
3X	.692	1.161 1.68	-.243	-.318 1.31	.450	.785 1.75
4X	.605	.892 1.48	-.289	-.391 1.35	.316	.445 1.41
5X	.535	.668 1.25	-.337	-.468 1.39	.198	.128 .65
1QB	.625	1.096 1.75	-.090	-.089 1.00	.536	1.020 1.90
2QB	.512	.869 1.70	-.151	-.197 1.30	.361	.664 1.84
3QB	.407	.651 1.60	-.206	-.277 1.35	.201	.338 1.68
4QB	.329	.478 1.45	-.266	-.380 1.43	.063	.042 .67
5QB	.261	.273 1.05	-.328	-.505 1.54	-.067	-.257 3.85
1Z	.160	.277 1.74	.165	.322 1.96	.324	.620 1.91
2Z	.078	.134 1.72	.080	.147 1.85	.158	.284 1.80
4Z	-.063	-.108 1.72	-.063	-.116 1.85	-.126	-.246 1.95
5Z	-.129	-.219 1.70	-.128	-.230 1.79	-.257	-.451 1.75
1QC	-.087	-.084 .97	.682	1.310 1.92	.595	1.233 2.07
2QC	-.148	-.184 1.24	.529	.939 1.77	.381	.752 1.98
3QC	-.203	-.262 1.29	.398	.552 1.39	.195	.289 1.48
4QC	-.263	-.353 1.34	.314	.375 1.19	.050	-.010 -.20
5QC	-.325	-.452 1.39	.255	.200 .78	-.070	-.261 3.75
1Y	-.153	-.168 1.10	1.101	2.452 2.23	.948	2.272 2.40
2Y	-.197	-.228 1.16	.825	1.493 1.81	.629	1.243 1.98
3Y	-.239	-.290 1.22	.658	.952 1.45	.419	.636 1.52
4Y	-.283	-.356 1.26	.559	.690 1.23	.276	.309 1.12
5Y	-.329	-.464 1.41	.504	.548 1.09	.175	.059 .34
LOAD PX	-100.0	-100.0	0.	.1	-100.0	-100.0
LOAD PY	-0.	.1	-100.0	-100.0	-100.0	-98.1
ACTUAL PX		-19.3		.0		-19.6
ACTUAL PY		.0		-19.1		-19.2

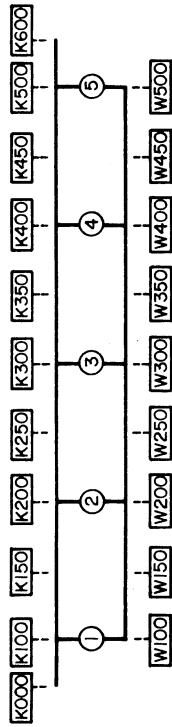
TABLE 38C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 60 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	-431	-587	56	70	-374	-474
K	K100	-341	-1133	48	142	-292	-1040
K	K150	-438	-373	60	41	-348	-292
K	K200	-271	-581	42	80	-229	-507
K	K250	-291	-281	52	59	-204	-183
K	K300	-245	-479	44	61	-201	-398
K	K350	-361	-345	39	36	-306	-277
K	K400	-211	-447	44	60	-167	-356
K	K450	-280	-350	35	35	-226	-242
K	K500	-227	-312	51	43	-176	-256
K	K600	-261	-263	58	26	-203	-196
W	W100	1365	1320	-178	-51	1187	1233
W	W150	1059	1197	-164	-56	895	1127
W	W200	1043	1000	-21	-88	966	890
W	W250	970	904	-181	-20	789	842
W	W300	792	911	-171	-140	625	739
W	W350	796	728	-187	-95	683	618
W	W400	816	701	-187	-157	537	527
W	W450		992	-187	-20	905	391
W	W500		715	-187	-216	498	503
LOAD	PX (KIPS)	-100.0	-100.0	0.	.1	-100.0	-100.0
LOAD	PY (KIPS)	-0.	.1	-100.0	-100.0	-100.0	-98.1
ACTUAL	PX (KIPS)		-19.3		.0		-19.6
ACTUAL	PY (KIPS)		.0		-19.1		-19.2

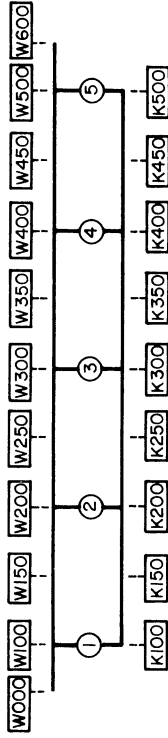
TABLE 38D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 60 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	184	546	473	337	658	937
W	W100	189	430	427	350	615	827
W	W150	185	440	291	376	476	750
W	W200	256	423	149	417	405	809
W	W250	147	431	222	254	370	570
W	W300	130	394	298	167	428	545
W	W350	114	311	315	175	430	486
W	W400	-91	143	197	148	-289	294
W	W450	-82	95	-141	142	-224	256
W	W500	-100	88	-197	166	-489	228
W	W600	-82	26	-141	156	-224	198
K	K100	-91	-320	-197	-252	-289	-474
K	K150	-535	-506	-223	-209	-695	-666
K	K200	-218	-218	-219	-209	-358	-363
K	K250	-182	-205	-237	-97	-305	-323
K	K300	-100	-304	-66	-103	-165	-338
K	K350	-264	-267	-118	-118	-319	-321
K	K400	-66	-210	-105	-143	-172	-288
K	K450	-164	-183	-163	-160	-271	-285
K	K500	-58	-154	-129	-164	-187	-279

LOAD PX (KIPS) -100.0 -100.0  
 LOAD PY (KIPS) -0.1

ACTUAL PX (KIPS) -19.3  
 ACTUAL PY (KIPS) .0

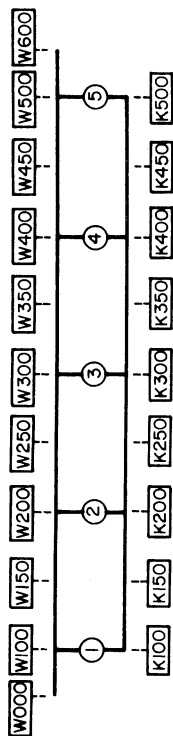
LOAD PX (KIPS) -100.0 -100.0  
 LOAD PY (KIPS) -100.0 -98.1

ACTUAL PX (KIPS) -19.6  
 ACTUAL PY (KIPS) -19.2

TABLE 38E

SUMMARY OF STRAINS (MICRC IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



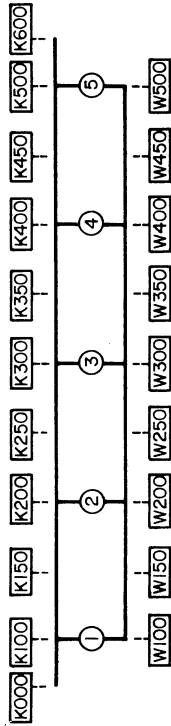
SECTION C

TENSION = + K = CONCRETE STRAIN METERS

COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	425	332	302	826	728	1166
W	W100	387	292	279	656	666	1002
W	W150	244	243	203	474	484	796
W	W200	280	351	203	529	484	893
W	W250	149	156	241	313	396	468
W	W300	154	121	241	303	396	491
W	W350	231	94	121	211	353	312
W	W400	165	172	121	141	353	341
W	W450	130	135	95	81	400	214
W	W500	304	154	95	32	400	181
W	W600	326	158	62	-25	388	116
K	K100	-178	-288	-137	-461	-315	-630
K	K150	-226	-208	-95	-421	-229	-536
K	K200	-134	-218	-95	-200	-229	-331
K	K250	-196	-201	-95	-230	-163	-334
K	K300	-67	-155	-95	-198	-163	-283
K	K350	-110	-192	-52	-94	-163	-234
K	K400	-110	-205	-52	-85	-163	-232
K	K450	-241	-239	-37	-131	-171	-316
K	K500	-133	-237	-37	-137	-171	-320
LOAD	PX (KIPS)	-100.0	-100.0	0.	.1	-100.0	-100.0
LOAD	PY (KIPS)	-0.	.1	-100.0	-100.0	-100.0	-98.1
ACTUAL	PX (KIPS)	-19.3	.0	.0	.0	-19.6	-19.6
ACTUAL	PY (KIPS)	.0	-19.1	-19.1	-19.2	-19.2	-19.2

**TABLE 38F**  
 SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

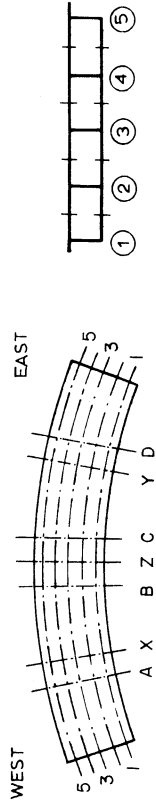


SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(1-X)		(1-Y)		(1-X)+(1-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	51	-5	-407	-338	-355	-288
K	K100	43	38	-331	-456	-287	-390
K	K150		150		-607		-523
K	K200	37	70	-252	-513	-215	-444
K	K250		48		-413		-335
K	K300	38	46	-206	-361	-168	-309
K	K350		101		-443		-390
K	K400	37	62	-170	-291	-133	-257
K	K450		76		-385		-357
K	K500	42	29	-179	-257	-137	-228
K	K600	48	-34	-201	-91	-153	-81
W	W100			1480	1113	1297	1006
W	W150				1520		1451
W	W200			1147	1259	983	1066
W	W250				533		813
W	W300			930	734	753	564
W	W350				617		511
W	W400			715	622	552	405
W	W450				502		369
W	W500			696	634	519	489
LOAD	PX (KIPS)	-100.0	-100.0	0.	.1	-100.0	-100.0
LOAD	PY (KIPS)	-0.	.1	-100.0	-100.0	-100.0	-98.1
ACTUAL	PX (KIPS)		-19.3		.0		-19.6
ACTUAL	PY (KIPS)		.0		-19.1		-19.2

**TABLE 38G**  
 DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )  
 MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



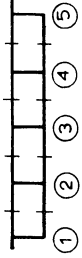
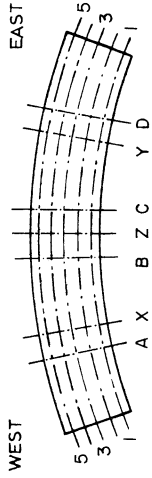
SECTION	GIRDER	(1-X)			(1-Y)			(1-X) + (1-Y)					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	116.1	20.8	97.8	18.9	-16.1	16.2	-6	1.3	100.0	21.8	93.2	20.8
A	2	139.9	25.1	149.4	29.0	-21.8	22.0	-8.1	14.0	118.0	25.8	139.1	31.1
A	3	119.5	21.4	123.4	23.9	-22.1	22.2	-14.6	25.2	97.4	21.3	105.0	23.5
A	4	107.1	19.2	93.1	18.0	-22.7	22.8	-19.6	33.7	84.4	18.4	73.3	16.4
A	5	74.6	13.4	52.3	10.1	-16.8	16.9	-15.0	25.8	57.8	12.6	36.9	8.3
A	SUM	557.1		516.1		-99.4		-58.1		457.7		447.4	
B	1	-27.6	15.6	-55.8	25.1	-56.6	22.9	-42.8	25.4	-80.1	20.0	-104.5	26.5
B	2	-42.4	24.0	-67.4	30.3	-63.5	25.8	-55.2	32.7	-100.5	25.0	-120.1	30.5
B	3	-53.3	30.2	-61.8	27.8	-39.7	16.1	-30.6	18.1	-87.6	21.8	-90.8	23.0
B	4	-34.5	19.6	-28.0	12.6	-48.1	19.5	-22.6	13.4	-78.4	19.5	-51.7	13.1
B	5	-18.8	10.6	-9.2	4.1	-38.6	15.7	-17.6	10.4	-54.7	13.6	-27.1	6.9
B	SUM	-176.6		-222.2		-246.6		-168.7		-401.3		-354.2	
C	1	-47.2	21.3	-35.1	26.1	-39.5	21.9	-87.0	34.9	-86.7	21.5	-128.4	31.3
C	2	-55.4	25.0	-44.0	32.7	-48.2	26.7	-83.8	33.6	-103.4	25.7	-131.1	31.9
C	3	-36.9	16.7	-18.3	13.6	-50.8	28.2	-52.0	20.8	-86.4	21.5	-78.2	19.1
C	4	-45.8	20.6	-21.0	15.6	-28.7	15.9	-24.6	9.9	-75.0	18.6	-53.5	13.0
C	5	-36.4	16.4	-16.2	12.1	-13.2	7.3	-2.0	.8	-50.8	12.6	-19.2	4.7
C	SUM	-221.7		-134.5		-180.5		-249.3		-402.4		-410.5	
D	1	-16.4	16.8	-8.2	12.9	126.4	22.8	109.2	21.4	110.0	24.1	105.7	24.2
D	2	-21.8	22.4	-13.6	21.2	148.9	26.9	176.5	34.6	127.0	27.8	160.9	36.8
D	3	-21.6	22.2	-19.6	30.8	115.7	20.9	98.3	19.3	94.1	20.6	80.2	18.3
D	4	-21.6	22.2	-19.6	30.8	97.4	17.6	80.6	15.8	75.8	16.6	56.9	13.0
D	5	-15.9	16.3	-8.8	13.9	65.6	11.8	45.0	8.8	49.7	10.9	33.8	7.7
D	SUM	-97.3		-63.8		553.9		509.6		456.6		437.5	
LOAD	PX (KIPS)	-100.0		-100.0		0.		.1		-100.0		-100.0	
LOAD	PY (KIPS)	-0.		.1		-100.0		-100.0		-100.0		-98.1	
ACTUAL	PX (KIPS)			-19.3		.0		.0				-19.6	
ACTUAL	PY (KIPS)			.0				-19.1				-19.2	

TABLE 38H

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
APPLIED AFTER 60 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

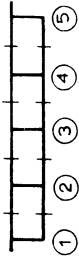
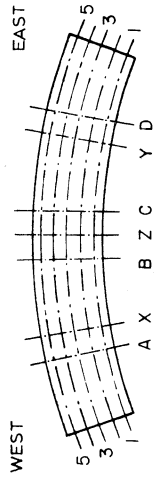


SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)		
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT
A	1	116.1	242.4	33.0	-16.1	-37.4	37.4	100.0	247.9	39.0
A	2	139.9	145.4	19.8	-21.8	-21.5	21.5	118.0	117.1	18.4
A	3	119.5	122.8	16.7	-22.1	-17.1	17.0	97.4	96.9	15.2
A	4	107.1	132.6	18.1	-22.7	-14.4	14.3	84.4	102.0	16.0
A	5	74.6	90.8	12.4	-16.8	-9.8	9.8	57.8	71.9	11.3
A	SUM	557.1	734.0		-99.4	-100.2		457.7	635.8	
B	1	-27.6	-74.8	21.8	-56.6	-40.6	20.8	-80.1	-99.2	21.3
B	2	-42.4	-84.4	24.6	-63.5	-50.6	25.9	-100.5	-124.4	26.7
B	3	-53.3	-84.7	24.6	-39.7	-30.9	15.8	-87.6	-101.0	21.7
B	4	-34.5	-67.3	19.6	-48.1	-43.0	22.1	-78.4	-89.7	19.2
B	5	-18.8	-32.5	9.4	-38.6	-30.0	15.4	-54.7	-52.0	11.2
B	SUM	-176.6	-343.7		-246.6	-195.1		-401.3	-466.2	
C	1	-47.2	-46.4	16.5	-39.5	-75.4	29.2	-86.7	-97.9	22.9
C	2	-55.4	-52.3	22.2	-48.2	-71.7	27.8	-103.4	-103.9	24.4
C	3	-36.9	-58.1	20.7	-50.8	-53.0	20.5	-86.4	-85.7	20.1
C	4	-45.8	-67.5	24.0	-28.7	-29.5	11.4	-75.0	-75.5	17.7
C	5	-36.4	-46.9	16.7	-13.2	-28.5	11.0	-50.8	-63.6	14.9
C	SUM	-221.7	-281.1		-180.5	-258.2		-402.4	-426.6	
D	1	-16.4	-19.8	20.2	126.4	121.9	21.5	110.0	102.4	21.3
D	2	-21.8	-25.3	25.8	148.9	148.6	26.2	127.0	116.4	24.2
D	3	-21.6	-18.0	18.4	115.7	120.7	21.3	94.1	99.2	20.6
D	4	-21.6	-23.2	23.6	97.4	99.6	17.6	75.8	92.9	19.3
D	5	-15.9	-11.9	12.1	65.6	75.9	13.4	49.7	69.7	14.5
D	SUM	-97.3	-98.2		553.9	566.6		456.6	480.5	
LOAD	PX (KIPS)	-100.0	-100.0		0.	.1		-100.0	-100.0	
LOAD	PY (KIPS)	-0.	.1		-100.0	-100.0		-100.0	-98.1	
ACTUAL	PX (KIPS)		-19.3			.0			-19.6	
ACTUAL	PY (KIPS)		.0			-19.1			-19.2	



TABLE 381

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT ENTIRE GROSS SECTION N.A.  
RESULTS FOR POINT LOADS  
APPLIED AFTER 60 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



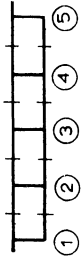
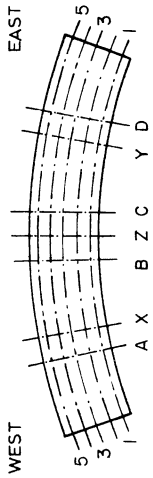
SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	116.1	20.8	162.3	26.5	-16.1	16.2	-17.1	22.3	100.0	21.8	162.3	50.5
A	2	139.9	25.1	147.7	24.1	-21.8	22.0	-14.1	18.4	118.0	25.8	129.3	24.3
A	3	119.5	21.4	123.2	20.1	-22.1	22.2	-15.7	20.4	97.4	21.3	101.4	19.1
A	4	107.1	19.2	110.8	18.1	-22.7	22.8	-17.2	22.4	84.4	18.4	86.1	16.2
A	5	74.6	13.4	69.5	11.3	-16.8	16.9	-12.7	16.5	57.8	12.6	52.5	9.9
A	SUM	557.1		613.5		-99.4		-76.9		457.7		531.7	
B	1	-27.6	15.6	-66.4	22.9	-56.6	22.9	-41.6	22.7	-80.1	20.0	-101.6	23.4
B	2	-42.4	24.0	-76.9	26.5	-63.5	25.8	-52.7	28.7	-100.5	25.0	-122.5	28.2
B	3	-53.3	30.2	-74.5	25.7	-39.7	16.1	-30.7	16.8	-87.6	21.8	-96.5	22.2
B	4	-34.5	19.6	-49.8	17.2	-48.1	19.5	-33.9	18.5	-78.4	19.5	-72.7	16.8
B	5	-18.8	10.6	-22.1	7.6	-38.6	15.7	-24.5	13.4	-54.7	13.6	-40.9	9.4
B	SUM	-176.6		-239.6		-246.6		-183.4		-401.3		-434.2	
C	1	-47.2	21.3	-41.3	19.2	-39.5	21.9	-80.6	31.7	-86.7	21.5	-111.5	26.6
C	2	-55.4	25.0	-54.1	25.1	-48.2	26.7	-77.1	30.3	-103.4	25.7	-116.1	27.7
C	3	-36.9	16.7	-40.4	18.7	-50.8	28.2	-52.6	20.7	-86.4	21.5	-82.4	19.6
C	4	-45.8	20.6	-46.7	21.7	-28.7	15.9	-27.3	10.8	-75.0	18.6	-65.7	15.7
C	5	-36.4	16.4	-33.2	15.4	-13.2	7.3	-16.7	6.6	-50.8	12.6	-43.8	10.4
C	SUM	-221.7		-215.8		-180.5		-254.3		-402.4		-419.5	
D	1	-16.4	16.8	-13.4	16.9	126.4	22.8	114.9	21.5	110.0	24.1	104.3	22.8
D	2	-21.8	22.4	-18.8	23.8	148.9	26.9	164.1	30.7	127.0	27.8	141.1	30.9
D	3	-21.6	22.2	-15.6	19.6	115.7	20.9	108.3	20.2	94.1	20.6	88.7	19.4
D	4	-21.6	22.2	-21.2	26.8	97.4	17.6	89.1	16.6	75.8	16.6	73.0	16.0
D	5	-15.9	16.3	-10.2	12.9	65.6	11.8	58.8	11.0	49.7	10.9	49.8	10.9
D	SUM	-97.3		-79.2		553.9		535.2		456.6		456.8	
LOAD	PX (KIPS)	-100.0		-100.0		0.		0.		-100.0		-100.0	
LOAD	PY (KIPS)	-0.		-0.		-100.0		-100.0		-100.0		-100.0	
ACTUAL	PX (KIPS)			-19.3		-19.3		-19.3		-19.3		-19.3	
ACTUAL	PY (KIPS)			0.		0.		0.		0.		0.	

TABLE 38J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 60 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	(1-X)			(1-Y)			(1-X)+(1-Y)		
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT
A	1	116.1	20.8	162.8	-16.1	16.2	-27.6	100.0	21.8	162.3
A	2	139.9	25.1	147.9	-21.8	22.0	-14.6	118.0	25.8	130.7
A	3	119.5	21.4	123.2	-22.1	22.2	-15.4	97.4	21.3	102.2
A	4	107.1	19.2	108.7	-22.7	22.8	-18.1	84.4	18.4	84.9
A	5	74.6	13.4	63.9	-16.8	16.9	-14.1	57.8	12.6	48.9
A	SUM	557.1		606.5	-99.4		-89.8	457.7		528.9
B	1	-27.6	15.6	-63.9	-56.6	22.9	-41.9	-80.1	20.0	-102.6
B	2	-42.4	24.0	-73.1	-63.5	25.8	-53.7	-100.5	25.0	-121.4
B	3	-53.3	30.2	-71.7	-39.7	16.1	-30.7	-87.6	21.8	-94.7
B	4	-34.5	19.6	-50.9	-48.1	19.5	-32.7	-78.4	19.5	-70.4
B	5	-18.8	10.6	-24.1	-38.6	15.7	-23.8	-54.7	13.6	-40.6
B	SUM	-176.6		-283.8	-246.6		-182.6	-401.3		-429.7
C	1	-47.2	21.3	-40.7	-39.5	21.9	-82.4	-86.7	21.5	-116.8
C	2	-55.4	25.0	-51.0	-48.2	26.7	-80.4	-103.4	25.7	-123.7
C	3	-36.9	16.7	-40.2	-50.8	28.2	-52.4	-86.4	21.5	-80.9
C	4	-45.8	20.6	-46.4	-28.7	15.9	-26.5	-75.0	18.6	-62.2
C	5	-36.4	16.4	-34.8	-13.2	7.3	-23.8	-50.8	12.6	-47.9
C	SUM	-221.7		-213.1	-180.5		-265.5	-402.4		-431.6
D	1	-16.4	16.8	-11.6	126.4	22.8	112.9	110.0	24.1	104.8
D	2	-21.8	22.4	-18.3	148.9	26.9	168.2	127.0	27.8	148.0
D	3	-21.6	22.2	-15.0	115.7	20.9	105.8	94.1	20.6	87.2
D	4	-21.6	22.2	-20.6	97.4	17.6	86.4	75.8	16.6	70.4
D	5	-15.9	16.3	-9.5	65.6	11.8	53.9	49.7	10.9	45.0
D	SUM	-97.3		-75.1	553.9		527.2	456.6		455.4
LOAD	PX (KIPS)	-100.0		-100.0	0.		.1	-100.0		-100.0
LOAD	PY (KIPS)	-0.		.1	-100.0		-100.0	-100.0		-98.1
ACTUAL	PX (KIPS)			-19.3			.0			-19.6
ACTUAL	PY (KIPS)			.0			-19.1			-19.2

TABLE 39A

SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 60 KSI COND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

REACTION OR LOAD	(3-X)		(3-Y)		(3-X)+(3-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	-0.07	5.63	-2.53	-9.14	-2.60	-3.71
2E	-1.42	-6.64	8.65	23.15	7.23	14.46
3E	-1.32	-2.99	15.17	9.33	13.86	6.95
4E	-1.78	-3.30	9.25	.24	7.47	6.72
5E	-3.27	-.25	8.15	12.28	4.88	7.62
1F	-3.10	4.88	37.97	46.78	34.87	37.58
2F	-3.02	-.21	38.15	47.78	35.13	30.22
3F	37.65	32.18	3.40	-11.86	34.26	35.33
4F	37.57	33.59	-3.58	-10.42	34.00	39.98
1W	.98	12.89	-.08	-.45	.90	11.35
2W	8.09	-2.67	-1.37	.83	6.72	-2.06
3W	9.08	-3.91	-1.35	-2.99	7.73	.54
4W	9.17	25.30	-1.83	-1.32	7.34	12.83
5W	11.45	10.71	-3.22	-4.02	8.23	9.94
RE	-7.86	-7.55	38.69	35.86	30.84	32.04
RF	69.10	70.44	69.16	72.28	138.25	143.11
RW	38.77	42.32	-7.85	-7.95	30.92	32.60
SUMR	100.01	105.21	100.00	100.19	200.02	207.75
PX	-100.00	-100.00	-.0	.05	-100.00	-100.00
PY	-.0	-.04	-100.00	-100.00	-100.00	-104.43
SUMP	-100.00	-100.04	-100.00	-99.95	-200.00	-204.43
SUMR/SUMP	1.00	1.05	1.00	1.00	1.00	1.02
TW	56.66	60.75	-17.34	-23.90	39.31	31.05
MF	122.04	91.65	-124.65	-175.26	-2.60	11.27
TF	-.24	9.75	-.54	.66	-.78	18.02
TE	-17.39	-21.66	56.50	51.28	39.11	38.39
ACTUAL PX		-19.08		.01		-18.93
ACTUAL PY		-.01		-19.41		-19.77

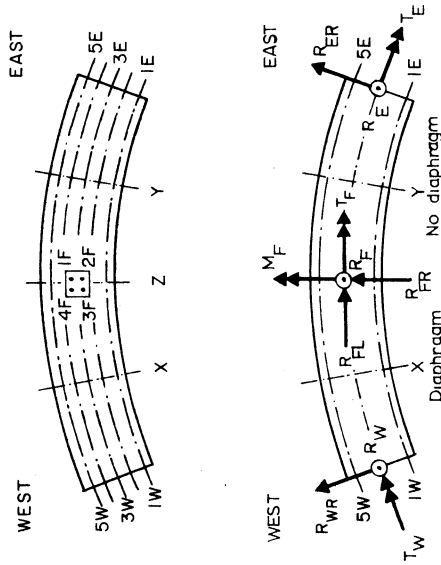
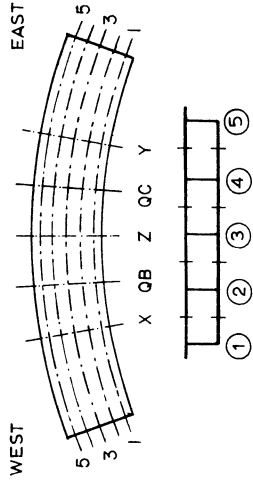


TABLE 39B

SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

RESULTS FOR POINT LOADS  
APPLIED AFTER 60 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



DEFLECTION AT POINT	{3-X}		{3-Y}		NORMALIZED POINT LOADS AT		{3-X} + {3-Y}			
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM		
1X	.692	1.192	1.72	1.72	-239	-473	1.98	.453	-819	1.81
2X	.740	1.315	1.78	1.78	-249	-517	2.08	.491	.904	1.84
3X	.793	1.471	1.86	1.86	-260	-540	2.08	.532	1.019	1.91
4X	.809	1.480	1.83	1.83	-273	-563	2.06	.536	.995	1.86
5X	.831	1.513	1.82	1.82	-288	-591	2.06	.544	.996	1.83
1QB	.421	.694	1.65	1.65	-207	-421	2.03	.214	.363	1.70
2QB	.441	.752	1.70	1.70	-215	-429	1.99	.225	.389	1.73
3QB	.460	.786	1.71	1.71	-222	-437	1.97	.238	.425	1.78
4QB	.481	.839	1.75	1.75	-235	-460	1.96	.246	.449	1.83
5QB	.500	.858	1.71	1.71	-245	-506	2.06	.255	.421	1.65
1Z	.013	.018	1.38	1.38	.011	.008	.70	.024	.051	2.11
2Z	.007	.005	.56	.56	.007	.003	.48	.014	.006	.42
4Z	.007	-.001	-.07	-.07	.006	.001	.18	.012	0.	0.
5Z	.012	.017	1.37	1.37	.009	.021	2.23	.022	.044	2.06
1QC	-.208	-.350	1.68	1.68	.408	.713	1.75	.200	.321	1.61
2QC	-.216	-.363	1.68	1.68	.442	.826	1.87	.226	.415	1.84
3QC	-.221	-.403	1.82	1.82	.489	.922	1.89	.267	.475	1.78
4QC	-.234	-.426	1.82	1.82	.476	.904	1.90	.243	.442	1.82
5QC	-.244	-.442	1.81	1.81	.479	.875	1.83	.235	.385	1.63
1Y	-.243	-.412	1.70	1.70	.658	1.152	1.75	.415	.694	1.67
2Y	-.251	-.440	1.75	1.75	.735	1.376	1.87	.484	.864	1.79
3Y	-.260	-.481	1.85	1.85	.894	1.901	2.13	.634	1.340	2.11
4Y	-.272	-.507	1.87	1.87	.793	1.504	1.90	.521	.950	1.82
5Y	-.284	-.541	1.91	1.91	.773	1.414	1.83	.489	.845	1.73
LOAD	-100.0	-100.0			-0.	.1		-100.0	-100.0	-100.0
LOAD	-0.	-0.			-100.0	-100.0		-100.0	-104.4	-104.4
ACTUAL									-18.9	-18.9
ACTUAL									-19.8	-19.8

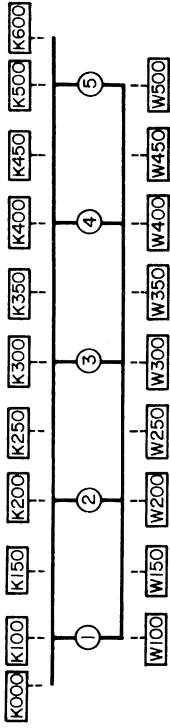
TABLE 39C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)				
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST			
K	K000	-314	-371	-811	68	117	251	-245	-309	-683
K	K100	-277	-811	-806	59	251	243	-218	-683	-678
K	K150	-251	-390	-452	50	86	54	-201	-306	-367
K	K200	-268	-508	-305	52	151	153	-216	-430	-446
K	K250	-249	-292	-477	50	63	67	-199	-229	-241
K	K300	-266	-474	-381	58	126	126	-208	-398	-400
K	K350	-289	-387	-512	65	94	93	-223	-319	-313
K	K400	1044	-499	-428	-217	133	133	-199	-417	-431
K	K450	969	-340	-416	-196	82	93	-208	-274	-354
K	K500	1048	-416	-284	-211	126	129	-208	-346	-344
K	K600	958	-284	1107	-210	87	87	-223	-240	-240
W	W100	993	993	992	-217	-238	-238	826	825	825
W	W150	833	833	777	-196	-192	-179	772	699	650
W	W200	946	946	943	-196	-234	-255	761	761	758
W	W250	881	881	857	-211	-198	-190	835	722	695
W	W300	1177	1177	1172	-211	-278	-277	826	941	937
W	W350	955	955	976	-196	-221	-221	762	782	788
W	W400	1124	1124	1107	-210	-278	-275	771	882	863
W	W450	975	975	913	-210	-211	-209	789	789	725
W	W500	982	1106	1117	-210	-301	-304	835	835	844
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-0.	.1	.1	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	-0.	-0.	-0.	-100.0	-100.0	-100.0	-100.0	-104.4	-104.4
ACTUAL	PX (KIPS)	-19.1	-19.1	-19.1	.0	.0	.0	-18.9	-18.9	-18.9
ACTUAL	PY (KIPS)	-0.	-0.	-0.	-19.4	-19.4	-19.4	-19.8	-19.8	-19.8

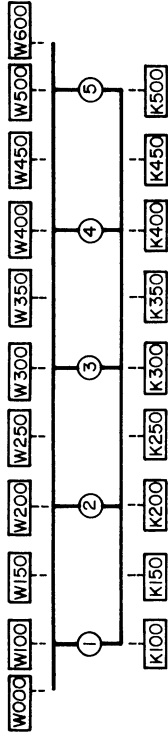
TABLE 39D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 60 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

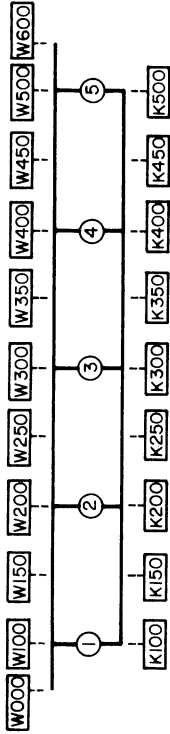


GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	194	295	448	315	642	646
W	W100	196	249	399	279	596	576
W	W150		267		323		582
W	W200	222	434	314	349	536	775
W	W250		405		258		746
W	W300	335	496	214	229	549	776
W	W350		411		285		803
W	W400	226	323	308	275	534	628
W	W450		316		288		697
W	W500	201	323	381	309	582	628
W	W600	186	344	408	309	594	643
K	K100	-90	-171	-180	-232	-271	-394
K	K150		-170		-380		-533
K	K200	-99	-233	-149	-217	-248	-433
K	K250		-266		-238		-459
K	K300	-133	-282	-92	-231	-225	-482
K	K350		-247		-234		-477
K	K400	-102	-202	-145	-228	-248	-453
K	K450		-206		-217		-408
K	K500	-92	-184	-168	-201	-260	-417
LOAD	PX (KIPS)	-100.0	-100.0	-0.	.1	-100.0	-100.0
LOAD	PY (KIPS)	-0.	-0.	-100.0	-100.0	-100.0	-104.4
ACTUAL	PX (KIPS)		-19.1		.0		-18.9
ACTUAL	PY (KIPS)		-0.		-19.4		-19.8

TABLE 39E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 60 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

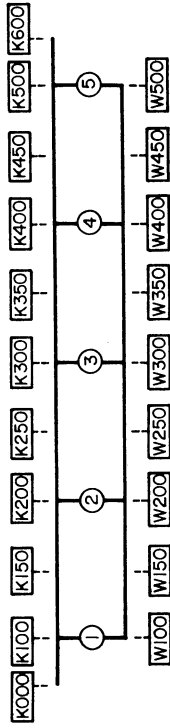
GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
W	W000	451	365	365	185	302	636
W	W100	403	298	301	187	251	591
W	W150		256	274		250	
W	W200	309	344	343	232	417	541
W	W250		193	203		434	
W	W300	204	184	193	368	521	572
W	W350		192	222		363	
W	W400	309	331	339	226	392	535
W	W450		262	276		279	
W	W500	393	298	292	178	287	571
W	W600	421	304	304	159	311	580
K	K100	-182	-228	-222	-87	-133	-269
K	K150		-211	-204		-120	
K	K200	-147	-206	-208	-103	-201	-250
K	K250		-211	-214		-280	
K	K300	-88	-187	-187	-145	-373	-234
K	K350		-198	-205		-274	
K	K400	-146	-203	-205	-100	-176	-247
K	K450		-291	-280		-182	
K	K500	-174	-223	-219	-80	-137	-255
LOAD	PX (KIPS)	-100.0	-100.0		-0.	.1	-100.0
LOAD	PY (KIPS)	-0.	-0.		-100.0	-100.0	-100.0
ACTUAL	PX (KIPS)		-19.1			.0	-18.9
ACTUAL	PY (KIPS)		-0.			-19.4	-19.8

LOAD	TYPE	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
K	K100	-182	-228	-222	-87	-133	-269
K	K150		-211	-204		-120	
K	K200	-147	-206	-208	-103	-201	-250
K	K250		-211	-214		-280	
K	K300	-88	-187	-187	-145	-373	-234
K	K350		-198	-205		-274	
K	K400	-146	-203	-205	-100	-176	-247
K	K450		-291	-280		-182	
K	K500	-174	-223	-219	-80	-137	-255
LOAD	PX (KIPS)	-100.0	-100.0		-0.	.1	-100.0
LOAD	PY (KIPS)	-0.	-0.		-100.0	-100.0	-100.0
ACTUAL	PX (KIPS)		-19.1			.0	-18.9
ACTUAL	PY (KIPS)		-0.			-19.4	-19.8

TABLE 39F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 60 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(3-X)		(3-Y)		(3-X)+(3-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
K	K000	62	52	-278	-177	-215	-142
K	K100	53	74	-241	-284	-187	-224
K	K150		173		-594		-462
K	K200	45	125	-231	-505	-186	-404
K	K250		126		-467		-361
K	K300	46	100	-238	-384	-192	-300
K	K350		174		-689		-553
K	K400	44	155	-225	-500	-181	-383
K	K450		208		-693		-540
K	K500	50	140	-226	-475	-176	-376
K	K600	57	41	-250	-165	-193	-137
W	W100	-224	-147	1042	780	818	571
W	W150		-169		873		645
W	W200	-199	-225	994	1162	794	880
W	W250		-194		1122		872
W	W300	-211	-233	1049	1271	837	950
W	W350		-195		1154		910
W	W400	-192	-278	958	1208	766	930
W	W450		-206		928		707
W	W500	-206	-239	955	1011	749	809
LOAD	PX (KIPS)	-100.0	-100.0	-C.	.1	-100.0	-100.0
LOAD	PY (KIPS)	-0.	-0.	-100.0	-100.0	-100.0	-104.4
ACTUAL	PX (KIPS)		-19.1		.0		-18.9
ACTUAL	PY (KIPS)		-0.		-19.4		-19.8

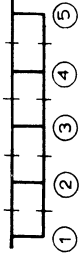
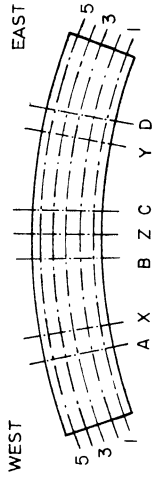


TABLE 39G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE)

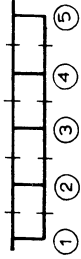
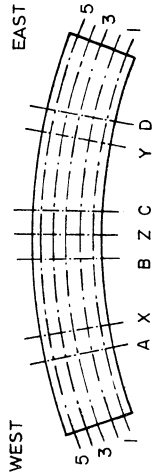
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR POINT LOADS  
APPLIED AFTER 60 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	(3-X)			(3-Y)			(3-X) + (3-Y)					
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT			
A	1	92.9	16.3	67.3	11.5	-19.5	16.7	-14.6	10.7	73.4	16.2	56.0	12.0
A	2	129.6	22.8	127.3	21.8	-26.1	22.4	-29.7	21.8	103.5	22.9	103.2	22.1
A	3	130.4	22.9	150.8	25.9	-25.8	22.2	-34.6	25.3	104.6	23.1	121.1	26.0
A	4	127.8	22.5	150.9	25.9	-26.0	22.3	-35.8	26.2	101.8	22.5	118.8	25.5
A	5	88.4	15.5	87.1	14.9	-19.0	16.3	-21.9	15.0	69.4	15.3	66.7	14.3
A	SUM	569.0		583.4		-116.3		-136.5		452.7		465.8	
B	1	-27.5	12.5	-33.9	12.0	-48.8	18.4	-37.4	17.3	-77.0	15.9	-74.0	14.8
B	2	-48.2	22.0	-63.5	22.5	-61.5	23.2	-51.1	23.6	-109.9	22.7	-112.5	22.5
B	3	-66.7	30.4	-82.1	29.1	-48.3	18.3	-43.1	19.9	-113.8	23.5	-125.2	25.1
B	4	-49.2	22.4	-59.8	21.2	-60.0	22.7	-46.2	21.4	-109.2	22.5	-107.0	21.4
B	5	-27.9	12.7	-42.9	15.2	-46.1	17.4	-38.5	17.8	-74.5	15.4	-80.8	16.2
B	SUM	-219.6		-282.2		-264.8		-216.4		-484.4		-499.4	
C	1	-49.2	18.6	-39.8	19.3	-26.8	12.0	-34.4	12.2	-76.4	15.7	-76.3	14.9
C	2	-60.9	23.0	-47.8	23.1	-50.2	22.4	-64.5	22.9	-110.5	22.8	-117.0	22.8
C	3	-46.9	17.7	-32.7	15.8	-72.3	32.3	-78.6	27.9	-116.8	24.1	-119.6	23.3
C	4	-60.4	22.8	-48.8	23.6	-49.2	22.0	-64.5	22.9	-109.0	22.4	-119.0	23.2
C	5	-47.5	17.9	-37.7	18.2	-25.2	11.3	-39.6	14.1	-73.0	15.0	-80.5	15.7
C	SUM	-265.0		-206.7		-223.7		-281.6		-485.8		-512.4	
D	1	-20.0	17.2	-12.1	10.4	92.3	16.2	64.7	10.7	72.3	16.0	47.1	10.2
D	2	-26.5	22.7	-27.0	23.3	132.1	23.2	147.0	24.3	105.6	23.3	111.0	24.0
D	3	-25.8	22.2	-27.6	23.8	131.1	23.0	161.0	26.7	105.3	23.3	123.4	26.7
D	4	-25.6	22.0	-32.2	27.8	127.5	22.4	154.4	25.6	102.0	22.5	120.0	26.0
D	5	-18.6	16.0	-17.1	14.7	85.8	15.1	76.8	12.7	57.2	14.8	60.1	13.0
D	SUM	-116.4		-115.9		568.7		603.9		452.3		461.6	
LOAD	PX (KIPS)	-100.0		-100.0		-0.		.1		-100.0		-100.0	
LOAD	PY (KIPS)	-0.		-0.		-100.0		-100.0		-100.0		-104.4	
ACTUAL	PX (KIPS)			-19.1				.0				-18.9	
ACTUAL	PY (KIPS)			-0.				-19.4				-19.8	

**TABLE 39H**  
 DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )



MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION	GIRDER	(3-X)			(3-Y)			(3-X) + (3-Y)			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	92.9	221.0	29.5	-19.5	16.7	31.2	73.4	16.2	184.7	29.5
A	2	129.6	142.4	19.0	-26.1	22.4	32.3	103.5	22.9	118.4	18.9
A	3	130.4	126.3	16.8	-25.8	22.2	31.5	104.6	23.1	104.4	16.7
A	4	127.8	147.7	19.7	-26.0	22.3	36.0	101.8	22.5	124.1	19.8
A	5	88.4	112.9	15.0	-19.0	16.3	32.1	69.4	15.3	94.6	15.1
A	SUM	569.0	750.4		-116.3		-191.6	452.7		626.2	
B	1	-27.5	-28.4	10.6	-48.8	18.4	52.8	-77.0	15.9	-81.0	14.7
B	2	-48.2	-61.8	23.1	-61.5	23.2	76.6	-109.9	22.7	-135.8	24.6
B	3	-66.7	-82.7	31.0	-48.3	18.3	74.0	-113.8	23.5	-144.6	26.2
B	4	-49.2	-61.6	23.1	-60.0	22.7	69.0	-109.2	22.5	-123.7	22.4
B	5	-27.9	-32.7	12.2	-46.1	17.4	36.0	-74.5	15.4	-66.3	12.0
B	SUM	-219.6	-267.1		-264.8		-308.3	-484.4		-551.4	
C	1	-49.2	-38.1	13.8	-26.8	12.0	18.7	-76.4	15.7	-59.2	10.5
C	2	-60.9	-61.7	22.3	-50.2	22.4	56.6	-110.5	22.8	-122.0	21.7
C	3	-46.9	-64.4	23.2	-72.3	32.3	109.0	-116.8	24.1	-180.7	32.2
C	4	-60.4	-67.4	24.3	-49.2	22.0	59.0	-109.0	22.4	-128.6	22.9
C	5	-47.5	-45.3	16.4	-25.2	11.3	9.8	-73.0	15.0	-71.4	12.7
C	SUM	-265.0	-277.0		-223.7		-269.7	-485.8		-561.9	
D	1	-20.0	-26.7	13.5	92.3	16.2	92.5	72.3	16.0	73.1	13.8
D	2	-26.5	-41.1	20.7	132.1	23.2	153.7	105.6	23.3	118.3	22.3
D	3	-25.8	-39.0	19.6	131.1	23.0	141.7	105.3	23.3	103.1	19.5
D	4	-25.6	-49.8	25.0	127.5	22.4	161.7	102.0	22.5	124.5	23.5
D	5	-18.6	-42.1	21.2	85.8	15.1	142.0	67.2	14.8	110.5	20.9
D	SUM	-116.4	-198.7		568.7		691.6	452.3		529.4	
LOAD	PX (KIPS)	-100.0	-100.0		-0.		.1	-100.0		-100.0	
LOAD	PY (KIPS)	-0.	-0		-100.0		-100.0	-100.0		-104.4	
ACTUAL	PX (KIPS)		-19.1				.0			-18.9	
ACTUAL	PY (KIPS)		-0				-19.4			-19.8	

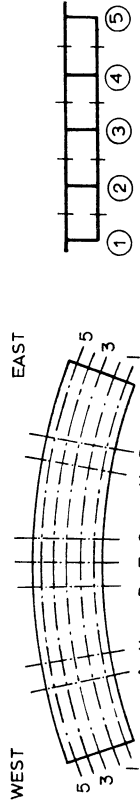


TABLE 39J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 60 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

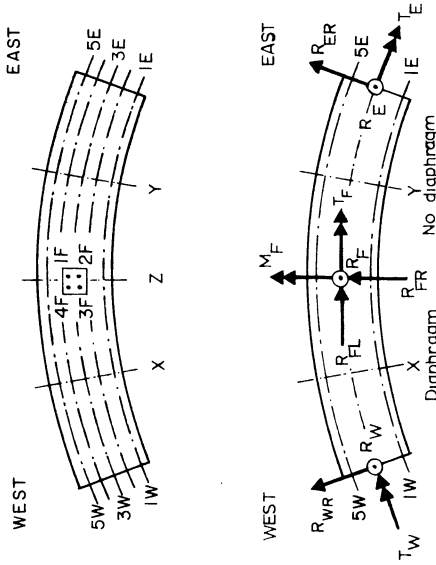


SECTION	GIRDER	(3-X)			(3-Y)			(3-X)+(3-Y)			
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	
A	1	92.9	16.3	136.2	20.7	-19.5	16.7	-37.4	16.2	114.1	21.3
A	2	129.6	22.8	132.7	20.2	-26.1	22.4	-30.8	22.9	108.8	20.4
A	3	130.4	22.9	143.7	21.9	-25.8	22.2	-33.6	20.7	116.1	21.7
A	4	127.8	22.5	149.9	22.8	-26.0	22.3	-35.8	22.1	120.6	22.6
A	5	88.4	15.5	94.1	14.3	-19.0	16.3	-24.9	15.3	74.8	14.0
A	SUM	569.0		656.7		-116.3		-162.5		452.7	534.4
B	1	-27.5	12.5	-31.6	11.4	-48.8	18.4	-44.2	17.2	-77.0	15.9
B	2	-48.2	22.0	-62.9	22.7	-61.5	23.2	-60.8	23.6	-109.9	22.7
B	3	-66.7	30.4	-82.3	29.8	-48.3	18.3	-58.4	22.7	-113.8	23.5
B	4	-49.2	22.4	-60.5	21.9	-60.0	22.7	-56.5	22.0	-109.2	22.5
B	5	-27.9	12.7	-39.2	14.2	-46.1	17.4	-37.6	14.6	-74.5	15.4
B	SUM	-219.6		-276.6		-264.8		-257.4		-484.4	-519.3
C	1	-49.2	18.6	-39.1	16.5	-26.8	12.0	-28.9	10.3	-76.4	15.7
C	2	-60.9	23.0	-53.1	22.4	-50.2	22.4	-62.0	22.1	-110.5	22.8
C	3	-46.9	17.7	-48.3	20.3	-72.3	32.3	-91.3	32.6	-116.8	24.1
C	4	-60.4	22.8	-55.8	23.5	-49.2	22.0	-62.8	22.4	-109.0	22.4
C	5	-47.5	17.9	-41.0	17.3	-25.2	11.3	-35.3	12.6	-73.0	15.0
C	SUM	-265.0		-237.2		-223.7		-280.3		-485.8	-532.8
D	1	-20.0	17.2	-17.1	11.8	92.3	16.2	72.4	11.5	72.3	16.0
D	2	-26.5	22.7	-32.0	22.1	132.1	23.2	149.0	23.6	105.6	23.3
D	3	-25.8	22.2	-31.2	21.5	131.1	23.0	156.2	24.7	105.3	23.3
D	4	-25.6	22.0	-38.3	26.5	127.5	22.4	156.5	24.8	102.0	22.5
D	5	-18.6	16.0	-26.3	18.1	85.8	15.1	97.6	15.4	67.2	14.8
D	SUM	-116.4		-144.9		568.7		631.7		452.3	483.7
LOAD	PX (KIPS)	-100.0		-100.0		-0.		.1		-100.0	
LOAD	PY (KIPS)	-0.		-0.		-100.0		-100.0		-100.0	
ACTUAL	PX (KIPS)	-0.		-19.1		.0		.0		-18.9	
ACTUAL	PY (KIPS)	-0.		-0.		-19.4		-19.4		-19.8	

**TABLE 40A**  
SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 60 KSI COND. LOADING.  
TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

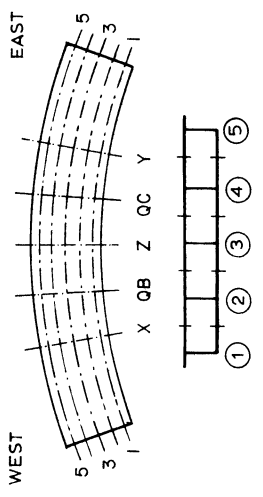
REACTION OR LOAD	(5-X)		(5-Y)		(5-X)+(5-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	-8.14	3.79	-23.25	-13.02	-31.39	-15.19
2E	-2.93	-12.97	-1.70	-15.92	-4.63	-24.17
3E	-1.37	-4.07	2.03	6.13	.67	4.00
4E	-.71	-.15	12.87	20.24	12.16	22.31
5E	2.95	3.27	46.35	37.64	49.30	39.26
1F	10.14	1.85	53.96	57.26	64.09	92.40
2F	-17.30	-30.51	26.17	14.34	8.87	14.85
3F	26.89	39.24	-17.04	-19.69	9.84	-14.60
4F	54.33	66.23	10.75	22.64	55.07	60.38
1W	-26.90	-13.16	-8.12	-6.40	-35.03	-25.38
2W	.30	-16.53	-2.90	-1.85	-2.60	-13.35
3W	5.47	-10.48	-1.39	-3.03	4.08	-2.55
4W	14.38	40.72	-.72	-.16	13.66	27.93
5W	42.90	35.99	3.00	1.29	45.91	41.97
RE	-10.20	-10.13	36.30	35.07	26.11	26.21
RF	74.05	76.81	73.83	74.55	147.88	153.03
RW	36.15	36.54	-10.13	-10.15	26.02	23.62
SUMR	100.00	103.22	100.00	99.47	200.01	207.86
PX	-100.00	-100.00	-.06	.06	-100.00	-100.00
PY	-.06	.06	-100.00	-100.00	-100.00	-103.56
SUMP	-100.00	-99.94	-100.00	-99.94	-200.00	-203.56
SUMR/SUMP	1.00	1.03	1.00	1.00	1.00	1.02
TW	395.40	400.21	62.83	45.15	458.34	452.78
MF	132.56	201.19	-129.62	-102.97	2.94	-92.20
TF	82.32	89.02	83.37	127.87	165.65	228.79
TE	62.78	30.31	395.63	353.72	458.42	399.78
ACTUAL PX		-19.54		.01		-19.27
ACTUAL PY		.01		-19.32		-19.95



**TABLE 40B**  
SUMMARY OF DEFLECTIONS ( INCHES )

DEFLECTIONS POSITIVE DOWNWARDS

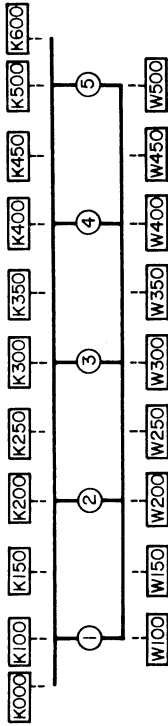
RESULTS FOR POINT LOADS  
APPLIED AFTER 60 KSI COND. LOADING,  
SIMPLY SUPPORTED, NO RESTRAINTS.



DEFLECTION AT POINT	(5-X)		(5-Y)		(5-X)+(5-Y)	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1X	.535	.888	1.666	1.666	1.666	1.666
2X	.673	1.261	1.87	1.87	1.87	1.87
3X	.831	1.666	2.00	2.00	2.00	2.00
4X	1.019	2.080	2.04	2.04	2.04	2.04
5X	1.234	2.534	2.05	2.05	2.05	2.05
1QB	.267	.462	1.73	1.73	1.73	1.73
2QB	.372	.684	1.84	1.84	1.84	1.84
3QB	.489	.929	1.90	1.90	1.90	1.90
4QB	.636	1.237	1.95	1.95	1.95	1.95
5QB	.791	1.511	1.91	1.91	1.91	1.91
1Z	-.127	-.183	1.45	1.45	1.45	1.45
2Z	-.061	-.079	1.29	1.29	1.29	1.29
4Z	.078	.099	1.27	1.27	1.27	1.27
5Z	.158	.249	1.57	1.57	1.57	1.57
1QC	-.331	-.610	1.84	1.84	1.84	1.84
2QC	-.287	-.547	1.90	1.90	1.90	1.90
3QC	-.244	-.514	2.11	2.11	2.11	2.11
4QC	-.209	-.461	2.21	2.21	2.21	2.21
5QC	-.168	-.390	2.32	2.32	2.32	2.32
1Y	-.337	-.641	1.90	1.90	1.90	1.90
2Y	-.311	-.627	2.01	2.01	2.01	2.01
3Y	-.288	-.610	2.12	2.12	2.12	2.12
4Y	-.266	-.575	2.16	2.16	2.16	2.16
5Y	-.246	-.544	2.21	2.21	2.21	2.21
LOAD PX	-100.0	-100.0				
LOAD PY	-0.	.1				
ACTUAL PX	-19.5					
ACTUAL PY	.0					

TABLE 40C

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

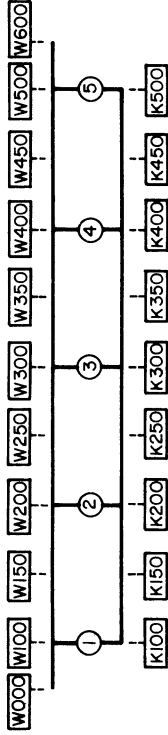


SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		NORMALIZED POINT LOADS AT		(5-X)+(5-Y)		
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	ADJUST
K	K000	-303	-392	83	96	234	234	-219	-262	-262
K	K100	-250	-746	71	234	232	232	-178	-466	-461
K	K150	-376	-450	60	78	105	105	-167	-242	-302
K	K200	-228	-467	61	141	149	149	-200	-299	-313
K	K250	-293	-293	55	55	53	53	-222	-218	-249
K	K300	-262	-470	58	125	122	122	-268	-318	-336
K	K350	-280	-396	67	89	82	82	-337	-271	-291
K	K400	-335	-583	75	133	133	133	-432	-427	-424
K	K450	-412	-514	75	75	84	84	-431	-281	-300
K	K500	-412	-583	75	128	130	130	-290	-432	-431
K	K600	-412	-389	75	87	87	87	-290	-290	-290
W	W100	928	864	-265	-264	-260	-260	663	477	487
W	W150	862	802	-236	-187	-183	-183	626	500	418
W	W200	1033	919	-250	-230	-226	-226	782	575	555
W	W250	1091	640	-228	-249	-209	-209	1071	275	693
W	W300	1315	1151	-243	-289	-285	-285	1292	758	760
W	W350	-100.0	1082	-0.	-211	-206	-206	-100.0	768	883
W	W400	-100.0	1337	-100.0	-245	-241	-241	-100.0	1006	1010
W	W450	-100.0	974	-100.0	-257	-214	-214	-100.0	608	1227
W	W500	-100.0	1645	-100.0	-304	-300	-300	-100.0	1292	1320
LOAD	PX (KIPS)	-100.0	-100.0	-0.	.1	.1	.1	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	-0.	.1	-100.0	-100.0	-100.0	-100.0	-100.0	-103.6	-103.6
ACTUAL	PX (KIPS)	-19.5	.0	.0	.0	.0	.0	-19.3	-19.3	-19.3
ACTUAL	PY (KIPS)	.0	.0	-19.3	-19.3	-19.3	-19.3	-20.0	-20.0	-20.0

**TABLE 40D**  
 SUMMARY OF STRAINS (MICRC IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

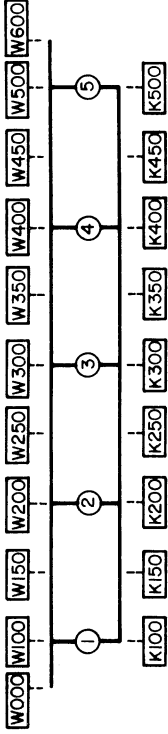
GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		NORMALIZED POINT LOADS AT		(5-X)+(5-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	252	141	499	299	499	299	751	506
W	W100	245	160	443	257	443	259	688	473
W	W150		164		333		339		493
W	W200	249	446	325	299	325	306	574	772
W	W250		464		210		245		719
W	W300	382	593	232	230	232	226	615	892
W	W350		535		375		407		904
W	W400	303	519	389	379	389	387	692	963
W	W450		509		349		416		990
W	W500	318	594	526	433	526	445	845	1072
W	W600	309	668	564	427	564	427	873	1141
K	K100	-110	-190	-195	-285	-195	-273	-306	-493
K	K150		-92		-463		-440		-633
K	K200	-113	-277	-155	-212	-155	-214	-268	-524
K	K250		-346		-208		-210		-600
K	K300	-153	-245	-102	-234	-102	-232	-255	-543
K	K350		-229		-277		-270		-540
K	K400	-139	-239	-187	-293	-187	-303	-326	-536
K	K450		-370		-254		-282		-638
K	K500	-147	-305	-236	-356	-236	-351	-384	-570
LOAD	PX (KIPS)	-100.0	-100.0	-0.	.1	-0.	.1	-100.0	-100.0
LOAD	PY (KIPS)	-0.	.1	-100.0	-100.0	-100.0	-103.6	-100.0	-103.6
ACTUAL	PX (KIPS)		-19.5		.0		-19.3		-19.3
ACTUAL	PY (KIPS)		.0		-19.3		-20.0		-20.0



TABLE 40E

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION C

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

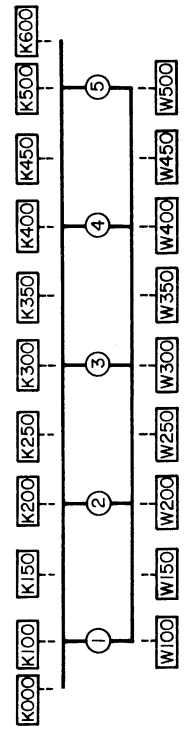
GAGE TYPE	GAGE LOC.	(5-X)		(5-Y)		(5-X)+(5-Y)	
		THEORY	MEASR	THEORY	MEASR	THEORY	MEASR
W	W000	511	377	199	117	711	504
W	W100	451	313	209	148	661	455
W	W150	274	311	165	172	431	437
W	W200	338	359	217	319	555	730
W	W250	221	249	357	358	588	607
W	W300	240	262	357	465	598	835
W	W350	280	331	310	362	667	791
W	W400	388	514	310	587	698	1224
W	W450	397	426	546	542	963	991
W	W500	510	438	376	738	886	1248
W	W600	545	454	383	847	929	1334
K	K100	-200	-271	-89	-241	-290	-499
K	K150	-271	-273	-97	-167	-422	-388
K	K200	-260	-266	-97	-188	-259	-404
K	K250	-293	-290	-144	-201	-249	-471
K	K300	-258	-268	-144	-206	-249	-411
K	K350	-256	-267	-145	-374	-331	-584
K	K400	-263	-261	-145	-267	-331	-532
K	K450	-430	-400	-177	-34	-405	-525
K	K500	-278	-275	-177	-451	-405	-691
LOAD	PX (KIPS)	-100.0	-100.0	-0.	.1	-100.0	-100.0
LOAD	PY (KIPS)	-0.	.1	-100.0	-100.0	-100.0	-103.6
ACTUAL	PX (KIPS)	-19.5	.0	.0	.0	-19.3	-19.3
ACTUAL	PY (KIPS)	.0	.0	-19.3	-19.3	-20.0	-20.0

**TABLE 40F**  
SUMMARY OF STRAINS (MICRC IN/IN)

RESULTS FOR POINT LOADS  
APPLIED AFTER 60 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION D

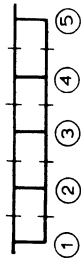
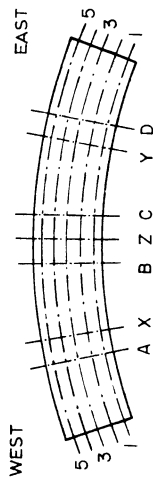
TENSION = +      K = CONCRETE STRAIN METERS  
COMPRESSION = -      W = WELDABLE STRAIN GAGES



GAGE TYPE	GAGE LOC.	NORMALIZED POINT LOADS AT (5-X)			NORMALIZED POINT LOADS AT (5-Y)			(5-X)+(5-Y)		
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
K	K000	75	61	61	-243	-139	-139	-167	-111	-111
K	K100	64	88	93	-205	-212	-227	-141	-160	-175
K	K150		185	176		-443	-444		-409	-410
K	K200	54	154	155	-190	-375	-357	-135	-328	-307
K	K250		158	180		-380	-426		-335	-369
K	K300	55	132	137	-226	-379	-402	-171	-332	-357
K	K350		223	221		-560	-614		-533	-595
K	K400	52	209	193	-264	-536	-527	-212	-535	-523
K	K450		304	353		-739	-802		-740	-846
K	K500	59	217	232	-318	-566	-582	-259	-540	-567
K	K600	67	54	217	-379	-250	-566	-312	-218	-540
W	W100	-271	-215	-214	829	535	539	558	437	455
W	W150		255	-254		568	554		458	444
W	W200	-240	-301	-298	806	774	774	566	637	632
W	W250		-269	-248		723	675		595	558
W	W300	-252	-315	-311	1015	1003	1014	762	885	904
W	W350		-240	-233		1050	987		989	911
W	W400	-226	-310	-312	1187	1668	1600	960	1599	1523
W	W450		-256	-255		1498	1366		1434	1309
W	W500	-242	-316	-317	1386	510	532	1143	406	427
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-0.	.1		-100.0	-100.0	
LOAD	PY (KIPS)	-0.	.1		-100.0	-100.0		-100.0	-103.6	
ACTUAL	PX (KIPS)		-19.5			.0			-19.3	
ACTUAL	PY (KIPS)		.0			-19.3			-20.0	

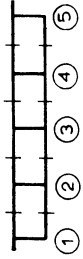
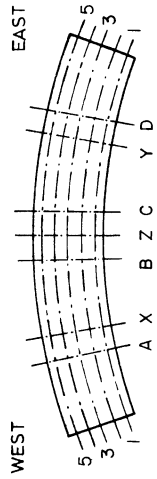
**TABLE 40G**  
 DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	83.4	59.7	9.0	-23.6	-16.3	11.9	59.8	13.4	32.8	6.7
A	2	115.8	122.1	18.4	-31.3	-30.0	22.0	84.5	19.0	80.4	16.4
A	3	126.6	156.0	23.5	-30.5	-35.7	26.2	96.0	21.6	111.1	22.6
A	4	143.1	195.9	29.5	-30.3	-32.6	23.8	112.8	25.4	155.5	31.6
A	5	113.2	129.4	19.5	-22.0	-22.0	16.1	91.3	20.5	111.7	22.7
A	SUM	582.1	663.0		-137.8	-136.7		444.4		491.6	
B	1	-33.3	-19.0	5.5	-54.0	-34.1	14.5	-87.5	14.9	-57.9	9.3
B	2	-54.8	-60.8	17.6	-65.8	-45.1	19.2	-120.3	20.5	-109.4	17.6
B	3	-77.2	-99.8	28.8	-54.7	-43.9	18.7	-130.4	22.2	-151.3	24.4
B	4	-65.5	-90.5	26.2	-77.6	-60.9	25.9	-142.7	24.3	-163.1	26.3
B	5	-42.9	-75.8	21.9	-64.2	-51.3	21.8	-107.2	18.2	-138.9	22.4
B	SUM	-273.7	-345.9		-316.3	-235.4		-588.1		-620.6	
C	1	-55.2	-42.3	15.5	-28.0	-16.1	5.0	-83.5	14.3	-55.2	8.9
C	2	-68.0	-52.5	19.2	-48.5	-47.5	14.8	-116.3	19.9	-102.2	16.5
C	3	-56.1	-44.5	16.3	-73.3	-74.8	23.3	-127.8	21.9	-129.2	20.8
C	4	-76.9	-75.2	27.6	-68.5	-90.9	28.3	-144.5	24.7	-176.7	28.5
C	5	-62.3	-58.2	21.3	-50.4	-91.7	28.6	-112.2	19.2	-157.0	25.3
C	SUM	-318.5	-272.6		-268.8	-321.1		-584.3		-620.3	
D	1	-24.1	-18.3	12.1	76.3	42.5	8.1	52.2	11.7	35.3	7.5
D	2	-31.8	-38.0	25.0	108.9	95.3	18.1	77.1	17.3	77.2	16.5
D	3	-30.7	-36.8	24.3	125.0	122.3	23.3	94.2	21.2	108.4	23.1
D	4	-30.2	-37.6	24.8	152.7	200.6	38.2	122.5	27.5	190.7	40.7
D	5	-21.9	-21.0	13.9	120.6	64.7	12.3	98.7	22.2	57.2	12.2
D	SUM	-138.7	-151.6		583.5	525.4		444.7		468.8	
LOAD	PX (KIPS)	-100.0	-100.0		-0.	.1		-100.0		-100.0	
LOAD	PY (KIPS)	-0.	.1		-100.0	.0		-100.0		-103.6	
ACTUAL	PX (KIPS)	-0.	-19.5		-19.3	.0		-19.3		-20.0	
ACTUAL	PY (KIPS)	.0	.0		.0	.0		.0		.0	

**TABLE 40I:**  
**DISTRIBUTION OF MOMENTS TO EACH GIRDER**  
**( KIP-FT AND PERCENTAGE )**



MOMENTS ABOUT TENSION FLANGE STEEL

RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI CCND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

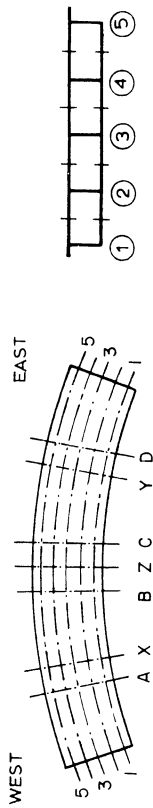
SECTION	GIRDER	(5-X)			(5-Y)			(5-X) + (5-Y)			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	83.4	14.3	17.2	-23.6	17.2	32.3	59.8	13.4	120.0	22.9
A	2	115.8	19.9	22.7	-31.3	22.7	18.6	84.5	19.0	95.1	18.1
A	3	126.6	21.7	22.2	-30.5	22.2	14.7	96.0	21.6	95.8	18.3
A	4	143.1	24.6	22.0	-30.3	22.0	18.0	112.8	25.4	112.5	21.4
A	5	113.2	19.5	16.0	-22.0	16.0	16.4	91.3	20.5	101.2	19.3
A	SUM	582.1	771.8	-137.8	-137.8	-191.3		444.4		524.6	
B	1	-33.3	12.2	17.1	-54.0	17.1	18.1	-87.5	14.9	-98.9	14.6
B	2	-54.8	20.0	20.8	-65.8	20.8	22.2	-120.3	20.5	-151.7	22.4
B	3	-77.2	28.2	17.3	-54.7	17.3	20.7	-130.4	22.2	-166.5	24.6
B	4	-65.5	23.9	24.5	-77.6	24.5	23.6	-142.7	24.3	-161.1	23.8
B	5	-42.9	15.7	20.3	-64.2	20.3	15.3	-107.2	18.2	-100.0	14.7
B	SUM	-273.7	-295.0	-316.3	-316.3	-367.1		-588.1		-678.1	
C	1	-55.2	17.3	10.4	-28.0	10.4	12.4	-83.5	14.3	-84.5	13.8
C	2	-68.0	21.4	18.1	-48.5	18.1	21.6	-116.3	19.9	-121.6	19.9
C	3	-56.1	17.6	27.3	-73.3	27.3	28.4	-127.8	21.9	-145.9	23.9
C	4	-76.9	24.2	25.5	-68.5	25.5	22.7	-144.5	24.7	-155.7	25.5
C	5	-62.3	19.5	18.8	-50.4	18.8	14.9	-112.2	19.2	-103.8	17.0
C	SUM	-318.5	-370.5	-268.8	-268.8	-310.4		-584.3		-611.5	
D	1	-24.1	17.4	13.1	76.3	13.1	10.6	52.2	11.7	60.5	9.4
D	2	-31.8	22.9	18.7	108.9	18.7	17.1	77.1	17.3	102.2	15.9
D	3	-30.7	22.2	21.4	125.0	21.4	19.5	94.2	21.2	119.6	18.6
D	4	-30.2	21.8	26.2	152.7	26.2	26.0	122.5	27.5	178.2	27.7
D	5	-21.9	15.8	20.7	120.6	20.7	26.9	98.7	22.2	183.8	28.5
D	SUM	-138.7	-272.6	583.5	583.5	673.7		444.7		644.2	
LOAD	PX (KIPS)	-100.0	-100.0	-100.0	-100.0	-100.0	.1	-100.0	-100.0	-100.0	-100.0
LOAD	PY (KIPS)	-0.	-0.	-0.	-0.	-0.	-0.	-0.	-0.	-0.	-0.
ACTUAL	PX (KIPS)	-19.5	-19.5	-19.3	-19.5	-19.3		-19.3	-19.3	-19.3	-19.3
ACTUAL	PY (KIPS)	.0	.0	.0	.0	.0		.0	.0	.0	.0

TABLE 401

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 60 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.

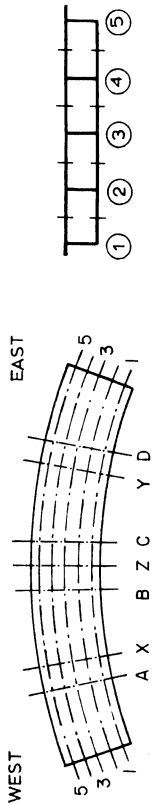


SECTION	GIRDER	(5-X)			(5-Y)			(5-X)+(5-Y)			
		THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	THEORY K-FT	EXPERIMENTAL K-FT	PCT	
A	1	83.4	115.9	14.3	-23.6	-36.6	17.2	59.8	13.4	71.8	14.2
A	2	115.8	129.2	19.9	-31.3	-32.5	22.7	84.5	19.0	87.0	17.2
A	3	126.6	145.2	21.7	-30.5	-32.4	22.2	96.0	21.6	104.3	20.6
A	4	143.1	181.6	24.6	-30.3	-33.4	22.0	112.8	25.4	136.3	26.9
A	5	113.2	139.8	19.5	-22.0	-26.2	16.0	91.3	20.5	107.1	21.1
A	SUM	582.1	711.8		-137.8	-161.1		444.4		506.5	
B	1	-33.3	-24.0	12.2	-54.0	-52.1	17.1	-87.5	14.9	-80.6	12.4
B	2	-54.8	-63.9	20.0	-65.8	-65.4	20.8	-120.3	20.5	-132.9	20.4
B	3	-77.2	-85.3	28.2	-54.7	-61.7	17.3	-130.4	22.2	-159.8	24.5
B	4	-65.5	-80.4	23.9	-77.6	-75.2	24.4	-142.7	24.3	-162.0	24.8
B	5	-42.9	-64.2	15.7	-64.2	-54.1	20.3	-107.2	18.2	-117.4	18.0
B	SUM	-273.7	-317.8		-316.3	-308.4		-588.1		-652.7	
C	1	-55.2	-46.5	17.3	-28.0	-28.5	10.4	-83.5	14.3	-71.4	11.6
C	2	-68.0	-69.3	21.4	-48.5	-58.4	18.1	-116.3	19.9	-113.0	18.4
C	3	-56.1	-69.3	17.6	-73.3	-82.2	27.3	-127.8	21.9	-138.5	22.5
C	4	-76.9	-82.6	24.2	-68.5	-79.6	25.5	-144.5	24.7	-165.1	26.8
C	5	-62.3	-59.2	19.5	-50.4	-66.5	18.8	-112.2	19.2	-127.6	20.7
C	SUM	-318.5	-326.9		-268.8	-315.2		-584.3		-615.6	
D	1	-24.1	-23.1	17.4	76.3	55.4	13.1	52.2	11.7	46.6	8.5
D	2	-31.8	-43.0	22.9	108.9	104.1	18.7	77.1	17.3	88.3	16.1
D	3	-30.7	-42.2	22.2	125.0	126.3	21.4	94.2	21.2	113.4	20.7
D	4	-30.2	-53.1	21.8	152.7	189.3	26.2	122.5	27.5	185.2	33.8
D	5	-21.9	-44.3	15.8	120.6	116.6	20.7	98.7	22.2	113.7	20.8
D	SUM	-138.7	-205.7		583.5	591.8		444.7		547.2	
LOAD	PX (KIPS)	-100.0	-100.0		-0.	.1		-100.0		-100.0	
LOAD	PY (KIPS)	-0.	.1		-100.0	.0		-100.0		-103.6	
ACTUAL	PX (KIPS)		-19.5			.0				-19.3	
ACTUAL	PY (KIPS)		.0			.0				-20.0	

**TABLE 40J**  
 DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI CCND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	(5-X)			(5-Y)			(5-X) + (5-Y)			
		THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	THEORY K-FT	PCT	EXPERIMENTAL K-FT	
A	1	83.4	14.3	117.7	17.2	37.7	23.4	59.8	15.4	75.2	14.5
A	2	115.8	19.9	127.6	22.7	32.2	19.9	84.5	19.0	85.7	16.5
A	3	126.6	21.7	148.9	20.8	33.5	20.7	96.0	21.6	106.4	20.5
A	4	143.1	24.6	186.6	22.0	33.2	20.6	112.8	25.4	142.7	27.5
A	5	113.2	19.5	135.4	16.0	24.9	15.4	91.3	20.5	109.1	21.0
A	SUM	582.1		716.2		-137.8		444.4		519.3	
B	1	-33.3	12.2	-23.9	17.1	-54.0	17.1	-87.5	14.9	-79.1	12.2
B	2	-54.8	20.0	-62.9	20.8	-65.8	20.3	-120.3	20.5	-125.9	19.4
B	3	-77.2	28.2	-92.4	27.8	-54.7	20.2	-130.4	22.2	-156.9	24.2
B	4	-65.5	23.9	-85.0	25.5	-77.6	24.3	-142.7	24.3	-162.4	25.0
B	5	-42.9	15.7	-68.7	20.6	-64.2	18.0	-107.2	18.2	-125.5	19.3
B	SUM	-273.7		-332.9		-316.3		-588.1		-649.8	
C	1	-55.2	17.3	-45.8	10.4	-28.0	9.3	-83.5	14.3	-70.5	11.3
C	2	-68.0	21.4	-65.4	18.1	-48.5	17.1	-116.3	19.9	-109.1	17.5
C	3	-56.1	17.6	-67.1	27.3	-73.3	24.4	-127.8	21.9	-134.6	21.6
C	4	-76.9	24.2	-79.7	25.1	-68.5	26.2	-144.5	24.7	-170.3	27.4
C	5	-62.3	19.5	-58.9	18.6	-50.4	23.0	-112.2	19.2	-138.1	22.2
C	SUM	-318.5		-316.8		-268.8		-584.3		-622.7	
D	1	-24.1	17.4	-21.6	10.9	76.3	13.1	52.2	11.7	42.3	7.6
D	2	-31.8	22.9	-41.8	21.1	108.9	18.7	77.1	17.3	85.4	15.3
D	3	-30.7	22.2	-40.5	20.5	125.0	21.4	94.2	21.2	111.6	20.1
D	4	-30.2	21.8	-50.9	25.7	152.7	26.2	122.5	27.5	187.5	33.7
D	5	-21.9	15.8	-43.0	21.8	120.6	20.7	98.7	22.2	129.4	23.3
D	SUM	-138.7		-197.8		583.5		444.7		556.1	
LOAD	PX (KIPS)	-100.0		-100.0		-0.		-100.0		-100.0	
LOAD	PY (KIPS)	-0.		.1		-100.0		-100.0		-103.6	
ACTUAL	PX (KIPS)			-19.5		.0		-19.3		-19.3	
ACTUAL	PY (KIPS)			.0		-19.3		-20.0		-20.0	

**TABLE 41A**  
SUMMARY OF REACTIONS (KIPS OR FT-KIPS)

SEE FIGURE FOR POSITIVE DIRECTIONS RESULTS FOR POINT LOADS  
 MF = MOMENT AT FOOTING ABOUT Z-AXIS APPLIED AFTER 60 KSI CCND. LOADING.  
 TF = MOMENT AT FOOTING ABOUT 3-AXIS SIMPLY SUPPORTED, NO RESTRAINTS.

NORMALIZED POINT LOADS AT

REACTION OR LOAD	(1-X)+(5-Y)		THEORY		EXPERM	
	THEORY	EXPERM	THEORY	EXPERM	THEORY	EXPERM
1E	-15.18	-12.62				
2E	-1.65	-7.28				
3E	.72	5.43				
4E	9.96	15.86				
5E	36.73	28.36				
1F	37.82	52.77				
2F	37.77	34.40				
3F	31.36	17.03				
4F	31.41	33.69				
1W	29.07	28.08				
2W	8.98	11.13				
3W	2.20	5.82				
4W	.15	3.13				
5W	-9.33	-15.19				
RE	30.58	29.75				
RF	138.36	137.89				
RW	31.07	32.97				
SUMR	200.01	200.61				
PX	-100.00	-100.00				
PY	-100.00	-97.55				
SUMP	-200.00	-197.55				
SUMR/SUMP	1.00	1.02				
TW	-220.32	-243.24				
MF	-19.22	-54.67				
TF	.15	52.54				
TE	296.99	270.41				
ACTUAL PX						-19.40
ACTUAL PY						-18.93

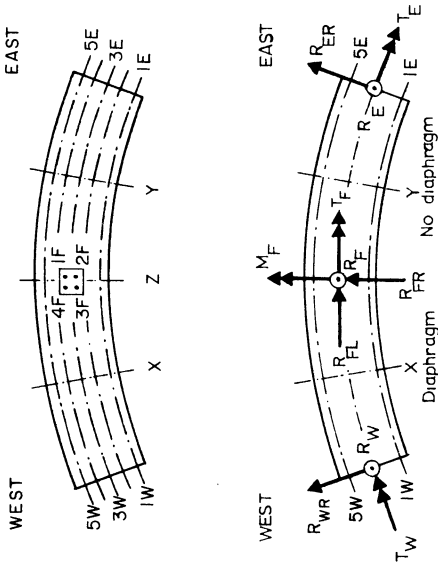
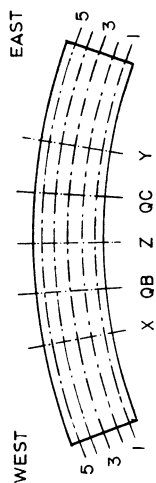


TABLE 41B

SUMMARY OF DEFLECTIONS ( INCHES )  
 DEFLECTIONS POSITIVE DOWNWARDS  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI CCND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS AT

\*\*\*\*\*  
 THEORY EXPERM E/T \*\*\*\*\*  
 \*\*\*\*\*  
 THEORY EXPERM E/T \*\*\*\*\*

DEFLECTION AT POINT	( 1-X ) + ( 5-Y )		
	THEORY	EXPERM	E/T
1X	.613	1.239	2.02
2X	.500	.926	1.85
3X	.408	.688	1.68
4X	.340	.468	1.38
5X	.289	.284	.98
1QB	.300	.548	1.83
2QB	.230	.404	1.76
3QB	.166	.253	1.52
4QB	.122	.146	1.19
5QB	.094	.055	.58
1Z	.034	.010	.31
2Z	.016	.004	.22
4Z	.016	.079	4.84
5Z	.033	.121	3.63
1QC	.167	.145	.87
2QC	.200	.257	1.29
3QC	.265	.437	1.65
4QC	.375	.774	2.06
5QC	.504	1.104	2.19
1Y	.351	.404	1.15
2Y	.417	.583	1.40
3Y	.535	.898	1.68
4Y	.726	1.441	1.98
5Y	1.032	2.415	2.34
LOAD PX	-100.0	-100.0	
LOAD PY	-100.0	-97.6	
ACTUAL PX		-19.4	
ACTUAL PY		-18.9	

\*\*\*\*\*  
 THEORY EXPERM E/T \*\*\*\*\*  
 \*\*\*\*\*  
 THEORY EXPERM E/T \*\*\*\*\*



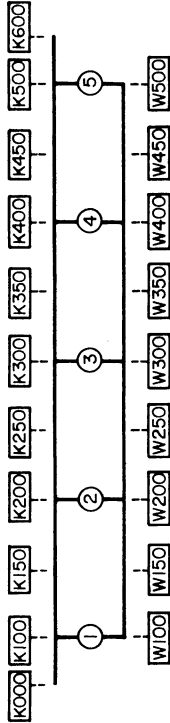
TABLE 41C

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION A

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	(1-X)+(5-Y)	THEORY	MEASR	ADJUST
*****					
THEORY MEASR ADJUST					
*****					
THEORY MEASR ADJUST					
*****					
THEORY MEASR ADJUST					
*****					

K	K000	-347	-469	-1008
K	K100	-269	-1008	-964
K	K150	-339	-284	-339
K	K200	-211	-476	-513
K	K250	-183	-193	-187
K	K300	-152	-368	-362
K	K350	-159	-258	-242
K	K400	-186	-306	-306
K	K450	-159	-175	-193
K	K500	-186	-209	-213
K	K600	-159	-159	-159

W	W100	1100	1072	1083
W	W150	823	933	971
W	W200	720	824	809
W	W250	568	826	721
W	W300	573	706	700
W	W350	573	595	553
W	W400	573	525	516
W	W450	573	728	374
W	W500	573	501	506

LOAD	PX (KIPS)	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-97.6
ACTUAL	PX (KIPS)	-19.4	
ACTUAL	PY (KIPS)	-18.9	

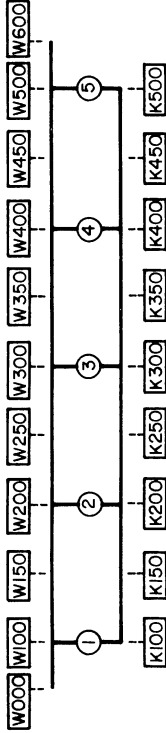
TABLE 41D

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS APPLIED AFTER 60 KSI COND. LOADING. SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION B

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



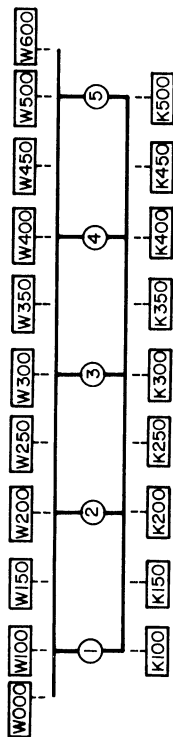
NORMALIZED POINT LOADS AT

GAGE TYPE	GAGE LOC.	(1-X)+(5-Y)		*****		*****		*****		
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
W	W000	684	865							
W	W100	632	710							
W	W150	510	767							
W	W200	510	705							
W	W250	488	607							
W	W300	488	682							
W	W350	536	681							
W	W400	536	576							
W	W450	657	548							
W	W500	678	539							
W	W600	678	488							
K	K100	-287	-527							-498
K	K150	-935	-899							-368
K	K200	-238	-351							-365
K	K250	-202	-301							-436
K	K300	-202	-435							-459
K	K350	-253	-454							-433
K	K400	-253	-423							-388
K	K450	-295	-353							-363
K	K500	-295	-373							-363

LOAD	PX (KIPS)	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-97.6
ACTUAL	PX (KIPS)	-19.4	
ACTUAL	PY (KIPS)	-18.9	

TABLE 41E

SUMMARY OF STRAINS (MICRO IN/IN)  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION C  
 TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES

GAGE TYPE	GAGE LOC.	(1-X)+(5-Y)		NORMALIZED POINT LOADS AT		THEORY	MEASR	ADJUST	*****	THEORY	MEASR	ADJUST	*****	THEORY	MEASR	ADJUST	*****	
		THEORY	MEASR	ADJUST	ADJUST													
W	W000																	
W	W100	624	463	463	463													
W	W150	596	454	442	427													
W	W200	498	704	696	537													
W	W250		529	537	689													
W	W300	512	671	689	615													
W	W350		538	537	846													
W	W400	541	830	846	704													
W	W450		700	704	924													
W	W500	680	920	924	1035													
W	W600	709	1035	1035														
K	K100																	
K	K150	-267	-444	-440	-285													
K	K200	-232	-330	-327	-385													
K	K250		-326	-385	-304													
K	K300	-211	-308	-308	-506													
K	K350		-509	-506	-418													
K	K400	-256	-404	-404	-230													
K	K450		-196	-196	-632													
K	K500	-310	-615	-615														

LOAD PX (KIPS) -100.0 -100.0  
 LOAD PY (KIPS) -100.0 -97.6  
 ACTUAL PX (KIPS) -19.4  
 ACTUAL PY (KIPS) -18.9

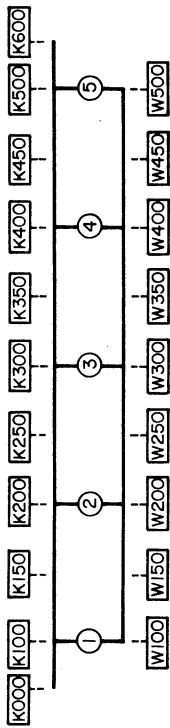
TABLE 41F

SUMMARY OF STRAINS (MICRO IN/IN)

RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI COND. LOADING,  
 SIMPLY SUPPORTED, NO RESTRAINTS.

SECTION D

TENSION = + K = CONCRETE STRAIN METERS  
 COMPRESSION = - W = WELDABLE STRAIN GAGES



NOF MALIZED POINT LOADS AT

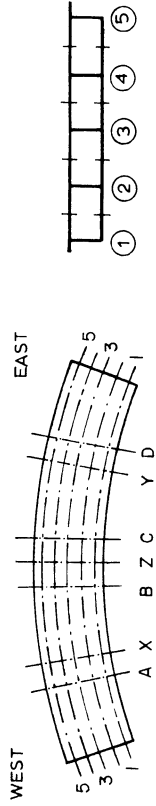
GAGE TYPE	GAGE LOC.	(1-X)+(5-Y)		*****		*****		*****		
		THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST	THEORY	MEASR	ADJUST
K	K000	-191	-86		-86					
K	K100	-161	-133		-143					
K	K150		-304		-298					
K	K200	-152	-285		-276					
K	K250		-277		-324					
K	K300	-187	-311		-326					
K	K350		-494		-528					
K	K400	-227	-491		-481					
K	K450		-714		-787					
K	K500	-275	-542		-560					
K	K600	-330	-237		-542					
W	W100	646	395		405					
W	W150		413		403					
W	W200	642	554		551					
W	W250		531		488					
W	W300	837	832		846					
W	W350		823		787					
W	W400	1024	1517		1453					
W	W450		1333		1199					
W	W500	1209	335		357					

LOAD	PX (KIPS)	-100.0	-100.0
LOAD	PY (KIPS)	-100.0	-97.6
ACTUAL	PX (KIPS)	-19.4	
ACTUAL	PY (KIPS)	-18.9	

TABLE 41G

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )  
MOMENTS ABOUT COMPRESSION FLANGE MID-DEPTH

RESULTS FOR POINT LOADS  
APPLIED AFTER 60 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS AT

\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

\*\*\*\*\*  
THEORY K-FT PCT  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

SECTION	GIRDER	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
A	1	92.4	22.0	77.6	19.3
A	2	108.5	25.9	121.1	30.1
A	3	88.9	21.2	95.6	23.8
A	4	76.8	18.3	70.2	17.5
A	5	52.6	12.5	37.2	9.3
A	SUM	419.3		401.6	

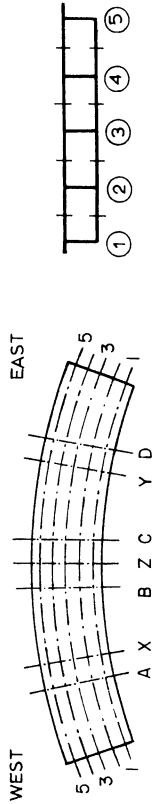
SECTION	GIRDER	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
B	1	-80.8	16.6	-92.7	19.5
B	2	-106.4	21.9	-110.0	23.1
B	3	-105.0	21.6	-109.5	23.0
B	4	-111.4	22.9	-96.1	20.2
B	5	-83.2	17.1	-67.7	14.2
B	SUM	-486.9		-475.9	

SECTION	GIRDER	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
C	1	-76.1	15.6	-54.0	10.8
C	2	-104.4	21.3	-97.3	19.6
C	3	-109.0	22.3	-106.4	21.4
C	4	-113.5	23.2	-125.8	25.3
C	5	-86.5	17.7	-114.1	22.9
C	SUM	-489.5		-497.6	

SECTION	GIRDER	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
D	1	59.9	12.3	32.0	7.5
D	2	87.1	17.9	67.6	15.9
D	3	103.4	21.3	98.0	23.1
D	4	131.1	27.0	177.5	41.8
D	5	104.7	21.5	49.1	11.6
D	SUM	486.2		424.1	

LOAD	PX (KIPS)	PY (KIPS)
LOAD	-100.0	-100.0
ACTUAL	-100.0	-100.0
ACTUAL	-19.4	-18.9

**TABLE 41H**  
 DISTRIBUTION OF MOMENTS TO EACH GIRDER  
 ( KIP-FT AND PERCENTAGE )



MOMENTS ABOUT TENSION FLANGE STEEL  
 RESULTS FOR POINT LOADS  
 APPLIED AFTER 60 KSI COND. LOADING.  
 SIMPLY SUPPORTED, NO RESTRAINTS.

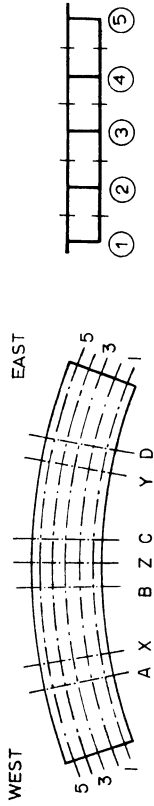
SECTION	GIRDER	(1-X)+(5-Y)		NORMALIZED POINT LOADS AT		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	92.4	22.0	242.4	41.3				
A	2	108.5	25.9	113.2	19.3				
A	3	88.9	21.2	89.0	15.2				
A	4	76.8	18.3	85.2	14.5				
A	5	52.6	12.5	56.8	9.7				
A	SUM	419.3		586.5					
B	1	-80.8	16.6	-125.9	21.1				
B	2	-106.4	21.9	-149.3	25.0				
B	3	-105.0	21.6	-130.7	21.9				
B	4	-111.4	22.9	-127.1	21.3				
B	5	-83.2	17.1	-64.2	10.7				
B	SUM	-486.9		-597.1					
C	1	-76.1	15.6	-68.5	14.7				
C	2	-104.4	21.3	-94.2	20.2				
C	3	-109.0	22.3	-116.7	25.0				
C	4	-113.5	23.2	-111.5	23.9				
C	5	-86.5	17.7	-76.0	16.3				
C	SUM	-489.5		-466.9					
D	1	59.9	12.3	45.3	7.8				
D	2	87.1	17.9	85.4	14.8				
D	3	103.4	21.3	106.5	18.4				
D	4	131.1	27.0	162.0	28.0				
D	5	104.7	21.5	179.3	31.0				
D	SUM	486.2		578.5					
LOAD	PX (KIPS)	-100.0		-100.0					
LOAD	PY (KIPS)	-100.0		-97.6					
ACTUAL	PX (KIPS)			-19.4					
ACTUAL	PY (KIPS)			-18.9					

TABLE 411

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE)

MOMENTS ABOUT ENTIRE GROSS SECTION N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 60 KSI CCND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



NORMALIZED POINT LOADS AT

\*\*\*\*\*  
THEORY K-FT PCT  
\*\*\*\*\*  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

\*\*\*\*\*  
THEORY K-FT PCT  
\*\*\*\*\*  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

(1-X)+(5-Y)  
\*\*\*\*\*  
THEORY K-FT PCT  
\*\*\*\*\*  
EXPERIMENTAL K-FT PCT  
\*\*\*\*\*

SECTION	GIRDER	THEORY K-FT	PCT	EXPERIMENTAL K-FT	PCT
A	1	92.4	22.0	151.2	31.2
A	2	108.5	25.9	117.6	24.3
A	3	88.9	21.2	92.6	19.1
A	4	76.8	18.3	76.9	15.9
A	5	52.6	12.5	46.0	9.5
A	SUM	419.3		484.3	

B	1	-80.8	16.6	-111.1	20.5
B	2	-106.4	21.9	-131.8	24.3
B	3	-105.0	21.6	-121.2	22.3
B	4	-111.4	22.9	-113.3	20.9
B	5	-83.2	17.1	-65.8	12.1
B	SUM	-486.9		-543.2	

C	1	-76.1	15.6	-62.0	12.9
C	2	-104.4	21.3	-95.6	19.9
C	3	-109.0	22.3	-112.1	23.3
C	4	-113.5	23.2	-117.9	24.5
C	5	-86.5	17.7	-93.0	19.3
C	SUM	-489.5		-480.7	

D	1	59.9	12.3	37.9	7.7
D	2	87.1	17.9	75.6	15.3
D	3	103.4	21.3	101.8	20.6
D	4	131.1	27.0	170.6	34.6
D	5	104.7	21.5	107.2	21.7
D	SUM	486.2		493.2	

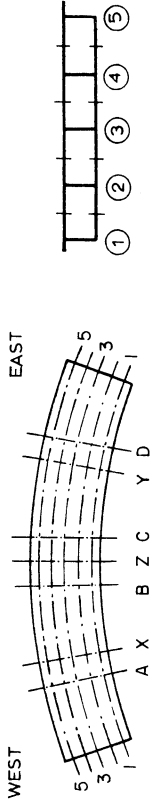
LOAD	PX (KIPS)	-100.0
LOAD	PY (KIPS)	-100.0
ACTUAL	PX (KIPS)	-97.6
ACTUAL	PY (KIPS)	-19.4
		-18.9

TABLE 41J

DISTRIBUTION OF MOMENTS TO EACH GIRDER  
( KIP-FT AND PERCENTAGE )

MOMENTS ABOUT GIRDER EXPERIMENTAL N.A.

RESULTS FOR POINT LOADS  
APPLIED AFTER 60 KSI COND. LOADING.  
SIMPLY SUPPORTED, NO RESTRAINTS.



SECTION	GIRDER	(1-X)+(5-Y)		THEORY		EXPERIMENTAL	
		K-FT	PCT	K-FT	PCT	K-FT	PCT
A	1	92.4	22.0	155.2	32.0		
A	2	108.5	25.9	118.0	24.3		
A	3	88.9	21.2	93.3	19.2		
A	4	76.8	18.3	75.8	15.6		
A	5	52.6	12.5	43.0	8.9		
A	SUM	419.3		485.4			
B	1	-80.8	16.6	-106.3	20.3		
B	2	-106.4	21.9	-123.3	23.6		
B	3	-105.0	21.6	-117.8	22.5		
B	4	-111.4	22.9	-109.3	20.9		
B	5	-83.2	17.1	-66.3	12.7		
B	SUM	-486.9		-523.0			
C	1	-76.1	15.6	-61.2	12.6		
C	2	-104.4	21.3	-96.3	19.8		
C	3	-109.0	22.3	-109.6	22.5		
C	4	-113.5	23.2	-121.1	24.9		
C	5	-86.5	17.7	-98.6	20.3		
C	SUM	-489.5		-486.8			
D	1	59.9	12.3	35.4	6.9		
D	2	87.1	17.9	73.5	14.4		
D	3	103.4	21.3	100.4	19.6		
D	4	131.1	27.0	173.7	33.9		
D	5	104.7	21.5	128.6	25.1		
D	SUM	486.2		511.6			
LOAD	PX (KIPS)	-100.0		-100.0			
LOAD	PY (KIPS)	-100.0		-97.6			
ACTUAL	PX (KIPS)			-19.4			
ACTUAL	PY (KIPS)			-18.9			

NORMALIZED POINT LOADS AT

\*\*\*\*\*  
THEORY  
K-FT PCT  
\*\*\*\*\*  
EXPERIMENTAL  
K-FT PCT  
\*\*\*\*\*

\*\*\*\*\*  
THEORY  
K-FT PCT  
\*\*\*\*\*  
EXPERIMENTAL  
K-FT PCT  
\*\*\*\*\*